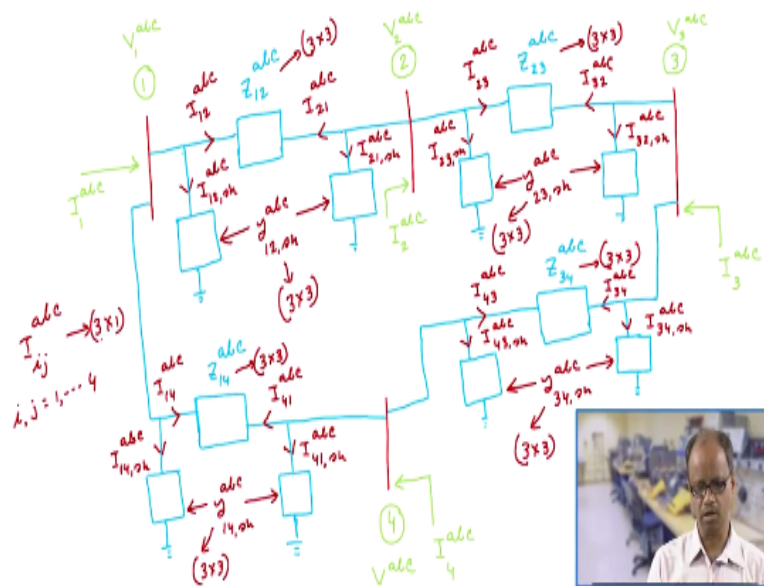


Computer Aided Power System Analysis
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Lecture - 51
Fault Analysis (Cont)

Hello friends. Welcome to this lecture on Computer Aided Power System Analysis. We have been discussing the process of building the Y bus matrix for an unbalanced 3 phase network so let us continue.

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So what we have done is that we have taken a simple 4 bus, 4 line system and we have also drawn its equivalent circuit as shown. Now with this equivalent circuit now in this equivalent circuit we have already integrated all these voltages as well as the currents. And also we have talked about the various impedances as well as the admittances and now we are ready to start writing the equations.

But before we start writing the equation for this entire network we should first talk about that how to write down the equations for individual current in the series branch as well as the individual current in the shunt branch because once we understand that how to write down the equations for the individual currents in the series branch as well as individual current in the shunt branch then we would be able to write down these equations for this entire network.

So let us consider again as usual which we have already shown that a line between bus m and

n and that particular and in that line bus voltage at bus m is given by V_{mabc} as well as bus n V_{nabc} and here I_{mnabc} and here let us say that we said it is I_{mn} , shunt abc. So now let us try to try to write down the equation for this 2 current.

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$$\begin{bmatrix} V_m^a \\ V_m^b \\ V_m^c \end{bmatrix} = \begin{bmatrix} V_n^a \\ V_n^b \\ V_n^c \end{bmatrix} + \begin{bmatrix} Z_{mn}^{aa} & Z_{mn}^{ab} & Z_{mn}^{ac} \\ Z_{mn}^{ba} & Z_{mn}^{bb} & Z_{mn}^{bc} \\ Z_{mn}^{ca} & Z_{mn}^{cb} & Z_{mn}^{cc} \end{bmatrix} \begin{bmatrix} I_{mn}^a \\ I_{mn}^b \\ I_{mn}^c \end{bmatrix}$$

$I_{mn}^p \rightarrow$ complex current flowing in phase 'p' of the series branch of the line between the buses 'm' and 'n'. $p = a, b, c$


$$I_{mn}^{abc} = \begin{bmatrix} I_{mn}^a & I_{mn}^b & I_{mn}^c \end{bmatrix}^T \rightarrow (3 \times 1)$$

$$V_m^{abc} - V_n^{abc} = Z_{mn}^{abc} I_{mn}^{abc}$$

$$\Rightarrow I_{mn}^{abc} = \left[Z_{mn}^{abc} \right]^{-1} (V_m^{abc} - V_n^{abc})$$

$$= Y_{mn}^{abc} (V_m^{abc} - V_n^{abc})$$

$Y_{mn}^{abc} = \left[Z_{mn}^{abc} \right]^{-1}$
 $\downarrow (3 \times 3)$



So now what do we have is we have V_m if I write down in the matrix V_m , V_n or rather if I apply this KVL- $V_m - V_n$, V_n that is obviously would be given by. So this voltage- this voltage would be obviously given by this total drop in this series branch and total drop in the series branch would be given by Z_{mnabc} so that is essentially Z_{mnaa} , Z_{mnab} , Z_{mnac} then Z_{mnba} , Z_{mnbb} , Z_{mnbc} that is the convention we have taken yes.

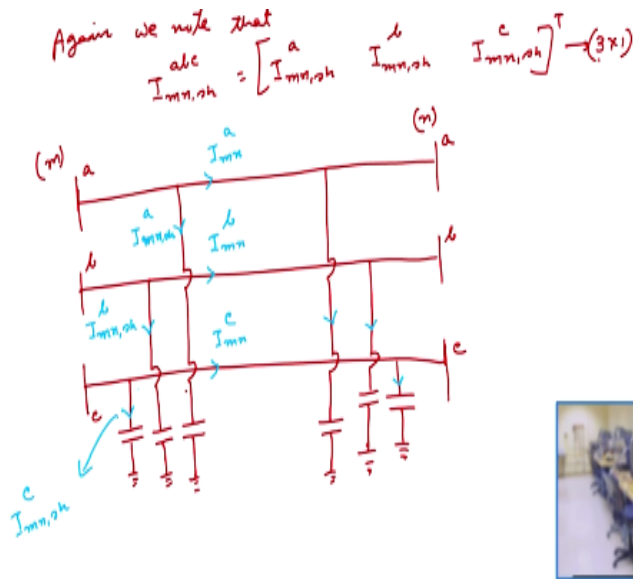
And lastly Z_{mnca} Z_{mncb} , Z_{mncc} * I_{mna} , I_{mnb} , I_{mnc} . What is this quantity I_{mna} , I_{mnb} , I_{mnc} . So we will write I_{mnp} is actually the complex current flowing in phase P of the series branch of the line between the buses m and n and where of course P= phase a, phase b, phase c. So here when we are writing that this is I_{mnabc} so we must note now probably we are now sure that when I say that I_{mnabc} is actually a vector and this is I_{mna} , I_{mnb} , I_{mnc} transpose.

So this is again a 3 cross 1 transpose. So then therefore this equation can be written as so this equation can be written as $V_m - V_n = Z_{mnabc} * I_{mnabc}$. So then therefore $I_{mnabc} = Z_{mnabc}^{-1} (V_m - V_n)$ because it is a 3 cross 3 matrix inverse * $V_m - V_n$. So we call it let us say $Y_{mnabc} * (V_m - V_n)$ so that is the expression of the current I_{mnabc} . We note that Y_{mnabc} is Z_{mnabc}^{-1} we note that Y_{mnabc} is Z_{mnabc} inverse.

So this is again 3 cross 3 matrix right. So this is the expression of I_{mnabc} . Now what is the

expression of current $I_{mn, sh}$.

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Again we note so basically we note that $I_{mn, shunt abc} = I_{mn, shunt phase a}, I_{mn, shunt phase b}, I_{mn, shunt phase c}$. So these are the 3 individual currents transpose this is a 3 cross 1. So essentially what is happening essentially physically what is happening that I do have a line between bus m and n bus m and n. So physically there are 3 lines right. So this is phase a, phase b, phase c this is bus m, this is bus n.

And we have already denoted that well there are impedances individual $(\)$ (08:45) they are impedances mutual impedances between any 2 phases. On top of that there are also shunt line charging susceptance or shunt half line charging susceptances between any phase at the ground between any phase in the ground because of their proximity I mean they will have their individual admittance and also because of their proximity.

They will also have their mutual admittance between these 2 and this 2 as well as this 2. So this and again so this is it. So when we are saying I_{mna} , so I_{mna} is actually this current. So when you are saying that it is I_{mna} is actually this current I_{mnb} is actually I_{mnc} is actually this current and when we are talking about $I_{mn, sh}^a$ this is $I_{mn, sh}^a$ so this is the shunt. This is $I_{mn, shunt}$ for b and this is similarly $I_{mn, shunt}$ at phase c.

So these are the 3 currents we are talking about. Similarly, also there are 3 currents here similarly over there also current $(\)$ (10:34). So basically or physically this is the case right. We have just now derived the expression of these 3 currents in terms of these 3 voltages and

as well as this 3 voltages. Now we have to derive the expression of these 3 currents in terms of this voltage and as well as the (\cdot) (10:58) matrix.

Now if we look at this obviously the current here because this is the shunt current it would be something like this voltage multiply by this admittance, but because this is a 3 phase voltage so this is the 3 cross 1 this is the 3 cross 3.

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$$\begin{bmatrix} I_{mn,sh}^a \\ I_{mn,sh}^b \\ I_{mn,sh}^c \end{bmatrix} = \begin{bmatrix} y_{mn,sh}^{aa} & y_{mn,sh}^{ab} & y_{mn,sh}^{ac} \\ y_{mn,sh}^{ba} & y_{mn,sh}^{bb} & y_{mn,sh}^{bc} \\ y_{mn,sh}^{ca} & y_{mn,sh}^{cb} & y_{mn,sh}^{cc} \end{bmatrix} \begin{bmatrix} V_m^a \\ V_m^b \\ V_m^c \end{bmatrix}$$

(3×1) (3×3) (3×1)

$I_{mn,sh}^{abc} = y_{mn,sh}^{abc} V_m^{abc}$



So then we can simply write down the equation is $I_{mn, sh}^a = I_{mn, sh}^b$ and $I_{mn, sh}^c$ so this is a 3 cross 1 matrix and this would be $y_{mn, sh}^{aa}$, $y_{mn, sh}^{ab}$, $y_{mn, sh}^{ac}$, $y_{mn, sh}^{ba}$, $y_{mn, sh}^{bb}$, $y_{mn, sh}^{ca}$, $y_{mn, sh}^{cb}$, $y_{mn, sh}^{cc} * V_m^a$, V_m^b , V_m^c right. So this is the 3 cross 1 vector this is the 3*3 matrix this is the 3 cross 1 vector. So we write that $I_{mn, sh}^{abc}$ is nothing $y_{mn, sh}^{abc} * V_m^{abc}$.

So this is the relation between the bus voltages this bus and this current. So similarly the current here would be if I say that this is $I_{mn, sh}^{abc}$ at this stage it would be and this current would be nothing but $y_{mn, sh}^{abc} * V_m^{abc}$. So let us say this current would be nothing but so this current I can write that this current is nothing but $y_{mn, sh}^{abc} * V_m^{abc}$ right. So with this background so now we are ready to write down the equation for this entire system. So we write down the equations for this system.


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Equations for the complete system

Bus 1

$$\begin{aligned}
 I_1^{abc} &= I_{12,sh}^{abc} + I_{12}^{abc} + I_{14,sh}^{abc} + I_{14}^{abc} \\
 &= y_{12,sh}^{abc} V_1^{abc} + y_{12}^{abc} (V_1^{abc} - V_2^{abc}) + y_{14,sh}^{abc} V_1^{abc} + y_{14}^{abc} (V_1^{abc} - V_4^{abc}) \quad \text{--- ①} \\
 &= \left(y_{12,sh}^{abc} + y_{12}^{abc} + y_{14,sh}^{abc} + y_{14}^{abc} \right) V_1^{abc} - y_{12}^{abc} V_2^{abc} - y_{14}^{abc} V_4^{abc} \quad \text{--- ①} \\
 y_{12}^{abc} &= \left(Z_{12}^{abc} \right)^{-1}; \quad y_{14}^{abc} = \left(Z_{14}^{abc} \right)^{-1}; \quad y_{23}^{abc} = \left(Z_{23}^{abc} \right)^{-1}
 \end{aligned}$$

Bus 2

$$\begin{aligned}
 I_2^{abc} &= I_{21,sh}^{abc} + I_{21}^{abc} + I_{23,sh}^{abc} + I_{23}^{abc} \\
 &= y_{12,sh}^{abc} V_2^{abc} + y_{12}^{abc} (V_2^{abc} - V_1^{abc}) + y_{23,sh}^{abc} V_2^{abc} + y_{23}^{abc} (V_2^{abc} - V_3^{abc})
 \end{aligned}$$


So equations for the complete system. So now here we have already shown that if I take this injected current this injected current= ultimately this current+ this current+ this current+ this current. So then therefore we can write down that I_1^{abc} . So I_1^{abc} = you can write down that now $I_{12, sh}^{abc}$ is nothing but $y_{12, sh}^{abc} * V_1^{abc}$. Now here we can write that $I_{12, sh}^{abc}$ + I_{12}^{abc} + I_{14}^{abc} + $I_{14, sh}^{abc}$ + $I_{14, shunt}^{abc}$ + I_{14}^{abc} .

So this is from the applying KCL. Now I want to shunt abc is nothing but $y_{12, shunt}^{abc} * V_1^{abc}$. I_1^{abc} would be $y_{12}^{abc} * V_1^{abc} - V_2^{abc}$ right y_{12}^{abc} is similarly $I_{14, shunt}^{abc}$ would be $y_{14, shunt}^{abc} * V_1^{abc}$ please look at this if I look at this because this shunt branch is also ultimately connected at this branch. So then therefore $I_{14, sh}^{abc}$ would be this admittance * this I mean this admittance matrix * this particular voltage vector+ it is I_{14}^{abc} is $y_{14}^{abc} * V_1^{abc} - V_4^{abc}$.

So then therefore if I now take all this V_1^{abc} terms together so $y_{12, sh}^{abc}$ + y_{12}^{abc} + $y_{14, sh}^{abc}$ + y_{14}^{abc} there should not be any comma here y_{14}^{abc} . So this * $V_1^{abc} - y_{12}^{abc} * V_2^{abc} - y_{14}^{abc} * V_4^{abc}$ so this is equation one. Here we note that y_{12}^{abc} is actually Z_{12}^{abc} inverse and $y_{14}^{abc} = Z_{14}^{abc}$ inverse. So this is at bus 1. At bus 2 what would be the current this is at bus 2.

At bus 2 if I look at this picture I_2^{abc} would be= this current+ this current+ this current+ this current. So we can write down $I_2^{abc} = I_{21, shunt}^{abc}$, I_{21}^{abc} , $I_{23, shunt}^{abc}$ and I_{23}^{abc} . So at bus 2 $I_2^{abc} = I_{21, shunt}^{abc}$ + I_1^{abc} + $I_{23, shunt}^{abc}$ + I_{23}^{abc} right. An $I_{21, shunt}^{abc}$ would be nothing but $y_{21, shunt}^{abc}$. In fact, it should be $y_{12, shunt}^{abc}$ because

y₁₂, shunt abc because this same admittance is connected.

So it is y₁₂, shunt abc so we should write y₁₂, shunt abc* V_{2abc}+ y_{12abc}* V_{2abc}-V_{1abc}+ I₂₃, shunt abc is y₂₃, shunt abc* V_{2abc}+y_{23abc} *V_{2abc}- V_{3abc}. We again note that y_{23abc} is nothing but Z_{23abc} inverse. So therefore I_{2abc}= -y_{12abc} V_{1abc}. So it is -y_{12abc} *V_{1abc}+ y₁₂, shunt abc+ y_{12abc} sorry.

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$$\Rightarrow I_2^{abc} = -y_{12}^{abc} V_1^{abc} + (y_{12,2h}^{abc} + y_{12}^{abc} + y_{23,2h}^{abc} + y_{23}^{abc}) V_2^{abc} - y_{23}^{abc} V_3^{abc} \quad \text{--- (2)}$$

Bus 3

$$I_3^{abc} = I_{32,2h}^{abc} + I_{32}^{abc} + I_{34,2h}^{abc} + I_{34}^{abc}$$

$$= y_{23,2h}^{abc} V_3^{abc} + y_{23}^{abc} (V_3^{abc} - V_2^{abc}) + y_{34,2h}^{abc} V_3^{abc} + y_{34}^{abc} (V_3^{abc} - V_4^{abc})$$

$$\Rightarrow I_3^{abc} = -y_{23}^{abc} V_2^{abc} + (y_{23,2h}^{abc} + y_{23}^{abc} + y_{34,2h}^{abc} + y_{34}^{abc}) V_3^{abc} - y_{34}^{abc} V_4^{abc} \quad \text{--- (3)}$$

$$y_{34}^{abc} = (Z_{34}^{abc})^{-1}$$

Bus-4

$$I_4^{abc} = I_{41,2h}^{abc} + I_{41}^{abc} + I_{43,2h}^{abc} + I_{43}^{abc}$$



s

y₁₂, shunt abc+ y_{12abc}+ y₂₃, shunt abc+ y_{23abc} that is= V_{2abc}- y_{23abc}* V_{3abc}- y_{23abc} * V_{3abc}. So this is equation 2. At bus 3 what we have so at bus 3 if I apply this same principle I_{3abc}= I₃₂, shunt abc+ I_{32abc}+ I₃₄, shunt abc+ I_{34abc}. So it is I₃₂, shunt abc. So it is I₃₂ y_{3abc} it is I₃₂, shunt abc+ I_{32abc}+ y₃₄, shunt abc+ y_{34abc}. Y_{32abc} is so it is y₂₃ shunt abc* V_{3abc}+y_{23abc} * V_{3abc}-V_{2abc} and this is y₃₄, shunt abc*V_{3abc}+ y_{34abc} * V_{3abc} -V_{4abc}.

So then therefore I_{3abc} is essentially V₂ V₄ so it is -y_{23abc} V_{2abc}+ y₂₃, shunt abc+ y_{23abc}+ y₃₄, shunt abc+ y_{34abc} *V_{3abc}-y_{34abc} *V_{4abc}. So this is equation 4 and we again note that y_{34abc}= Z_{34abc} inverse right. Similarly, at bus 4 very quickly if we write at bus 4. I_{4abc}= I₄₁, shunt abc+ I_{41abc}+ I_{43abc}+ I₄₃, shunt abc. So it is I₄₁, shunt abc+ I_{41abc}+ I₄₃, shunt abc+ I_{43abc}.

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$$\begin{aligned}
I_4^{abc} &= y_{14,abc} V_4^{abc} + y_{14}^{abc} (V_4^{abc} - V_1^{abc}) + y_{34,abc} V_4^{abc} + y_{34}^{abc} (V_4^{abc} - V_3^{abc}) \\
&= -y_{14}^{abc} V_1^{abc} - y_{34}^{abc} V_3^{abc} + (y_{14,abc} + y_{14}^{abc} + y_{34,abc} + y_{34}^{abc}) V_4^{abc} \\
&\dots \textcircled{4}
\end{aligned}$$

So then therefore $I_4^{abc} = y_{14, abc} * V_4^{abc} + y_{14}^{abc} * V_4^{abc} - V_1^{abc} + y_{34, abc} * V_4^{abc} + y_{34}^{abc} * V_4^{abc} - V_3^{abc}$. So if I take them together so I get $-y_{14}^{abc} V_1^{abc} - y_{34}^{abc} * V_3^{abc} + y_{14, abc} + y_{14}^{abc} + y_{34, abc} + y_{34}^{abc} * (())$ (28:42). So you see we have got all this 4 equations here. So now what we have to do we have to now write all this 4 equations in a matrix form and then what kind of conclusion we can draw. This, we will do in the next lecture. Thank you.