

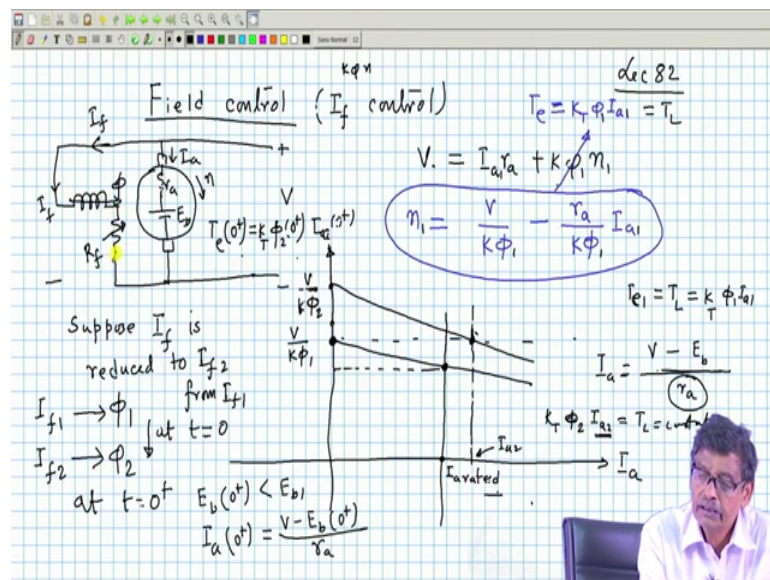
Electrical Machines- I
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Lecture - 82
Speed Control of Shunt Motor - III

Welcome to this lecture and we have been discussing about the Speed Control of DC motor. We discussed in the earlier lectures, the speed control of the DC motor by controlling its armature voltage or by connecting some external resistances in the armature circuit. If, it is to be controlled by armature voltage method, then field circuit should be separated and, you apply a variable DC voltage. Armature registers control is inefficient, so armature voltage is a nice method and you can control this speed down to zeros very smoothly and this is done.

And, this method of speed control is most suited for the load, whose stock demands is constant at various rpm's that is what I told. Now, today I will discuss about another interesting method that is the field control.

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Field control, that is also called I_f field current control, I_f control. And, I will also restrict our discussion till now on DC shunt motor or separately excited motor whenever it will be necessary. Since, you will be controlling the field current therefore, the circuit adopted is like this, this is your armature ok. And, this your field circuit, here I will

connect supply and this is the thing these are connected parallel and here a constant voltage is applied.

This time, what I will do? I will control the field current by varying some external resistance connected in the circuit. So, that these flux per pole I will be controlling, ok. This is what I will do? [FL] In this case to understand first before I write down the equation, in the same way let us try to see physically what is going to happen. One thing is cleared here it is r_a and e_b , suppose the machine is running steadily at some constant rpm drawing some armature current I_a .

And, field current is set to some values so, that it is drawing I_f , field current. Now, in this case once again the equation remain same, you have to start with the armature KVL equation applied voltage. This time this armature voltage I am not varying so, b is equal to $I_a r_a$, r_a also I will not play with no external resistance in the armature circuit, neither I am varying the voltage applied across the armature so, $I_a r_a$ circuit plus $K \phi$ into speed. This time, I will be varying the flux this quantity I am varying and your n is equal to then V by $K \phi$ minus r_a by $K \phi$ into I_a this is the equation, is not.

And, remember the electromagnetic torque developed by the machine is equal to $\sum T$ into ϕ into I_a is not, no matter what you are controlling this is the rule for electromagnetic torque. Now, suppose I say that the machine is operating steadily, this axis is I_a , I say and this is the speed. Suppose, field current was rated field current initially operating point, so that the no load speed was here suppose and no load speed was V by K . And, let us say that initial operating point all the quantities are like this I_{a1} , I_{a1} , ϕ_1 got the point, it was drawing and speed was n_1 say.

So, what I am telling machine is running steadily at some field flux say ϕ_1 , speed is n_1 , n_1 , then applied voltage is V which is held fixed $I_{a1} r_a$ plus back EMF from this I get these values. Therefore, at that value of field current, this characteristics if I draw, suppose this is the no load speed. So, it will be V by $K \phi_1$.

And, then it is characteristics if you increase the current will be like this slope is r_a by $K \phi_1$. And, suppose it is the load torque; suppose, load torque is constant T_L constant. Then operating point will be here and this is suppose and the speed at which the machine will be running way is this one, this is the thing, [FL] ok. Now, what we will be doing?

So, T_e is equal to T_L and that is equal to $K T \phi_1 I_a$ this is the equation it is running here.

Let us assume that this current whatever it is the rated current of the machine, ok. It is supplying intersection of the torque speed curve of the motor and the load torque gives you this 1 point of intersection. Now, suppose I suddenly increase this resistance field circuit resistance. Suppose, I_f is reduced to say $I_f 2$.

Initially it was $I_f 1$, $I_f 1$ produced flux ϕ_1 . Now, $I_f 2$ will produce flux ϕ_2 . And, ϕ_2 will be less than ϕ_1 , because I have increased this resistance r_f applied voltage is fixed here because the field circuit. So, flux is reduced; reduce to field current is suppose I_f is reduce to $I_f 2$ from $I_f 1$ got the point, this is the equation [FL].

Let us first observe or explain the sequence of events that will go on. Initially, this was the operating point ϕ_1 . Now, suppose I have suddenly reduce the field current from $I_f 1$ to $I_f 2$ at T equal to 0. Can speed change instantaneously? No, that is the mechanical inertia decides that. So, at T equal to 0 plus which thing will change, flux has been reduced. Therefore, your back emf must have drawn back emf depends on the product of field current and speed.

So, if you suddenly say that flux has been brought down from ϕ_1 to ϕ_2 speed cannot change instantaneously that is fine, but flux you have brought down. Therefore, back emf which is $K \phi \omega$ speed has not changed must drop down. Therefore, armature current at T equal to 0 plus must go up is not armature current will grow up.

So, at T equal to 0 plus, what is T equal to 0? At T is equal to 0 I have this is what I have done at T equal to 0 ϕ_1 to ϕ_2 . At T is equal to 0 plus I am examining E_b to; $E_b 0$ plus must be less than $E_b 1$ that is all that is what I am telling speed cannot change flux you have reduce it will. If, that be the case then your armature current at 0 plus must go up because armature current is after all V minus E_b at 0 plus divided by r_a , r_a I have not changed. So, the armature current will go up.

Now, the question is I had assumed load torque true demand constant ok, whatever it is constant load torque. Earlier electromagnetic torque was equal to load torque in this condition, this was equal to T_L steadily running. Now, I have reduce the flux from ϕ_1

to ϕ^2 , then this is at T equal to 0 plus I am examining. What has happened to my electromagnetic torque developed?

Now, electromagnetic torque develop at T equal to 0 plus is once again the same relation suppose $K^2 \phi^2$ into I_a^2 0 plus, I am sorry I will write it in a nicer way. So, T_e at 0 plus will be the torque constant into ϕ^2 at 0 plus into I_a^2 at 0 plus is not, this product will decide what is the electromagnetic torque developed.

Now, we are in a fix now a bit, because of the fact ϕ has reduced armature current has increased. So, whether the electromagnetic torque developed at T equal to 0 plus is greater than the electromagnetic torque which was developed by the motor at T equal to 0 minus.

That is what one should ask, then only I will say motor will start accelerating or decelerating, because load torque is constant. The fact is this, this armature current at any time armature current is applied voltage minus back emf divided by r_a this is the current. Now, if you reduce the flux by say 2 percent increase in the armature current. It can be easily shown; it will be many folds then that.

Are you getting me what I am telling? Ok. This flux is reduce armature current has increased whether the product will be greater than the previous electromagnetic torque. I am telling it will be greater, because of the fact the increment in the armature current will be many fold than the reduction in the flux, because you are dividing it by a very small quantity r_a got the point, this is at the most crucial point.

We will solve problem you can easily see that. Therefore, what is going to happen then the electromagnetic torque developed by the motor at T equal to 0 plus will be more than the electromagnetic torque, the motor developed at T equal to 0 minus. And, I am telling load torque is constant therefore, motor will start accelerating from T equal to 0 plus onwards, if it accelerates, its armature current will then start falling.

And, finally, once again it will draw final steady state armature current, which will make $K T \phi^2$ into the final armature current to be equal to same load torque, load torque I have assumed constant. So, what do I say about the armature current drawn from the supply, when we have reduce the flux with constant load torque present on the shaft.

So, new armature current will be this is constant I have assumed. Therefore, new armature current is T_L by $K_T \phi^2$ and ϕ^2 I have I know I have deliberately reduced it.

So, the armature the new armature current drawn will be more than what was I_a earlier got the point. Therefore, we reduce the field current load torque constant, final armature current drawn by the machine will go up and up. Unlike the D.C armature control method; armature control method, there armature current was always constant and that is why we told it is better suited for constant load torque.

But, in case of field control I immediately discovered that if the load torque is constant as I told you I would always like to see the motor is drawing armature is carrying always constant current rated current. But, if it was earlier at this point carrying rated current and if I have reduced the flux, the current drawn new armature current drawn at steady state will be more than these if load torque is constant got the point.

Here of course, ϕ is not constant therefore, it is difficult to say that this is load torque are you getting ok, load torque is load torque constant. But, see so now, let us see in the characteristics terms what is going to happen? If, you have reduce the field current, new torque slip characteristics look at this ϕ I have reduced. So, new no load speed will be V by $K \phi^2$, it will be here.

And, then it will fall, but the slope will not be parallel. Because, ϕ has this is the slope of the line ϕ I have reduced. So, slope decrement in speed will be in at a much faster rate, this will no longer be parallel as we have seen it was parallel in case of armature voltage control, but it will be like this. So, it was drawing this much current. Here, I cannot show the load characteristics, if this is I_a , because load torque is I_a into ϕ , ok.

So, it is I_a only I_a armature current. Now, what I am telling, if, the load torque is constant it will run at higher speed, but with increased armature current. May be here, it was running here. Now, we have reduce the field current it will run there, if the load torque is constant. Mind you load torque is what product of armature current and the flux per pole, here it was I_a rated; here it will be how much is the load torque at this point.

This new I_a^2 into ϕ^2 ; $I_a^2 \phi^2$ is more than this. Therefore, load torque is increased like that load torque is will remain constant and it will run at the speed. Therefore, it

looks like the field control method better do not use it for constant load torque. If, the mechanical load is constant then better do not adopt to run the motor at higher and higher speed for constant load torque.

If, load torque is constant we have reduced phi, simply look at the statistic equation phi into I a. If, your initial current was I a rated, if you have reduce the flux, what will be the new armature current it must go up. So, that the product remains constant and if your initial current was I rated your new I a will be more than the rated values, that I do not like is not. Therefore, and; obviously, what happen if I go on increasing field current see at based this resistance.

If, you decrease this resistance, then only field current will be increased. So, at best you make this R f external 0 you cannot make r f negative is not. Therefore, variation of field current method means, flux control. You only increase the resistance, you cannot increase the field current beyond this value V by resistance of this coil at base you can make R f equal to 0, no.

So, this speed control above the rated speed is adopted by flux control, go on reducing the field current speed will raise. Now, the question is see I think you have got me I will try to summarize the result.

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field control

$T_{e1} = K_T \phi_1 I_{a1}$

$= K_T \phi_2 I_{a2}$

we reduce the flux ϕ_1 to ϕ_2

if $T_L = \text{constant}$

$K_T \phi_1 I_{a1} = K_T \phi_2 I_{a2}$

$I_{a2} = \frac{\phi_1}{\phi_2} I_{a1 \text{ rated}}$

$\phi_2 < \phi_1$

$I_{a2} > I_{a1 \text{ rated}}$

$\phi_1 I_{a \text{ rated}}$ is suitable to drive constant mechanical load.

But it is suitable for constant power load.

Power = $T_L \times \omega_r = \text{const}$

or $T_L \propto \frac{\text{const}}{\omega_r}$

Suppose, field control I am talking about field control. Electromagnetic torque developed by the machine is $K T \phi I_a$ that is known. In field control what I will be doing, I will reduce the flux; we reduce the flux. So, suppose initially electromagnetic torque was this steady operating point I am telling. If, you reduce the flux from ϕ_1 to ϕ_2 , then how much is the electromagnetic torque developed by the machine, it will be $K T \phi_2 I_a$. And, this armature current I_a , what I am telling is if you insist that T_L equal to constant; T_L equal to constant, I will say then $K T \phi_1 I_{a1}$ is equal to $K T \phi_2 I_{a2}$, that is what it will be steady operating point.

But, I know and suppose if I_{a1} is rated, then what will be I_{a2} ? I_{a2} will be ϕ_1 / ϕ_2 into I_{a1} rated, but ϕ_2 is less than ϕ_1 therefore, I_{a2} will become greater than I_{a1} rated that is what I wanted to tell. So, if somebody connects a constant mechanical load and initially it is drawing rated armature current, then he reduces the flux, then immediately current armature current will become more than that.

Therefore, this drive these method of control of speed is not suitable to drive constant mechanical load.

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It is not suitable very important to drive the constant mechanical load. See, your ultimate thing is you would always like to see your armature is carrying rated current that is the crucial thing. But, it is suitable for; constant power load.

What is constant power load? It is also the load characteristics, constant mechanical power load. Suppose, you have a load whose T_L into ω_r is equal to constant, what is ω_r load speed, then or T_L is proportional to constant by n_r , n_r is the load torque speed ω_r is $2\pi n_r$ etcetera. So, it will be proportional to these this is what power that is mechanical load whatever you have connected, it tells that it always requires constant power, that is now it is running at 100 rpm torque is so much.

So, torque into speed this product remains constant, that is if you want to run it at higher speed, it requires lesser torque. What is the constant power load? Higher the speed is that load requires lesser torque to be applied it is the characteristics of the load. Such a load is caused should be then called constant power load, higher speed torque requirement is

lesser. And, for such load this field control is absolutely failed? why, I will tell just verbally today, then I will explain next day with the help of some example.

That, if you higher speed you want to you want to run it D.C motor at higher speed, higher than the rated speed you reduce the field current. But, your load torque is such that when it runs at higher speed, it required lesser torque to be produced by the machine, then what will happen, ϕ you have increased. So, armature current will decrease then, initially if it was carrying rated current making ϕ_1 into I_a rated is the torque. Next time, it is ϕ_2 , but the armature current new armature current drawn will be such that this product remains same as these, I mean into speed.

Therefore, you see this type of a control of speed will be most suitable for loads which requires constant power mechanical load, torque into speed is constant. Speed make high then T_L required by the load is less therefore, T required developed by the motor will be less and T is ϕ into I_a^2 therefore, ϕ_2 into I_a^2 will be less. So, I_a^2 will be less I mean may be of the same rated current, you think about it and next time we will continue with our discussion with some numerical example.

So, remember that this field current method is suitable for constant power drive and armature voltage method is suitable for constant torque drive. And, armature voltage method is adopted whenever you want to control the speed below the rated speed and field control method is to be adopted when you want to control the speed above the rated speed. We will continue our discussion next time.

Thank you.