

Optimal Control
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Lecture - 25
Frequency Domain Interpretation of LQR
(Linear Time Invariant System)

Welcome class for this session. Today we will discuss about the Frequency Domain Interpretation of a LQR System, and this we will do for the linear time invariant system. In the previous class we have discussed about how we can develop the optimal control law for a time varying and the time invariant system. This optimal control law can be determined if we can find out the solution of a Riccati equation.

So, for time varying case my Riccati equation is a differential matrix Riccati equation and for the time invariant case this is an algebraic equation, which can be in both cases this is a non-linear equation. For the time varying case it can be solved using numerical techniques. And for analytical solutions also we have seen how we can determine the value of the Riccati coefficient P by different ways. We have also discussed about the stability of the LQR system and we have shown for time varying as well as the time invariant case. In both cases my system is a stable system.

Whatever be the condition of the matrix A , but the closed loop system $A - BK$ will always be a stable system. So, today we will discuss about the frequency domain interpretation, which means what is that; if we will have the frequency response analysis and we are willing to find out the gain margin and the phase margin of the system, how we can find all this.

So, this we are taking for the linear time invariant system, so we will consider an LTI system as $\dot{X}(t) = AX(t) + BU(t)$.

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Frequency-Domain Interpretation

Consider a linear, time-invariant controllable system,

$$\dot{X}(t) = A X(t) + B U(t) \quad (1)$$

The optimal closed loop control which minimises the cost function,

$$J = \frac{1}{2} \int_0^{\infty} [X' Q X + U' R U] dt$$

is given by,

$$U^*(t) = -R^{-1} B' P X^*(t) = -K X^*(t) \quad (2)$$



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Objective is we have to determine the optimal control law $U(t)$ which will minimize the performance index J as $\frac{1}{2} \int_0^{\infty} [X' Q X + U' R U] dt$. So, if we will solve this problem we know we can find the optimal control law which is minus $R^{-1} B' P X(t)$, where $R^{-1} B' P$ we call the K .

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Frequency-Domain Interpretation

Matrix ' P ' is the solution of the non-linear **Matrix Algebraic Riccati Equation (ARE)**,

$$PA + A'P + Q - PBR^{-1}B'P = 0 \quad (3)$$

The optimal state trajectory is given by the solution of,

$$\dot{X}^*(t) = [A - BR^{-1}B'P]X^*(t) = [A - BK]X^*(t) \quad (4)$$



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So, this is minus $KX(t)$ where P is the solution of my algebraic Riccati equation which is $PA + A'P + Q - PBR^{-1}B'P = 0$. So, if I can solve this algebraic Riccati equation to find the P I can find out the U which is $R^{-1}B'P$. R I know, B I know P we already have determined. So, I can find out the K . So, if I will apply the control law $U = -KX$. So, this is $AX(t) - BKX(t)$. So, $A - BK$ $A - BK$ $R^{-1}B'P$ is nothing but my close loop matrix. And we already have shown that in this system whatever be the matrix A my lose loop system always is a stable system.

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Frequency-Domain Interpretation



The open loop characteristic equation is given by,

$$\Delta_o = |sI - A| \tag{5}$$

The closed loop characteristic equation is given by,

$$\begin{aligned} \Delta_c &= |sI - A + BK| \\ &= |I + BK[sI - A]^{-1}| \cdot |sI - A| \\ \Delta_c &= |I + BK[sI - A]^{-1}| \Delta_o \end{aligned} \tag{6}$$

Eqn. (6) gives the relation between open-loop and closed-loop characteristic equation of the system.


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Now, if we see the characteristics equation of my close loop and the open loop system.

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Open loop $\dot{x}(t) = Ax(t) + Bu(t)$; $U(t) = -R^{-1}B'Px(t)$
 $= -Kx(t)$

Characteristic Eqn for open loop

$$\Delta_o = |sI - A|$$

Closed loop system

$$\dot{x}(t) = (A - BK)x(t)$$

Characteristic Eqn for closed loop system

$$\Delta_c = |sI - (A - BK)| = 0 = |sI - A + BK|$$

$$\Delta_c = |(I + BK(sI - A)^{-1})(sI - A)| = 0$$

My open loop system is $\dot{x}(t) = Ax(t) + Bu(t)$ and $U(t)$ is nothing but $-R^{-1}B'Px(t)$, and which nothing but we are saying this is U equal to $-KX(t)$. So, my characteristic equation for open loop system which I mention as the Δ_o it is nothing but; my $sI - A$, determinant of $sI - A$.

So, this is the characteristic equation for the open loop. And what is my close loop system? My close loop system is $\dot{x}(t) = (A - BK)x(t)$. For close loop system my characteristic equation is nothing but $sI - (A - BK)$ in place of A I have my $A - BK$ matrix. So, determinant of this must be equal to 0.

So, that we are saying here if this is the open loop characteristics equation determinant of $sI - A$ and for close loop this is Δ_c this is $sI - A + BK$ or we can write $sI - A - BK$ in bracket. So, this equation can be written in the form as determinant of $sI - A$ the whole determinant must be 0. And this is my Δ_c close loop.

So, these closes loop characteristic equation. So, what we have done? If I will explain this as $sI - A + BK$, so I am taking these two as outside. So, if will take $sI - A$ outside. So, this is $I + BK(sI - A)^{-1}$. So if I multiplying this, this is sI

minus A this would become unity and I get the SI minus A plus BK. So, this close loop equation I can further simplify.

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$$\Delta_u = \det (sI - A) \cdot \det \left(I + \frac{B}{n} \frac{(sI - A)^{-1}}{m} \right) = 0$$

$$\Delta_{cl} = \det (sI - A) \cdot \det (I + K (sI - A)^{-1} B) = 0 \quad \left\{ \begin{array}{l} \det (I + mn) \\ = \det (I + nm) \end{array} \right.$$

S-domain Block diagram

$K (sI - A)^{-1} B$ — loop gain
 $I + K (sI - A)^{-1} B$ — Return characteristic matrix

So, I am writing this close loop characteristic equation as: so in place of state line determinant I am writing the determinant of say- what is this? This is the determinant of this matrix and determinant of this matrix.

If I will explain this I can write determinant of SI minus A multiplied with the determinant of I plus B k SI minus A inverse SI minus A inverse, and this is nothing equal to my 0. So, for the second determinant we use the identity determinant I plus m n is equal to determinant I plus n m. So, if you will use this identity with considering k SI minus A inverse as my m and B as n. So, in this if we will apply this identity determinant I plus m n. So, I can write my close loop characteristic equation as determinant SI minus A multiplied with determinant I plus k SI minus A inverse B: this is equal to 0.

So, this close loop matrix we are writing as determinant of I plus B k SI minus A inverse into SI or this is my close loop characteristic equation. Where, delta 0 we are seeing SI minus A. So, this B k we have written as k SI minus A inverse B. So, this equation here

delta 0 is nothing but my SI minus A this I am expanding as determinant SI minus A determinant I plus k SI minus A inverse B.

Now if we will see the s domain block diagram of the system. So, this is my plant and plant is nothing but my SI minus A inverse B. So, this is my U s this will be nothing but my X s, here we are adding the k which is nothing but R inverse B prime P, this is given here with negative sign and sorry; this we can write as capital R s which is nothing but we have taken as 0. In LQR system my R s is 0.

So, I can represent the s domain block diagram by this.

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Frequency-Domain Interpretation

The closed loop system can be represented as,

Fig. 1 : System with Closed Loop Optimal Control

Loop Gain Matrix : $-K[sI - A]^{-1}B$

Return Difference Matrix : $I + K[sI - A]^{-1}B$

So, my overall block diagram is s I minus A inverse B, K multiplied with the K which is giving me nothing but the R s value. So, this is the relation between R s and x s. So, my if we will see K s I minus A inverse B, if I am multiplying this nothing but giving me the loop gain and if I am writing the characteristic equation this is I plus K s I minus A inverse B this is known as my return difference matrix. So, in frequency domain I can represent my LQR system as given by this block diagram, which is similar to as given here with this block diagram. Where K S I minus A inverse B is nothing but my loop

gain, and if I am writing $I + kSI - A^{-1}B$ this is my return difference matrix.

So, this is the representation of LQR system in frequency domain we can represent. Our objective here is to determine the gain and the phase margin of this system. So, system is represented here what will my gain margin and the phase margin that we are trying to find out. So, this we can prove using our ARE. So, consider arithmetic Riccati equation what is that this is my PA.

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ARE

$$-PA - A'P + PBR^{-1}B'P - Q = 0$$

Add and Subtract PS

$$PS - PA - A'P + PBR^{-1}B'P - Q = 0$$

$$P(SI - A) + (-SI - A')P + PBR^{-1}B'P - Q = 0$$

Pre multiply $B'(-SI - A')^{-1}$ and Post multiply by $(SI - A)^{-1}B$

$$B'(-SI - A')^{-1} [P(SI - A) + (-SI - A')P + PBR^{-1}B'P - Q] (SI - A)^{-1}B = 0$$

$$B'(-SI - A')^{-1}PB + B'P(SI - A)^{-1}B + B'(-SI - A')^{-1}PBR^{-1}B'P(SI - A)^{-1}B - Q(SI - A)^{-1}B = 0$$

So, I write this in the form $-PA - A'P + PBR^{-1}B'P - Q = 0$, so nothing but if I will take the minus kalman. So, this will be in the standard form $PA + A'P - PBR^{-1}B'P + Q = 0$. So, this is my matrix; sorry arithmetic Riccati equation.

So, in this we will add and subtract P into S . So, what we are doing we are adding PS and subtracting PS . Basically we are doing $PS - PA$, and this PS I am subtracting here $PS - A'P$ and this I will kept as such $PBR^{-1}B'P - Q$. So, if I will take P common from these two term. So, this is $PSI - A$ and from here I will write this as $-sI$ because s is a scalar function. So, I can write this as sP

S or $P(S - A')$ and this P . I will write on the right hand side. So, considering these two term including the negative this I am writing as $P(S - A)$ and this I am writing as $-SI - A'P$, and this I will write as such $PBR^{-1}B'P - Q$ equal to 0.

So, in this equation we are pre multiply with and post multiply by $SI - A$ inverse B . Now this equation I am pre multiplying with $B' - SI - A'$ inverse and post multiplying with $SI - A$ inverse B , this means this whole equation is pre multiplied by $B' - SI - A'$ inverse, this is $P(SI - A) + (-SI - A'P) + PBR^{-1}B'P - Q$ and post multiply with $SI - A$ inverse B .

So, now just pre multiply and post multiply this with if I will expand this what I will get? $B' - SI - A'$ inverse P , this $SI - A$ $SI - A$ inverse sorry $SI - A$ inverse will give me the I and this multiplied with B . So, this is $B' - SI - A'$ inverse PB , with second term if I will multiply. So, $-SI - A'$ inverse this will give me $+B'P$ this two term will give me $B'P$ and post multiply with $SI - A$ inverse B . So, these two term I will get from these two term and here, this is multiplied with $B' - SI - A'$ inverse $PBR^{-1}B'P - Q$ with $SI - A$ inverse B . So, by expanding this we are getting this term.

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$(sI - A)^{-1}$ is the state transition matrix $\phi(s)$
 $(-sI - A')^{-1} \rightarrow \phi'(-s)$

$$B' \phi'(-s) P B + B' P \phi(s) B + B' \phi'(-s) P B R^{-1} B' P \phi(s) B = B' \phi'(-s) Q \phi(s) B$$

Add "R" on both side.

$$B' \phi'(-s) P B + B' P \phi(s) B + B' \phi'(-s) P B R^{-1} B' P \phi(s) B + R = B' \phi'(-s) Q \phi(s) B + R$$

$$K = R^{-1} B' P \Rightarrow R K = B' P \Rightarrow K' R = P B$$

$$B' \phi'(-s) K' R + R K \phi(s) B + B' \phi'(-s) K' R R^{-1} R K \phi(s) B + R = B' \phi'(-s) Q \phi(s) B + R$$

$$B' \phi'(-s) K' R + R K \phi(s) B + B' \phi'(-s) K' R K \phi(s) B + R = B' \phi'(-s) Q \phi(s) B + R$$

What is $(sI - A)^{-1}$? $(sI - A)^{-1}$ is the transition matrix, is the state transition matrix and this we represent as $\phi(s)$ and so therefore, $(-sI - A')^{-1}$, I can represent as $\phi'(-s)$. So, I will use for $(sI - A)^{-1}$ as $\phi(s)$ which is my state transition matrix and $(-sI - A')^{-1}$ this is the transpose conjugate transpose of my state transition matrix.

So, in this time if I will write I can write this as $B' P \phi(s) B + B' P \phi(s) B + B' \phi'(-s) P B R^{-1} B' P \phi(s) B$ and this I am writing Q on the other side as $B' \phi'(-s) Q \phi(s) B$. So, by expanding this I am writing Q on right hand side. In this equation add R on both the side by adding R what actually we will get? We get this $P B + B' P \phi(s) B + B' \phi'(-s) P B R^{-1} B' P \phi(s) B + R$ and similarly on this side $B' \phi'(-s) Q \phi(s) B + R$.

So, now the whole equation I can represent by this. So, now, we know K equal to minus my K is $R^{-1} B' P$ or I can write this as $R K = B' P$ and $K' R = P B$. So, I can use these relations because I know the controller gain K is nothing but my $R^{-1} B' P$, if I will pre multiply this equation by R. So, this is nothing but $R K = B' P$ if I will take the transpose of this $K' R = P B$. So, in this equation I will write $P B$ as $K' R$. So, $B' \phi'(-s) Q \phi(s) B + R$

for the first term, the second term is $B' P$ which I am writing as $R k \phi' s B$ plus B' prime ϕ' prime minus s .

Now, see $P B$ is in this equation $P B$ is k prime R , k prime R I am writing for $P B R$ inverse as such $B' P$ is $R k$ and this I will write as such $\phi' s B$ plus R and this side is $B' Q \phi' s B$ plus (Refer Time: 00:00); now in this $R r$ inverse will become i . So, this is k prime $R k$. So, $B' P$ prime minus $S K$ prime R plus $R k \phi' s B$ plus B' prime ϕ' prime minus s and this I can write k prime $R k \phi' s B$ plus R and this is nothing but equal to my $B' \phi'$ prime minus $s Q \phi' s B$ plus R .

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$$(I + K \phi(-s) B)' R (I + K \phi(s) B) = B' \phi'(-s) Q \phi(s) B + R$$

$$B' \phi'(-s) K' R + R K \phi(s) B + B' \phi'(-s) K' R R^{-1} R K \phi(s) B + R = B' \phi'(-s) Q \phi(s) B + R$$

$$B' \phi'(-s) K' R + R K \phi(s) B + B' \phi'(-s) K' R K \phi(s) B + R = B' \phi'(-s) Q \phi(s) B + R$$

Now, see in this if I will consider the left hand side. So, this equation I can write in the form as I plus sorry ϕ' prime minus $s Q \phi' s B$ plus R . So, this equation I am writing as I plus $k \phi'$ minus $s B$ prime B whole transpose, this is the transpose multiplied with the $R I$ plus $k \phi' s B$. So, $I \phi'$ will take the transpose and explain this I will get the same term which I have on this write hand side.

So, my overall system can be represented in this particular form, which we can see here this is nothing but I plus $K \phi'$ minus $s B$ whole transpose R multiplied with I plus $K \phi' s B$ equal to $B' \phi'$ prime minus s .

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Frequency-Domain Interpretation

Adding 'R' on both sides of eqn. (11),

$$\mathbf{R} + \mathbf{B}'\Phi'(-s)\mathbf{K}'\mathbf{R} + \mathbf{R}\mathbf{K}\Phi(s)\mathbf{B} + \mathbf{B}'\Phi'(-s)\mathbf{K}'\mathbf{R}\mathbf{K}\Phi(s)\mathbf{B} = \mathbf{B}'\Phi'(-s)\mathbf{Q}\Phi(s)\mathbf{B} + \mathbf{R}$$

$$[\mathbf{I} + \mathbf{K}\Phi(-s)\mathbf{B}]'\mathbf{R} + [\mathbf{I} + \mathbf{B}'\Phi'(-s)\mathbf{K}']\mathbf{R}\mathbf{K}\Phi(s)\mathbf{B} = \mathbf{B}'\Phi'(-s)\mathbf{Q}\Phi(s)\mathbf{B} + \mathbf{R}$$

$$[\mathbf{I} + \mathbf{K}\Phi(-s)\mathbf{B}]'\mathbf{R} + [\mathbf{I} + \mathbf{K}\Phi(-s)\mathbf{B}]'\mathbf{R}\mathbf{K}\Phi(s)\mathbf{B} = \mathbf{B}'\Phi'(-s)\mathbf{Q}\Phi(s)\mathbf{B} + \mathbf{R}$$

$$[\mathbf{I} + \mathbf{K}\Phi(-s)\mathbf{B}]'\mathbf{R}[\mathbf{I} + \mathbf{K}\Phi(s)\mathbf{B}] = \mathbf{B}'\Phi'(-s)\mathbf{Q}\Phi(s)\mathbf{B} + \mathbf{R} \quad (11)$$

Eqn. (11) is called as Kalman equation in frequency domain.

$$[\mathbf{I} + \mathbf{K}[-s\mathbf{I} - \mathbf{A}]^{-1}\mathbf{B}]'\mathbf{R}[\mathbf{I} + \mathbf{K}[s\mathbf{I} - \mathbf{A}]^{-1}\mathbf{B}] = \mathbf{B}'[-s\mathbf{I} - \mathbf{A}]^{-1}\mathbf{Q}[s\mathbf{I} - \mathbf{A}]^{-1}\mathbf{B} + \mathbf{R}$$

So, this equation is called the Kalman equation in the frequency domain, for LQR system this Kalman equation we can find using our a R e with the a R e we have got our Kalman equation in the frequency domain, and what is my phi minus s this is minus SI minus A inverse phi s is SI minus A inverse.

So, another way to represent this equation is I plus K minus SI minus A inverse B R multiplied with the I plus K SI minus A inverse B equal to B prime minus SI minus A prime inverse which is phi prime minus s multiplied with Q SI minus A inverse B plus R. Now in the next class we will see that how this equation can be utilized to determine the gain margin and the phase margin of a LQR system.

So this class we stop here. And further we will continue our discussion in the next class to determine the gain margin and the phase margin of this LQR system.

Thank you very much.