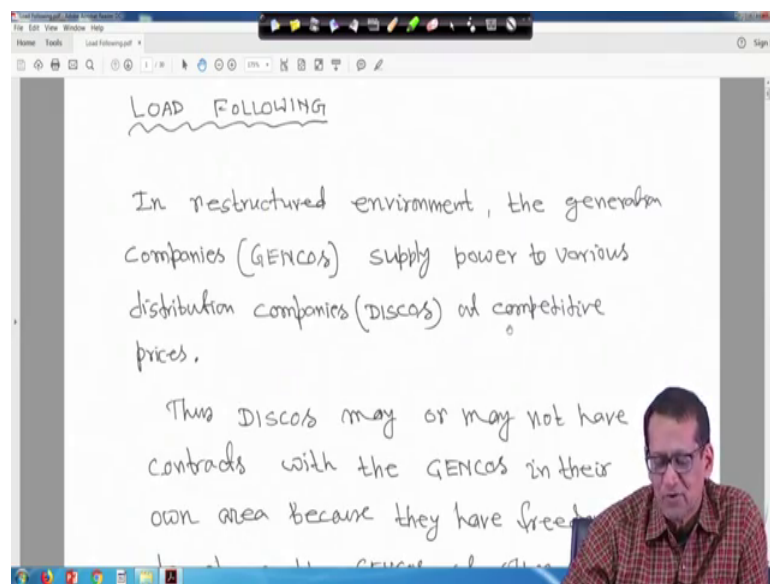


Power System Dynamics, Control and Monitoring
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Department of Electrical Engineering
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Lecture - 46
AGC in deregulated system (Contd.)

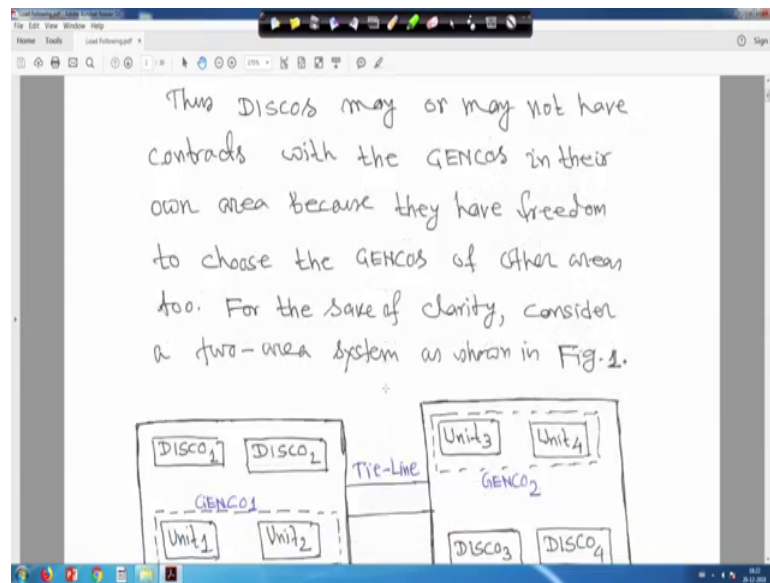
We are back again. So, although previous one also load following, but this is another version right; another type of modelling.

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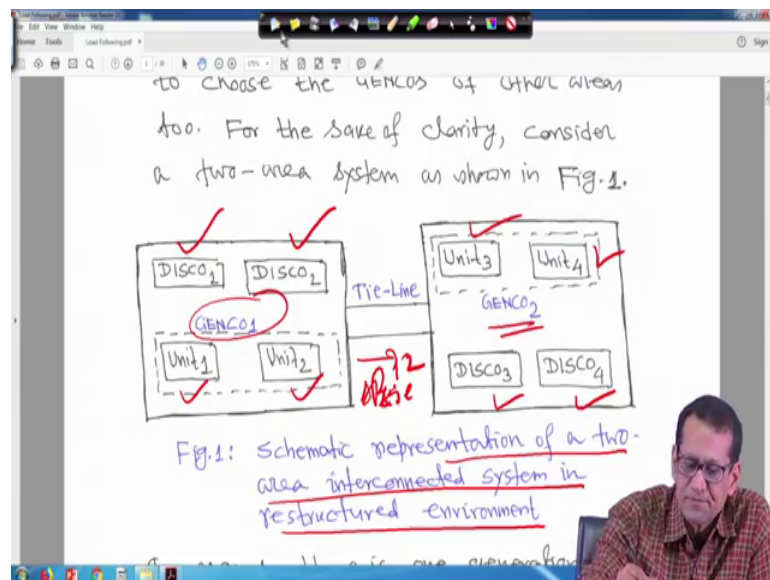
So, load following I told you what is load following right. So, when load disturbance is there generation will chase load such that generation will match the load in other way right and at steady state ideal condition. So, generation is equal to load plus of course, losses are there, but we will not consider that right. So, in just we have seen that in restructured environment the generation companies that is GENCOs supply power to various distribution companies in short we call DISCOs right at competitive prices.

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Now, thus DISCOs may or may not have contact with other with the GENCOs in their own area I told you because they have freedom to choose the GENCOs of other areas too; for the sake of clarity consider a two area system as shown in figure 1.

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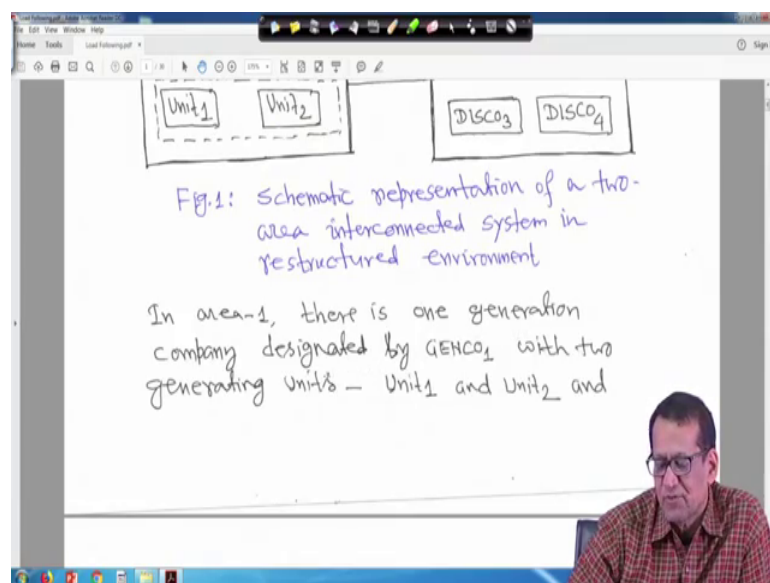


Here what we are what we are our modelling is same, but what we are trying to make it suppose in area 1; it is DISCO 1 and it is DISCO 2 right and in area 2 this is DISCO 3 and DISCO 4 that is your distribution companies.

Now area 1 one generation companies they are GENCO 1, but it has 2 units 2 generating units unit 1 and unit philosophy remains same. In the previous case we saw GENCO 1 and GENCO 2 and assuming that one generating units or its equivalent right. So, question may be many many units are there with same rating same turbine generating unit everything right.

So, but here philosophy remains same everything is same, but this GENCO 1, but generation company one has 2 units unit 1 and unit 2. Similarly generation GENCO 2 it had 2 units unit 2 unit 3 and unit 4 and this is that scheduled tie line power flow that is ΔP tie your 1 2 right; same as before same as before only mathematically or block diagram way slightly we have change right. So, this is schematic representation of a 2 area interconnected system in restructured environment right.

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. So, in area 1 now there is one generation company designated by GENCO 1 with 2 generating units it is unit 1 and unit 2.

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The screenshot shows a whiteboard with the following handwritten text:

(L2)
two distribution companies designated by DISCO₁ and DISCO₂.

Similarly, in area-2, there is only generation company, GENCO₂ and two distribution companies designated by DISCO₃ and DISCO₄.

GENCO₂ has also got two generating units - Unit₃ and Unit₄.

In the bottom right corner, there is a video feed of a man with glasses and a red plaid shirt.

And 2 distribution companies designated by DISCO 1 and DISCO 2 right.

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The screenshot shows a whiteboard with the following handwritten text:

DISCO₁ and DISCO₂.

Similarly, in area-2, there is only one generation company, GENCO₂ and two distribution companies designated by DISCO₃ and DISCO₄.

GENCO₂ has also got two generating units - Unit₃ and Unit₄.

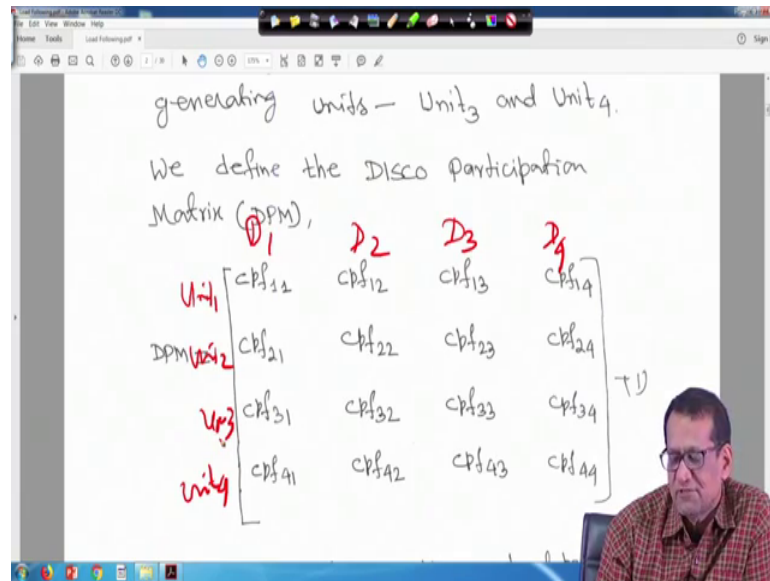
We define the DISCO participation Matrix (DPM),

In the bottom right corner, there is a video feed of the same man as in the previous slide.

Similarly, in area 2 there is only one generation companies; I have missed one right there is only one generation company GENCO 2 and two distribution companied designated by DISCO 3 and DISCO 4.

So, GENCO 2 also got 2 generating units unit 3 and unit 4. So, we define the DISCO participation matrix it will remain same it will remain same as before right.

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So, this is the DISCO participation matrix. So, there we are writing GENCO and this is where I am making in short DISCO 1 DISCO 2 DISCO 3 DISCO 4 distribution companies I am making it D 1 D 2 D 3 D 4. So, this is D 1 this is D 2 this is D 3 and this is D 4 and there it was GENCO 1 GENCO 2 GENCO 3 GENCO 4 and here instead of that we write it is unit 1, this is unit 2, this is unit 3 and this is your unit 4 right.

So, this way I instead of GENCO 1 GENCO 2 GENCO 3 GENCO 4 we are writing unit 1 unit 2 unit 3 and unit 4. And philosophy remains same that is you have same contact participation factor that matrix and this side will be; if you want to find out the contact demand this side will be same as before delta P L 1, delta P L 2, delta P L 3, delta P L 4. So, contact participation contact your what you call demand for GENCO unit 1 unit 2 and unit 3 and unit 4 will be $cpf_{11} \Delta P L 1 + cpf_{12} \Delta P L 2 + cpf_{13} \Delta P L 3 + cpf_{14} \Delta P L 4$ and so on right.

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The screenshot shows a video lecture interface. At the top, there are labels for columns: CPF_{41} , CPF_{42} , CPF_{43} , and CPF_{44} . The main text on the whiteboard reads: "In Eqn.(2), cpfs are the contract participation factors. In DPM, the number of rows is equal to the number of generating units, i.e. Unit₁ and Unit₂ of G". A presenter is visible in the bottom right corner.

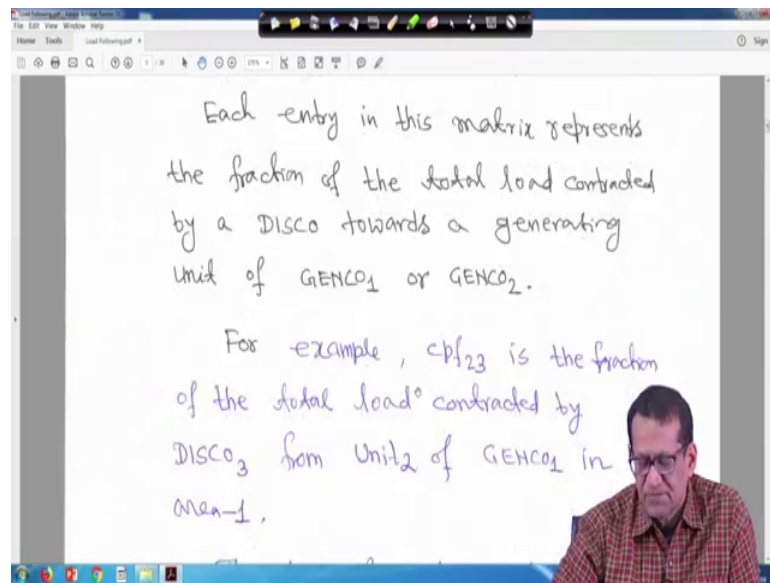
So, meaning is same that actually actual essence remains same right. So, this is equation 1; equation 1 cpfs are the contract participation factor that we know in DPM the number of rows equal to the number of generating units right.

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The screenshot shows a video lecture interface. The text on the whiteboard reads: "Units, i.e. Unit₁ and Unit₂ of GENCO₁ and Unit₃ and Unit₄ of GENCO₂ while the number of columns is equal to the number of DISCOs, i.e., DISCO₁, DISCO₂, DISCO₃ and DISCO₄. Each entry in this matrix represents the fraction of the total load carried by a DISCO towards a generator". A circled number "13" is in the top right corner. A presenter is visible in the bottom right corner.

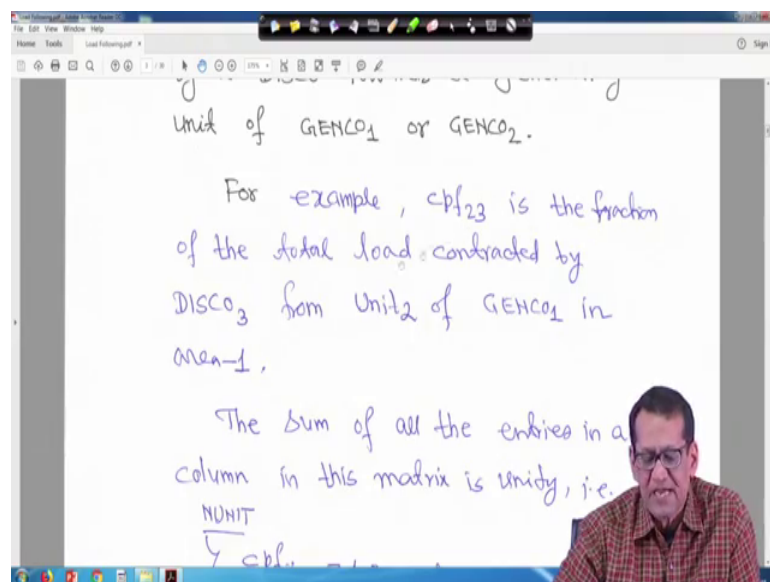
That is unit 1 unit 2 of GENCO 1 and unit 3 unit 4 of GENCO 2 that I told you while the number of column is equal to the number of DISCOs that is DISCO 1, DISCO 2, DISCO 3 and DISCO 4 right.

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So, each entry in this matrix represent the fraction of the total load contracted by a DISCO towards a generating unit of GENCO 1 or GENCO 2; this already we have discussed right

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But still for example, cpf_{23} is the fraction of the total load contracted by DISCO 3 from unit 2 of GENCO 1 in area 1; this is the meaning here right. There it was GENCO 1, GENCO 2, GENCO 3 this is from the unit 2 of GENCO 1 in area 1 that is cpf_{23} right this is the dif[ferent]- just different.

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area-1,
 The sum of all the entries in a column in this matrix is unity, i.e.;

$$\sum_{i=1}^{NUFIT} cpf_{ij} = 1.0 ; j = 1, 2, \dots, NDISCO \quad \text{---(2)}$$

NUFIT = total number of generating units
 NDISCO = total number of distribution companies

So, the sum of all the entries in a column that we have seen that is one because i is equal to 1 to N is equal to unit means the number of your generating units. So, cpf_{ij} is equal to 1.0 and j is equal to 1, 2 number of discos; so, N DISCO right here it is 4 because 4 distribution companies are there together area 1 2; area 2 2 right.

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Therefore, the expression for contracted power of generating units with DISCOs is given as;

$$\Delta P_{gci} = \sum_{j=1}^{NDISCO} cpf_{ij} \Delta P_{tj}, \quad i=1, 2, \dots, NUFIT \quad \text{---(3)}$$

where
 ΔP_{gci} = contracted power of i-th generating unit.

So, ; so therefore, the expression for contracted power of generating units with DISCOs is given as ΔP_{gci} .

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... the expression for contracted power of generating units with DISCOs is given as:

$$\Delta P_i = \Delta P_{gci} = \sum_{j=1}^{N_{DISCO}} c_{pfij} \Delta P_{Lj}, \quad i=1,2,\dots, N_{UNIT} \quad (3)$$

where

ΔP_{gci} = contracted power of i -th generating unit.

ΔP_{Lj} = total demand of DISCO j .

It is same as ΔP_i as before previously we have taken that ΔP_i right it is same as your ΔP_{gci} ; the contracted power. Even j is equal to your N_{DISCO} and it is $c_{pfij} \Delta P_{Lj}$; i is equal to 1 to N_{UNIT} right. There we are writing i is equal to 1 to N_{GENCO} , but here we are writing 1 to N_{UNIT} and total number of unit. So, here it is i is equal to 1 2 3 and 4 right.

So, there were ΔP_{gci} the contracted power of i th generating unit and ΔP_{Lj} total demand of DISCO j .

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ΔP_{gci} = contracted power of i -th generating unit.

ΔP_{Lj} = total demand of DISCO j .

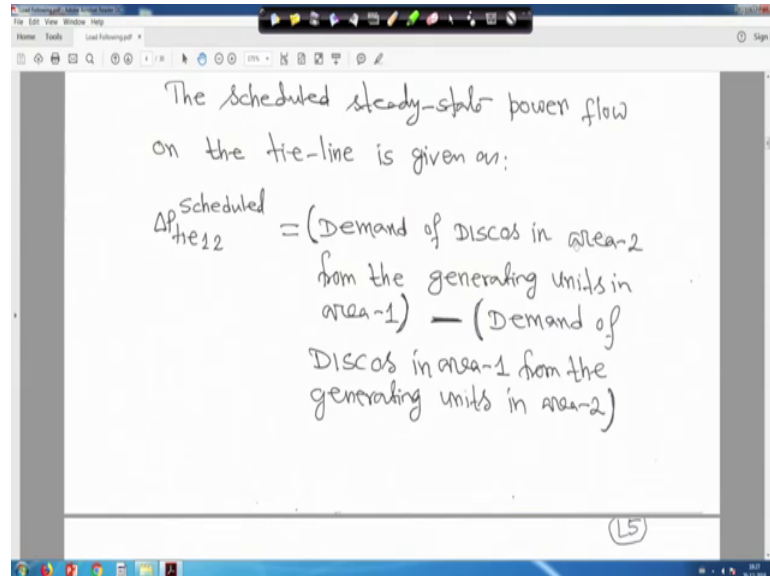
c_{pfij} = contract participation factor.

The scheduled steady-state power flow on the tie-line is given as:

$$\Delta P_{tie12}^{scheduled} = (\text{Demand of DISCOs in area-2 from the generating units})$$

The distribution company j right; cpf_{ij} contract participation factor right; so same as before.

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The scheduled steady-state power flow on the tie-line is given as:

$$\Delta P_{tie12}^{scheduled} = (\text{Demand of DISCOs in area-2 from the generating units in area-1}) - (\text{Demand of DISCOs in area-1 from the generating units in area-2})$$

(15)

The scheduled steady power flow on the tie line is given as it is same as before the demand of DISCOs in area 2 from the generating units in area 1 minus demand of DISCOs in area 1 from the generating units in area 2 and it is 1 2 schedule. By chance whatever data you have taken by chance the ΔP_{tie12} schedule become negative say minus 0.2; that means, basically power is flowing from 2 to 1 right; so, that is the direction- actual direction; so, this is we have also seen.

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$$\Delta P_{tie12}^{scheduled} = \sum_{i=1}^2 \sum_{j=3}^4 c_{pfij} \Delta P_{Lj}$$

$$\rightarrow \sum_{i=3}^4 \sum_{j=1}^2 c_{pfij} \Delta P_{Lj} \quad \text{--- (4)}$$

The tie-line power error is defined as.

$$\Delta P_{tie12}^{error} = \Delta P_{tie12}^{actual} - \Delta P_{tie12}^{scheduled} \quad \text{--- (5)}$$

At the steady-state, the tie-line

Therefore delta P tie 1 2 schedule same as before that sigma i is equal to 1 to 2 if j is equal to 3 to 4; c_{pfij} delta P L j minus sigma I is equal to 3 3 to 4 sigma j is equal to 1 to 2 c_{pfij} delta P L j; this is equation 4. This equation already we have seen for 2 GENCOs 2 DISCOs in each area for 2 area system right; so same equation same equation.

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$$\sum_{i=3}^4 \sum_{j=1}^2 c_{pfij} \Delta P_{Lj} \quad \text{--- (4)}$$

The tie-line power error is defined as.

$$\Delta P_{tie12}^{error} = \Delta P_{tie12}^{actual} - \Delta P_{tie12}^{scheduled} \quad \text{--- (5)}$$

At the steady-state, the tie-line power error, ΔP_{tie12}^{error} , vanishes as the actual tie-line power flow reaches the scheduled power flow.

And the tie line power error also defined as delta P tie 1 2 actual minus delta P tie 1 2 scheduled right.

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power error, ΔP_{tie12}^{error} , vanishes as the actual tie-line power flow reaches the scheduled power flow.

This error signal is used to generate the respective area control error (ACE) signals as in the traditional scenario, i.e.

$$ACE_1 = B_1 \Delta f_1 + \Delta P_{tie12}^{error} \quad (6)$$
$$ACE_2 = B_2 \Delta f_2 + a_{12} \Delta P_{tie12}^{error} \quad (7)$$

So, at the steady state ΔP_{tie12} error will be vanish. So, in that case at steady state ΔP_{tie12} actual is equal to ΔP_{tie12} schedule that also we have seen right.

Now, changes will come. So, this error signal is used to generate the respective area control error ace signal as in the traditional scenarios. That is ACE 1 is equal to your B 1 Δf_1 plus ΔP_{tie12} error and similarly ACE 2 will be B 2 Δf_2 plus a 1 2 ΔP_{tie12} error this is equation 7 right.

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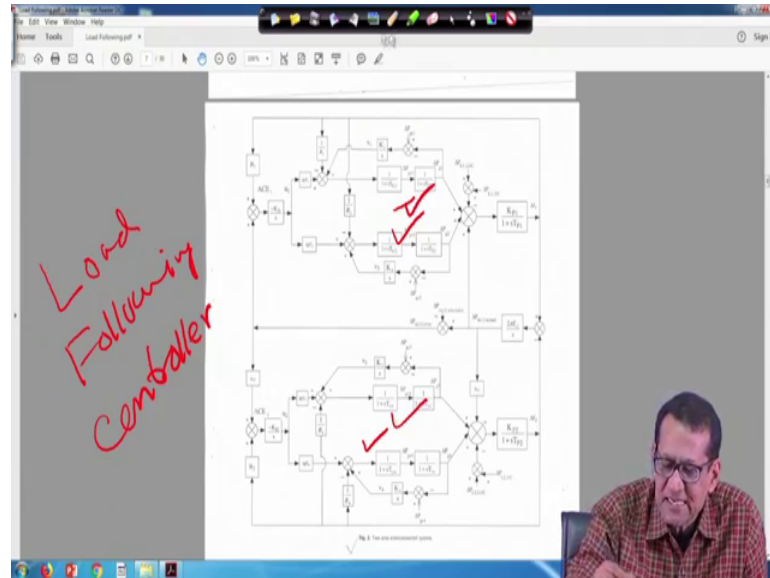
Fig.2 shows the block diagram representation of the two-area system shown in Fig.1.

Each area is equipped with an AGC controller. Each unit of the GENCOs is equipped with a load following controller.

A demand signal ΔP_{gcl} that arrives directly from the load is compared with the power output of Unit 1 (ΔP_{g1})

Now, figure 2 shows block diagram representation first I will come to the block diagram then all this explanation right.

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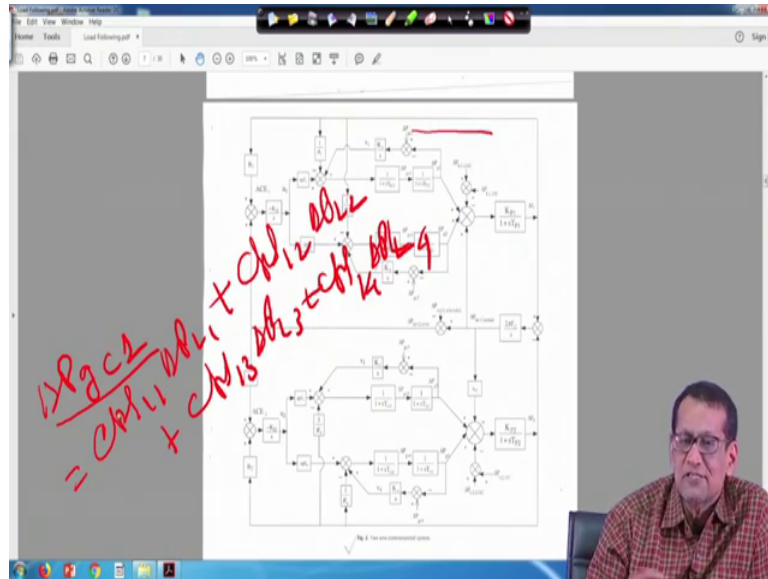
So, let me reduce the volume sorry reduce the size because I have to accommodate all these right.

So, first area 1 and area 2 just hold on it is it is accommodated right ; now in this case what happen actually that your what we have to do is ah; so difference of this one with the previous one I mean I mean lot of difference is there in the block diagram. Now the question is that when you are naming as a load following; that means, for the generator 1; those who will be in the load following they need a load following controller right they need a load following controller.

So, if you look into the diagram; this is actually unit 1 in area 1 this is whole is a area in area 1 that whole is a GENCO 1 right and this is your unit 2 and area 2 this is unit 3 and this is unit 4. And same as the before that that your previous case the total DISCO 1, DISCO 2, DISCO 3, DISCO 4 how was cpf is coming right.

Here that is not shown because that is understandable right, but question is that that thing your in this case what happen suppose first for the sake of understanding that each your what you call that unit must have one load following controller. So, this ΔP_{gc1} is nothing, but the contracted power demand.

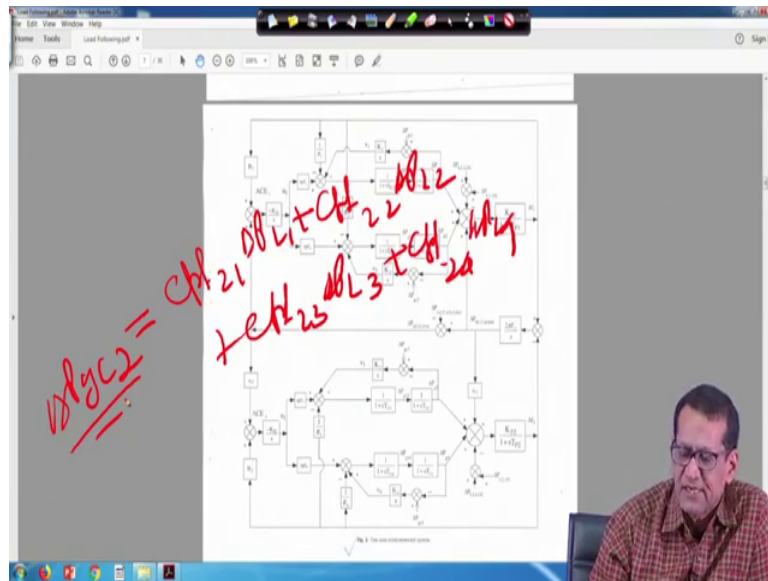
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So, for example, for unit 1 I am writing it is I am making it here ΔP_{gc1} that is with unit 1 the contracted power demand; it is your what you call each distribution companies there are 4 DISCO 1, DISCO 2, DISCO 3, and DISCO 4. So, they demand power say ΔP_{L1} , ΔP_{L2} , ΔP_{L3} and ΔP_{L4} right and your contract participation factor you have.

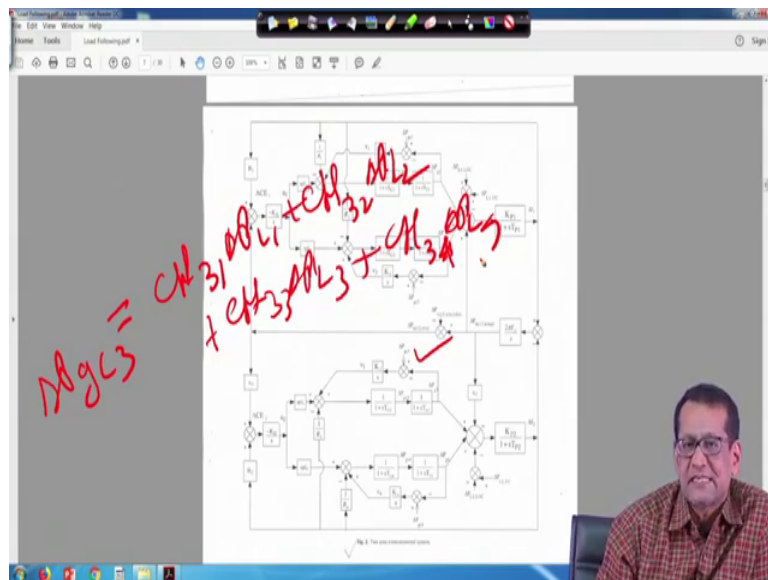
So, therefore, ΔP_{gc1} will be your cpf_{11} same as before ΔP_{L1} ; I am overwriting on it then $\text{cpf}_{12} \Delta P_{L2}$ plus $\text{cpf}_{13} \Delta P_{L3}$ plus $\text{cpf}_{14} \Delta P_{L4}$ right ΔP_{L4} . So, this is actually ΔP_{gc1} same as which before it is nothing, but the ΔP_{L1} or ΔP_{gc1} right. So, here it is making ΔP_{gc1} right. So, this is my ΔP_{gc1} . So, same as before, but control structure here; here we need a load following controller.

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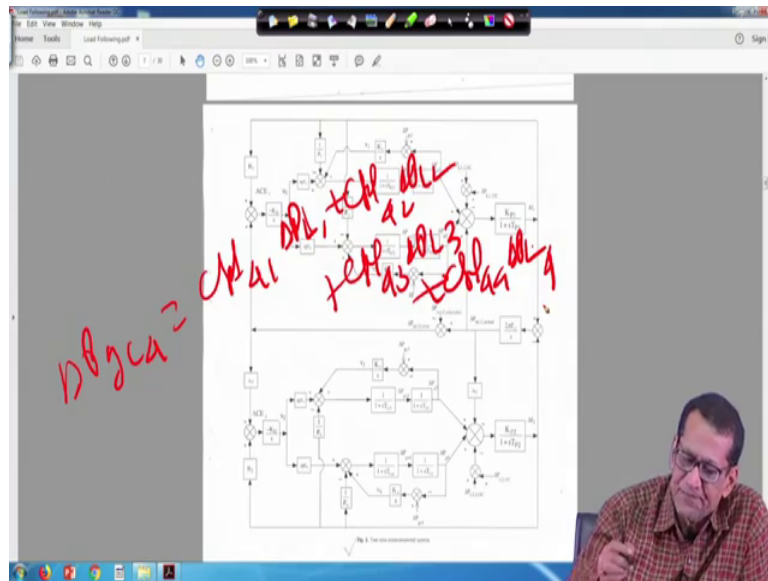
So, similarly for delta P g just for your understanding writing everything delta P g c P g c 2 will be cpf 2 1; I am overwriting on it delta P L 1 plus cpf 2 2 delta P L 2 plus cpf 2 3 delta P L 3 plus cpf 2 4 delta P L 4; that is nothing this is the contract demand by the unit 2 in area 1 right because in area 1 2; one GENCO, but 2 units unit 1 and unit 2 right.

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So, this is for delta P g c 2; similarly for delta P g c 3 in area 2. So, del[ta]- that is the contract demand. So, this one will be cpf 3 1 delta P L 1 plus cpf 3 2 delta P L 2 right plus cpf 3 3 delta P L 3 plus cpf 3 4 ; delta P L 4 this is delta P g c 3.

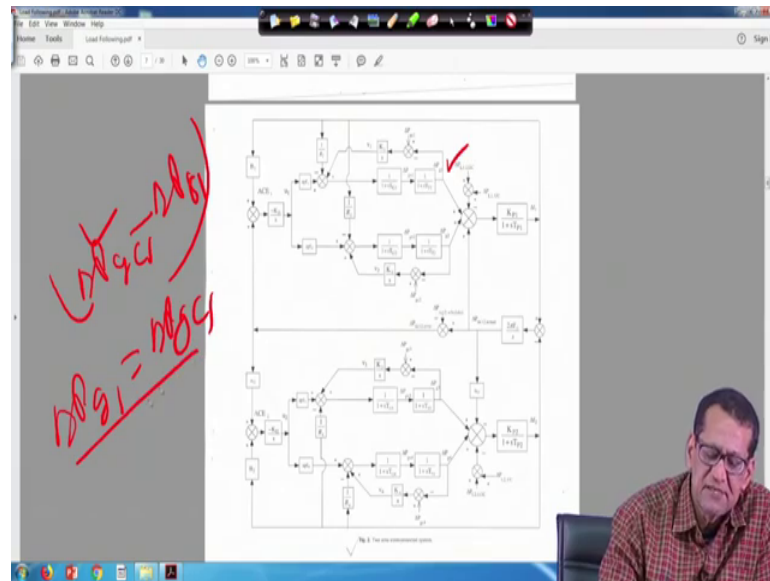
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Similarly, your ΔP_{gc4} right is equal to cpf_{41} , ΔP_{L1} plus cpf_{42} ; ΔP_{L2} plus cpf_{43} ; ΔP_{L3} plus cpf_{44} , ΔP_{L4} right. So, this is the contract this is the power actually whatever contracts the various distribution companies they have the contract; so each generating unit has to generate that much of power ΔP_{gc1} ΔP_{gc2} ΔP_{gc3} and ΔP_{gc4} , for your I mean your what you call by the your units unit 1 unit 2 in area 1 and unit 3 and unit 4 in area 2 respectively right.

. So, that is why this ΔP_{gc1} ; P_{gc1} , this is coming there it the ΔP_1 , ΔP_2 , ΔP_3 and ΔP_4 it was going to the input that is your turbine govern that signal was going that this much power has to be generated. But here what we are doing is input is anywhere nowhere here nowhere here input is nowhere here right nowhere right input is somewhere here we are giving. Now question is that your this is ΔP_{gc1} ; then here the ΔP_{gc1} feedback is here; so these two are compared.

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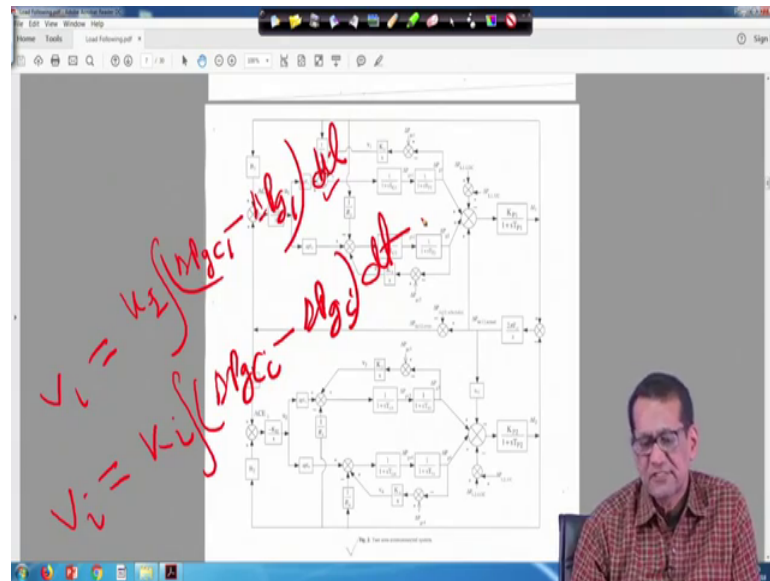
That is your $\Delta P_{g1} - \Delta P_{d1}$; this is the contracted one and this ΔP_{g1} that is generated by your what you call by the generating unit 1 right.

So, at steady state at steady state this ΔP_{g1} it has to be is equal to ΔP_{d1} because this power has to be generated. For that what we are doing is we are putting a load following controller that is $\frac{1}{s}$ upon s is the one integral controller in this case; no P or P_i or $P_i D$ I have used simply I have put a we put a we have put a your what you call put an integral controller right.

So, that is then its gain is k_1 right. Similarly an feedback is coming here it is coming here right; that means, this generation that ΔP_{g2} - as we are taking this ΔP_{d2} and this contractor is power demand this controller is $\frac{1}{s}$; that means, ΔP_{g2} will chase ΔP_{d2} ; that is load following right. So, it will it will I mean steady state ΔP_{g2} will be is equal to ΔP_{d2} right; it will chase that this contracted power demand right.

Similarly, for unit 2 also you have a ΔP_{d2} and this is ΔP_{g2} and this is integral controller your k_2 upon s ; that means, that output that is its output is v_1 ; output is v_1 .

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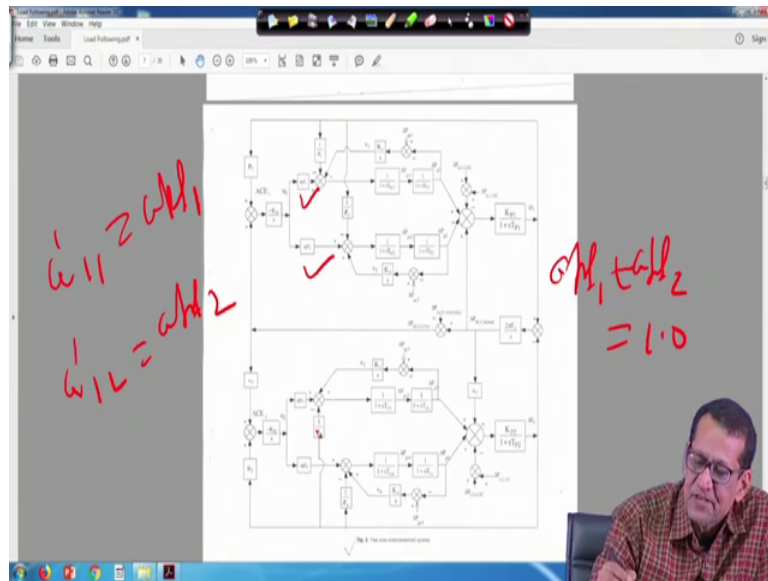


So, B_1 is equal to actually k_1 ; this integral this thing then which is 1 upon s ; so integral controller. So, it is actually $\Delta P_{gci} - \Delta P_{gi}$ actually dt right. So, this is v_1 ; so that then that v_1 is coming here as an input right. Or in general or in general that v_i for i th unit is equal to k_i that gain of i 'th unit integral gain of that i th load following controller rather right; then integral of $\Delta P_{gci} - \Delta P_{gi}$ dt right. So, this actually this load following controller actually will force actually generation to match the contracted power demand at steady state.

So, similarly here also controller is there similarly here also controller is there; similarly here also load following controller is there. But there is no need that all the generating unit will everyone needs that it show you that load following controller, it depends on the system right. Suppose this unit suppose this unit may have a load following controller because; suppose some DISCOs have contract with that and this unit may this unit maybe it has no contract with any DISCOs right.

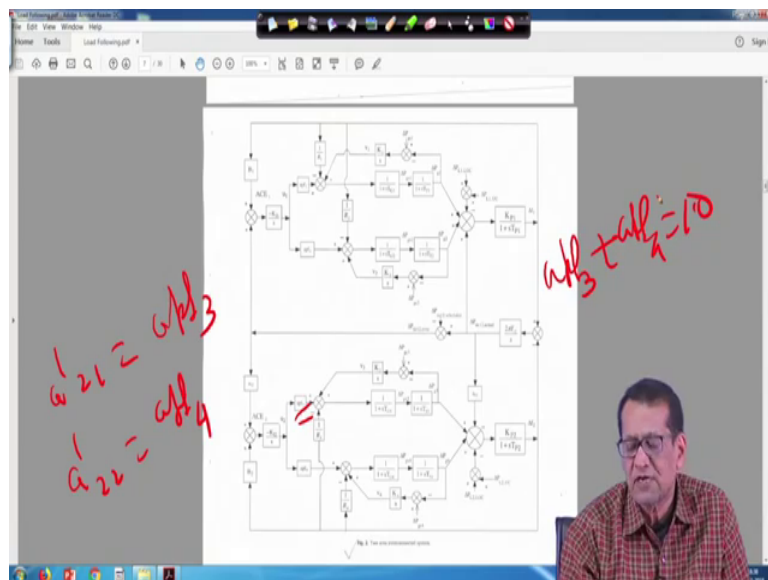
So, in that case this may not be in this thing this will be in AGC; now another thing is that in this case another thing that we have taken a $p_f 1$ and a $p_f 2$ ACE participation factor it is same as before, but as it is a load following. So, I have changed I have just changed this your what you call that terminology- that terminology right.

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It was actually a dash 1 1 in the previous case; it is nothing, but same thing a p f 1, that is ACE participation factor. Similarly previous case a dash 1 2 is equal to a p f actually it is 2 and a p f 1 and same as before a p f 1 plus a p f 2 it is actually 1.0 right.

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Similarly for this case your for this case right; so it is a dash 1 1 a dash 1 2. So, a dash 2 1 is nothing, but your a p f 3 right this is ACE participation factor for unit 3. And similarly for this one a dash 2 2 is a p f that a c s ACE participation factor for unit 4; that means,

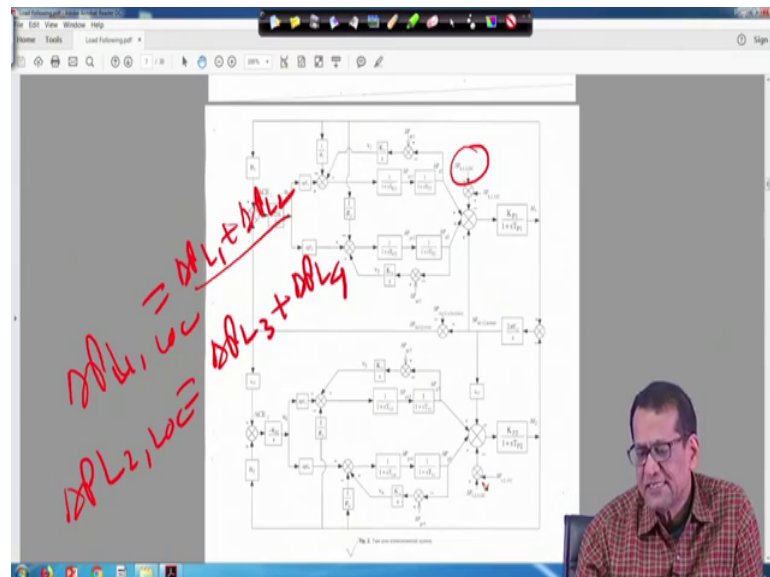
here also same thing a p f 3 plus a p f 4 it has to be is equal to 1.0 right. So, these are your what you call ACE participation factor.

So, basically this a p f this here also a p f 1, a p f 2 and a p f 3, a p f 4. So, basically your they have effect on the transient behaviour of the responses dynamic response the responses, but it has no effect and the steady state as long as uncontracted power demand is not there; if it is there it has effect that we will see. Now next one is same as before this is $\Delta P_{tie 1 2}$ actual and this is $\Delta P_{tie 1 2}$ schedule this feedback is given here we have seen same the same as before.

And this is $\Delta P_{tie 1 2}$ error. So, this way this is $B_1 \Delta f_1$ because this is Δf_1 . So, it is $B_1 \Delta f_1$ this $\Delta P_{tie 1 2}$ error and this is actually your a c 1 right. Similarly here also it is $B_2 \Delta f_2$ plus a 1 2 $\Delta P_{tie 1 2}$ error. So, this is actually your a c 2 and this 2 as integral your what you call input to the integral controller; it is minus k_{i1} upon s this is minus k_{i2} upon s right. So, these two are your integral controller for this AGC right.

Now, and next is next for this block diagram this $\Delta P_{L 1}$ local same as before.

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So, $\Delta P_{L 1}$ local is equal to nothing, but $\Delta P_{L 1}$ plus $\Delta P_{L 2}$ that is your that is in area 1; we have 2 distribution companies that is why their demand is $\Delta P_{L 1}$ and $\Delta P_{L 2}$.

So, ΔP_L local - p_L local will be $\Delta P_L 1$ plus $\Delta P_L 2$. Similarly for $\Delta P_L 2$ local is equal to $\Delta P_L 3$ plus $\Delta P_L 4$ right this is in area 2. And if there is any uncontracted power demand if there is any uncontracted power demand and in that case that it is ΔP_L one you see that is uncontracted power demand in area 1.

If apart from their contracted power demand if any if any if any excess power demand needs by any distribution companies in area 1 that will be reflected in area 1. And it is expected that that you have a that units generating units in area 1 they have to supply this power right according to ACE participation factor.

Similarly, for area 2 also that ΔP_L your what you call that your uncontracted power demand whatever it has it has to be supplied by the same generating unit in area 2 right. So, ; that means, major difference is that this load following controller; so load following controller; so, philosophy actually totally changed right previous one was something and here it is something, but you do not need. So, many load following controller because all the DISCOs may not have contract with generating units in area right. So, this is the your what you call that philosophy.

Now, then ; so now this whatever about the block diagram I explained this is the figure 2 shows the block diagram representation of the 2 area system shown in figure 1 right. Figure 1 has schematic and figure 2 I explain to you now each area is equipped with an AGC controller.

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equipped with a load following controller.

A demand signal ΔP_{Ld} that arrives directly from the load is compared with the power output of Unit i (P_{Gi}) to yield a mismatch and this mismatch is given as an input to a reset controller (load following controller) that will force the mismatch to zero so that the generator follows the load.

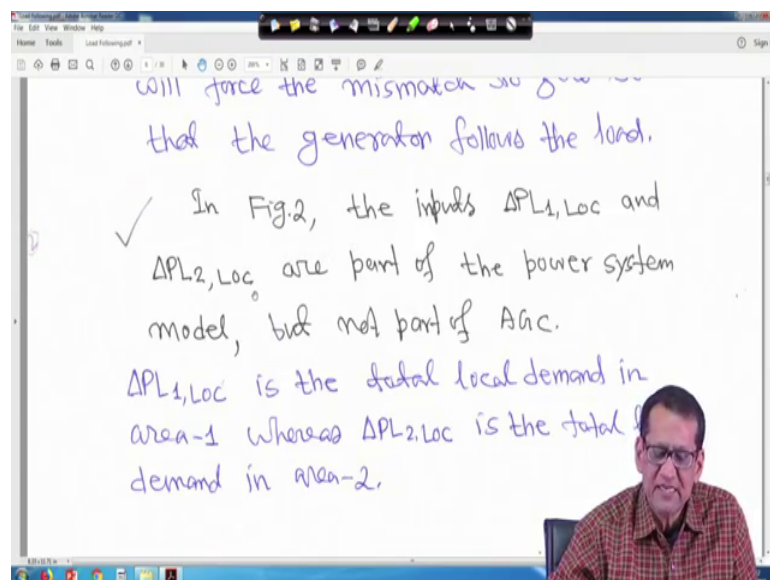
In Fig.2, the inputs ΔP_L , L_{oc}

The image shows a whiteboard with handwritten text in blue ink. The text describes a load following controller that compares a demand signal ΔP_{Ld} with the power output of a generator unit P_{Gi} to create a mismatch. This mismatch is then fed into a reset controller, which forces the mismatch to zero, ensuring the generator follows the load. The text also mentions inputs ΔP_L and L_{oc} in the context of Figure 2. In the bottom right corner, there is a small video inset of a man with glasses and a red checkered shirt, who is the lecturer.

So, each unit of the GENCOs is equipped with a load following controller right. So, a demand signal that is ΔP_{g1} that arrives directly from the load is compared with the power output of unit 1 that is ΔP_{g1} I told you. To yield a mismatch and this mismatch is given as an input to the reset controller that is nothing, but the load following controller right.

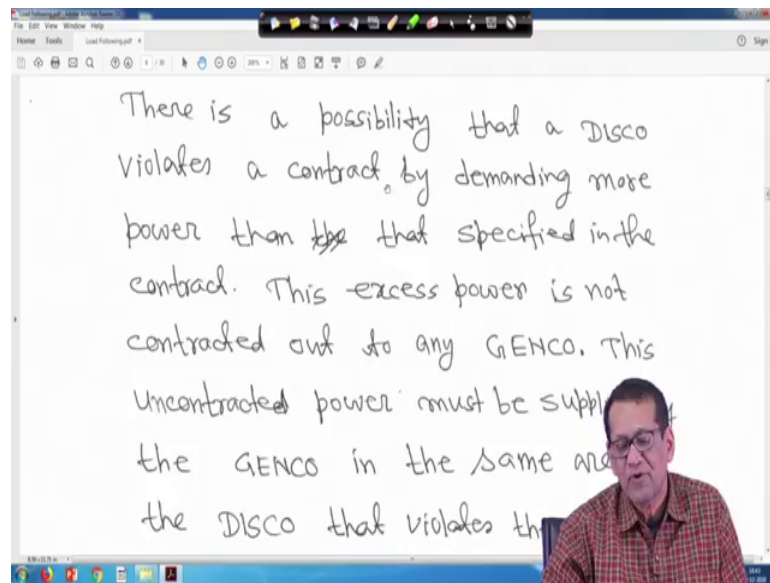
So, that will actually force the mismatch to zero so that the generation follows the load; so that is called as load following. So, in figure 2 that I already explained let me let me just little bit enlarge it.

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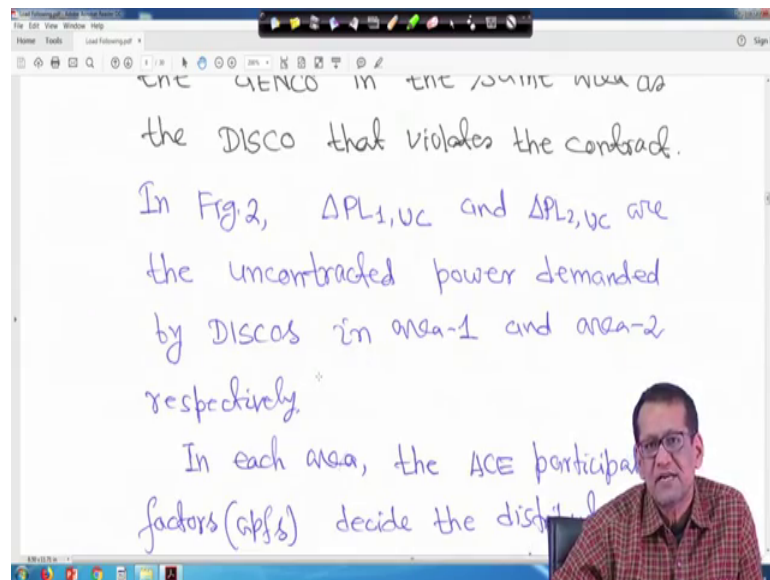
So, in figure 2 the inputs $\Delta P_{L1,Loc}$ and $\Delta P_{L2,Loc}$ are part of the power system model, but not part of AGC that also we have explained before. $\Delta P_{L1,Loc}$ is the total local demand in area 1 whereas, $\Delta P_{L2,Loc}$ is the total local demand in area 2 that also I have explained to you right; diagram also everything I have block diagram I have explained right.

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So, there is a possibility that that uncontracted power demand that a DISCO violates a contract by demanding more power than that specified in the contract right. So, this excess power is not contracted out to any GENCO; this uncontracted power must be supplied by the GENCO in the same area as the DISCO that violates the contract right.

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So, in figure 2 I told you $\Delta PL_{1,UC}$ and $\Delta PL_{2,UC}$ are the uncontracted power demand that is $\Delta PL_{1,UC}$ and $\Delta PL_{2,UC}$ are the uncontracted power demanded by DISCOs in area 1 and area 2 respectively right.

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In each area, the ACE participation factors (apfs) decide the distribution of uncontracted power in the steady state among various generating units.

State Space Representation

The state-space equation for F... can be given as:

$$\dot{X} = AX + BU + B'V + \Gamma P + \Gamma'P' - \dots$$

So, in each area the ACE participation factor also I explained to you right; decide the distribution of uncontracted power in the steady state among various generating units right.

Next is the state space representation. So, the state space equivalent of figure this 2; it can be represent as \dot{X} is equal to AX right plus BU plus B dash V because this B term is coming $B_1 B_2 B_3 B_4$ because of load following controller; B dash and γ capital P and γ dash; P dash; I am made it this is equation 8 right.

So, you have 5 terms on the right hand side $A B B$ dash γ and γ dash and your the your what you call $A A X BU B$ dash $V \gamma$ capital P and γ dash capital P dash right. So, we have 5 terms.

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Where

$$X = \begin{bmatrix} \Delta f_1 & \Delta f_2 & \Delta P_{tie12} & \Delta P_{g1} & \Delta P_{g2} & \Delta P_{g3} & \Delta P_{g4} \\ & & \Delta P_{gV1} & \Delta P_{gV2} & \Delta P_{gV3} & \Delta P_{gV4} \end{bmatrix}^T \dots (9)$$

$$U = \begin{bmatrix} u_1 & u_2 \end{bmatrix}^T \dots (10)$$

So, where X is equal to the state variables; so you have these your 2 generating units are there.

So, 1 2 3 4 this is actual this is a delta P tie 1 2 actual 4 5 6 7 right 8 9 10 11. So, there are 11 state variables are there; so state space matrix will be 11 into 11 right and U there are two input, that two integral controllers are there for 2 areas. So, u 1 and u 2 this transpose this is all transpose it is given right.

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$$V = \begin{bmatrix} v_1 & v_2 & v_3 & v_4 \end{bmatrix}^T \dots (11)$$

$$P = \begin{bmatrix} \Delta PL_1 & \Delta PL_2 & \Delta PL_3 & \Delta PL_4 \end{bmatrix} \dots (12)$$

and

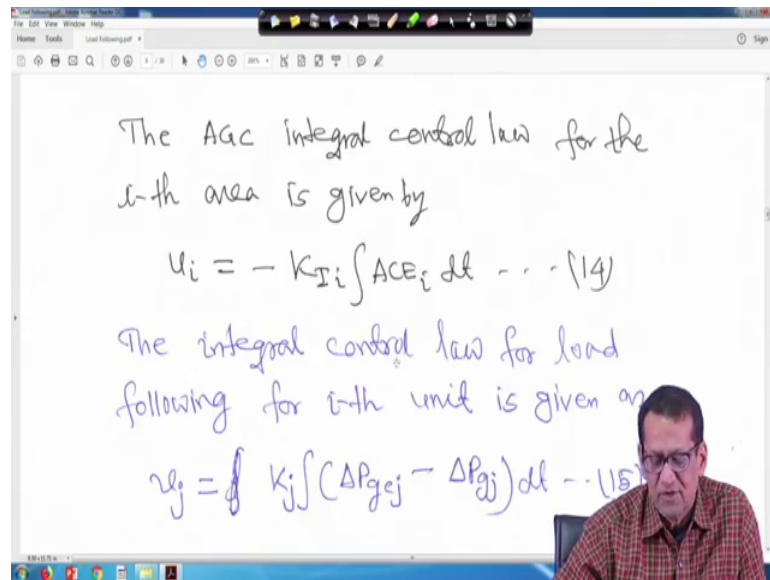
$$P' = \begin{bmatrix} \Delta PL_{2,vc} & \Delta PL_{2,vc} \end{bmatrix}^T \dots (13)$$

The AGC integral control law for the i -th area is given by

$$u_i = -k_i \cdot (\Delta f_i)$$

. So, next is V there are 4 load following controllers in general. So, that is why v 1, v 2, v 3 and v 4 transpose right and P there are 4 distribution companies their power demanded are delta P L 1, delta P L 2, delta P L 3 and delta P L 4 and P dash that is uncontracted power demand delta P L 1 uc and delta P L 2 v c transpose.

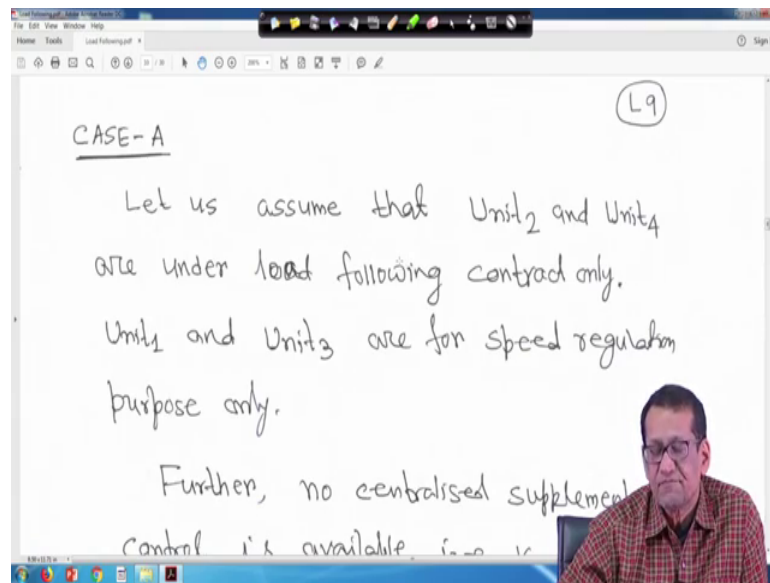
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In the previous case we took small p, but here I have taken P dash right the AGC integral control law for the ith area is given by that is u i that is your AGC controller minus K I i integral of ACE i dt, where K I i is the integral gain of area i and integral ACE i dt is the area control error of area i right.

So, integral control law for the load following for ith unit is given as; so v j it is actually it will be jth unit right it is actually it is not a it is jth unit. Because here it is written j j j and j; so it will be your jth unit right. So, it is actually v j is equal to K j integral of delta P g c j minus delta P g j right. So, this is a load following controller expression.

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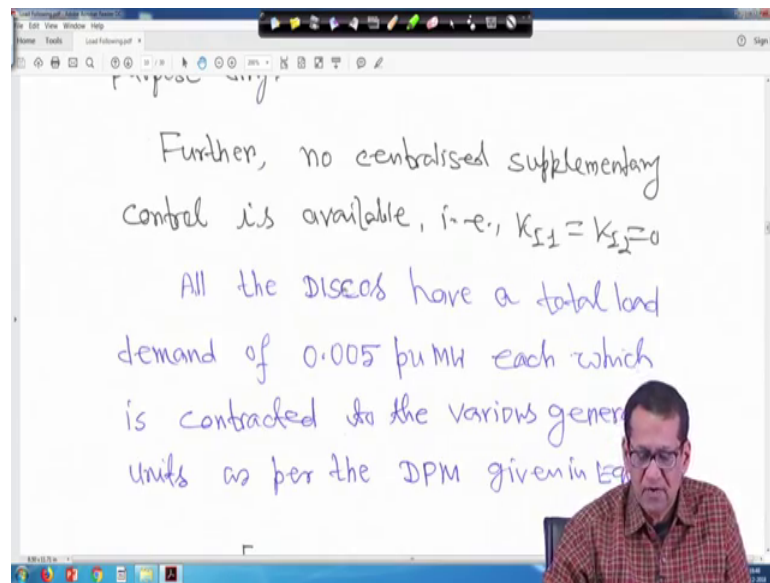


So, now we will make some case studies right. So, let us assume that let us assume that unit 2 and unit 4 are under load following contract only; that means, in area 1 your area 1 that your unit 2 is there and area 2 unit 4 is there. So, these two are load following contract only unit 1 and unit 3 are for speed regulation purpose only right.

So, further no centralised supplementary control is available that is $K I 1$ is equal to $K I 2$ is equal to 0; that means, in this diagram in this diagram that is unit 2 and unit 4 under load following; that means, if I come back to this diagram once again right ah. Let me just make it to half right. So in this diagram that your that unit 2 and unit 4 are load following; that means, this is unit 2 and this is unit 4 these 2 will be load following.

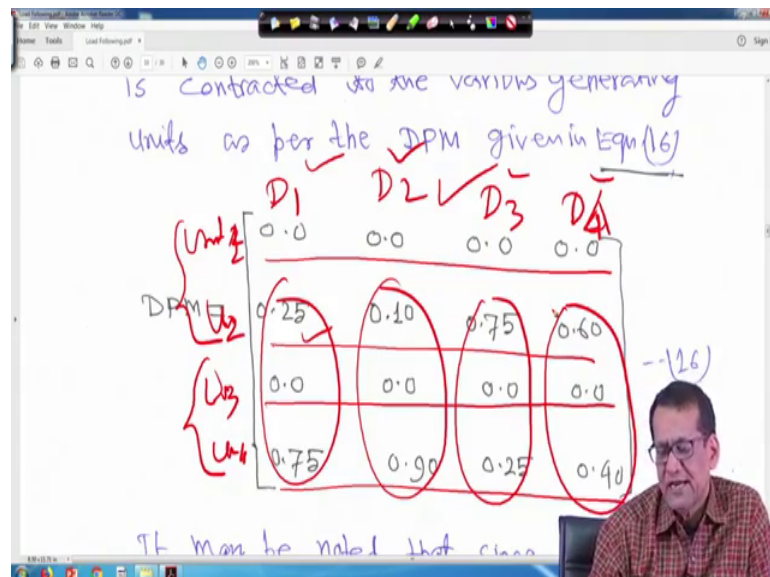
And these two are will be will be just under AGC, but that no supplementary controller; that means, this part will not be there; this part will not be there and we will examine this case because $K I 1$ and $K I 2$ are 0s right. So, let me go back to that further I told you no centralised supplementary controller is available.

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And all the DISCOs have a total load demand of 0.005 per unit megawatt right. Each which is I mean 0.005 per unit megawatt is which is contracted to the various generating units as per the DPM given in equation 16. So, this is actually DISCO participation matrix is taken.

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So, in this case in this case that unit 2 and unit 4; they are actually in the load following. That means, DISCOs have contract they actually this is your distribution company 1; I am putting D 1, D I instead of DISCOs it will I have to take more space, this is D 2, this

is D 3 and this is D 4 right this is D 4 distribution DISCO 1; DISCO 1, DISCO 2, DISCO 3 DISCO 4.

And this is my unit 1 I am making it short unit 1 it is unit 2 it is unit 3 and it is unit 4 right. So, all are unit 3 unit 4 this is unit 1 and this is unit 2 unit 3 and unit 4 right. So, unit 1 and unit 3 are not under any load following that is why they are they have no contract with any DISCOs; that is why cpf is 0, this row is 0.

Similarly for unit 3 this row is zero because it has no contract with any other areas any other your what you call they your this your this DISCOs. So, the DISCO have no contract with them here also nothing, but for a unit 2 and unit 2 in area 1 because this is your area 1 and this is in area 2 because area 1 unit 1 unit 2 area 2 unit 3 and unit 4 right.

And their participation cpf is given like this right and their cpf is given like this, but if you add this it will be 1; 0.75, 0.25; when we add this it will be 1, if you add this it will be 1 and if you add this column wise it will be 1 right. So, this distribution participation matrix is taken right.

So, with this thank you very much, we will be back again in the next lecture.