


DC Power Transmission Systems
Prof. Krishna S
Department of Electrical Engineering
Indian Institute of Technology, Madras

Lecture - 34
Normalization

So, let us summarize some of the equations that we have derived so far.

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Summary

$0 < u \leq 60^\circ$

$$V_d = \frac{V_{d0}}{2} [\cos \alpha + \cos(\alpha + u)] \Rightarrow \bar{V}_d = \frac{1}{2} [\cos \alpha + \cos(\alpha + u)]$$


$$\bar{I}_d = \bar{I}_s [\cos \alpha - \cos(\alpha + u)] \Rightarrow \bar{I}_d = \frac{1}{2} [\cos \alpha - \cos(\alpha + u)]$$

$$V_d = \frac{V_{d0}}{2} [-\cos \gamma - \cos(\gamma + u)] \Rightarrow \bar{V}_d = \frac{1}{2} [-\cos \gamma - \cos(\gamma + u)]$$

$$\bar{I}_d = \bar{I}_s [\cos \gamma - \cos(\gamma + u)] \Rightarrow \bar{I}_d = \frac{1}{2} [\cos \gamma - \cos(\gamma + u)]$$

$$V_d = V_{d0} \cos \alpha - R_c \bar{I}_d \Rightarrow \bar{V}_d = \cos \alpha - \bar{I}_d$$

$$V_d = -V_{d0} \cos \gamma + R_c \bar{I}_d \Rightarrow \bar{V}_d = -\cos \gamma + \bar{I}_d$$




So, we will divide this into two sets of equations; one set is for u greater than 0 and less than or equal to 60 degrees, the other set is for u greater than or equal to 60 degrees and less than 120 degrees. So, we got a few equations for u greater than 0 and less than or equal to 60 degrees. So, write all these equations; the first equation is relating V_d , V_{d0} , α and u . So,

V_d is equal to V_{do} by $2 \cos \alpha + \cos \alpha + u$; I_d is equal to $I_s \cos \alpha - \cos \alpha + u$.

Then we also got an equation relating V_d , V_{do} and γ . So, we have V_d is equal to V_{do} by $2 \cos \gamma - \cos \gamma + u$. Similarly there is an equation relating I_d , I_s , γ and u . So, I_d is $I_s \cos \gamma - \cos \gamma + u$ and there is an equation relating V_d , V_{do} , α , R_c , and I_d . So, we got V_d equal to $V_{do} \cos \alpha - R_c I_d$. And the last equation that we consider always the relation between V_d , V_{do} , γ , $R_c I_d$, so that is V_d is equal to $\cos \gamma V_{do} + R_c I_d$. So, these six equations were obtained for u greater than 0 and less than 60 degrees. We got similar equations for u greater than or equal to 60 degrees and less than 120 degrees.

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$60^\circ \leq u < 120^\circ$

$$V_d = \frac{\sqrt{3} V_{do}}{2} [\cos(\alpha - 30^\circ) + \cos(\alpha + u + 30^\circ)] \Rightarrow \bar{V}_d = \frac{\sqrt{3}}{2} [\cos(\alpha - 30^\circ) + \cos(\alpha + u + 30^\circ)]$$

$$\hat{I}_d = \frac{I_s}{\sqrt{3}} [\cos(\alpha - 30^\circ) - \cos(\alpha + u + 30^\circ)] \Rightarrow \bar{I}_d = \frac{1}{2\sqrt{3}} [\cos(\alpha - 30^\circ) - \cos(\alpha + u + 30^\circ)]$$


$$V_d = \frac{\sqrt{3} V_{do}}{2} [-\cos(\gamma - 30^\circ) - \cos(\gamma + u + 30^\circ)] \Rightarrow \bar{V}_d = \frac{\sqrt{3}}{2} [-\cos(\gamma - 30^\circ) - \cos(\gamma + u + 30^\circ)]$$

$$\hat{I}_d = \frac{I_s}{\sqrt{3}} [\cos(\gamma - 30^\circ) - \cos(\gamma + u + 30^\circ)] \Rightarrow \bar{I}_d = \frac{1}{2\sqrt{3}} [\cos(\gamma - 30^\circ) - \cos(\gamma + u + 30^\circ)]$$

$$V_d = \sqrt{3} V_{do} \cos(\alpha - 30^\circ) - 3 R_c \hat{I}_d \quad \Rightarrow \bar{V}_d = \sqrt{3} \cos(\alpha - 30^\circ) - 3 \bar{I}_d$$

$$V_d = -\sqrt{3} V_{do} \cos(\gamma - 30^\circ) + 3 R_c \hat{I}_d \quad \Rightarrow \bar{V}_d = -\sqrt{3} \cos(\gamma - 30^\circ) + 3 \bar{I}_d$$

Normalization




So, let me summarize those equations also; $60^\circ \leq u < 120^\circ$. So, V_d is equal to $\frac{\sqrt{3}}{2} V_{do} \cos(\alpha - 30^\circ) + u \cos \alpha$; then the equation relating I_d and I_s is, $I_d = I_s \left[\frac{\sqrt{3}}{2} \cos(\alpha - 30^\circ) - \cos \alpha \right]$.

V_d is equal to $\frac{\sqrt{3}}{2} V_{do} \cos(\gamma - 30^\circ) - u \cos \gamma$. And the relation between I_d and I_s for 3 and 4 valve conduction mode or of course from 3 valve conduction mode is, $I_d = I_s \left[\frac{\sqrt{3}}{2} \cos(\gamma - 30^\circ) - \cos \gamma \right]$. Then you have two more equations involving R_c . So, $V_d = \frac{\sqrt{3}}{2} V_{do} \cos(\alpha - 30^\circ) - 3 R_c I_d$. Now V_d is equal to $-\frac{\sqrt{3}}{2} V_{do} \cos(\gamma - 30^\circ) + 3 R_c I_d$.

So, I have 6 equations, so for 3 and 4 valve conduction mode and 3 valve conduction mode and 6 equations which is applicable for 2 and 3 valve conduction mode as well as 3 valve conduction; because both these sets of equations are valid for $u = 60^\circ$. Now we are all familiar with what is known as normalization; normalization is something which is common in power system analysis.

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$$\bar{I}_d = \frac{I_s}{\sqrt{3}} [\cos(\alpha - 30^\circ) - \cos(\alpha + \mu + 30^\circ)]$$


$$V_d = \frac{\sqrt{3} V_{do}}{2} [-\cos(\gamma - 30^\circ) - \cos(\gamma + \mu + 30^\circ)]$$

$$\bar{I}_d = \frac{I_s}{\sqrt{3}} [\cos(\gamma - 30^\circ) - \cos(\gamma + \mu + 30^\circ)]$$

$$V_d = \sqrt{3} V_{do} \cos(\alpha - 30^\circ) - 3 R_c \bar{I}_d$$

$$V_d = -\sqrt{3} V_{do} \cos(\gamma - 30^\circ) + 3 R_c \bar{I}_d$$

Normalization

$$\bar{V}_d = \frac{V_d}{V_{do}}, \quad \bar{I}_d = \frac{I_d}{2 I_s}$$



So, it will help in simplifying the equations. So, let us see how we normalize the equations which are applicable to the converter; of course, we will consider only the right quantities on the DC side. So, we need to find what are the suitable phase values? So, if I take the DC side voltage or the DC side current; then I need to find the appropriate phase values, so I get normalized value or the quantity implied by dividing the quantity by the DC value.

So, if I take the DC side voltage V_d , the average value of the DC side voltage V_d . So, we choose the base value as V_{do} , so I normalize the DC side voltage by dividing it by V_{do} to get what is known as the V_d in per unit. So, I differentiate between the actual V_d and the V_d in per unit by a bar.

So, \bar{V}_d is the DC side voltage in per unit, which is defined as the actual V_d divided by the phase value V_{do} . Similarly if I take the current I_d , the normalized current or current in per

unit on the DC side is defined as the actual current divided by the base value. So, here we choose the base value as $2 I_s$.


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$$V_d = \frac{3\sqrt{2}}{\pi} V$$

$$I_s = \frac{V}{\sqrt{2} \omega L}$$

Let V , ω , and L be constants.
 Then V_d and I_s are constants.
 The other quantities $V_d, I_d, \alpha, u, \gamma$ may vary.



If you look at the expression for V_d and I_s ; V_d is $3\sqrt{2}$ by π V , where V is the RMS value of line to line voltage and I_s is V by $\sqrt{2} \omega L$, ω is the operating value of the angular frequency and L is the inductance in each phase on the AC side. So, if I assume V , ω and L to be constant. So, let V , ω and L be constants. So, it actually means V_d and I_s are constants; then V_d and I_s are constants. So, there are other quantities which may vary, there are, so the other quantities. So, what are the other quantities? The other quantities are $V_d, I_d, \alpha, u, \gamma$ may vary.

So, what we will do is, we will try to rewrite the equations that we wrote just now in terms of the quantities in per unit. So, I have V_d and I_d in equations that I have written just now. So,

I will normalize these equations and try to write these equations in terms of V_d bar or I_d bar, which are nothing, but the voltage and current in per unit.

So, if I look at these equations, I mean I get the equations in per unit either by dividing it by V_d o, which is the base value of V_d or dividing it by $2 I_s$ which is the base value of the current. So, if you look at these set of equations for u greater than 0 and less than or equal to 60 degrees, I have 6 equations. So, the first equation as, I mean has to be divided by V_d o; because all the quantities in this equations are voltage, ok. The second equation of course, all the quantities are current; so if I want the right quantities in per unit, I have to divide the second equation by $2 I_s$.

So, let us try to do this normalization by taking one equation at a time. So, if I take the first equation. So, I divide both sides of this equations by V_d o; then I get on the left hand side V_d by V_d o which is nothing but V_d bar. On the right hand side V_d o in the numerator gets cancelled by the V_d o in the denominator. So, I get on the right hand side $1/2 \cos \alpha$ plus $\cos \alpha$ plus u .

So, I can do the normalization of current also. So, if I take the second equation, I divide the left hand right hand sides by $2 I_s$. So, I_d by $2 I_s$ is nothing, but I_d bar on the left hand side. So, on the right hand side I get $1/2 \cos \alpha$ minus $\cos \alpha$ plus u .

So, the third equation is V_d bar equal to $1/2 \cos \gamma$ minus $\cos \gamma$ plus u ; and the fourth equation is V_d bar sorry, fourth equation is I_d bar equal to $1/2 \cos \gamma$ minus $\cos \gamma$ plus u . Then the next equation is V_d equal to V_d o $\cos \alpha$ minus $R_c I_d$. So, I have to divide this equation by V_d o; the left hand side is V_d bar, the right hand side is first option minus. So, the second term is $R_c I_d$, so if I divide this by V_d o. So, if I use the definition of R_c , then the second term on the right hand side of this equation after normalization is I_d bar. And the last equation is V_d bar is equal to $\cos \gamma$ plus I_d .

Now if you notice the equations that I have obtained from the original equations, so there is no V_d o there is no I_s . So, what I have on the in the revised set of equations is V_d bar, I_d bar, α and u ; and of course, in some equation there is a γ (Refer Slide Time: 13:18).


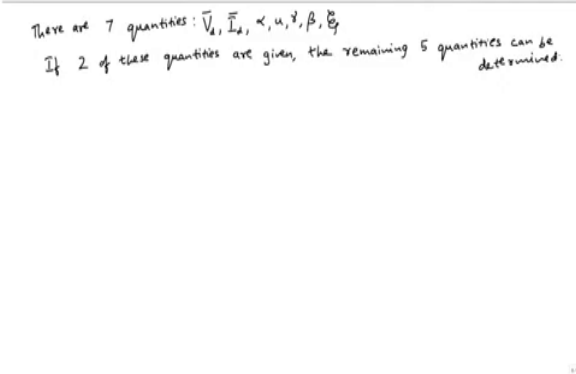

So, I do not have V_d anywhere, and after normalization I do not have I_s , I do not even have R_c , ok

So, I can similarly get the equations in per unit for this set of equations, which are which is applicable for u greater than and equal to 60 degrees and less than 120 degrees. So, the first equation is normalized by dividing by V_d . So, the left hand side is V_d bar is equal to $\frac{\sqrt{3}}{2} \cos(\alpha - 30^\circ)$, plus $\cos(\alpha + u + 30^\circ)$. Then the second equation is normalized by dividing by $2 I_s$; so I get I_d bar equal to $\frac{1}{2} \frac{\sqrt{3}}{2} \cos(\alpha - 30^\circ) - \cos(\alpha + u + 30^\circ)$.

And the next equation is divided by V_d on both sides. So, I get on the left hand side V_d bar. So, is equal to $\frac{\sqrt{3}}{2} \cos(\gamma - 30^\circ) - \cos(\gamma + u + 30^\circ)$. Next equation is divided by $2 I_s$, I get I_d bar is equal to $\frac{1}{2} \frac{\sqrt{3}}{2} \cos(\gamma - 30^\circ) - \cos(\gamma + u + 30^\circ)$. The next equation I have V_d , V_d , α , $R_c I_d$; so after normalization I will not have V_d , I will not have R_c .

So, I get V_d bar equal to $\frac{\sqrt{3}}{2} \cos(\alpha - 30^\circ)$. So, if I use the definition of R_c . So, R_c is defined as V_d by $2 I_s$. So, I get the second term on the right hand side of this equation as, $3 I_d$ bar; and the last equation is obtained by dividing both sides by V_d , I get V_d bar equal to $-\frac{\sqrt{3}}{2} \cos(\gamma - 30^\circ) + 3 I_d$. So, what we have done is; obtain the equations in per unit V_d , per unit I_d , instead of the actual V_d and actual I_d .

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So, there are 7 quantities. So, let me write down what are the quantities. There are 7 quantities; the \bar{V}_d or V_d bar which is the V_d in per unit, \bar{I}_d bar is nothing but I_d in per unit, alpha, u, gamma, beta, and psi. So, there are 5 angles and the voltage \bar{V}_d bar, the current \bar{I}_d bar.

So, among these 7; if 2 of these quantities are given, the remaining 5 can be determined. So, if 2 of these quantities are given; the remaining 5 quantities can be determined. So, we can use the different equations that we have derived. So, derive the values of these 5 quantities from the given values of 2 quantities, ok.