

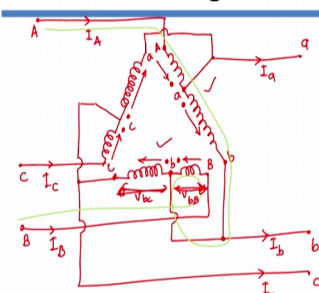
Electrical Distribution System Analysis
Dr. Ganesh Kumbhar
Department of Electrical Engineering
Indian Institute of Technology, Roorkee

Lecture – 20
Modeling of Step Voltage Regulators
Part III

Dear students, we are studying Modeling of Voltage Step voltage Regulators. And in the last class we have seen line drop compensator circuit. And we have seen that it is basically used to control the voltage regulator based on drop which is happening inside your feeder. And then we have gone for three phase voltage regulator.

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Three-Phase Regulator: Closed Delta Connected





$$\begin{aligned}
 V_{AB} &= V_{Aa} + V_{ab} + V_{bB} \\
 &= -\frac{N_2}{N_1} V_{Ab} + V_{ab} + \frac{N_2}{N_1} V_{bc} \\
 &= \left(1 - \frac{N_2}{N_1}\right) V_{ab} + V_{bc} - V_{bc} + \frac{N_2}{N_1} V_{bc} \\
 &= aR V_{ab} + \left(1 - \left(1 - \frac{N_2}{N_1}\right)\right) V_{bc} \\
 &= aR V_{ab} + \left(1 - aR\right) V_{bc} \\
 &= aR_{ab} V_{ab} + \left(1 - aR_{bc}\right) V_{bc} \quad \text{--- (1)}
 \end{aligned}$$

$$V_{BC} = aR_{bc} V_{bc} + \left(1 - aR_{ca}\right) V_{ca} \quad \text{--- (2)}$$

$$V_{CA} = aR_{ca} V_{ca} + \left(1 - aR_{ab}\right) V_{ab} \quad \text{--- (3)}$$

$$V_{Bb} = -\frac{N_2}{N_1} V_{bc}$$

$$V_{bB} = +\frac{N_2}{N_1} V_{bc}$$



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In today's lecture, start with three single phase regulators if they are connected in delta fashion. So, if they are connected in delta fashion, the connections will be something like this. So, it will be in delta. So, again there will be regulating winding. And this is your common winding for one phase this is regulator and common winding for second phase; this is regulating and common or shunt winding for third phase. Now, connection of these will be something like this. So, your A phase will be connected here; so this is capital A. Then your B phase will be connected here; so this is your B phase. And your C phase will be connected here.

And then this regulated terminal. So, basically we know that this is regulator terminal, which you are taking out and this will be small a terminal; this regulator terminal we are taking it out. This will become your small b terminal. And if you take this regulator terminal out, it will become your small c terminal. And to connect this in delta fashion, what we need to do is we need to connect this with a, and we need to connect this with b here, and we need to connect this with c here.

So, in this case also I am considering this single phase regulator which are connected in delta, I am considering for raising position. So, when you are raising, we have seen that your dots are placed at the load terminals; both the dots will be at load terminals. And in that case your currents will be this current is small I small a, I small b and this is I small c. This will be I capital A this is I capital B and this will be I capital C.

And then current direction here the I a current is entering to this node means it should leave to this node it is entering means it should leave this dot this is entering to this dot means it should leave this dot here. So, this is basically if you see this terminal a terminal is coming here; your b terminal is coming here; and your c terminal is coming here. And this is your capital A terminal; this is your capital B terminal and this is your capital C terminal. And this is again small a terminal which is same; here I am getting this as a small b terminal, and here I am getting small c terminal.

Now, to get the voltage and current relationships, we can write equation for say V ab. So, if I write voltage V ab, so basically it will be the current this circuit I am considering from here to here, and then from here to here it will go like this, and then from here to here and then it will be coming like this if you. So, if you consider this loop here, it will be basically voltage V ab. So, if you write the equations for it, so V ab will be nothing but the drop which is happening from this point to this point it will be V A small a plus from this point to this point it will be V A small b terminal because this terminal is small b. And then this terminal is same as here, so then plus V small b capital B.

Then we know that this relation between V aa and V ab they will be just related by your turns ratio. And if you see V aa. So, this to this voltage and V ab dots are in the same us you can say in a opposite direction. So, it will be minus N_2 by N_1 times of V ab because if you see this drops small V ab these drops are this drop across V aa will be just opposite of V ab because dots are opposite plus your V ab plus if you observe this drop

from voltage from b to capital B and b to c since if you see this voltages drop drops will be in the same direction.

So, in that case your voltage V_{db} will be N_2 by N_1 times of voltage V_{bc} basically this voltage here from this point to this point. So, this basically this voltage is V_{bc} and this voltage is V_{bb} . So, this direction is V_{bb} is like this and this direction is V_{bb} like this. Since the dots are here the polarity will be same, so that is why I am getting plus sign here. If you it would have been V_{bb} then it should be minus N_2 by N_1 times V_{bc} . Since, it is V_{bB} , it is plus N_2 by N_1 times V_{BC} .

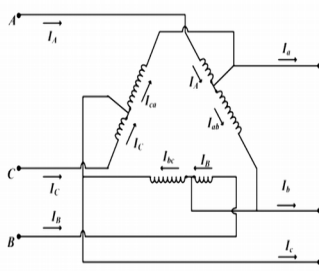
So, in this case I can take V_{ab} common from these two terms. So, it will be $1 - N_2$ divided by N_1 V_{ab} plus I am just adding V_{bc} and subtracting the same term. So, it will be just V_{bc} minus V_{bc} same term I add it and subtracted no change in equation plus N_2 divided by N_1 into V_{bc} . Now, it will be turns ratio we have seen aR . So, this equation we have seen that it is $1 - N_2$ by N_1 we have considered aR , and then V_{ab} plus $1 - 1 - N_2$ by N_1 into your V_{bc} . So, in this case it will be aR into V_{AB} plus $1 - 1$ minus again this term is nothing but your aR and then it is V_{bc} .

Now, this aR is actually controlled by this regulator which is between a and b phase and this aR is related to this second regulator which is placed between phase b and c so that is why to discriminate that we can say that this is aR_{ab} into V_{AB} , because this depends upon top position of regulator placed between a and b plus $1 - 1$ minus this is since this is depend on b and c, it should be $1 - aR_{bc}$ into V_{bc} .

So, if you apply same steps for other voltages, we can write them directly. So, V_{BC} will be equal to aR_{bc} into V_{bc} plus $1 - aR_{ca}$ into V_{ca} and then V_{CA} will be equal to aR_{ca} into V_{ca} plus $1 - aR_{ab}$ into V_{ab} . And then we have got these three equations, this is equation number 1; this is equation number 2; and this is equation number 3.

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Three-Phase Regulator: Closed Delta Connected



$$\begin{bmatrix} V_{AB} \\ V_{BC} \\ V_{CA} \end{bmatrix} = \begin{bmatrix} aR_{ab} & (1-aR_{bc}) & 0 \\ 0 & aR_{bc} & (1-aR_{ca}) \\ (1-aR_{ab}) & 0 & aR_{ca} \end{bmatrix} \begin{bmatrix} V_{ab} \\ V_{bc} \\ V_{ca} \end{bmatrix}$$

$$[V_{LL\ ABC}] = [aR_D] [V_{LL\ abc}]$$



$$[W] [V_{LL\ ABC}] = [W] [aR_D] [V_{LL\ abc}]$$

$$[V_{LN\ AB}] = [W] [aR_D] [0] [V_{LN\ abc}] \quad \text{--- (1) -->}$$

$$[A] = [W] [aR_D] [D]^*$$

$$[B] = [0]_{3 \times 3}$$

$$[V_{LN\ ABC}] = [a] [V_{LN\ abc}] + [b] [I_{abc}] \quad \text{--- (2) -->}$$

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Now if you write these three equations in matrix form, I will get this term here. So, it will be V_{AB} , V_{BC} , and V_{CA} on left hand side, we are having, and then in this matrix we will see what we are getting, and then left hand side, this three voltages V_{ab} , V_{bc} , and V_{ca} . Now, if you see this equation, first equation is aR_{ab} getting multiplied to V_{ab} , and V_{bc} is getting multiplied by $1 - aR_{bc}$. So, here, it is aR_{ab} , and V_{bc} is getting multiplied by $1 - aR_{bc}$, and here we are getting 0. Similarly, from second equation, it will be aR_{bc} , and here we are getting $1 - aR_{ca}$, here we getting $1 - aR_{ab}$, here 0 and aR_{ca} .

So, we have got now relation between voltages. So, collectively I can write, this is V_{line} to line voltages of all the three phases on primary side that is why capital ABC , this matrix I can say aR matrix of your delta, or I can just write D , instead of delta D . And this will be again these are line to line voltages, so $V_{line\ to\ line\ small\ abc}$, because they are on secondary side of regulator.

Now, to write the write it as the $abcd$ parameter, we know that we need line to neutral quantities. To convert these quantities into line to neutral, what we can do, we can multiplied by W matrix, which we have seen in transformer modeling. So, it will be W both the sides, we are multiplying it by W , multiplied by aR in delta fashion, multiplied by $V_{line\ to\ line\ small\ abc}$.

And we have seen that this quantity is nothing but V line to neutral voltages on A B C side, so we have got required voltage relation, and then W into a R D basically this matrix, and this line to line voltages, we can convert into line to neutral by multiplying, or you can say D multiplied by V L N a b c will basically we can get it, this V L L term. So, we have got this term here, and we can compare this with our normal a b c d terminology, which is V L N a b c, we are having a matrix V L N small a b c plus b into your I a b c

Now, if you compare equation number 1, and equation number 2. We can write your a parameter for this type of regulator will be given by W multiplied by a R D, which is basically this matrix here multiplied by D matrix. W and D matrix, we have already seen in our transformer chapter, so this is your a parameter. And your b parameter will be equal to matrix of 0s, so it will be 3 by 3 matrix of 0s, because there in this equation, equation number 1, there is no term related to I a b c.

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Three-Phase Regulator: Closed Delta Connected

$$\begin{aligned}
 I_a &= I'_a + I_{ca} \\
 &= I'_a - I_{ab} + I_{ca} \\
 &= I'_a - \frac{N_2}{N_1} I_A + \frac{N_2}{N_1} I_C \\
 &= \left(1 - \frac{N_2}{N_1}\right) I'_a + I_C - I_A + \frac{N_2}{N_1} I_C \\
 &= \left(1 - \frac{N_2}{N_1}\right) I'_a + \left(1 - \left(1 - \frac{N_2}{N_1}\right)\right) I_C \\
 &= a R_{ab} I'_a + (1 - a R_{ca}) I_C \quad \text{--- ①} \\
 I_b &= a R_{bc} I'_b + (1 - a R_{ab}) I_A \quad \text{--- ②} \\
 I_c &= a R_{ca} I'_c + (1 - a R_{cb}) I_B \quad \text{--- ③}
 \end{aligned}$$

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Now, similarly we can get relation between currents. Now, to get the relation between the currents, so that we can get c and d parameter, what we can do we can apply kcl at this particular point. And to apply kcl at that point, I am just I am saying this current is I a dash. So, this current we already seen I a, this is I a, this is I a dash, this is I capital A.

So, if you apply kcl at this point, and from this side, we have seen that this I c a current is coming. So, it will be, so current I a will be equal to your current I a dash plus current I c

a. Now, if you see I_a dash, I_a dash having two parts, so I_a dash is nothing but I_a minus I_b , because I_a current is coming like this, and I_b is going like this. So, it will be I_a capital A minus I_b plus I_c .

Now, if you see the relation between current I_a and current I_b , they will be related by your turns ratio, this is turns N_2 , and these are the turns N_1 here. So, we can easily write I_b , this current. So, I_a minus, it will be the current direction is same, so it is just N_2 by N_1 times of capital I_A . So, I_b , so this current will be N_2 by N_1 times of I_a .

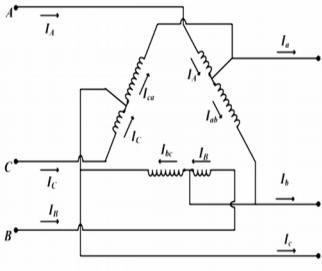
Plus if you observe this current, this current will be N_2 by N_1 times of I_c , because this is this number of turns are N_2 here the number of turns are N_1 . So, this I_c a will also be N_2 by N_1 times of I_c capital C is capital here. So, in this case also we can take I_a common out, so 1 minus N_2 divided by N_1 into I_A , and here just I am adding and subtracting term, which is I_c , to simplify this equation. And this term is as it is, so it will be plus N_2 by N_1 into your I_c .

So, from this I can easily write, it will be 1 minus N_2 by N_1 into I capital A plus, I can write this term 1 minus 1 minus N_2 by N_1 into your I_c . So, in this case, it will become a R turns ratio into I_A plus it is 1 minus a R into your I_c . Now, a R in this case, for first case I_A current related to the regulator, which is placed between phases a and b. So, this will depend upon tap, which is tap of regulator placed between a and b that is why I am writing a b. And this is related to this regulator here, which is placed between phase c and a. So, that is why, here it is c and a.

Exactly similar, up to follow the similar step, I can write other two equations. I can write equation for I_b , which will be equal to a R c b into, or you can say b c, it will be b c into I_b plus 1 minus a R a b into I_A . And your I_c will be a R c a into I_c plus 1 minus a R c b into your I_b . So, here also we have got three equations, this is equation number 1, this is equation number 2, and this is equation number 3. And we can write this three equations into matrix form.

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Three-Phase Regulator: Closed Delta Connected



$$\begin{bmatrix} I_A \\ I_B \\ I_C \end{bmatrix} = \begin{bmatrix} aR_{ab} & 0 & (1-aR_c) \\ (1-aR_b) & aR_{bc} & 0 \\ 0 & (1-aR_c) & aR_{ca} \end{bmatrix} \begin{bmatrix} I_{ab} \\ I_{bc} \\ I_{ca} \end{bmatrix}$$



$$[I_{abc}] = [aRI_D] [I_{ABC}]$$

$$[I_{ABC}] = [aRI_D]^{-1} [I_{abc}] \quad \text{--- (2)}$$

$$C = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

$$[d] = [aRI_D]^{-1}$$

$$[I_{ABC}] = [C] [V_{LN}_{abc}] + [d] [I_{abc}] \quad \text{--- (4)}$$

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So, if you write these three equations into matrix form, on this side we have seen it is I_a , I_b , and I_c , and they will be related by capital I_A , I_B , and I_C . And in equation number 1, we are getting multiplied with respect to I_A , and then 1 is respect to I_c . So, in this case, it will be aR_{ab} here, and 0 1 minus aR_{ca} .

Then in second case, we are getting terms related to I_B and I_A . So, here we are getting 1 minus aR_{ab} , and here we are getting aR_{bc} , and this term is 0 . And in third case, we are getting 1 minus aR_{bc} , and here we are getting aR_{ca} . So, we have got this matrix here, so these are line currents.

So, this I_{abc} collectively I can write it, and this matrix I can say another matrix, which is aRI_{Δ} connected, and this is I_{abc} . So, I can write your I_{abc} capital ABC will be equal to aRI_{Δ} inverse into I_{abc} ok. And if you compare it, with respect to our standard $abcd$ parameter equation, which is basically I_{ABC} is equal to C into V_{LN} small abc plus matrix d into your I_{abc} . So, if you compare this, there is no term this is say equation number 3, and equation number 4.

So, if you compare 3 and 4, there is no term, which is related to V_{LN} abc into this equation. So, that is why C matrix will be matrix of 0 0 0 . And your d matrix will be equal to your aRI_{Δ} inverse, where this aRI_{Δ} matrix is basically this matrix here. So, what $abcd$ parameters for closed delta connected regulator; One more regulator they use, which is called as open delta connected regulator.

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Open Delta Connected Regulator

$$\begin{aligned}
 V_{AB} &= V_{Aa} + V_{aB} \\
 &= -\frac{N_2}{N_1} V_{ab} + V_{ab} \\
 &= \left(1 - \frac{N_2}{N_1}\right) V_{ab} \\
 &= aR_{ab} V_{ab} \quad \checkmark \quad \text{--- (1)} \\
 V_{BC} &= aR_{cb} V_{bc} \quad \checkmark \quad \text{--- (2)} \\
 V_{AB} + V_{BC} + V_{CA} &= 0 \\
 V_{CA} &= -V_{AB} - V_{BC} \\
 &= -aR_{ab} V_{ab} - aR_{cb} V_{bc} \quad \text{--- (3)} \\
 &= \underline{\underline{V_{ca}}}
 \end{aligned}$$

$\underline{\underline{V_{ca}}}$

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And in this case, there are two regulators, which are connected in open delta, instead of making it closed delta. So, we can use it only using two regulators. First let us see, how they are connected. So, in this case, as I told you there are only two regulators, so one regulator say, this is regulating winding, and this is main winding, it is connected like this. Another regulator is say connected like this, so this is regulating winding, and say this is your main winding.

So, in this case what they do, this will be connected to terminal A, this will be connected to terminal B, and your this it will be connected to terminal capital C. And regulator terminal will take will be taken out, so this will be taken out, and this will become your small a terminal, this will be taken out, and this will become small b terminal, and this regulator terminal will be taken it out, and it will become c terminal. So, by controlling only two regulators, we can control the voltages at a b c phases

So, in this case, you can say this current will be I a, this current will be I small b, this will be I small c, this will be I A, this will be I capital C, and this will be I capital D. So, in this case again I am considering this, in raise position that is why, dots will be at the load terminals, both the dots have same. So, in this case current, which is flowing like this I A, then current I 1 will be through this regulator. And in this case also, I c is coming towards dot, so this current will be going away from the dot.

And now, this terminal is actually both, it is capital B, as well as your small b. Now, to get a and b parameters, as I told you, we need to write voltage equations. So, we can write voltage equation for V_{AB} , so if you write voltage equation V_{AB} will be just this voltage drop plus, the voltage drop across this regulating winding. So, it will be this terminal is small a. So, it will be V_{Aa} plus your V_{ab} , because this is actually both the terminal a small b, as well as capital B. So, I just write as it a small b, because both terminals are same.

So, in this case, we can easily see this V_{Aa} , and V_{ab} , they are related, and they are related by turns ratio. And the since the dots are opposite of these direction, your V_{Aa} dot will be, this N_1 minus N_2 divided by N_1 , and it will be minus N , because these two voltages are in opposite direction, so it is V_{ab} plus your V_{Aa} . So, it will be just 1 minus N_2 by N_1 into your V_{ab} ok, this is nothing but your a R.

Now, since this regulator is placed between phases a and b. So, we can say it is a R_{ab} into your V_{ab} . Exactly similar way, we can apply voltage between V_{BC} . So, V_{BC} also we can similarly, write it will be a R_{cb} into V_{bc} . And then V_{AB} , since this is actually three phase three wire connection V_{AB} plus V_{BC} plus V_{CA} , they will be equal to 0.

So, in this case, I can write V_{CA} , because this voltage is not available, which is equal to minus V_{AB} minus V_{BC} . So, in that case, it will be minus a R_{ab} V_{ab} , because we have derived here V_{ab} , and V_{bc} is derived here that is a R_{cb} into V_{bc} . So, we have got three equations here, 1, 2, and 3 if you write them in matrix form, and we will get required your a and b parameters.

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Open Delta Connected Regulator

$$\begin{bmatrix} V_{AB} \\ V_{BC} \\ V_{CA} \end{bmatrix} = \begin{bmatrix} aR_{ab} & 0 & 0 \\ 0 & aR_{cb} & 0 \\ -aR_{ab} & -aR_{cb} & 0 \end{bmatrix} \begin{bmatrix} V_{ab} \\ V_{bc} \\ V_{ca} \end{bmatrix}$$

$$[V_{LLABC}] = [aR_{OD}] [V_{LLabc}]$$

$$[W] [V_{LNABC}] = [W] [aR_{OD}] [V_{LLabc}]$$

$$[V_{LNABC}] = [W] [aR_{OD}] [D] [V_{LNabc}] \quad \text{--- (1)}$$

$$[a] = [W] [aR_{OD}] [D] \quad \checkmark$$

$$[b] = [0]_{3 \times 3} \quad \checkmark$$

$$[V_{LNAB}] = [a] [V_{LNabc}] + [b] [I_{abc}] \quad \text{--- (2)}$$

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So, let us write them into matrix format. So, from first equation, so we are getting here on this side V_{AB} , V_{BC} , and V_{CA} , which is equal to some matrix multiplied by V_{ab} . And we have seen that V_{ab} is just related to V_{AB} , V_{bc} is just related to V_{BC} . However, V_{ca} is related to both having minus sign. So, in this case, so it will be just $aR_{ab} \ 0 \ 0$, V_{BC} is related to V_{bc} , so $aR_{cb} \ 0$, and here minus aR_{ab} , and aR_{cb} both are minus term here 0 , because in all the three equation we are not getting any term, which is related to $V_{small \ c}$. So, that that particular term will get multiplied by 0 here so, here we are getting 0 everywhere.

So, I can write it like V_{LLABC} , because these line to line voltages, which will be equal to this matrix I am calling a R . And since it is your open delta connector I can just say OD a ROD multiplied by here also we are getting line to line voltages $V_{LLsmall \ abc}$.

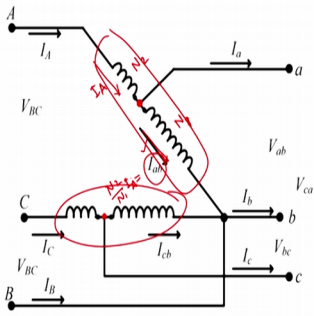
And then exactly similar way, where we are connect line to neutral voltages. So, this will be converted by multiplying by W matrix V_{LL} is equal to just add a multiplied by W . And this will become line to neutral voltages V_{LNABC} will be equal to W into a ROD into your, so convert this into line to neutral voltages, it will be D matrix conversion $V_{LNsmall \ abc}$.

So, in this case, if you compare with standard equations, which are basically V_{LNAB} C , which is equal to a parameter into $V_{LNsmall \ abc}$ plus your b parameter into I_{abc} .



So, if you compare this equation number 1, with respect to equation number 2 there is no term, which is related to currents here. So, your a parameter will be your W multiply by a R O D into your D matrix. And your b will be matrix of 0s having 3 by 3. And this a R O D is nothing but basically this matrix, which you are derived it here. So, the here we have got a and b parameter.

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Open Delta Connected Regulator



$$\begin{aligned}
 I_a &= I_A - I_{ab} \\
 &= I_A - \frac{N_2}{N_1} I_A \\
 &= \left(1 - \frac{N_2}{N_1}\right) I_A \\
 I_a &= a R_{ab} I_A \Rightarrow I_A = \frac{1}{a R_{ab}} I_a \quad \text{--- (1)} \\
 I_c &= a R_{cb} I_C \Rightarrow I_C = \frac{1}{a R_{cb}} I_c \quad \text{--- (3)} \\
 \Sigma \quad I_A + I_B + I_C &= 0 \\
 I_B &= -I_A - I_C \\
 I_B &= -\frac{1}{a R_{ab}} I_a - \frac{1}{a R_{cb}} I_c \quad \text{--- (2)}
 \end{aligned}$$

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Let us see how we can get c and d parameters. And for c and d parameters, we should write the current relationships. So, currents for writing the current relationships, we can apply kcl at this particular point. So, here the current is I A, and this current I a b, and this I a. So, I can write I a will be equal to I capital A minus your I a b.

And we have seen that this I a, and I a b, they are related by turns ratio. And thus direction of the currents, if this is they are same, it will be I A minus your N 2 by N 1 into I A, because this winding is having N 2 N 1 number of turns, and this winding is having N 2 number of turns. So, this current I a b current will be equal to N 2 by N 1 times your current I A. So, here I can just again it will be 1 minus N 2 by N 1 into I A.

So, your I a will be equal to a R. Now, since this you are considering this regulator between a and b phase, so it will be a R a b into I A. Similarly, I can write for I c also, so I c for this particular current, and this current I c, which is basically flowing from this one. So, by applying kcl at this node I can get similar equation, and this will be a R c b

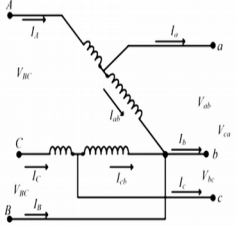
into your I capital C. And third relations, I can get from adding all the three currents, so addition of all the three current should be equal to 0.

So, before that actually what I can do this equation, I can say I capital A will be equal to 1 upon a R a b into I small a. And this equation, I can write I C will be equal to 1 upon a R c b into I c. And then, we have seen that I A plus I B plus I C, three currents should be equal to 0. In that case, I can write I B is equal to minus I A and minus I C. So, this will be equal to minus 1 upon a R a b into I small a minus 1 upon a R c b into I C.

So, we have got three equations, this is 1, 2, and 3 ok. So, this equation related to I B. So, equation for I B, I just write instead of 3 I will make this I will write away this as a this will also 2, and this will be 3. So, writing this 1, 2, 3 equations into matrix form.

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Open Delta Connected Regulator





$$\begin{bmatrix} I_A \\ I_B \\ I_C \end{bmatrix} = \begin{bmatrix} \frac{1}{aR_{ab}} & 0 & 0 \\ -\frac{1}{aR_{ab}} & 0 & -\frac{1}{aR_{cb}} \\ 0 & 0 & \frac{1}{aR_{cb}} \end{bmatrix} \begin{bmatrix} I_a \\ I_b \\ I_c \end{bmatrix}$$

$$[I_{ABC}] = [aR_{IOP}] [I_{abc}] \quad \text{--- (3)}$$

$$[c] = [0]_{3 \times 3}$$

$$d = [aR_{IOP}]$$

$$[I_{ABC}] = [c] [V_{Iabc}] + [d] [I_{abc}] \quad \text{--- (4)}$$



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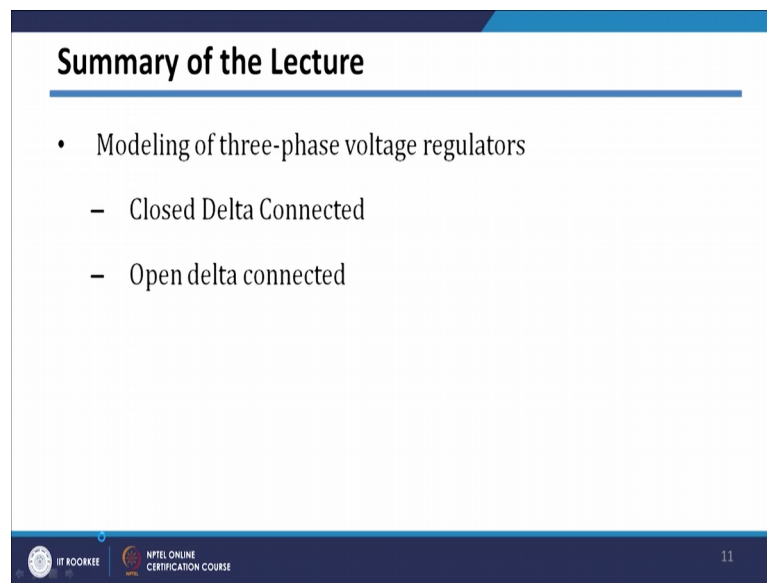
I will get this equation here. So, I A, I B, and I C three currents, which will be equal to some matrix here, multiplied by I small a, small b, and small c, and this will be 1 upon a R a b 0 0. And for D I B equation, we are getting terms related to I A, and I C and both terms are negative. So, I B equation will be one minus 1 upon a R a b 0 minus 1 upon a R c b,

And here third equation, which is just related to I c so, it is 1 upon a R c b. So, we have got this equation here, and this will be I A B C, which will be equal to I can say this as a a R I open delta calculation into your I a b c. Again we can compare with this standard

equation that is I_{ABC} is equal to C into V_{LNabc} plus your d into I_{abc} . So, if you compare this is say equation number 3, and equation number 4.

So, if you compare 3 with 4, there is no term related to V_{LNabc} . So, that is why, your c matrix will be matrix of 0s 3 by 3 size. And your d matrix will be equal to a R I O D matrix, which is basically this matrix. So, for this configuration also we have found out a bcd parameter open delta configuration.

(Refer Slide Time: 35:32)

A presentation slide titled "Summary of the Lecture" with a blue header and footer. The main content area is white and contains a bulleted list. The footer includes logos for IIT Roorkee and NPTEL, along with the text "NPTEL ONLINE CERTIFICATION COURSE" and the slide number "11".

Summary of the Lecture

- Modeling of three-phase voltage regulators
 - Closed Delta Connected
 - Open delta connected

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Here we come into the end of this particular lecture. And in this lecture, we have seen modeling of three phase voltage regulator. And basically we have seen two types of configurations here, one is closed delta connected regulators, where the three regulators are connected as a closed delta, and another is open delta connected regulator, where only two regulators are used. And using or controlling this two voltage regulator, we can control the voltage of the three phases at the output side.

So, here we end modeling of three phase regulator. In the next class, we will see few examples, so that we will understand it better.

Thank you.