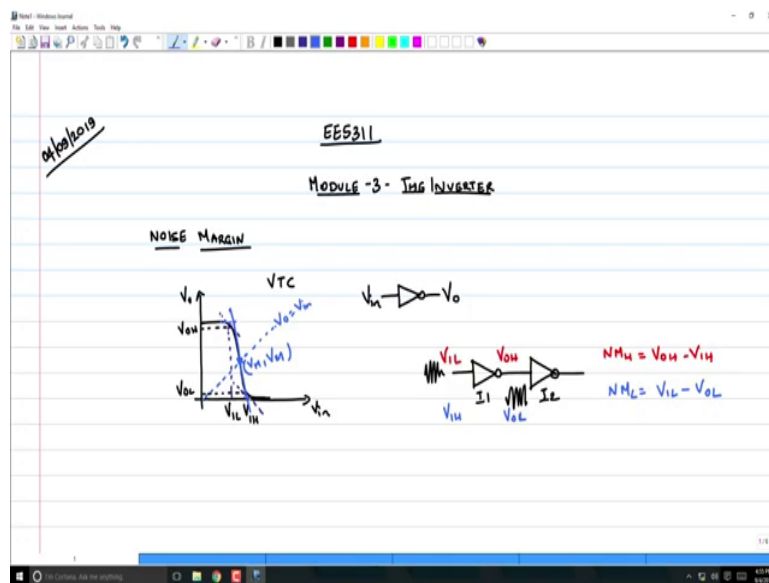


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Lecture - 22
Noise Margin Analysis- Long Channel Device Inverter

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So, we were discussing Noise Margin last time right and what was the idea here? We basically had the Voltage Transfer Characteristics: VTC V_o versus V_i for an inverter like this V_i in V_o out ok. So, the VTC is like this and we said that the point at which the slope becomes minus 1 is of significance because before that right or outside that this signal gets attenuated or noise gets attenuated, within that region the noise gets amplified. And therefore, the region of importance is between the points at which the slope is minus 1, ok.

That is why minus 1 is a magic number here ok. So, we basically said that this was V_{IL} this was V_{IH} right, the corresponding y axis coordinates were defined to be V_{OL} and this was defined to be V_{OH} , ok. So, the idea of noise margin is if I have one inverter driving another inverter like this and I have noise fluctuating here right, then how does it go and get how does it affect.

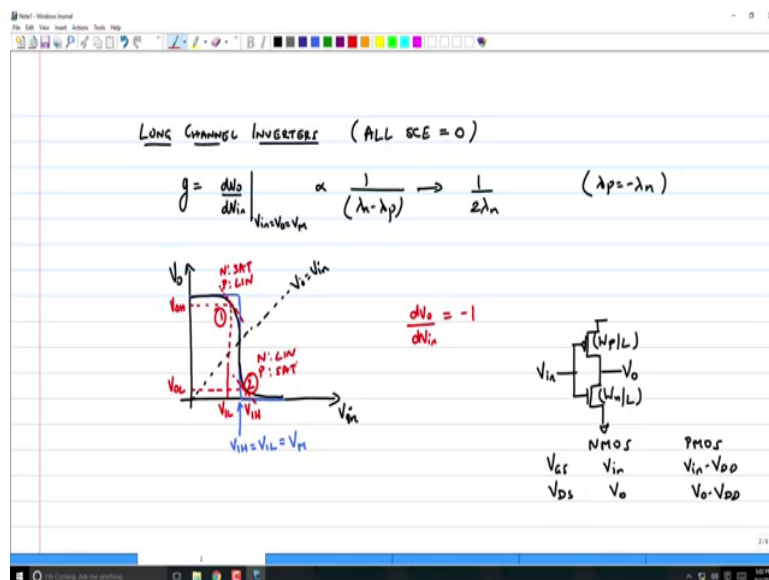
You know if I have noise on each of these nodes, then how does the signal propagation get affected was the question right. So, for example if the input was V_{IL} , then the output of the first inverter which is I_1 and this is I_2 output of the first inverter, I_1 would be V_{OH} right, but for V_{OH} to get recognized as a logic high for inverter 2 V_{OH} has to be greater than V_{IH} , right.

So, therefore, the noise margin high is V_{OH} minus V_{IH} . Similarly if you give V_{IH} here, then you would get V_{OL} here. The output of the first inverter will give you V_{OL} and for V_{OL} to get recognized as the logic low on inverter 2 V_{OL} has to be less than V_{IL} . Therefore, the noise margin low is V_{IL} minus V_{OL} .

Why noise margin? Because I have that much of margin for the noise to actually cause a fluctuation and not cause a change in the output right. That is the margin that I have and that is why it is called Noise Margin and of course, to derive this you know we had to make some assumptions. Earlier we said that we will take this point where V_{in} is equal to V_{out} , right. This is V_{out} equal to V_{in} and this point we would call it V_M , V_M that is both input and output are the trip point V_M .

And, it would be said that we will just extrapolate this slope right and then whatever intersects here this is what we call V_{IL} and this point we called as V_{IH} right. This is what we did earlier. So, last class we stopped at the point when we started discussing Long Channel Inverter. Suppose we had a long channel device instead of a short channel device, then what would happen to this assumption is this model even valid right.

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So, let us go back to long channel inverters which means that all short channel effects equal to 0. No channel length modulation, the velocity saturation voltage is very high right. So, therefore from linear it will only go into saturation right and all these things basically just vanish from our discussion ok. So, now if you remember the gain expression right equal to dV_{out} by dV_{in} at V_{in} equal to V_{out} equal to V_M was proportional to 1 over λ_n minus λ_p , right.

And this is nothing, but if λ_p equals minus λ_n , then this would be 1 over $2\lambda_n$ right. So, because of very small value of λ_n channel length modulation, this gain is very high and we got some expressions from that right, but of course in a long channel inverter, what is λ_n ? 0 . So, therefore if I use this particular model to derive the V_{IL}

and V_{IH} of the inverter of a long channel inverter, what would happen is because at this point which is V_{in} equal to V_{out} , sorry without equal to V_{in} , right.

At this point if I consider the gain, it is minus infinity right. It is not plus infinity because the curve will fall minus infinity and therefore, if I do the same extrapolation the curve will just extrapolate like this and both V_{IH} V_{IH} equal to V_{IL} equal to V_m , they will both simply collapse to this point though whatever I have shown here is not the V_{TC} of a long channel inverter. This is the model, that we used where we extrapolated the slope at V_{in} equal to V_{out} equal to V_m and pull that line all the way up that is the blue line the actual V_{TC} is what is shown in black here, it will come like this. At this point, it will be minus infinity and then again it will be V_{in} like this.

So, clearly this model that we used earlier works only for short channel device inverters where λ_n and λ_p are non-zero, right. So, now the question is how do I derive an expression for V_{IL} and V_{IH} for a long channel inverter, right. So, it turns out that the model was used in the first place because the expressions, current expressions for short channel inverters was very complicated. And therefore, actually solving for this point when the slope is actually minus 1 on both sides was very hard.

Because, you had velocity saturation, then you had channel length modulation, you had so many things, right. There is so many dependence on V_{in} and V_{out} , so solving for this point where dV_{out}/dV_{in} is minus 1 was very hard in a short channeling matter. Therefore, we use the approximation and the model and that is a reasonable model, right. Now it turns out here that you do not have to actually use that model at all. You can derive everything from first principles, right.

This is p_{il} V_{IH} and this is V_{OH} and this is V_{OL} right. So, at 0.1 and this is 0.2 dV_{out}/dV_{in} equal to minus 1 that is a definition for the noise margin, right. So, in region one in which mode of operation is the NMOS which mode of operation is the PMOS yeah, ok. I need to this is something you should really get used to you know. So, maybe let us do it again.

So, that you this is V_{in} V_{out} , this is W_p by l , this is W_n by l in region one V_{OH} is nearly V_{DD} , very close to V_{DD} , right. So, let us again write these expressions V_{GS} V_{DS} sorry V_{DS} for NMOS and p mos. So, V_{GS} is what for the NMOS in terms of V_{in} and V_{out} V_{in} what about V_{DS} V_{out} PMOS V_{in} minus V_{DD} and V_{DS} V_{out} ok.

Now, V_{OH} is nearly V_{DD} right. Therefore V_{DS} for the NMOS is what V_{DD} nearly V_{DD} , right. V_{in} is what you can assume. It is just about threshold somewhere it is a very small value. So, in which region of operation is it V_{DS} is greater than V_{GS} minus V_t and therefore, NMOS has to be in saturation. So, in region one NMOS is in saturation PMOS is in linear right, in region two NMOS in linear PMOS is in saturation. So, we will now use these expressions in order to solve for the points V_{IL} and V_{IH} .

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$$I_{Dn} = \frac{1}{2} k_n' \frac{W_n}{L} (V_{in} - V_{tn})^2 \quad (\text{sat})$$

$$I_{Dp} = k_p' \frac{W_p}{L} (V_0 - V_{DD}) \left(V_{in} - V_{DD} - V_{tp} - \frac{(V_0 - V_{DD})}{2} \right)$$

$$I_{Dn} = -I_{Dp}$$

$$\Rightarrow \frac{1}{2} k_n' \frac{W_n}{L} (V_{in} - V_{tn})^2 = -k_p' \frac{W_p}{L} (V_0 - V_{DD}) \left(V_{in} - V_{DD} - V_{tp} - \frac{(V_0 - V_{DD})}{2} \right)$$

Diff wrt V_{in}

$$\Rightarrow k_n' \frac{W_n}{L} (V_{in} - V_{tn}) = -k_p' \frac{W_p}{L} \left[\left(\frac{dV_0}{dV_{in}} \right) \left(V_{in} - V_{DD} - V_{tp} - \frac{(V_0 - V_{DD})}{2} \right) + (V_0 - V_{DD}) \left(1 - \frac{1}{2} \frac{dV_0}{dV_{in}} \right) \right]$$

$$\text{Let } -k_p' \frac{W_p}{L} / k_n' \frac{W_n}{L} = \gamma$$

What is I_{DSn} ? What is the Saturation Current? Remember there is no velocity saturation. Now it is in it is a long channel inverter. So, directly it is going to go into saturation. So, what is I_{DSn} half $K_n' W_n$ by L into $V_{in} - V_{tn}$ whole square, right. This is in saturation current. What about I_{DSP} ? Yeah $K_p' W_p$ by L into it is a linear current, right. So, it is V_{DS} into $V_{GS} - V_{tp} - V_{DS}$ by 2. What is V_{DS} ? $V_{naught} - V_{DD}$ into $V_{in} - V_{DD} - V_{TP} - V_{naught} - V_{DD}$ by 2: right.

Now, again we impose our good old condition I_{DSn} equals minus I_{DSP} right two transistors in series one. Current is going up, one current is going down. They have to be the same and therefore, I_{DSn} equal to minus I_{DSP} which implies I can now write half into $K_n' W_n$ into $V_{in} - V_{tn}$ the whole squared equals minus $K_p' W_p$ by L into $V_{naught} - V_{DD}$ into $V_{in} - V_{DD} - V_{TP} - V_{naught} - V_{DD}$ I will just leave this as it is, ok.

I am not going to simplify that V_{DD} term for now, right. So, now what do you do, differentiate both sides with respect to V_{in} differentiate with respect to V_{in} implies $K_n' W_n$ $V_{in} - V_{tn}$ equals minus $K_p' W_p$ into dV_{naught} / dV_{in} into $V_{in} - V_{DD} - V_{TP} - V_{naught} - V_{DD}$ by 2 plus $V_{naught} - V_{DD}$ into 1 minus half dV_{naught} / dV_{in} , right. Now, let us let minus $K_p' W_p$ by $K_n' W_n$ equals r , right.

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Diff mode v_{in}

$$\Rightarrow k_n' u_n (v_{in} - v_{tn}) = -k_p' u_p \left[\left(\frac{dv_o}{dv_{in}} \right) (v_{in} - v_{DD} - v_{tp}) - \left(\frac{v_o - v_{DD}}{2} \right) + (v_o - v_{DD}) \left(1 - \frac{1}{2} \frac{dv_o}{dv_{in}} \right) \right]$$

Let $-k_p' u_p / k_n' u_n = r$

$$\Rightarrow (v_{in} - v_{tn}) = r \left[(-1) (v_{in} - v_{DD} - v_{tp}) - \left(\frac{v_o - v_{DD}}{2} \right) + (v_o - v_{DD}) \left(\frac{3}{2} \right) \right]$$

$$\therefore v_{in} = \frac{v_{tn} + r(v_{DD} + v_{tp} + 2(v_o - v_{DD}))}{(1 + r)}$$

Then I can say implies $V_{in} - V_{tn}$ equals r times dV_{out} by dV_{in} . What is dV_{out} by dV_{in} ? At that point minus 1 right; so, therefore I can write this as minus 1 and what is V_{in} at that point V_{IL} at that point when the slope is minus 1, there by definition it is V_{IL} right into $V_{IL} - V_{DD} - V_{TP} - V_{OH} - V_{DD}$ by 2 right.

Correct plus $p_{out} - V_{DD}$ into $1 - \frac{1}{2} \frac{dV_{out}}{dV_{in}}$ by dV_{in} will just become 3 by 2. So, can you now simplify and get me an expression for V_{IL} . Do not make any assumption right. V_{out} by the way is what actually it is V_{OH} , yeah. Can you now simplify this expression and get me the expression for V_{IL} ? Are you getting this expression? Are you getting this expression right ok.

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for V_{IH}

PMOS \rightarrow SAT

NMOS \rightarrow LIN

$$I_{DSP} = \frac{1}{2} K_p' \frac{W_p}{L_p} (V_{in} - V_{DD} - V_{tp})^2$$

$$I_{DSN} = K_n' \frac{W_n}{L_n} V_o \left[(V_{in} - V_{tn}) - \frac{V_o}{2} \right]$$

$$\Rightarrow I_{DSN} = -I_{DSP}$$

$$\Rightarrow K_n' \frac{W_n}{L_n} V_o \left[(V_{in} - V_{tn}) - \frac{V_o}{2} \right] = -K_p' \frac{W_p}{L_p} (V_{in} - V_{DD} - V_{tp})^2$$

$$\left(\frac{dV_o}{dV_{in}} = -1 \right) \quad \& \quad -K_p' \frac{W_p}{L_p} / K_n' \frac{W_n}{L_n} = r$$

$$\Rightarrow \frac{dV_o}{dV_{in}} \left[(V_{in} - V_{tn}) - \frac{V_o}{2} \right] + V_o \left[\frac{1}{2} \frac{dV_o}{dV_{in}} \right] = r (V_{in} - V_{DD} - V_{tp}) \quad \begin{matrix} V_{in} = V_{IH} \\ V_o = V_{OH} \end{matrix}$$

Now what about V_{OH} V_{OH} ? You got to do the exact opposite right. For V_{IH} PMOS is in which region? Saturation NMOS is in linear, ok. So, can we write the expressions of the currents i_{DSp} is $K_p' \frac{W_p}{L_p} (V_{in} - V_{DD} - V_{tp})^2$ which is nothing, but $V_{in} - V_{DD} - V_{tp}$ whole squared and i_{DSn} equals $K_n' \frac{W_n}{L_n} V_{DS} (V_{in} - V_{tn} - V_{DS}/2)$. What is V_{DS} for the NMOS? Yeah V_{naught} . What about $V_{in} - V_{tn} - V_{naught}/2$, right.

Again I go ahead and do the same thing if equals minus i_{DSp} which implies $K_n' \frac{W_n}{L_n} V_{naught} (V_{in} - V_{tn} - V_{naught}/2) = -K_p' \frac{W_p}{L_p} (V_{in} - V_{DD} - V_{tp})^2$. Again differentiate with respect to V_{in} dV_{out}/dV_{in} equal to minus 1 right. Use this fact implies $K_n' \frac{W_n}{L_n}$ and minus $K_p' \frac{W_p}{L_p}$ equals r which implies I can write dV_{out}/dV_{in} into $V_{in} - V_{tn} - V_{naught}/2$.

V_{th} by 2 plus V_{th} into 1 minus dV_{out} by V_{in} half, right equals V_{in} minus V_{DD} minus V_{TP} into r .

So, can you simplify this and tell me what you get for? Of course, here V_{in} is nothing, but V_{IH} V_{out} is nothing, but V_{OL} can you get me the expressions equal to dV_{th} .

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The image shows a digital notepad with the following handwritten equations:

$$\Rightarrow (1+r)V_{IH} = V_{Tn} + 2V_{OL} + r(V_{DD} + V_{TP})$$

$$\Rightarrow V_{IH} = \frac{V_{Tn} + 2V_{OL} + r(V_{DD} + V_{TP})}{1+r} = \frac{V_{Tn} + r(V_{DD} + V_{TP}) + 2V_{OL}}{1+r}$$

$$V_{IL} = \frac{V_{Tn} + r(V_{DD} + V_{TP} + 2(V_{OH} - V_{DD}))}{(1+r)} = \frac{V_{Tn} + r(V_{DD} + V_{TP}) + 2r(V_{OH} - V_{DD})}{1+r}$$

$$\Delta V_{IHM} = V_{IH} - V_{IL} = \frac{2V_{OL} - 2r(V_{OH} - V_{DD})}{(1+r)}$$

$$= \frac{2(V_{OL} - rV_{OH}) + 2r(V_{DD})}{(1+r)}$$

So, this is not. So, in this 3 by 2 V_{th} plus 2 V_{OL} plus r into V_{IH} is V_{Tn} plus 2 V_{OL} plus r into V_{DD} plus V_{TP} by you get this yeah good. So, I just derived the whole thing, so that you are you get used to this kind of solving of you know these equations. So, now let us compare the earlier expression that we also had right what was our V ? V_{IL} is V_{Tn} plus r into this. So, can I copy this?

Yeah. So, V_{IL} is this. So, can you compare these two expressions and see what do you get here. I am going to write this as $V_{Tn} + r \cdot V_{DD} + V_{TP} + 2 V_{OL}$ by $1 + r$ and this I am going to write as $V_{Tn} + r \cdot V_{DD} + V_{TP} + 2 r \cdot V_{OH} - V_{DD}$ by $1 + r$. So, what is this region between V_{IL} and V_{IH} ? How thin is this region right?

Ideally you would want it to be 0. You know 0 indeterminate region right, you want the inverter characteristic to fall sharply like this, but inevitably there is a small region. So, what is this ΔV_{IH} right which I am going to call it as $V_{IH} - V_{IL}$. Clearly you can see that this $V_{Tn} + r \cdot V_{DD} + V_{TP}$ is sort of gone, right. So, you basically have simply $V_{IH} - V_{IL}$, right; so, $2 V_{OL} - 2 r \cdot V_{OH} + V_{DD}$ by $1 + r$, right.

So, I can write this as $2 V_{OL} - r \cdot V_{OH} + 2 r \cdot V_{DD}$ by $1 + r$. Actually, that is not necessary, right. We do not need this. No this simplification is not necessary ok. So, what is V_{OL} ? It is a number which is very close to 0, V_{OH} number which is very close to V_{DD} , right. So, $V_{OH} - V_{DD}$ is a very very small negative number, V_{OL} is a very very small positive number. So, if you see this difference it is actually extremely small number.

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The image shows a handwritten derivation on a digital notepad. The equations are as follows:

$$\Rightarrow (1+r)V_{IH} = V_{TN} + 2V_{OL} + r(V_{DD} + V_{TP})$$

$$\Rightarrow V_{IH} = \frac{V_{TN} + 2V_{OL} + r(V_{DD} + V_{TP})}{1+r} = \frac{V_{TN} + r(V_{DD} + V_{TP}) + 2V_{OL}}{1+r}$$

$$V_{IL} = \frac{V_{TN} + r(V_{DD} + V_{TP} + 2(V_{OH} - V_{DD}))}{(1+r)} = \frac{V_{TN} + r(V_{DD} + V_{TP}) + 2r(V_{OH} - V_{DD})}{1+r}$$

$$\Delta V_{IH} = V_{IH} - V_{IL} = \frac{2V_{OL} - 2r(V_{OH} - V_{DD})}{(1+r)}$$

$$\text{Let } V_{OL} = V_{DD} - V_{OH}$$

$$\Rightarrow \Delta V_{IH} = \frac{2V_{OL} + 2r(V_{OL})}{(1+r)} = 2V_{OL} \leftarrow$$

So, for example you could assume let right V_{OL} equals V_{OH} minus V_{DD} or V_{DD} minus V_{OH} for symmetry, right. It is on either side. It is going by the same amount is what we are saying. So, if that is the case, then what does that thing simplify to V_{IH} is $2V_{OL}$ minus plus $2r$ into V_{OL} , sorry right. What is it simplify to $1 + r$ comes out and you have twice V_{OL} .

So, what are we saying for a long channel inverter, this region in which this the input is an indeterminate input is actually simply twice V_{OL} . It is such a small region it is almost like up to V_{DD} by 2, everything is logic low after V_{DD} by to everything is logic high, right. So, that is the reason I wanted to go through this long channel inversion inverted derivation because it allows me to show you exactly that this is true, clear.

So, that region in which because the slope is minus infinity at V_{in} equal to V_{out} equal to V_M that region also has to be very, very, very small for a long channel inverter, clear. Of

course, here I am assuming that V_{OL} equal to V_{DD} minus V_{OH} it is the fair thing actually because V_{OH} is supposed to be V_{DD} , V_{OL} is supposed to be ground ideally.

Any questions here? So, two things one short channel transistor, the equations are very complex because just think about this now in each of these terms if I add a $1 + \lambda V$ naught, just think about how you will do this differentiation and get the accurate answer. It is not possible. It is not even tractable and it is not even useful. The end of the day I do not even get a result like this where I can intuitively understand something from it, right.

It just makes it very complex and therefore, we resort to that approximation where we extrapolate that line act V_{in} equal to V_{out} equal to V_M with that same slope. And then, extrapolate those points as V_{IH} and V_{IL} right, but for the long channel device it is possible to derive these expressions very accurately clear. And, if you make the assumption that V_{OL} is equal to 0 and V_{OH} is V_{DD} , then you will find then this region ΔV_{IH} is basically 0.

So, that is also not true it. So, somewhere it is because V_{OH} and V_{OL} are not exactly V_{DD} and ground respectively. That is when this small indeterminate region actually comes into picture, ok. Here we have made no approximations whatsoever. All expressions are accurate here.