

Course Name: Design of Electric Motors

Professor Name: Dr. Prathap Reddy B

Department Name: Electronic Systems Engineering

Institute Name: Indian Institute of Science Bengaluru

Week: 08

Lecture: 42

Title: Design of Induction Machine- Rotor Design -3 (Rotor Slot Geometry)

Greetings to all, in the last lecture we have started doing the rotor core design equations right with respect to the number of slots, with respect to the bar currents and bar length etcetera. In this lecture, we will discuss rotor slot geometry equations like what is the slot depth, slot width and slot height and etcetera. We can see here this rotor slot geometry, this one rotor slot lamination we can see here. So, we have to find the what is the slot depth and back iron width and slot width and slot opening and etcetera. Let us consider the rotor slots, two rotor slots I have considered here. The slot width at the bottom side is w_{2r} and slot width at the top side of the slot is w_{1r} .

We can see here, t_r is the teeth width of the rotor and d_{cr} is the back iron width and r_{2r} is the radius at the bottom side of the rotor slot and d_{sr} is nothing but slot depth and r_{1r} is rotor slot radius at the top side of the slot and $d_{naught r}$ is the height of the slot opening and one more variable $b_{naught r}$, $b_{naught r}$ is nothing but slot opening width. So, with respect to this slot shape not only this slot any type of or any type of slot shape, we can have to find the slot dimensions. How to find the slot dimensions we will discuss. First $b_{naught r}$ the slot opening and r_{1r} radius at the top side of the rotor slot and r_{2r} and $d_{naught r}$.

These are the four parameters we have to assume as a designer choice. And the approximate equation for r_{2r} we can find. If you do not want to assume r_{2r} approximate equation also we can find the radius of the slot at the bottom side of the rotor slot. If we will consider the midpoint, let us consider this is the midpoint center point of the machine and if I will draw a line with respect to this point mid of the rotor slot to other slot midpoint or half cross section, then this angle is α that is slot angle with respect to the rotor. And half of this thing will be $\alpha/2$ right.

This period we know this width of the stator teeth we know. If we will see here the width of this portion is nothing but $t/2$ and width of this portion is $w_{2r}/2$ and height of this triangle we can consider it as a right angle triangle. This triangle is $\alpha/2$ and

this opposite side is w_{2r} plus t_r by 2 and this height will be from this point to this point is nothing but d_{lr} by 2 up to this point and after that d_{cr} and then r_{2r} . If I will write the sine angle with respect to this right angle triangle sine of α by 2 is equals to w_{2r} that is width of the rotor slot at the bottom side of the slot and teeth width t_r by 2 opposite by diagonal right. Diagonal width is d_{lr} by 2 that is inner diameter of the rotor by 2 plus back iron width of the rotor plus r_{2r} .

So, here we know the value of α , we know the value of w_{2r} and t_r and d_{cr} how to calculate we will discuss the equations. Once we know these values and we can calculate the r_{2r} this is one way of doing to find the radius of the rotor slot at the bottom side. Otherwise we can directly assume these four parameters as a designer choice initially itself. Next in order to find the width of the rotor slots w_{1r} and w_{2r} and teeth width t_r back iron width d_{cr} and slot depth d_{sr} . To calculate these parameters we have to analyze the flux densities at the different parts of the iron flux density at the back iron that is B_{cr} flux density at the teeth that is B_{tr} and flux density at the air gap is B_g .

First we will start with flux density at the air gap. To find the flux density at the air gap let us consider the equation with respect to the flux per pole ϕ_g average is equals to 2 by π into ϕ_g peak for the sinusoidal quantities that is equals to 2 by π flux peak value is nothing, but B_g peak value into area right A_g . Here area of cross section with respect to the air gap we have to consider the rotor outer diameter in terms of $D_{naught r}$ we have to represent. X axis length will be $\pi D_{naught r}$ divided by P and y axis length is nothing, but $l_e B_g$ peak will be there as it is. This is the ϕ_g average flux per pole from here we can calculate the B_{gr} peak that is equals to ϕ_g average divided by 2 into $D_{naught r}$ that is outer diameter of the rotor into length of the effective length of the rotor core B_g value in Tesla or Weber per meter square.

This equation is 34. Similarly, we have to calculate the flux densities at the teeth and back iron. Flux density at the teeth will be the flux lines are flowing in this manner and we have to find the cross sectional area with respect to this portion. So, here B_{tr} we have to calculate for that first we have to consider the flux at the teeth average with respect to pole is equals to 2 by π ϕ_t peak 2 by π ϕ_t peak is nothing, but B into A_t is nothing, but flux density at the teeth peak value into area is nothing, but A_t x axis will be Q_r into t_r by P that means, number of slots into number of teeth by P that is flux per pole we are calculating right into x axis y axis length will be l_e is the effective length of the core into k_s is the stacking factor steel stacking factor. So, from here we can calculate the B_{tr} peak is equals to π by 2 into ϕ_t average divided by t_r into Q_r into $l_e k_s$ and the number of poles this is equation number 35.

Next flux density at the back iron if we will see here the flux lines or flux per pole is dividing into two parts in the back iron this side ϕ_b by 2 and this side ϕ_b by 2. So, to find the flux at the back iron ϕ_b average by 2 is equals to directly we can represent in terms of B_{cr} peak into area is nothing, but d_{cr} into l_e into k_s this is y axis and d_{cr} is

nothing, but depth of the back iron is d_{cr} from here B_c peak value is equals to ϕ_c average by 2 into d_{cr} into length of effective length of the core into stacking factor this is equation number 36. Here the maximum flux with respect to the teeth whatever it is coming towards the back iron is splitting into two parts the flux per pole is splitting into two parts and flowing through the back iron that is why ϕ_c by 2 I have considered here that is B_c peak value is equals to this one.

Once after knowing the flux density values at the different parts of iron we can calculate the teeth width by doing the equation number 30 in order to calculate the t_r equation number 34 by 35 from the equation number 34 by equation number 35 then we will get the t_r value that is teeth width or tooth width is equals to π into $D_{naught r}$ outer diameter of the rotor divided by stacking factor into number of slots into B_{gr} divided by B_{tr} this equations we have already derived with respect to the stator same way we can derive it for rotor also this is equation number 37. In order to find the depth of the back iron we have to utilize the equation number 34 and equation number 36 d_{cr} is equals to depth of the back iron rotor outer diameter divided by number of poles into stacking factor into B_{gr} divided by B_{cr} this is equation number 38.

So, from the equation number 37 and 38 we can find the tooth width and depth of the back iron and the remaining things will be what is the width of the rotor slots at the top and bottom in order to find the widths w_1 and w_2 we have to analyze the perimeter. If we will see the perimeter with respect to the w_2r here w_2r plus t_r into Q_r is nothing, but the perimeter Q_r number of slots into w_2r is the width of the rotor slots at the bottom side and tooth width is nothing, but t_r this is the perimeter with respect to the bottom side of the rotor slot that is equals to π into $D_{naught r}$ π into in terms of D_{ir} we will write because w_2 is near to the with respect to the inner diameter of the rotor right D_{ir} plus 2 into d_{cr} that is depth of the back iron plus r_2r . So, from this equation we can find the value w_2r in mm here we know the value of t_r we know the value of D_{ir} that is inner diameter of the rotor and d_{cr} also we know and r_2r also we have assumed already then we can find the w_2r .

If we are deriving the w_2r value then we have to find the r_2r value first then only we have to find the w_2r value. Next thing for w_1 same way the number of slots at the rotor side into w_1r plus t_r is equals to the perimeter of the rotor at the top side of the rotor slot that is equals to π into $D_{naught r}$ minus 2 into $D_{naught r}$ plus r_1r .

Here we know the t_r value $D_{naught r}$ that is outer diameter of the rotor and small $d_{naught r}$ is nothing but height of the slot opening and r_1r is nothing but radius at the top side of the rotor slot. What we have done here is we have calculated the perimeter with respect to the different portion of the rotor slot. So, we can find the perimeter in terms of with respect to this portion as well as this portion w_1 plus t_r and w_2r plus t_r in terms of π D we have to represent then we will get the equation we will get the equation number 39 and 40 this is 39 and this is equation number 40. So, the remaining thing is slot depth

that is d_{sr} . So, from equation number 39 and 40 we can find the difference between w_{1r} minus w_{2r} into Q_r is equals to π into $2 d_{sr}$ will come.

Here π into D naught r minus 2 into slot opening height plus r_{2r} minus inner diameter of the rotor minus 2 into back iron width plus radius at the bottom side of the slot. This will eventually results in 2 into d_{sr} or this complete value in the bracket is equals to 2 into d_{sr} that is slot depth. So, from this equation we can find the d_{sr} value this is equation for d_{sr} it is 41. So, we have calculated the all dimensions of the stators rotor slot. Now, we will find the rotor slot area.

Let us consider this is the rotor slot here r_{1r} d_{sr} r_{2r} and d_{cr} and this is d naught r this is b naught that is slot opening. So, we have to find the slot area. Similar to the stator side slot area equation we can calculate the rotor slot area that is A_r is equals to w_{1r} plus w_{2r} by 2 into slot height that is d_{sr} plus r_{1r} into w_1 minus c_1 into r_{1r} plus r_{2r} into w_2 minus c_1 into r_{2r} . This is the slot area equation in mm square equation number 42. Here c_1 is a constant that is equals to 2 minus π by 2 similar to the stator side slot area c_1 is equals to some constant.

Now, we will find the slot area with respect to the copper function. I have not derived the output function and power equation in terms of rotor side copper function as well as rotor dimensions. If we will derive the copper function and output power equation in terms of output function with respect to the rotor dimension, then we can find the equation A_r into Q_r that is slot area into number of rotor slots is equals to π into D naught r square by 4 into copper function with respect to the rotor $f_{\lambda 2}$ of $\lambda 2$ function minus constant $\Delta 2$ divided by D naught r square. We can neglect this term and we can find the slot area by knowing the number of slots and outer diameter of the rotor and copper function A_r from this equation also we can find. Otherwise, we can go ahead with the equation number 42.

This equation will come if we will write the power equation in terms of some constant into D naught r cube le term with respect to the rotor volume if you will find the power equation, then we will get this kind of equation. As of now, we have discussed the rotor slot geometry and respective equations. So, if anyone is interested to derive the power equations in terms of rotors geometry, they can go through this reference paper sizing equations for the electrical machinery. From this reference only we have derived the power equations with respect to the stator slot geometry that is D cube l sizing equation we have derived from the similar to this reference. I have not derived the power equations with respect to the rotor slot geometry.

If anyone is interested, they can go through this reference paper and they can find the output power equation in terms of rotor slot geometry. We can see here the final output power in terms of rotor slot geometry here D power 2.5 l and D cube le equation also we can see here. Here this is D square l product with respect to the rotor and D cube l

product with respect to the stator. We can consider it as it is and we can find the output equations like $D^2 l$ product equation as well as $D^3 l$ product equations in terms of rotor slot geometry.

So, here rotor slot geometry we can see here this kind of rotor slot is considered the slot dimensions d_s , d_c , w_2 , w_1 and d_0 and r_1 all those things are considered. Here this is the closed type of rotor slot where slot opening b_0 may not required for closed slot. For open type of slots only we require the b_0 value and different perimeter equations and this is the copper function what I have discussed. You have to go through this equation number 22 to find the copper function such that inner diameter and outer diameter we can find. Generally, the slot opening b_0 value is equals to 0 for closed type of slots like squirrel cage rotors and b_0 value is equals to 2 to 5 times the conductor cross sectional area that is AC for open type of slots.

So, with this I am concluding this lecture. In this lecture we have discussed the rotor slot dimensions with respect to the slot depth, slot height and slot width and back iron width etc. Thank you.

Ref: