

Computer Aided Power System Analysis
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Lecture - 12
Newton - Raphson Load Flow (NRLF) in Polar Co-Ordinate

Hello welcome to this another lecture of this course computer aided power system analysis. In the last lecture we have looked at the basic procedure of the Newton – Raphson numerical method. Today, starting with this class, starting with this lecture as well as the for the next few lectures we would be discussing about how to apply this basic Newton – Raphson numerical method for the solution of the power flow equations.

Now as we have already indicated earlier Newton – Raphson method is actually of two type. One is called the polar method another is called the rectangular method. So first let us try to understand what is meant by the polar method and what is meant by the rectangular method and after that we will today start with the Newton – Raphson polar method.

(Refer Slide Time: 01:34)

Unknowns for load flow solution $\rightarrow \bar{V}_i \quad \forall i = 1, 2, \dots, N$
 $\Rightarrow \bar{V}_i = V_i \angle \theta_i$
 $= e_i + jf_i$
 Polar method: V_i, θ_i
 Rectangular method: e_i, f_i
 number of buses in the system
 $e_i = V_i \cos \theta_i$
 $f_i = V_i \sin \theta_i$
 Newton-Raphson load flow (NRLF) in Polar co-ordinate.
 Load-flow (power flow equations):
 $P_i = \sum_{k=1}^N V_i V_k Y_{ik} \cos(\theta_i - \theta_k - \alpha_{ik})$

So in polar method now we have already discussed that our unknowns are actually unknowns for load flow solution are actually complex voltage V_i for all $i = 1, 2$ to capital N where N is the number of bus in the system. Now because V_i is a complex quantity so then V_i can be written

as magnitude V_i and angle θ_i . And e_i also can be written as $e_i + jf_i$ where e_i is the real part and f_i is the imaginary part.

Of course e_i would be $= V_i \cos \theta_i$ and f_i would be $V_i \sin \theta_i$. So now what happens is that in the case of polar method our unknowns are V_i and θ_i . That is basically the magnitude and the angle. And in the rectangular method our unknowns are e_i and f_i . So then therefore so this is only difference. So then essentially in the case of the polar method we do solve for the angle directly as well as also the voltage magnitudes.

On the other hand in the rectangular method we do not solve for the voltage magnitude and the angle directly. We rather solve for the real and imaginary part of the voltages and then afterwards from this real and imaginary part of the voltages we do calculate the voltage magnitude and angles. Now from today we would be actually starting with Newton – Raphson polar method.

So we start with Newton – Raphson load flow, we call it NRLF, Newton – Raphson load flow in polar coordinate. We call it polar coordinate. Now we know that our load flow equations are load flow equations or rather power flow equations we also call load flow or power flow equations are $P_i = V_i \sum_{k=1}^N V_k Y_{ik} (\cos \theta_i - \theta_k - \alpha_{ik})$ where $k = 1$ to N .

(Refer Slide Time: 05:27)

$$Q_i = \sum_{k=1}^N V_i V_k Y_{ik} \sin(\theta_i - \theta_k - \alpha_{ik})$$

Three types of buses	known	unknown
slack-bus —	$V_i, \theta_i = 0$	—
PV bus —	V_i, P_i	$\theta_i \quad \forall i = 2, \dots, M$
PQ bus —	P_i, Q_i	$V_i, \theta_i \quad \forall i = M+1, \dots, N$

N-Bus system
M-generators
 1 → slack
 2, ..., *M* → PV
M+1, *M*+2, ..., *N* → PQ

In total
 θ_i to be calculated $\forall i = 2, \dots, M$
 V_i to be calculated $\forall i = M+1, \dots, N$
 Total number of unknown θ_i
 $= (N-1)$

And $Q_i = V_i \sum_{k=1}^N Y_{ik} \sin(\theta_i - \theta_k - \alpha_{ik})$ $k = 1$ to N . And we have already seen what are these quantities. For example Y_{ik} is nothing but the magnitude of the element of the bus admittance matrix corresponding to the i th or j th column and α_{ik} is the corresponding angle and P_i and Q_i are the injected real power and the injected reactive power at bus i . Now let us see that what is the total number of unknown.

So to essentially understand that we have to now first understand that what are the unknowns at different buses. Now we have already discussed that there are 3 types of buses. So there are 3 types of buses and these 3 types of buses, one is slack bus one is PV bus one is PQ bus. At slack bus known are V_i and θ_i that $= 0$. So then unknown are actually nothing, nil. Because we are only trying to solve for the voltage magnitude and angle at all the buses.

And after that if we know this voltage magnitude and angles at all the buses we would be able to calculate anything and everything. So then therefore here we do not take that our unknown is P_i and Q_i . Rather we say that at how many buses voltage magnitude or angle or both are unknown. I mean that is what we are now trying to see. At PV buses we know that our known is V_i and P_i . So then unknown would be θ_i and at PQ buses our specified quantities are P_i and Q_i .

So therefore my unknown would be V_i and θ_i . Now if I have got as we have already said, we always say that there are N - Bus system, M – generators. That is our convention. Bus 1 is slack, 2 to M are PV and $M + 1$ to $M + 2$ to N are PQ. So this is our convention. So then therefore θ_i would be known. So then therefore here this θ_i would be unknown for $i = 2$ to M and here V_i and θ_i would be unknown for $i = M + 1$ to N .

So then in total θ_i are unknown for θ_i to be calculated for all i if we do combine this is equal to 2 to N and V_i to be calculated for all $i = M + 1$ to N . So then therefore total number of unknown θ_i , this is equal to $(N - 1)$ here from here.

(Refer Slide Time: 09:51)

Total number of unknown $V_i = (N-M)$
 \Rightarrow Total number of unknown $= (N-1) + (N-M) = \underline{2N-M-1}$

We denote our unknown vectors as

$$\bar{V} = [V_{M+1}, V_{M+2}, \dots, V_N]^T \rightarrow (N-M) \times 1$$

$$\bar{\theta} = [\theta_2, \theta_3, \dots, \theta_N]^T \rightarrow (N-1) \times 1$$

$$P_i = \sum_{k=1}^N V_i V_k Y_{ik} \cos(\theta_i - \theta_k - \alpha_{ik}) = P_i(\bar{\theta}, \bar{V})$$

$$Q_i = \sum_{k=1}^N V_i V_k Y_{ik} \sin(\theta_i - \theta_k - \alpha_{ik}) = Q_i(\bar{\theta}, \bar{V})$$

And similarly total number of unknown $V_i =$ it would be $(N - M)$. So it is $(N - M)$. So then therefore total number of unknown $= (N - 1) + (N - M) = 2N - M$. Now we denote our unknown vectors as V . This is an unknown vector V and this is actually the unknowns are $[V_{M+1}, V_{M+2}, \dots, V_N]$ transpose. So this would be an $(N - M) \times 1$ vector and theta this is an unknown theta. This is theta 2, theta 3 up to theta N^T transpose. So it would be a column vector.

So it would be $(N - 1) \times 1$. Now when we look at the expression of P_i again I write it is $V_i V_k Y_{ik} \cos(\theta_i - \theta_k - \alpha_{ik})$ $k = 1$ to N . So we can see that in this expression of P_i these quantities V_{M+1}, V_{M+2}, V_N are already present as well as theta 2, theta 3, theta N are also present. So then therefore any expression of P_i can be written as some function we also call it I mean with an abuse of the convention or rather with an abuse of the notation we call it that P_i is a function of vector theta and vector V .

Similarly, we can write down that Q_i which is $k = 1$ to $N V_i V_k Y_{ik} \sin(\theta_i - \theta_k - \alpha_{ik})$. So this also can be written as that it is also a vector of sorry it is also an function of the unknown vectors theta and V . So then therefore each of this quantity is also a function of unknown vectors. Now let us see now what we have already said that our total number of unknown is $2N - N - 1$.

So now if we wish to solve for this total $2N - N - 1$ unknown quantities we also should have this many number of equations. So now let us see from where we will get this many number of equations. Now equations would be only found out only from the known quantities. Now let us see that what are the known quantities, the known quantities.

(Refer Slide Time: 14:16)

The handwritten notes show the following:

- known quantities
- $P_i : \forall i = 2, \dots, M \rightarrow$ PV bus \rightarrow Number $(M-1)$
- $P_i : \forall i = M+1, M+2, \dots, N$ } PQ-bus \rightarrow $(N-M)$
- $Q_i : \forall i = M+1, M+2, \dots, N$ } \rightarrow $(N-M)$
- Total $2N - M - 1$

Below this, the equations are written as functions of vectors $\bar{\theta}$ and \bar{V} :

- $P_i = P_i(\bar{\theta}, \bar{V}) = P_i(\theta_2, \theta_3, \dots, \theta_N, V_{M+1}, V_{M+2}, \dots, V_N)$
- $Q_i = Q_i(\bar{\theta}, \bar{V}) = Q_i(\theta_2, \theta_3, \dots, \theta_N, V_{M+1}, V_{M+2}, \dots, V_N)$
- Now, $P_i(\bar{\theta}, \bar{V}) = P_i^{qp}$; $Q_i(\bar{\theta}, \bar{V}) = Q_i^{qp}$

What are the known quantities we have? We have P_i is known for all $i = 2$ to M . So this is for PV bus. And for Q bus and for PQ bus P_i is known also for $i = M + 1, M + 2$ to N and Q_i is also known for $i = M + 1, M + 2$ to N . So this is for PQ bus. So here the number is $M - 1$. Here this number is $N - M$. And here this number is $N - M$. So if I add them together, total comes out to be $2N - M - 1$. So then therefore what we have got?

That we have got total number of equations that is total number of known quantities is also $2N - M - 1$ and also my total number of unknown quantities is also $2N - M - 1$. So then therefore this is solvable. Now the question is how do I solve it? Now we have said that P_i is actually a function of vector θ and vector V . So then I can write down that P_i is a function of θ_2, θ_3 up to θ_N . Then V_{M+1}, V_{M+2} to V_N .

Similarly, Q_i is also a function of this vector θ and vector V . So I can write down, if I expand this so this is a function of θ_2, θ_3 to $\theta_N, V_{M+1}, V_{M+2}$ to V_N . So then what I

have got? So I have got these are the my unknown quantities and these are my known quantities. Sorry, and basically these are my unknown quantities.

And these are my unknown quantities and my equations that is the functions are known which are basically or rather I do have some function which is a known value which is basically the function of this unknown quantity. So then therefore it fits exactly into the basic framework of the Newton – Raphson numerical method. So then what do I do? So as usual that we have to calculate the correction vector. Now in actual practice what we have?

That P_i which is a function of this vector θ and V has got is equal to some value P_i specified and Q_i which is also a function of this θ and V , vector V is actually = Q_i specified, correct? For example if I have a load bus, for example let us say bus 5 is a load bus and at that bus there is 100 MW real load and let us say 50 MVR reactive load so then if I do take our base MVA to be 100 MVA.

So then in that case what we will say that my P_5 specified would be = -1 per unit and Q_5 specified would be = -0.5 per unit. So then therefore these quantities would be known. Now, so then basically these are my equations. Now if I do expand these equations so then what do I get?

(Refer Slide Time: 19:23)

Applying Taylor series expansion:

$$P_i^{sp} = P_i(\bar{\theta}^{(k)}, \bar{V}^{(k)}) + \frac{\partial P_i}{\partial \theta_2} \Delta \theta_2 + \frac{\partial P_i}{\partial \theta_3} \Delta \theta_3 + \dots + \frac{\partial P_i}{\partial \theta_N} \Delta \theta_N + \frac{\partial P_i}{\partial V_{m+1}} \Delta V_{m+1} + \frac{\partial P_i}{\partial V_{m+2}} \Delta V_{m+2} + \dots + \frac{\partial P_i}{\partial V_N} \Delta V_N$$

Taylor series (pointing to the expansion)

P_i^{sp} (pointing to the left side of the expansion)

$$P_i(\bar{\theta}, \bar{V}) = P_i^{sp}$$

$$\Rightarrow P_i(\bar{\theta}^{(k)} + \Delta \bar{\theta}, \bar{V}^{(k)} + \Delta \bar{V}) = P_i^{sp}$$

Similarly:

$$Q_i(\bar{\theta}, \bar{V}) = Q_i^{sp}$$

$$\Rightarrow Q_i(\bar{\theta}^{(k)} + \Delta \bar{\theta}, \bar{V}^{(k)} + \Delta \bar{V}) = Q_i^{sp}$$

Taking Taylor series expansion:

$V_i = 2, \dots, N$

So applying Taylor series expansion, so now if I apply Taylor series expansion to all this, what I get? I get $P_i^{\text{specified}} = P_i(\theta^{\text{nought}}, V^{\text{nought}} + \frac{\partial P_i}{\partial \theta^2} \cdot \Delta \theta^2 + \frac{\partial P_i}{\partial \theta^3} \cdot \Delta \theta^3 \dots \frac{\partial P_i}{\partial \theta^N} \cdot \Delta \theta^N + \frac{\partial P_i}{\partial V^{M+1}}$. This equation would be for all $i = 2$ to N because we can see that P_i would be actually specified for 2 to N . So then if I apply this Taylor series expansion to this equation of P_i we get this, right?

And θ_0 and V_0 are the initial conditions. Now basically from where this equation comes? Basically this equation comes from the fact that we have got $P_i(\theta)$ so this is the equation which is a vector of θ and $V = P_i^{\text{specified}}$. So then if I wish to solve for it so then what I will get it. So then obviously I do not know θ , I do not know V but I want to solve for them. So then what I will do?

That I will assume some value of θ^{nought} and I will assume some value of V^{nought} and then I will actually basically calculate their correction vectors $\Delta \theta$ and ΔV . So that should be equal to $P_i^{\text{specified}}$. So then therefore from here what I will get is $P_i(\theta^{\text{nought}} + \Delta \theta)$, so θ^{nought} and $V^{\text{nought}} + \Delta V$ should be equal to $P_i^{\text{specified}}$. And this term and this term has been expanded through Taylor series.

So this term has been expanded through Taylor series. So this is Taylor series, right? Similarly, we have equation is Q_i which is a function of vector θ and vector V that is equal to $Q_i^{\text{specified}}$. So then again I take some initial guess plus some correction and I also take some initial guess here plus some correction. That would be equal to $Q_i^{\text{specified}}$. So now I do take, so now I again do take I mean do actually perform the first order Taylor series expansion of this expression as we have done here. So then if I do take by taking Taylor series expansion what we get?

(Refer Slide Time: 24:25)

$$Q_i^{opt} = Q_i(\bar{\theta}^{(i)}, \bar{V}^{(i)}) + \frac{\partial Q_i}{\partial \theta_2} \Delta \theta_2 + \frac{\partial Q_i}{\partial \theta_3} \Delta \theta_3 + \dots + \frac{\partial Q_i}{\partial \theta_N} \Delta \theta_N$$

$$+ \frac{\partial Q_i}{\partial V_{m+1}} \Delta V_{m+1} + \dots + \frac{\partial Q_i}{\partial V_N} \Delta V_N$$

$V_i = m+1, \dots, N$

Collecting all the above equations together and putting them in a matrix form, we get

We get is that Q_i specified = Q_i is a function of + $\frac{\partial Q_i}{\partial \theta_2} \Delta \theta_2 + \frac{\partial Q_i}{\partial \theta_3} \Delta \theta_3 + \dots + \frac{\partial Q_i}{\partial \theta_N} \Delta \theta_N$ plus this would be for $i = M + 1$ to N because we can see from here for Q_i , i varies from $M + 1$ to N . So then therefore if I do collect all these equations together and do write them into a matrix form, so then what do I get. So collecting all the above putting them in a matrix form we get, what do I get? So what do I get? We get something like this.

(Refer Slide Time: 26:52)

The image shows a handwritten matrix equation. On the left, there is a large matrix divided into two main sections by a horizontal line. The top section contains two Jacobian matrices, J_1 and J_2 , each with columns representing partial derivatives of Q_i with respect to $\theta_2, \theta_3, \dots, \theta_N$ and V_{m+1}, \dots, V_N . The bottom section contains two more Jacobian matrices, J_3 and J_4 , with similar partial derivative columns. To the right of the matrix is a column vector of parameter changes: $\Delta \theta_2, \Delta \theta_3, \dots, \Delta \theta_N, \Delta V_{m+1}, \dots, \Delta V_N$. This is followed by an equals sign and a column vector of cost function differences: $Q_2^{opt} - Q_2^{cal}, Q_3^{opt} - Q_3^{cal}, \dots, Q_N^{opt} - Q_N^{cal}$. The differences are grouped into $\Delta \bar{P}$ and $\Delta \bar{Q}$.

$\frac{\partial P_2}{\partial \theta_2}, \frac{\partial P_2}{\partial \theta_3}, \dots, \frac{\partial P_2}{\partial \theta_N}$. Then $\frac{\partial P_2}{\partial V_{N+1}}, \dots, \frac{\partial P_2}{\partial V_N}$. Then we do collect all this P s and we get $\frac{\partial P_N}{\partial \theta_2}, \frac{\partial P_N}{\partial \theta_3}, \dots, \frac{\partial P_N}{\partial \theta_N}$. Then we get $\frac{\partial P_N}{\partial V_{M+1}}, \dots, \frac{\partial P_N}{\partial V_N}$. Then start

the Q . Then $\frac{\partial Q_N}{\partial V_{M+1}}$, $\frac{\partial Q_N}{\partial V_N}$. So this big matrix multiplied by $\Delta \theta_2$, $\Delta \theta_3$ up to $\Delta \theta_N$.

Then ΔV_{M+1} , ΔV_N and this is P_2 specified – P_2 . Now for our convenience we term this Q_i calculated. Q_i calculated means, what is meant by Q_i calculated? Q_i calculated means that I do have expression of Q_i that is I mean $V_i V_Q Y_{ik} \sin(\theta_N - \theta_k - \alpha_{ik})$. There in that expression I will substitute the values of θ nought and V nought. That is basically the initial guesses of all this θ 's and all this V 's, unknown V 's.

And of course we already know the I mean what the other values of θ or V which are already known. So we do substitute these values of initial θ and initial V and then we calculate the value of Q_i . That is basically to get a numerical value of Q_i . So then this expression we say for the purpose of convenience as Q_i calculated. Similarly, this also expression, this expression we also call as P_i calculated.

Here also in that expression of P_i we do substitute the values of initial values of θ and initial values of V and then after that we do get some numerical values of P_i . So that is basically the calculated value of injected real and reactive power with the initial guess of angle and voltage. That is angle and voltage magnitude. So we write it as P_2 cal P_3 is $P - P_3$ cal. This P_N specified – P_N calculated. Then we have Q_{M+1} specified – Q_{M+1} calculated.

And then similarly Q_N specified – Q_N calculated. So this is what we get. So we have got a big matrix; big matrix here, big vector here, big vector here. So now let us partition them. So now what we get is we partition this big matrix like this. And we also partition this vector like this. And we also partition this vector like this. This matrix we call as $\frac{\partial p}{\partial \theta}$ matrix. So we call it this matrix, so this is the matrix J_1 . We call it this matrix J_2 . We call this matrix J_3 .

We call this matrix J_4 . This is a vector. We call this vector as $\Delta \theta$ vector. This is a vector we call it ΔV vector. This is a vector. This vector we call as ΔP vector. And this is a vector we call as ΔQ vector \bar{Q} vector. So then therefore with this terminology this entire matrix, big matrix can be written as more succinctly as

(Refer Slide Time: 34:08)

$$\begin{bmatrix} J_1 & J_2 \\ J_3 & J_4 \end{bmatrix} \begin{bmatrix} \Delta \bar{\theta} \\ \Delta \bar{v} \end{bmatrix} = \begin{bmatrix} \Delta \bar{p} \\ \Delta \bar{q} \end{bmatrix}$$

[Matrix J 1, matrix J 2, matrix J 3, matrix J 4] then [delta theta vector, delta V vector] = delta P vector is equal to and delta Q vector. So in this lecture what we have done? We have first discussed what is meant by Newton – Raphson polar and rectangular method. And then after that we have specified that what are the unknown quantities for Newton – Raphson polar technique and as well as the what are the equations for this Newton – Raphson polar technique.

And subsequently we have linearized them by following the basic procedure of Newton – Raphson numerical method and by doing so and after so and after collecting all these equations together we have arrived at this succinct matrix equation. So in the next lecture and onwards we would be looking into the more details of this matrix equation. Thank you.