

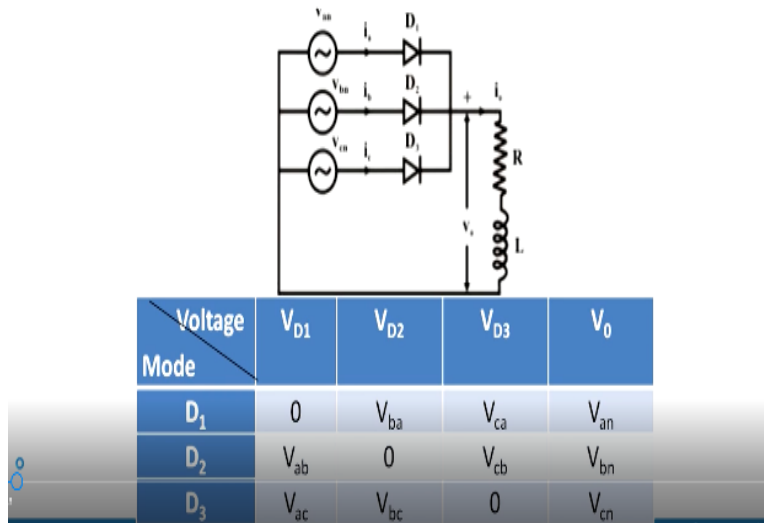
**Advance Power Electronics and Control**  
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**Lecture – 12**  
**Three Phase Converter I**

Welcome to our NPTEL lectures on advance power electronics and control. Today we are going to discuss three phase converter. We have discussed in details with a single phase converter now we are discussing with the three phase converter. We have we started with the same fashion as we have started the single phase converter.

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Three Phase half wave uncontrolled Rectifier



Since actually most of our supply is three phase three wave or four wave system and it makes sense for the high power applications for the dc motor mostly this kind of applications we convert directly three phase to dc. So this is the application part of it so we use this is basically three phase half wave uncontrolled rectifier fitted through the diodes and it is fitting data I assume that RL load.

So what happened? you can see that how conduction takes place. So the  $D_1$  will actually when it will conduct basically that would about to stop across it would be 0 and then you will get a voltage of  $V_{an}$  across this diode  $R_L$ . If  $D_2$  is conducting, then at that time basically it will block

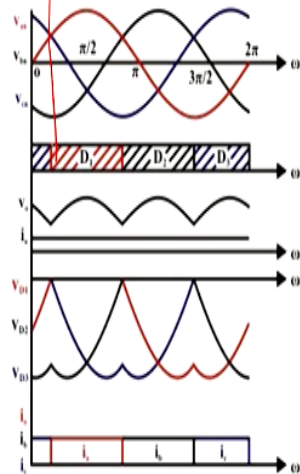
the voltage when D2 is conducting D1 will block the voltage of Vba it would be negative voltage and similarly it will block the voltage of the Vca.

So similarly when diode 2 was conducting so the third diode will block Vac sometime Vbc and once actually diode 3 is conducting then load will get the voltage Vcn. So load will get the voltage depending on the 180 degree mode of conduction for 360 degree Van Vbn and Vcn most positive phase will conduct so accordingly you will get the three different voltages.

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### Three Phase half wave uncontrolled Rectifier (Cont...)

- Due to R-L load converter operates in continuous conduction mode.
- As diode blocks -ve voltage, diode only conducts in that phase where phase voltage is maximum of three.
- As shown in waveform, phase current has DC component which flows through AC source and makes "DC Saturation" in ac side transformer. So this type of configuration is not preferred much.



So let us see how it works this is the actually the three phase voltages and our starting point will be actually this point where the voltage A actually a crossover the voltage C and thus voltage A become the actually most positive. You can see till this region that when actually  $\pi/6$  to  $150$  degree actually most positive phase is  $V_{an}$ . So definitely this will conduct for actually  $\pi/6$  to  $150$  degree so this will conduct. Similarly, after that you know  $V_b$  actually at this point crossover takes place

so since there is only a single diode in upper limb so crossover takes place and it will we have a crossover at this point where V phase becomes most positive place and thus it well conduct in this point. Similarly,  $V_c$  will conduct after actually the period to  $70$  degree and so on. So till this time  $D_1$  conduct till this time  $D_2$  conduct till this time  $D_3$  conduct and thereafter till this time  $D_3$

conducts and this is the output voltage. We will have a third harmonic oscillations we can find it out by analysis.

And this is actually the voltage blocking state or the different diode and this is VD1. VD1 will conduct actually this point to this point so it will be blocking the voltage red one. Similarly, VD2 will have this kind of fashion so and same way VD3 so it will conduct when actually at this instant so you will get a negative. So phase a or red phase will conduct for  $\pi/6$  to 150 degree for another 20 phase b and another 20 degree phase c.

So thus due to the RL load the converter operates in a continuous conduction mode if you assume that load current is quite high. As diode blocks the negative voltage the diode only conducts in that phase where the phase of voltage is maximum of these three. As shown in the wave form the phase current has DC component which flows to that AC source and makes DC saturation in the ac side of the transformer.

For this you know this kind of configuration we do not prefer so it may lead to the saturation of the input transformer. So three phase halfwave uncontrolled rectified we can see that what are the different values what we have seen in the say actually single phase.

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### Three Phase half wave uncontrolled Rectifier (Cont...)

Input three phase voltages

$$\left. \begin{aligned} V_{an} &= \sqrt{2}v \sin \omega t \\ V_{bn} &= \sqrt{2}v \sin(\omega t - 2\pi/3) \\ V_{cn} &= \sqrt{2}v \sin(\omega t + 2\pi/3) \end{aligned} \right\}$$

Output average and RMS voltages

$$V_{oavg} = \frac{3}{2\pi} \int_{\pi/6}^{5\pi/6} \sqrt{2}v \sin \omega t d(\omega t)$$

$$V_{orms} = \left[ \frac{3}{2\pi} \int_{\pi/6}^{5\pi/6} (\sqrt{2}v \sin \omega t)^2 d(\omega t) \right]^{1/2}$$

Output average current and Input RMS current

$$I_{oavg} = \frac{V_{oavg}}{R}$$

$$I_{iRMS} = I_{aRMS} = I_{bRMS} = I_{cRMS} = \frac{I_o}{\sqrt{3}}$$

Input Power factor (IPF) =  $\frac{\text{Active power Output}}{\text{RMS power Input}}$

$$(IPF) = \frac{V_{oavg} \times I_{oavg}}{3 \times V_i \times I_{iRMS}}$$

So we have actually  $V_{an}$   $V_{bn}$   $V_{cn}$  these are basically phase voltages and so output voltages you can see that from  $\pi/6$  to  $5\pi/6$  that means actually 30 degree to 150 degree. It will get a voltage of  $V_{an}$  and so write the  $V_{an}$  and you calculate over it similarly you can calculate actually output RMS voltage that is basically you get three such cycle so it does multiply by 3 same way for RMS value actually multiply by  $3 \int_{\pi/6}^{5\pi/6} \sqrt{2}v \sin \omega t^2 dt$ .

So you can get this actually the values for this RMS value as well as the average value you can calculate I had left it to the student to calculate. So similarly you can have the load current so that is  $V_{average}/R$  similarly  $i_{RMS} =$  it should be same input RMS that will be same for since it is a balanced system  $I_a$   $I_b$   $I_c$  should be same and we can find it out that it tell value will be actually  $i_0/\sqrt{3}$ .

So input power factor that is active power output which we have shown also in a single phase system by RMS input. So that is basically IPF actually voltage average\*current average/ $3*V_i*RMS$  so from there you can calculate physically the IPF.

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**Three Phase full wave uncontrolled Rectifier with R-L-E load**

Device Mode	$V_{D1}$	$V_{D2}$	$V_{D3}$	$V_{D4}$	$V_{D5}$	$V_{D6}$	$V_o$
$D_1, D_2$	0	0	$v_{ba}$	$v_{ca}$	$v_{ca}$	$v_{cb}$	$v_{ac}$
$D_2, D_3$	$v_{ab}$	0	0	$v_{ca}$	$v_{cb}$	$v_{cb}$	$v_{bc}$
$D_3, D_4$	$v_{ab}$	$v_{ac}$	0	0	$v_{cb}$	$v_{ab}$	$v_{ba}$
$D_4, D_5$	$v_{ac}$	$v_{ac}$	$v_{bc}$	0	0	$v_{ab}$	$v_{ca}$
$D_5, D_6$	$v_{ac}$	$v_{bc}$	$v_{bc}$	$v_{ba}$	0	0	$v_{cb}$
$D_6, D_1$	0	$v_{bc}$	$v_{ba}$	$v_{ba}$	$v_{ca}$	0	$v_{ab}$

Now, since we are discussed that this mode of the actually configuration is not preferred because it leads to the saturation of the transformer and the rate of the conversion of the power is very low generally use full control devices. The three phase full wave uncontrolled actually rectifier

with let us consider the R L E load. Now in this condition one diode from the upper leg and another diode from the lower leg will conduct.

And will actually since or one diode will conduct for the period of 120 degree so we have a different way to actually nomenclature it. Since D1 will conduct after 180 degree of its conduction so for this is and you know actually nomenclature will have a difference of 3. So that is D1 and D2 that is D1 and D4 will be the first leg and similarly D3 and D6 will be the second leg and D2 and D5 will be the 6 legs the combination is the odd combination will be up.

So D1 D3 D5 and D4 D6 D2 if you do like that then you will find that actually this sequence will come. If you name it this way actually this sequence will come. So first phase 60 degree so of course we start from the point where actually phase A and C get intersects at this point and we have waited from this point for 60 degree intervals. So it is it starts from  $\pi/6$  to  $\pi/2$  so what happened in that configurations.

Diode D1 and D2 conducts and when diode D1 and D2 conducts for this is you can see that these are 0 so and there and it is the ones actually there after what happened diode D2 D3 conducts there after D4 D3 conducts D4 D5 conducts D5 D6 conducts and then D6 D1 conducts then after D1 D2 conducts. So this will actually be the column you will get 0s so here D1 D2 conducts therefore D3 D4 start conducting it is blocking the voltage of  $v_{ba}$  and  $v_{ca}$ .

Then it is blocking the voltage of actually  $v_{ca}$  and  $v_{cb}$  and so on. So these are the pair of voltages that you continue to block. And accordingly you can actually find it out which voltage it is blocking and you can get the output voltage accordingly. So for this you know in load voltage will be delivered for this first 120 degree by actually D1 and D2 for 60 degree D1 and D2 and thus you get a voltage of actually PSE>

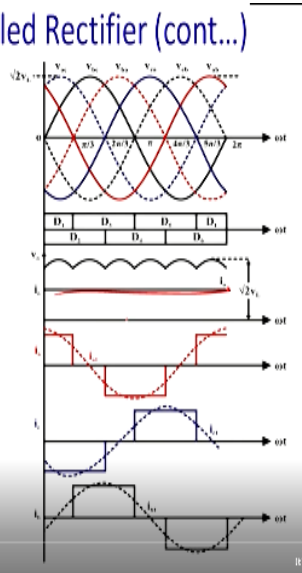
Similarly, you know when D2 D3 conducts you will get a voltage of  $v_{bc}$ . then after when D3 D4 conducts you get  $v_{ba}$  when actually D4 D5 conducts you get  $v_{ca}$ . When D D6 conducts again you will get actually reverse  $v_{cb}$  then when D6 D1 conducts you get  $v_{ab}$  and so on. So this cycle will

continue and one pair of actually diode will conduct a 60 degree and thus one single diode will conduct for the period of 120 degree.

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### Three Phase full wave uncontrolled Rectifier (cont...)

- R-L-E load represents a DC motor or battery.
- The load side inductance is quite high to keep the load current continuous.
- As load current is assumed to be continuous, one diode from upper side ( $D_1, D_3, D_5$ ) and one diode from lower side ( $D_2, D_4, D_6$ ) conduct at a time.
- But no two diodes from same leg conduct simultaneously. So it has six different diode conduction modes i.e.  $D_1D_2, D_2D_3, D_3D_4, D_4D_5, D_5D_6, D_6D_1$ .
- Each diode conducts for 120 degree and each conduction mode is of 60 degree.



So this is actually a wave form so we consider the RLE load represents the DC mode or the battery and the load side inductance is quite high to keep the load current continuous. So we have a ripple but actually this is a  $I_{dc}$  value and the load current assumed to be continuous one diode from the upper side is  $D_1, D_3, D_5$  and another diode from the lower side will conduct at a time. But no two diodes from the same leg will conduct simultaneously

Otherwise it surely leg shorting will take place ultimately no voltage will be delivered at right to the load. So it has 6 different diode mode of conduction these are  $D_1, D_2, D_3, D_4$  and so on. Each diode conducts for as I told you 120 degree and a pair of diode will conduct for the 60 degree. So this is the wave form so  $D_1$  will conduct actually thereafter  $D_3$  will come into the picture thereafter  $D_5$  thereafter  $D_1$  again.

Similarly, at this time  $D_1$  and  $D_2$  will conduct thereafter after actually at this point you know  $D_2$  will be actually  $D_1$  will be the outgoing Thyristors at 60 degree and  $D_2$  will be conducting and  $D_3$  will be the inductance. So similarly it will conduct like that and since there is a 6 such changes in 360 degree so you will have a 6 phase wave form and this value is given by under root of 2  $V_L$  and we assume that load current to be constant.

And this will be the pattern of the input current. Input current will be the stepped square wave so since actually this time D1 conducts so for this what will happen current will be positive. There after interval you can see that D4 once start conducting at this region so we will get a negative pulse from phase A. Again there is another pulse of 60 degree again it will pick up. So in a cycle of 360 it will conduct within positive or negative cycle for mode of 120 degree there will be a assume of in between 60 degree.

So there is sufficient time to actually commute similarly this is a current for phase B and phase C and this is the wave form drawn this is a fundamental of the input line currents.

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### Three Phase full wave uncontrolled Rectifier with R-L-E load

(Cont...)

For  $\pi/3 \leq \omega t \leq 2\pi/3$   

$$v_o = \sqrt{2}V_L \sin \omega t$$

$$V_{OAV} = \frac{3}{\pi} \int_{\pi/3}^{2\pi/3} \sqrt{2}V_L \sin \omega t \, d\omega t = \frac{3\sqrt{2}}{\pi} V$$

Input Power factor (IPF) =  $\frac{\text{Active power Output}}{\text{RMS power Input}}$

$$V_{ORMS} = \sqrt{\frac{3}{\pi} \int_{\pi/3}^{2\pi/3} 2V_L^2 \sin^2 \omega t \, d\omega t}$$

$$= \sqrt{\left(1 + \frac{3\sqrt{3}}{2\pi}\right)} V_L$$

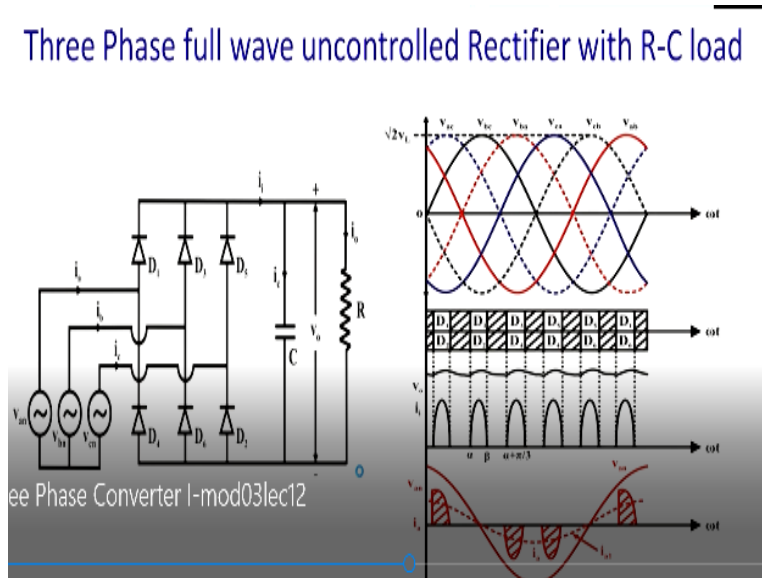
$$I_{IRMS} = \sqrt{\frac{2}{3}} I_{OAV}; \quad I_{OAV} = \frac{V_{OAV} - E}{R}$$

Now few parameters comes into the pictures now for as we start from this actually pi/3 to 2 pi/3 and AC is the amount of the voltage coming into the picture. So output voltage will be given by 3 pi/ 3 to pi 3 VL sin omega t from there we can get this basically the value of the RMS voltage. RMS voltage you can find it out at this 1+3 root 3/2 pi\*VL. So from there of course you know you have a RMS voltage just divide by the you can find it out the current.

So current will be basically root 2/3 \* which is assumed to be cost term that is output load current and the output load current is given by this basically Vab so that is the average voltage

that is  $\sqrt{3/2} / \pi * V_L - E / R$ . So from there we can calculate the RMS voltage as well as the RMS current. so input power factor for IPF will be the active power output/RMS power input.

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So now let us see that what happen if this actually three phase full wave uncontrolled rectifier fitting in RC load that is quite common you know actually most of the application nowadays are adjustable speed drive. In case of the adjustable speed drive actually you can have a variable kind of load and what happen you know you fit to an inverter to run it in the drives in a different manner.

And for this kind of wave form is quite common in case of this actually in different kinds of industrial applications and this capacitor essentially actually filtered out the ripple and gives you more or less a constant DC voltage. So similarly this is a three phase wave form as we have discussed so here what will happen till the input voltage this input voltage  $V_{an}$  is more than  $V_{ac}$  that will not conduct.

So output voltage you know it will hold by the capacitor this will have this kind of value you will have a ripple that depends on the load current as well as the size of the capacitor. So due to that what will happen if so till this voltage is more than this voltage diode will not be forward by us and thus no current will flow and thus diode current might be picky. So it will conduct or the D1 D2 will conduct for this pretty small interval on time.

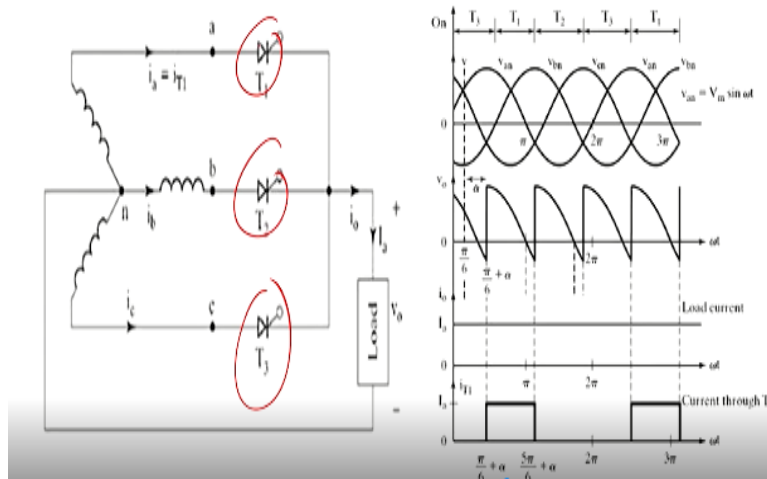


Let us see that it is  $\alpha + 2\beta$  similarly you know current will have this kind of choppy profile and it is quite disturbance and it is a unique problem to be solved for this is one of the issues with the power quality because you can see that actually it gives a choppy current and you have an actually a sinusoidal voltage. So this is a problem once you have an actually artsy kind of load and nowadays its prevalence

Now let us come to the three phase half-wave controller rectified. Now since most of the application we required are constrained source in DC kind of application for this is an we prefer to have a control rectifier.

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### Three Phase half wave controlled Rectifier



So there is a Thyristor  $i_{T1}$  and there is no difference in between the diode and the Thyristor we required to trigger the forward most forward Thyristor depending on the voltages and automatically other Thyristor will naturally commutate it. Because if this let us say that previously b phase was the most positive and Thyristor T2 was actually conducting the moment actually F has become more positive.

Or definitely the reverse bias will be applied and the thyristor will commute. So for this what we required to do let us assume let us start from the point where actually am is a most positive phase and it has been given at an angle delay angle  $\alpha$ . So it will trigger at an angle  $\alpha$  so that is

the point where actually T1 will be triggered on it will continue till conduction there after you know when it is actually you see that actually most positive phase is actually T2 phase b.

Then T2 decode so each thyristors will conduct for a period of the same wave 120 degree and so this will be the profile of the load voltages and like that you know controlled rectifier you get since it is a we assumed that actually this load is RL type of load for this is the negative portion of that load voltage will come into the picture and we assume and since this is a lot current is assumed to be constant so we will have a input current will be given by like this.

And but problem of this halfwave rectifier or the converter is same because you can see that and actually this load current is positive in input side and that leads to the saturation of the transformer so for this is an it is not at all used when most of them we are phasing out it same way we have a calculations, we can do the calculations that is a 3 pulses 360 degree cycles.

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### Three Phase half wave controlled Rectifier (Cont...)

Output average and RMS voltages

$$V_{oavg} = \frac{3}{2\pi} \int_{\alpha+\pi/6}^{\alpha+5\pi/6} \sqrt{2}v \sin \omega t d(\omega t)$$

$$V_{orms} = \left[ \frac{3}{2\pi} \int_{\alpha+\pi/6}^{\alpha+5\pi/6} (\sqrt{2}v \sin \omega t)^2 d(\omega t) \right]^{1/2}$$

Input Power factor (IPF) =  $\frac{\text{Active power Output}}{\text{RMS power Input}}$

$$(IPF) = \frac{V_{oavg} \times I_{oavg}}{3 \times V_i \times I_{iRMS}}$$

Output average current and Input RMS current

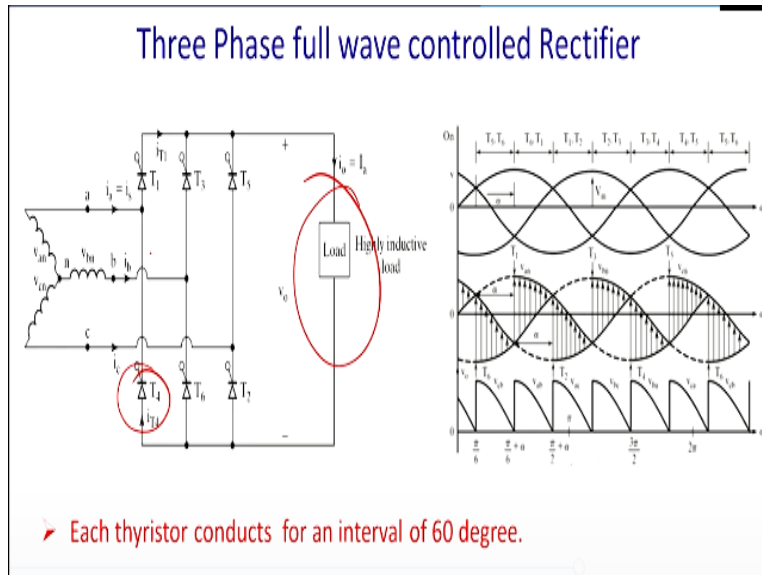
$$I_{oavg} = \frac{V_{oavg}}{R}$$

$$I_{iRMS} = I_{aRMS} = I_{bRMS} = I_{cRMS} = \frac{I_o}{\sqrt{3}}$$

So it is alpha+ pi/6 to alpha +5 pi/6 from there we can calculate the vRMS and IRMS and ultimately from there we can divided it by R to calculate the average current and IRMS you will find that I0/root 3 by simple calculations since it is a square. So similarly we can calculate the input power factor that is V output average/ I output average \*3\*Vrms\*Irms. So let us come to the more practicable solutions of the three phase.

And where load is assumed to be highly inductive three phase full wave rectifier and same the nomenclature we have used in case of the diode that is T1 T3 T5.

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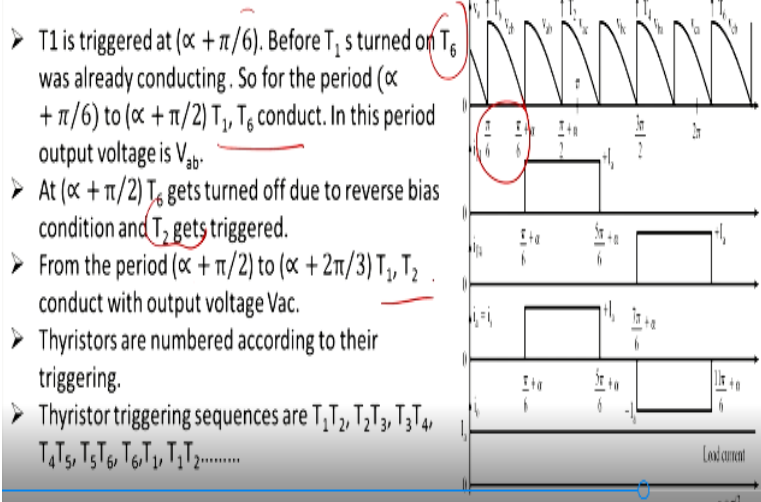
So since it will be conducting and one pair of Thyristor will be conducting for the period of 60 degree  $\pi/3$  and 1 thyristor itself will be conducting for the period of 120 degree and what will happen here in this case essentially we will have a same kind of actually nomenclature that is T1 T3 T5 are the upper thyristors and T4 T6 T2 are the lower thyristors. So you trigger the point where phase A and phase C are crossing over.

So given a delay angle  $\alpha$  so you will start from this point so T5 will be the outgoing Thyristor from the top and so T6 and T1 is conducting. So you will get phase A B across the load. Similarly, there after T1 T2 is conducting and you get AC to the load there after you get T2 T3 is conducting you get CB to the load so on and frequently you will get so you can see that here it is inactive so you get  $V_{an}$  into the load.

Similarly, you know you triggered this load Thyristor here there after you get  $V_{bm}$  to the load then you will get  $V_{cn}$  to the load. So here if you start from here so first you get  $V_{ab}$  there after you get  $V_{ac}$  across the load there after you get  $V_{bc}$  thereafter you get  $V_{ba}$  there after  $V_{ca}$  there after  $V_{cb}$  and this will continue. So this is the configuration of that full control bridge rectifier

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## Three Phase full wave controlled Rectifier (Cont...)



- $T_1$  is triggered at  $(\alpha + \pi/6)$ . Before  $T_1$  is turned on  $T_6$  was already conducting. So for the period  $(\alpha + \pi/6)$  to  $(\alpha + \pi/2)$   $T_1, T_6$  conduct. In this period output voltage is  $V_{ab}$ .
- At  $(\alpha + \pi/2)$   $T_6$  gets turned off due to reverse bias condition and  $T_2$  gets triggered.
- From the period  $(\alpha + \pi/2)$  to  $(\alpha + 2\pi/3)$   $T_1, T_2$  conduct with output voltage  $V_{ac}$ .
- Thyristors are numbered according to their triggering.
- Thyristor triggering sequences are  $T_1T_2, T_2T_3, T_3T_4, T_4T_5, T_5T_6, T_6T_1, T_1T_2, \dots$

So here it is same as we have discussed in case of the diodes so it is triggered for an angle  $\alpha$  to  $\pi/6$  before  $T_1$  is turned on  $T_1$  and  $T_6$  is conducting  $T_6$  is already conducting and  $T_5$  was the outgoing Thyristors. So the period  $\alpha$  actually it is  $\alpha + \pi/6$  to  $\alpha + \pi/2$  where the point  $T_1, T_6$  is conducting and this is the actually the configurations so you get  $cb$  there after  $ab$  and consequent voltages.

At  $\alpha + \pi/2$   $T_6$  gets turned off due to the reverse bias condition conduction and  $T_2$  get triggered. From this period actually  $\alpha + \pi/2$  to  $\alpha + 2\pi/3$   $T_1$  and  $T_2$  both are conducts. So Thyristors are according to be triggered in the sequence  $T_1, T_2, T_3, T_4, T_5, T_6$  and so on and this is basically assuming that is a constant load current so this is the current through the thyristor  $T_1$ .

And this is the current through the thyristors  $T_4$  that is the lower leg of the phase  $a$  and thus load current source current will be this and load current will be this since it is a positive or negative cycle so it can be used in case of the transformer also.

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## Three Phase full wave controlled Rectifier (Cont...)

Input three phase voltages

$$\begin{aligned}
 V_{an} &= \sqrt{2}v \sin \omega t \\
 V_{bn} &= \sqrt{2}v \sin \omega t - 2\pi/3 \\
 V_{cn} &= \sqrt{2}v \sin \omega t + 2\pi/3 \\
 V_{ab} &= V_{an} - V_{bn} = \sqrt{6}v \sin(\omega t + \pi/6)
 \end{aligned}$$

$$\text{Input Power factor (IPF)} = \frac{\text{Active power Output}}{\text{RMS power Input}}$$

$$(\text{IPF}) = \frac{V_{oavg} \times I_{oavg}}{3 \times V_i \times I_{iRMS}}$$

Output average and RMS voltages

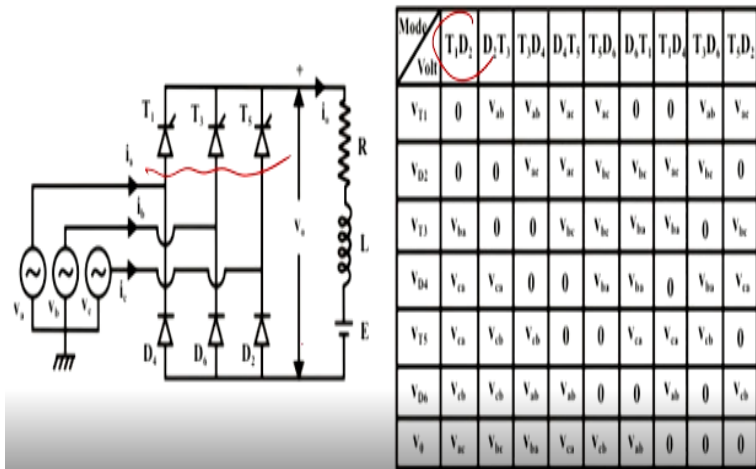
$$V_{oavg} = \frac{3}{\pi} \int_{\alpha+\pi/6}^{\alpha+\pi/2} \sqrt{6}v \sin(\omega t + \pi/6) d(\omega t)$$

$$V_{orms} = \left[ \frac{3}{\pi} \int_{\alpha+\pi/6}^{\alpha+\pi/2} (\sqrt{6}v \sin(\omega t + \pi/6))^2 d(\omega t) \right]^{1/2}$$

So it does not lead to the saturation on the transformer similarly we required to calculate that actually the Vrms and the average voltages. So students are requested to calculate this value you know actually this is a simple integrations and it is available in normal any textbook.

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## Three Phase full wave half controlled Rectifier



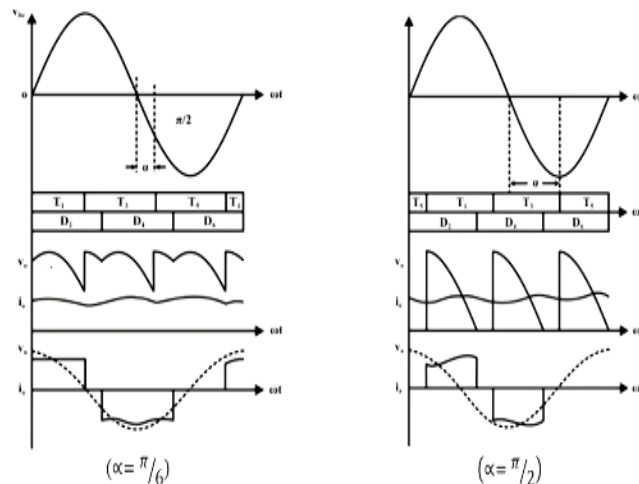
So this is the pattern same way we have discussed in case of the diode now this is for half controlled rectifier or converter. So here upper legs will be Thyristors and lower legs will be diode. So you have a control over triggering the thyristor and automatically actually negatives phase will be triggered depending on the actually which phase is most negative. So thus what you can see that let us see that again nomenclature will be the same.

As used in case of the full control converter so it is D4 D6 D2 I so when T1 an D1 is conducting so voltage across the thyristors 1 is 0 and will continue till 60 degree that it is blocking the voltage  $V_{ab}$  and ultimately what will happen though these are the voltage they will be blocking throughout it and so similarly when D2 is basically conducting and it will be conducting for the period of 120 degree.

So it will conduct till 30 degree to 150 degree thereafter other voltage will follow like that. So again it will be conducting here. Similarly, you can see that D3 will be conducting for the period here as well as here. So this is the case will be continue and its matrix will be actually featured him and accordingly it get a voltage.

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### Three Phase full wave half controlled Rectifier (Cont...)



So this will be the pattern so T1 will be conducting for this period as shown here and we can apply a delay to it and output voltage since we can change the delay so output voltage can be changed depending on the profile and assuming that load current is almost constant and so this will be the actually the input current and this will be the fundamental. Same way if you have actually this wave form where have a large delay angle?

So then what will happen? so you can see that this will be the pattern first it will trigger with the T5 thereafter T3 T1 thereafter T3 thereafter T5 and but what will happen then you can find that actually lower half will continue as per the sequence so (( )) (28:10) this leads to the actually a

discontinuous voltage we had talked about discontinuous current. So we will have a discontinuous voltage when actually it will be discontinuous.

If the triggering angle will be more than 90 degree in case half controlled converter three phase half controlled converter. And this will be that this kind of way for full control this will be the continuous form. So pattern of the wave form will change till  $\alpha = 0$  to 30 degree and thereafter  $\alpha$  more than 90 degree. We shall continue our discussions with the three phase half controller with his mathematical analysis in our next class. Thank you.