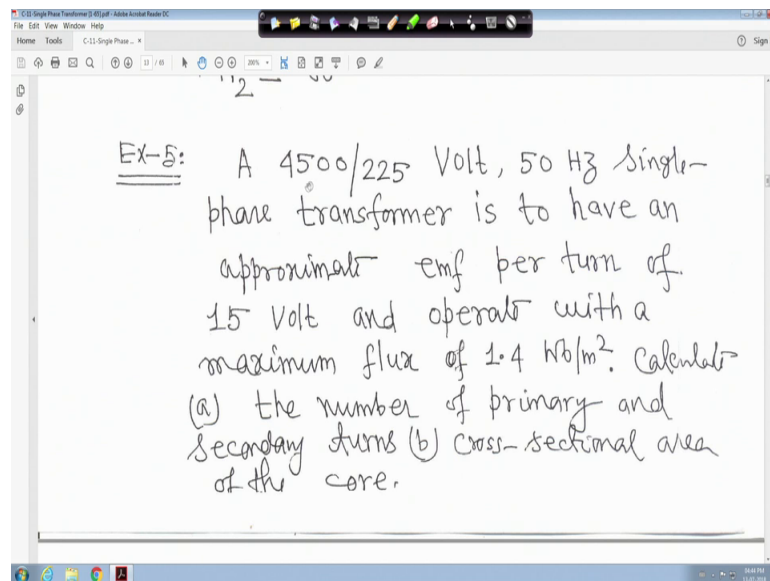


Fundamentals of Electrical Engineering
Prof. Debapriya Das
Department of Electrical Engineering
Indian Institute of Technology, Kharagpur

Lecture - 55
Single Phase Transformer (Contd.)

So, next we are back again, so let us take another example.

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Say 4500 upon 225 voltage in a step down transformer 50 Hertz, 50 Hertz means the frequency, right f is equal to 50 Hertz. Single phase transformer is to have an approximate unit per turn of 15 volt that is given and operate with a maximum flux of 1.4 Weber per meter square. Calculate the number of primary and secondary turns, cross-sectional area of the core right, this two things we have to determine.

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Soln (14)

(a) Emf per turn = $\frac{E_1}{N_1} = \frac{E_2}{N_2} = 15$.

$\therefore N_1 = \frac{E_1}{15} = \frac{4500}{15} = 300$

$N_2 = \frac{E_2}{15} = \frac{225}{15} = 15$

(b) $E_1 = 4.44 \phi_m f N_1$

So, emf per turn is equal to E_1 upon N_1 is equal to E_2 by N_2 is equal to 15, it is given therefore, N_1 is equal to E_1 upon 15 that is also V_1 up on E_1 . So, right is equal to E_2 upon N_2 is equal to 15 that way you can make it. So, it is given 4500 by 15. So, you will get it is 300 because it is primary side where 4500 volt. Similarly secondary side 225 Volt so; N_2 is equal to 225 by 15, so it is 15, right N_2 is 15.

(Refer Slide Time: 01:22)

(b)

$E_1 = 4.44 \phi_m f N_1$

$\therefore \phi_m = \frac{E_1}{4.44 f N_1} = \frac{4500}{4.44 \times 50 \times 300}$

$\therefore \phi_m = 0.0676 \text{ Wb}$

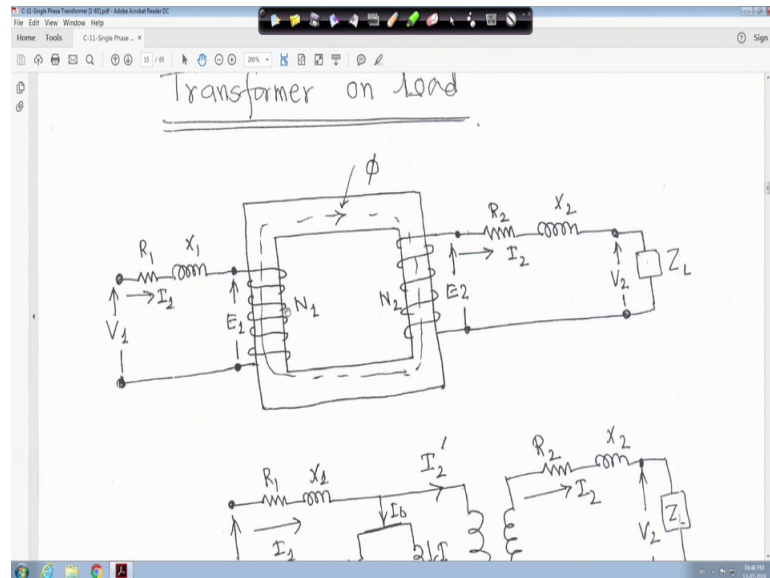
$\therefore A = \frac{\phi_m}{B_{\max}} = \frac{0.0676}{1.4} = 0.0483 \text{ m}^2$

$\therefore A = 483 \text{ cm}^2$

Now, we know E_1 is equal to $4.44 \phi_m f N_1$ therefore, ϕ_m is equal to you just put E_1 value and all these values. So, E_1 is 4500, so we will get 0.0676 Weber.

So, A , we know ϕ_m is equal to A into flux density, right. So, A is equal to ϕ_m by B_{max} . So, ϕ_m is given maximum flux density 1.4 Weber per meter square is given. So, it is basically 0.0483 meter square therefore, 483 centimeter square, right.

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So, now next is a transformer on no load, right when transformer sorry transformer on load when transformer is on load, so first this transformer on load. So, first when you will go through this first to draw this circuit, right then will see. So, we if you draw this your what you call the circuit. So, this is your this is your primary side and this is your secondary side, a the load is connected, a load is connected.

Now, from our magnetic circuit loop this R_1 and X_1 these are the two your therefore, a resistance and reactance of the winding. These two resistance we put it here, right as we nothing is here. So, this is your what you call E_1 , E_2 neglect all this E_2 neglect all this when E_1 is equal to it is the magnitude wise V_1 is equal to E_1 . But when it is loaded at that time this is $R_1 X_1$. So, this is Volt as if it is a ideal transformer $R_1 X_1$ is here so this is V_1 , is the this is E_1 and this is V_1 and arrow tips means its shows positive, right. And similarly here a load is there Z_L is the load, right and this is also bullet voltage across the load is V_2 and this R_2 and X_2 it was secondary side that resistance and reactance.

So, in that case so earlier in for no load cases we have seen that you are what you call there was no current flowing in the secondary, right. And only prime only you are what

you call that only primary side and alternating voltage are applied and this no load current yeah that is your what you call the current I_0 is very small that is called your exciting current it has two component, one is responsible for that your core losses another is for magnetizing component that is responsible for producing powers.

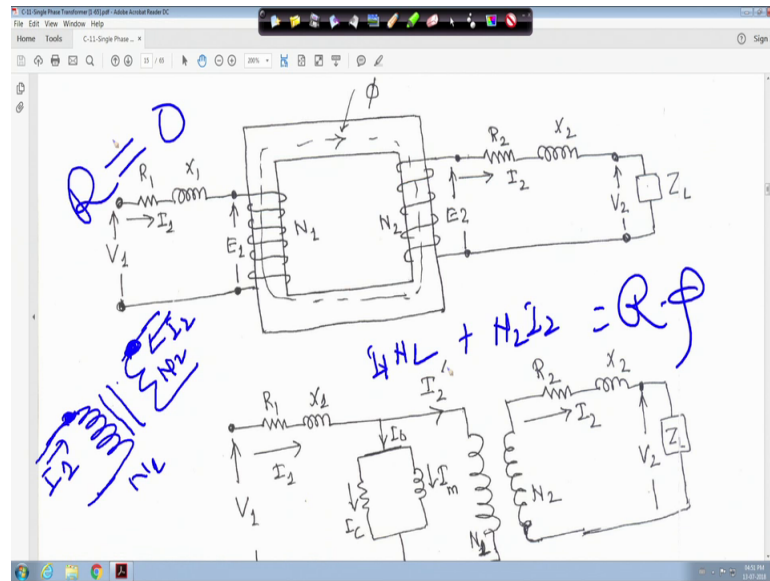
Now, in this case it is connected to the load. Now, before going to anything, so this is my N_1 turn and this is N_2 turn primary and secondary windings and this voltage is E_1 and this voltage is E_2 , right. What you call E_1 and E_2 voltage basically you can say this is the ideal transformer in this voltage.

So, now if you apply your that you are what you call that your magnetic circuit you have started the, right hand rule suppose this is the direction of the current is taken. Let me clear it. So, this is the direction of the current is taken, right. So, if you grasp a conductor in the direction of the flow of the current you will see term is up. So, flux direction from this side will be ϕ , right.

So, as load is connected load is connected therefore, the current will be flowing like this. So, again if you wrap the you what you call conductor in the direction of the current you will find this one also will be this way. That means, effective flux will be getting reduced. So, in that case what is actually what is happening that emf produce by this one say by this one it is it is sorry not emf, mmf; mmf produced by this one will be $N_1 I_1$ and, right and this one will be $N_2 I_2$ actually it will be $N_1 I_1$ is equal to minus of $N_2 I_2$ it is something like this it is something like this. Suppose, let me clear it.

Suppose I have this transformer, I have that this is a transformer symbol I have the transformer say this is my current I_1 , right. Let me clear it. Let me clear it let me make it a little better way just hold on, right just hold on.

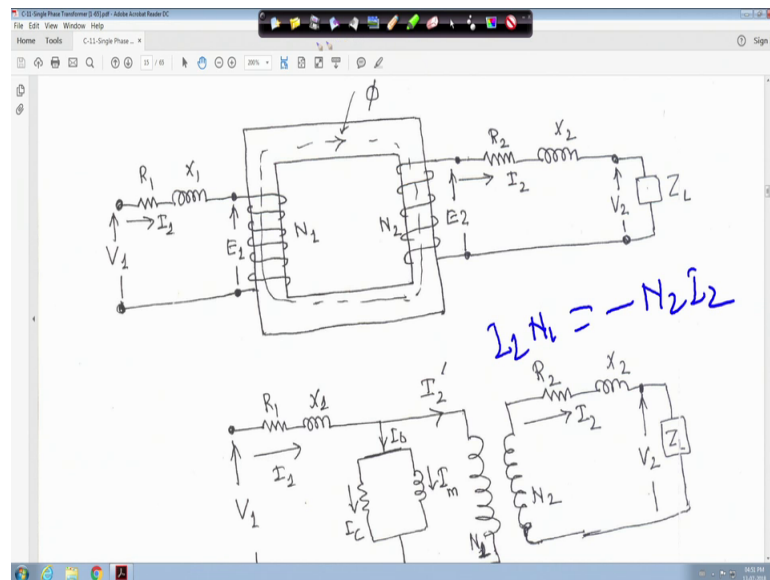
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Suppose this is my, this is my transformer, right and current actually flowing here is say I_1 for example. And trans here it is N_1 , and this is my secondary side, right primary secondary side and here also say current say this is I_1 turn this turn this is the N_2 and say current is here it is I_2 . So, I am taking just entering. Put a dot here, put a dot here for an ideal transformer, so you will see mmf on this side your $I_1 N_1$ and this side plus $N_2 I_2$ is equal to the reactance into ϕ , right. The way we have done it that you are what you call both current are entering into that dot the magnetic circuit whatever you have studied, right. In other if you do so you will find this two are additive because you apply the your what you call, right hand rule according to this.

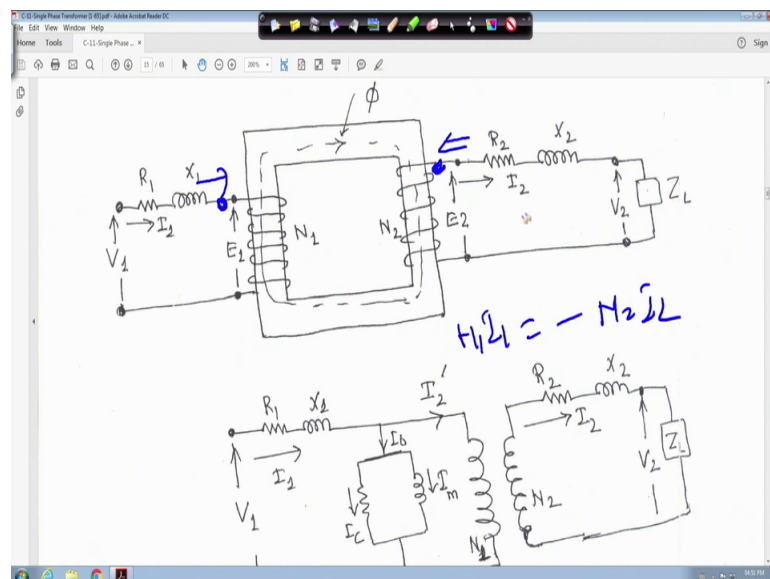
If you do so, but for an ideal transformer the reactance is look at the assumptions whatever made in force the reactance R is equal to your 0, right. If it is so that means, my N_1 your what you call $I_1 N_1$ plus $I_2 N_2$ is equal to 0, that means. Let me clear it.

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That means, my $I_1 N_1$ is equal to minus your $N_2 I_2$ that means, I_1 and I_2 there will be anti phase. $N_1 N_2$ the constant with it turns, right and I_1 and I_2 will be an anti phase. So, this is one way. Another, this is and another this one that is why that is why as it is minus.

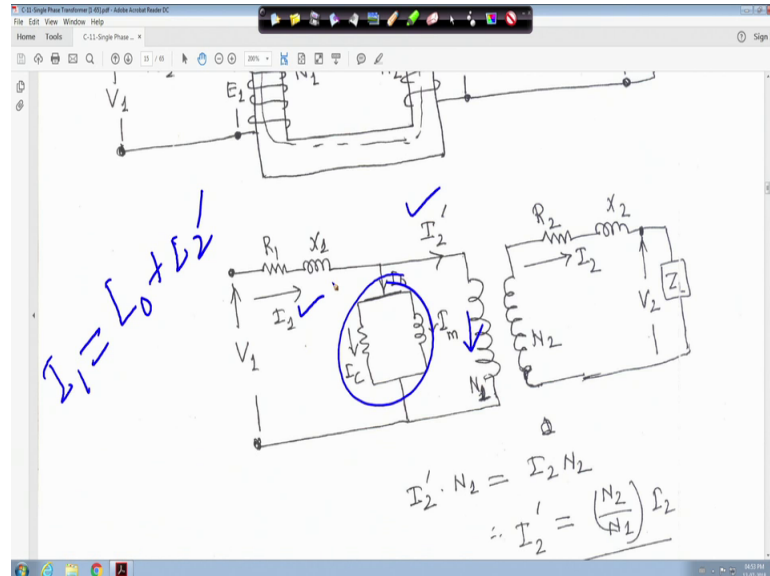
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So, we have the, if you put a dot here, if you put a dot here, and if you put a dot here, right if you take the direction of the current like this and these. So, $N_1 I_1$, your is equal to your minus $N_2 I_2$ that means, there in anti phase, right that means, that is why the

direction of the current is this way that is this going to the load. So, let me clear it, right. So, this is your what you call that why transformer is on load.

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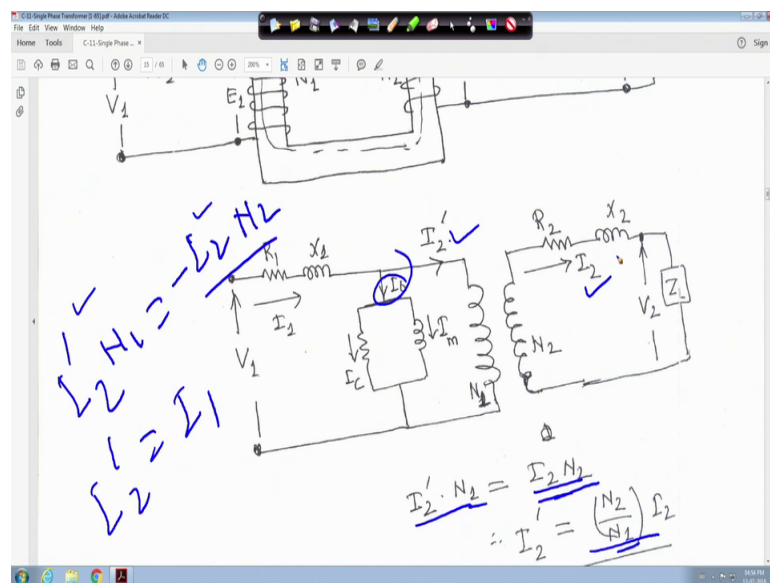
Therefore now this equivalent circuit actually we have seen that, right up is there later you can go through it, but whatever why told from my mouth just listen write up is there about this. So, the R_1 and X_1 is the primary side resistance and reactance and this is actually we are meant to this is your what you call that I_c and I_m that is your primary side we are giving the alternating supply.

So, this I_c current you are what you call a core loss component is there so, it can be represented by an equivalent resistance, right. Similarly magnetize in current I_m responsible for producing no load flux, right. So, it can be represented by your what you call; by an your what you call and in your in inductance. So, and this is the current I_0 . So, this means these two in for these to a parallel circuits. So, it give you that I_0 is equal to I_c minus $j I_m$.

And this is the secondary side that R_2 and X_2 and this is the current flowing through the load this is that your that ferromagnetic material primary ending secondary so on and this is the load. And this is the voltage that was the load is V_2 . Anybody aero it means instantaneous polarity plus and this is minus and this turn this is N_1 turn is an N_2 turns.

Now, I am clearing it now current from here from the source from the supply it is I_1 , but part of the current that I_0 is going here I_0 is equal to your I_c minus $j I_m$. But yes the current is I_2 dash that means, I been figure some that I_1 is equal to your I_0 plus I_2 dash, right. So, in this case what will happen this is the current going through the primary winding. Earlier I saw I_1 I_1 because for ideal transfer all these things are neglected. Now, this current I_2 dash N_1 as per our this thing this is I_2 dash N_1 mmf this thing is equal to $I_2 N_2$. So, I_2 dash when you solve the numerical it will be N_2 upon $N_1 I_2$ this we will do.

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But in that our explanation whatever was there that is actually should have come $I_2 N_1$ is equal to minus $I_2 N_2$, right. So, just in anti phase that means, I_2 dash and I_2 actually in anti phase is this I_0 is neglected then I_2 dash is equal to your I_1 that is why I wrote $N_1 I_1$ is equal to and from an ideal transformer, right. So, that means, mmf this side primary side must be equal to mmf of the secondary side as the magnitude on this sign come, right and this sign also I also I told you. So that means, I when you will draw the phasor diagram then this I_2 dash and this I_2 will be in anti phase that is 180 degree difference of phase shift.

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$$E_1 = -N_1 \frac{d\phi}{dt} = -N_1 \frac{d(\phi_{\max} \sin(\omega t))}{dt}$$

$$\therefore E_2 = -N_2 \phi_{\max} \omega \cos(\omega t)$$

$$\therefore E_2 = -2\pi f \phi_{\max} N_2 \cos(\omega t)$$

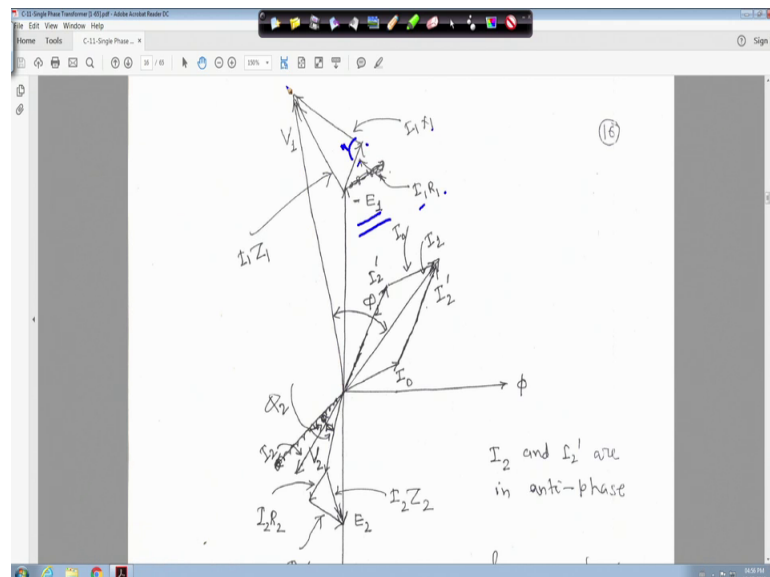
$$\therefore E_{2,rms} = \frac{-2\pi f \phi_{\max} N_2}{\sqrt{2}} = -4.44 \phi_{\max} f N_2$$

$$E_1 = 4.44 \phi_{\max} f N_1$$

$$E_2 = 4.44 \phi_{\max} f N_2$$

So, in this case we know that E 1 is equal to minus N 1 d phi by dt. So, you know E 1 is equal to this much, right this one already we have seen, already we have seen in magnetic circuit also we have solve one or two numerical. So, this is my E 1, in this is my E 2, earlier is this thing is given.

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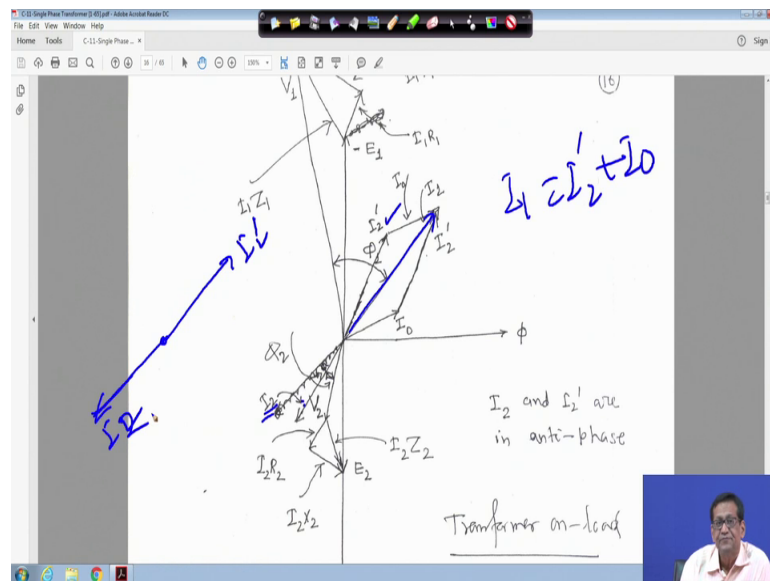


Now, now if you look at the phasor diagram let me let me reduce the zoom, right. So, if you see the phasor diagram first one or two things let me tell you, this is nothing. The way it was there I made it this will also nothing this will also nothing, right if it is cut.

So, in this case let me clear it in this case that V_1 and E_1 balance is lost because it is on it is on your what you call, it is on loaded, secondary side is loaded the and V_1 if you look into the circuit just first let me explain here. So, V_1 is equal to that is your minus E_1 then this one is $I_1 R_1$ and this one 90 degree with that this is 90 degree because it is reactance, so $I_1 X_1$, so this is my V_1 , right. So, let me clear it. So, if you just hold on. So, if you look into the circuit, if you look into this circuit, right if you look into this circuit so yeah if we when you draw this your phasor diagram. So, V_1 will be when you are taking that V_1 earlier for ideal transformer V_1 is equal to minus E_1 but now this R_1 are the loaded because of the transformer is loaded, secondary side is loaded. So, $R_1 I_1$, $R_1 I_1$ plus $j I_1 X_1$ turn (Refer Time: 12:18).

So, that is why V_1 is equal to minus E_1 plus your $I_1 R_1$ plus j your $I_1 X_1$, that is why this phasor diagram your what you call this phasor diagram is V_1 is equal to your minus E_1 plus $I_1 R_1$ plus your $j I_1 X_1$ this is the this one.

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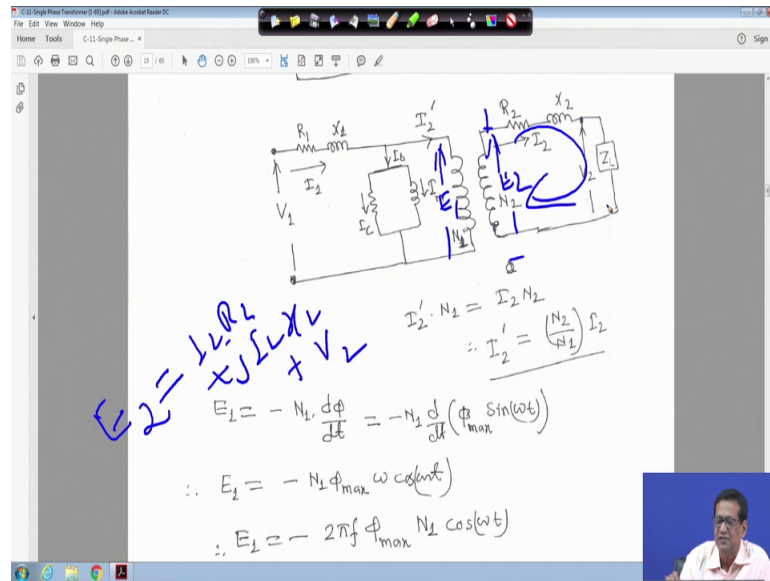


And second thing is that if you look into this if you look into this that your I_1 is equal to I_2 dash plus I_0 when you will make it you see the circuit diagram. Now, this is my I_0 that your no load current and this is my I_2 dash and this is your I_1 , right. But I_2 dash and I_2 the secondary current must be anti phase. So, that is why this one is I_2 that is written here this is I_2 actually the slightly it is if this thing. Suppose if it is there if

this is my if this is my I_2 dash then your what you call then this one this one will be my I_2 they will be in anti phase, right because of that convention.

So, that is why this is my I_2 dash and this is I_2 , I_2 is drawn here this phasor is I_2 , this phasor is I_2 . So, let me clear it. Therefore, in the secondary side so E_2 will be equal to if you look, E_2 will be equal to V_2 plus $I_2 R_2$ plus $j I_2 X_2$. If you apply we just let me clear it if you apply K v l in the circuit if you apply K v l in this circuit, right.

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So, this is your E_2 this is your E_2 , right in this circuit also this is my E_1 this is your E_2 and this is plus minus, right. So, if you your what you call if you apply K v l then you are E_2 will be is equal to, right this is your $I_2 R_2$ plus $j I_2 X_2$ and plus your V_2 , right. So, that is your, E_2 is equal to V_2 plus $I_2 R_2$ plus $j I_2 X_2$. So, you just apply K v l, just apply K v l here, right.

So, that means, this one that is E_2 is equal to V_2 plus $I_2 R_2$ and this $I_2 X_2$ these angle this angle will be 90 degree, right this angle will be 90 degree. And resultant will be this voltage drop will be I_2 into Z_2 similarly here also this part will be $I_2 I_1$ into Z_1 . And this current I_1 current I told you it will be I_0 phasor sum plus I_2 dash, right and angle between V_1 and I_1 will be say this angle is ϕ_1 , right. And similarly angle between I_2 and V_2 this angle is equal to ϕ_2 it is shown here it is ϕ_2 , right only thing is that this portion is nothing this portion is nothing but, similarly this portion is nothing, right.

So, I hope you are I_2 and I_2 dash are in anti phase. So, I hope that and this is the same as before the flux ϕ is your reference phasor, right. So, this is this phasor diagram the transfer on no load. I hope you have understood this say your what you call this just hold on this phasor diagram. So, there is that should not be any confusion any confusion, right.

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When the transformer is loaded, a current I_2 will flow in the secondary winding. The secondary mmf $I_2 N_2$ sets up a secondary flux that tends to reduce the flux produced by the primary mmf. As a result E_1 reduces, and the balance between V_1 and E_1 would no longer exist. Hence on load, the presence of secondary mmf necessitates the production of primary mmf equal in magnitude but opposite in direction.

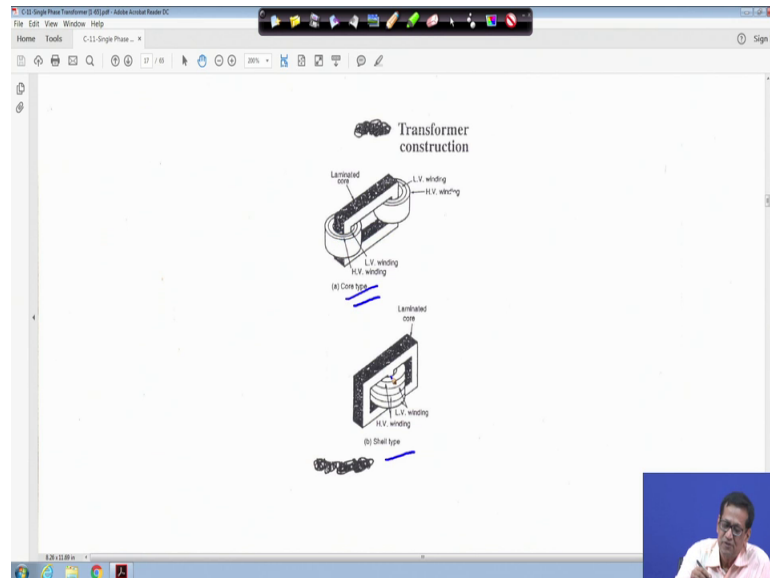
When that now there write up is there is just when the whatever I said when the transformer is loaded a current I_2 will flow in the secondary winding. The secondary mmf $I_2 N_2$ sets of a secondary flux that tends to reduce the flux produce by the primary mmf. That means, this is actually primary mmf whatever it was I_2 dash into N_1 and this is secondary mmf I_2 into N_2 .

And you use that what you call use that, right hand rule and then you will see the direction of the flux and then you will see so it will try to reduce that effective flux, right. That is what has been written here you apply the, right hand rule from a magnetic circuit, you grab the conductor in the direction of the flow of the current and your term will be the direction of the flux, right.

So, your $I_2 N_2$ sets of a secondary flux that tends to reduce the flux produced by the primary mmf. As a result E_1 reduces and the balance between V_1 and E_1 would not would no longer exist, right. Hence on load the presence of secondary mmf actually a necessitates the production of primary mmf equal in magnitude, but opposite in direction

that is your $N_1 I_2$ that is equal to minus your what you call $N_2 I_1$, if your I_0 is neglected then I_2 dash is equal to I_1 .

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Next is the little bit of construction of the transformer. So, this is I have taken from a book, right. So, generally that whatever we solved the numericals and other thing that is but very equivalent circuit. But if you look into that that lower that is this is core this is core type transformer that low voltage winding an above that your high voltage winding how they are there and this is laminated core. That is your real that is your practical transformer.

And if the shell type transformer is there if you look into that you will find low voltage winding and high voltage winding, then low voltage winding and high voltage winding, right. So, these are the two type different two different type of construction. Only one thing one thing I will tell you that you read any book and see the differences between the core type and your shell type what is the main different, right. This you should go out appear on here, I am skipping it that thing, right.

(Refer Slide Time: 18:18)

1.) Two types of single-phase transformers,
(a) core type (b) shell type.
The low and high voltage windings
are wound as shown to reduce
leakage flux.

2.) For power transformers, rated possibly
at several MVA and operating at a
frequency 50 Hz or 60 Hz (USA or Japan),
The core material used is usually

The screenshot shows a digital whiteboard interface with a toolbar at the top and a small video inset of a man in the bottom right corner. The text is handwritten in black ink on a white background.

So, in this case this kind of construction is made because it is core type and shell type the low and high voltage windings are wound as shown in reduce the leakage flux, right.

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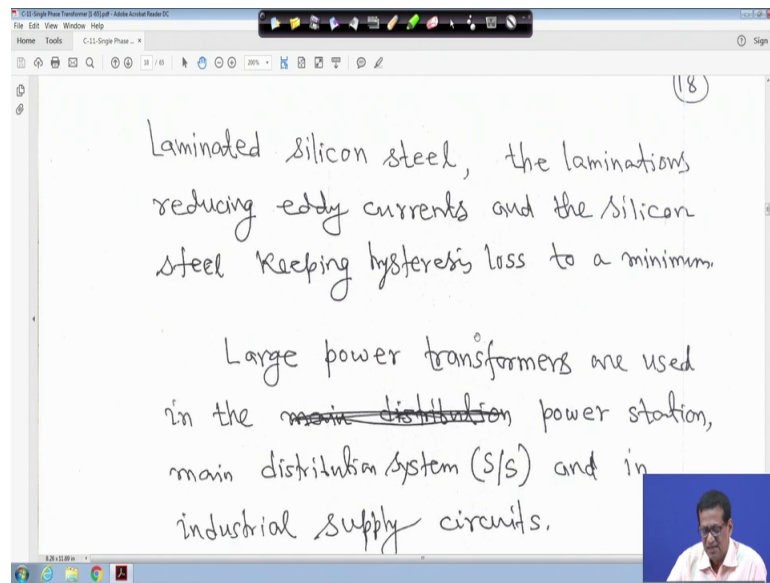
are wound as shown to reduce
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And similarly for power transformer rated possibly at several MVA and operating at a frequency 50 Hertz or 60 Hertz that is USA actually it is 60 Hertz and 50 Hertz or 60 Hertz both are there in Japan, right.

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(18)

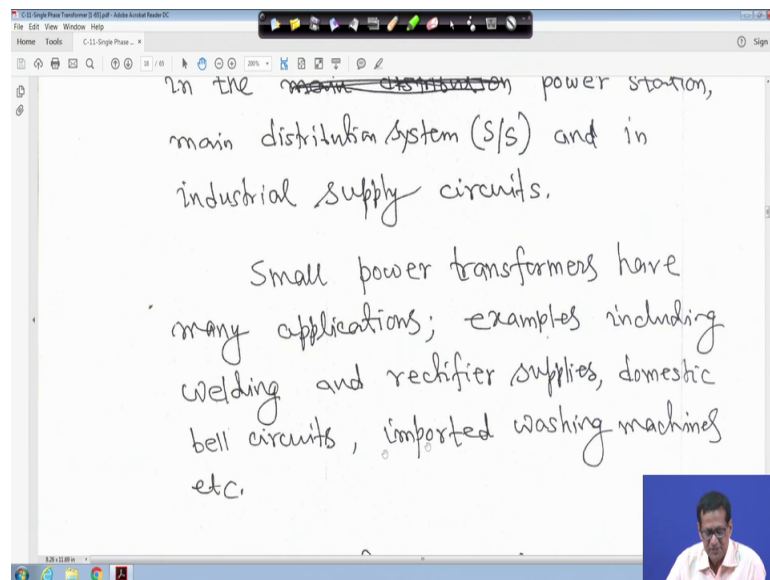
Laminated silicon steel, the laminations reducing eddy currents and the silicon steel keeping hysteresis loss to a minimum.

Large power transformers are used in the ~~main distribution~~ power station, main distribution system (S/S) and in industrial supply circuits.

The screenshot shows a digital whiteboard interface with a toolbar at the top and a small video inset of a man in the bottom right corner. The text is handwritten in black ink on a white background.

The core material used is usually your laminated silicon steel. The laminations reducing actually eddy current that is why laminated and the silicon steel keeping hysteresis loss to a minimum, right.

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In the ~~main distribution~~ power station, main distribution system (S/S) and in industrial supply circuits.

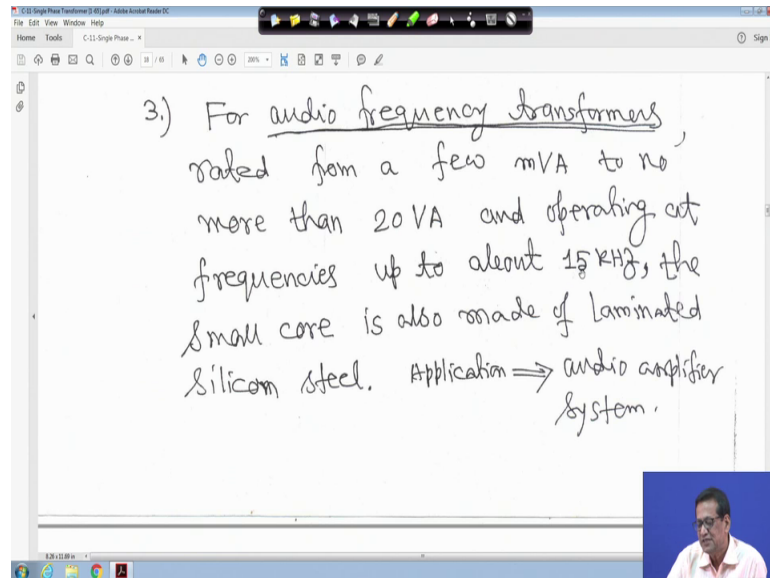
Small power transformers have many applications; examples including welding and rectifier supplies, domestic bell circuits, imported washing machines etc.

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And large power transformers are used in the power station main distribution system and in industrial supply circuit, right.

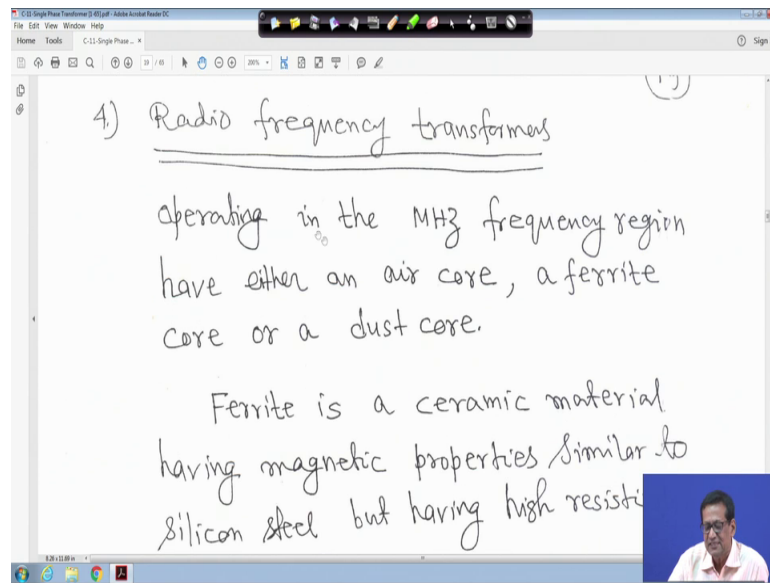
So, small power transformer have many applications. Example, including welding and rectifier supplies then domestic bell circuit imported washing machine it is I mean so many things are there for small power transformer.

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Now, then another thing this will not cover just for general knowledge. For audio frequency transformers rated from a few milli Volt ampere to not more than your 20 Volt ampere, and operating at frequencies up to your about 15 kiloHertz the small core is also made of laminated silicon steel application audio amplifier system. This is just for purpose of general knowledge will not study that.

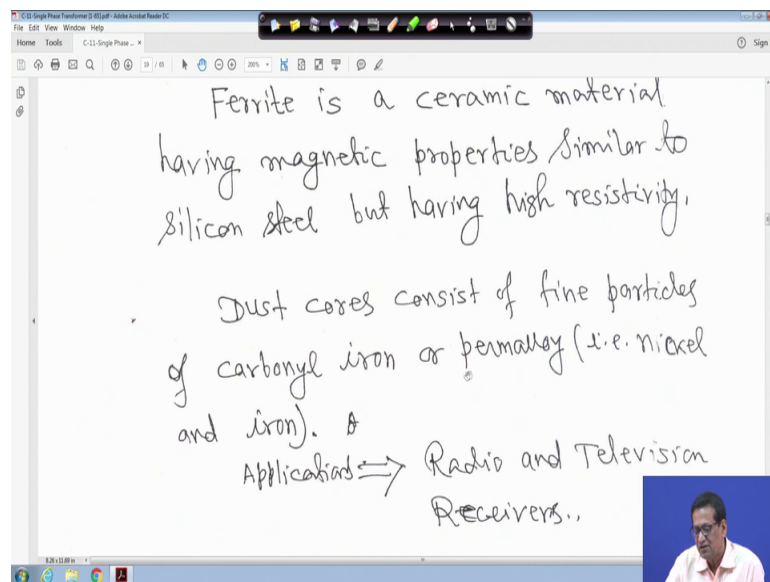
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1) Radio frequency transformers
operating in the MHz frequency region
have either an air core, a ferrite
core or a dust core.
Ferrite is a ceramic material
having magnetic properties similar to
silicon steel but having high resistivity.

Radio frequency transformer it is operating in the megaHertz frequency region, have either and air core a ferrite core or a dust core.

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Ferrite is a ceramic material
having magnetic properties similar to
silicon steel but having high resistivity.
Dust cores consist of fine particles
of carbonyl iron or permalloy (i.e. nickel
and iron).
Applications \Rightarrow Radio and Television
Receivers.

So, ferrite is a ceramic material having magnetic properties similar to silicon steel, but having high resistivity. Dust core consists of fine particles of carbonyl iron or your call permalloy that is your nickel and iron application radio and television receivers, right.

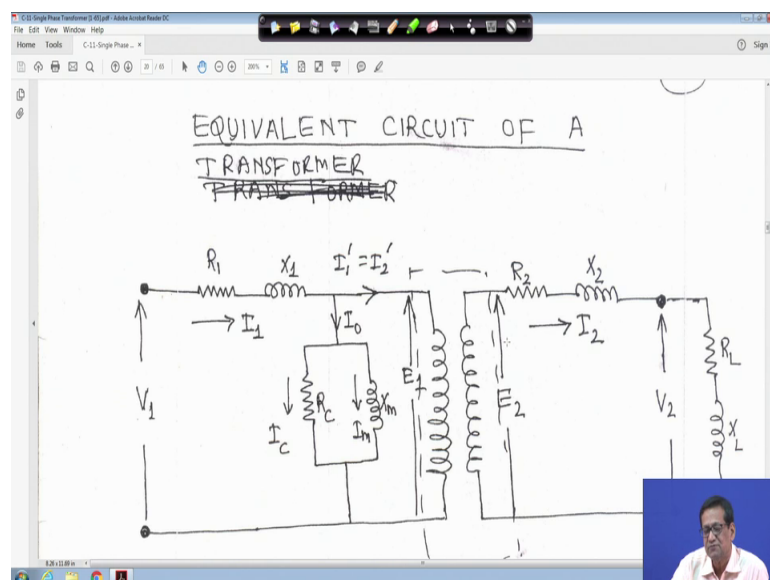
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5) Transformer windings.
Usually of enamel-insulated copper or aluminium.

6) cooling
Air in small transformers,
oil in large transformers

Now, next this transformer winding usually of enamel insulated copper or aluminium. If you; when you go through this in your college first year lab you can see that your windings of the transformer you open transformer, right. And cooling in brief air in small transformers and oil in large transformers, right cooling is a huge chapter, right in a electrical engineering for transformers so just to give you some general ideas.

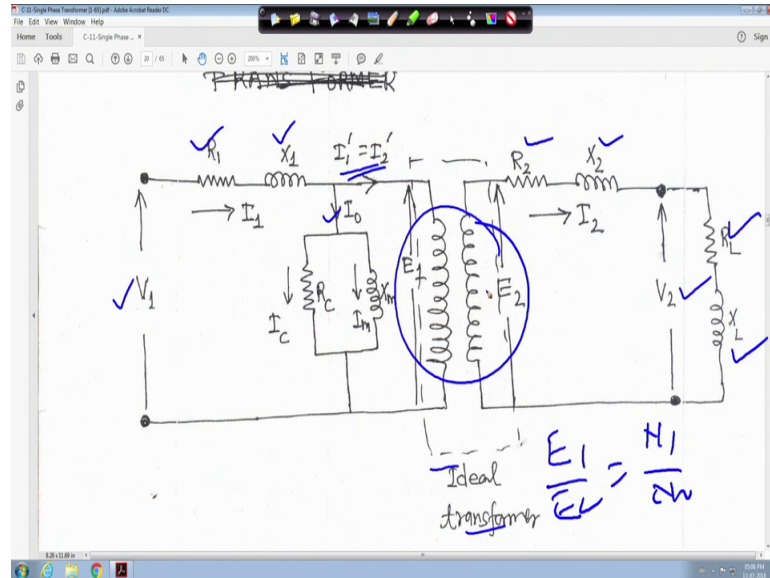
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Now, equivalent circuit of a transformer because we have seen transformer, but we have to obtain the equivalent circuit of transformer because you have to solve problem how to

solve the problem for an equivalent transformer or a equivalent transformer. For that we need to know the equivalent circuit of a transformer, right.

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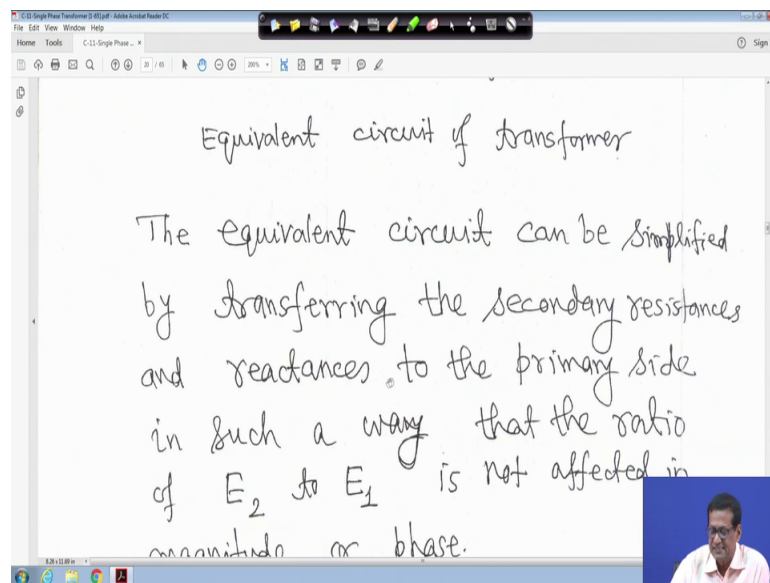
So, generally what happened that whenever look at that whenever a transformer your what you call is loaded, so load means say it load means say inductive load. So, suppose it resistance that you load resistance is R_L and say reactance is X_L j is not put any have, but when you solve the problem you have to put j the complex operator and voltage across the load is V_2 it is given here, right.

And this is $R_1 X_1$ the primary side resistance V_1 is the supply voltage, and current through this is I_0 that is your may your what you call that is your no load current and this current I_1 , I_1 is equal to I_0 plus I_2 dash that is phasor, right. And this current your this side we can call it is I_1 dash is equal to I_2 dash we can call also this is I_1 dash is equal to. So, I_2 dash, right.

So, and this is also $R_2 X_2$ that means, this winding as it nothing is there, there ideal transformer. So, this portions call ideal transformers, right. So that means, in this case your E_1 by E_2 equal to N_1 by N_2 is an ideal transformer as if everything is taken out from the transformer are represented by two winding. So, this is $E_1 E_2$. So, this at this portion that is why by dash line in this portion is shown by ideal transformer, right and current flowing through this load is I_2 and this current is I_1 and this is I_2 dash.

So, now, what we have to do is we have to make an equivalent circuit either it will bring either you bring all these parameters all these parameters to the primary side this is one way or you bring all these parameters to the secondary side either of this. So, who will take the secondary parameter to the primary side? So, how you will do it? So, then this is an ideal transformer the way we have represented everything as it this E_1 E_2 this is an ideal transformer that is written here, right.

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The screenshot shows a presentation slide with the following text:

Equivalent circuit of transformer

The equivalent circuit can be simplified by transferring the secondary resistances and reactances to the primary side in such a way that the ratio of E_2 to E_1 is not affected in magnitude or phase.

The slide is displayed in a software window titled 'C:\Single Phase Transformer (3).ppt - Adobe Acrobat Reader DC'. A small video inset in the bottom right corner shows a man speaking.

So, equivalent circuit of a transformer that is we have to this is this one we lot solve the problem we have to bring everything to one side that is say primary side.

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The equivalent circuit can be simplified by transferring the secondary resistances and reactances to the primary side in such a way that the ratio of E_2 to E_1 is not affected in magnitude or phase.

Now, the equivalent circuit can be simplified by transferring the secondary resistance and reactance to the primary side in such a way that the ratio of E_2 to E_1 is not affected in magnitude or phase. That means, this one as if it is an ideal transformer. So, E_1 to E_2 this is shown you will never be affected not R_2 or X_2 as well as this load also will transform to the primary side.

(Refer Slide Time: 23:35)

Resistance R_2 can be replaced by inserting an additional resistance R'_2 in the primary circuit such that the power absorbed in R'_2 when carrying current is equal to that in R_2 due to the secondary current, i.e.

$$I_1^2 R'_2 = I_2^2 R_2$$

Now, if you do so, if you do so, resistance R 2 can be replaced by inserting an additional resistance R 2 dash in the primary circuit such that the power absorbed in R 2 dash when carrying current your is equal to that in R 2 due to the secondary current, right.

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$$I_2'^2 R_2' = I_2^2 R_2$$

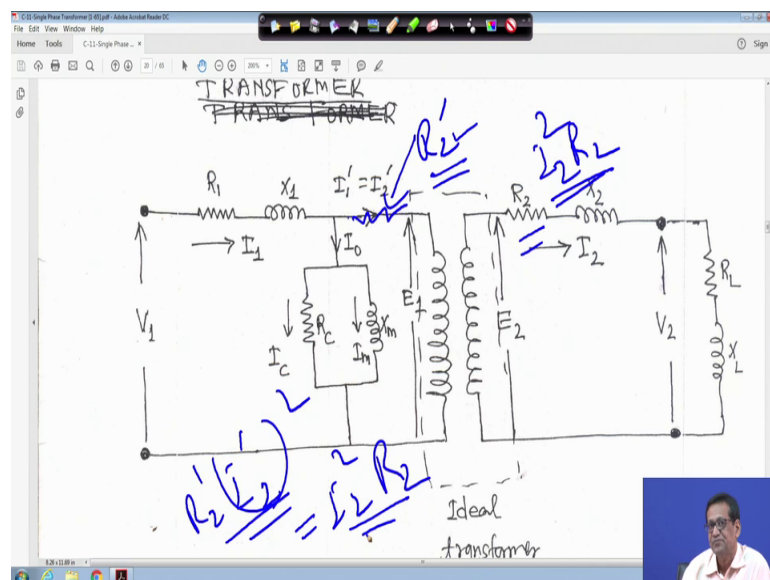
$$\therefore R_2' = \frac{I_2^2}{I_2'^2} R_2 = \left(\frac{I_2}{I_2'}\right)^2 R_2$$

$$\therefore R_2' = \left(\frac{N_1}{N_2}\right)^2 R_2 = K^2 R_2$$

$$\therefore R_2' = K^2 R_2$$

For example, for example, say take this circuit.

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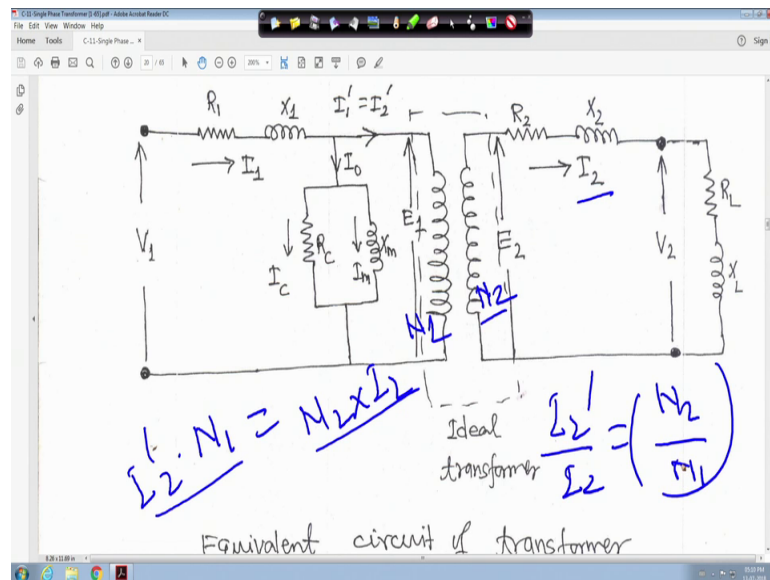
For example, I want to bring this one this side this side my power glass will be the current magnitude this is I 2 square is the magnitude in to R 2 to this is a power glass, right. Now, if I want to put that equivalent resistance similar to that on this supply your

what you call on the primary side in suppose I have a resistance here. And suppose this value is R_2 dash, right. Therefore, this side loss actually it will be R_2 dash there your I_2 dash square, right.

So, these loss and this I_2 square R_2 loss both has to be equal both has to be equal such that I will get the value of equivalent up to that, such that your what you call that your E_1 by E_2 ratio everything will remain same only thing is that, we have to insert one resistance we have to find on equivalent is R_2 dash, right whereas the loss of this one R_2 dash into I_2 dash square is equal to I_2 square R_2 this has to be same based on that only we transfer, right. So, if it is so, then in this case in this case I_2 dash square into R_2 dash is equal to I_2 square R_2 , right that is R_2 dash is equal to my I_2 square up on I_2 dash square into R_2 that is I_2 upon I_2 dash your what you call square into R_2 .

Now, from this and now I_2 upon I_2 dash is equal to N_1 upon N_2 because from this diagram your this, this one this trans for this one this trans ratio is N_1 and this trans ratio is N_2 , right.

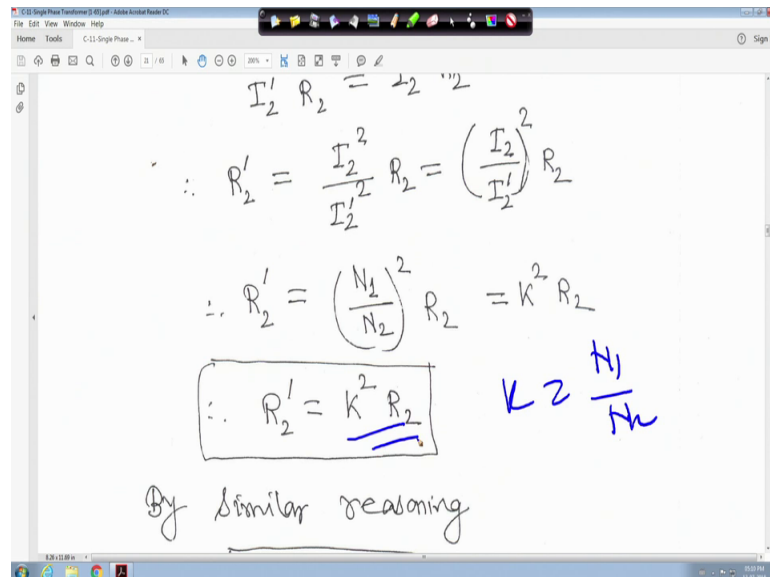
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And current here is I_2 dash therefore, you can make it I_2 dash into N_1 that is mmf of the primary side is equal to mmf of the secondary side that is N_2 into your N_2 into your I_2 , right. So, this is I_2 and at this N_2 . So, $N_2 I_2$ is equal to how to I_2 dash N_1 , right.

That means, I_2 dash upon I_2 is equal to N_2 upon N_1 , right or I_2 upon I_2 dash is equal to N_1 upon N_2 , right. So, that is what has been written here so that means, here you substitute that I_2 upon I_2 dash is equal to N_1 upon N_2 therefore, N_1 upon N_2 square into your R_2 .

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A screenshot of a digital whiteboard showing the derivation of the relationship between primary and secondary resistances in a transformer. The equations are written in black ink:

$$I_2' R_2 = I_2 R_2$$

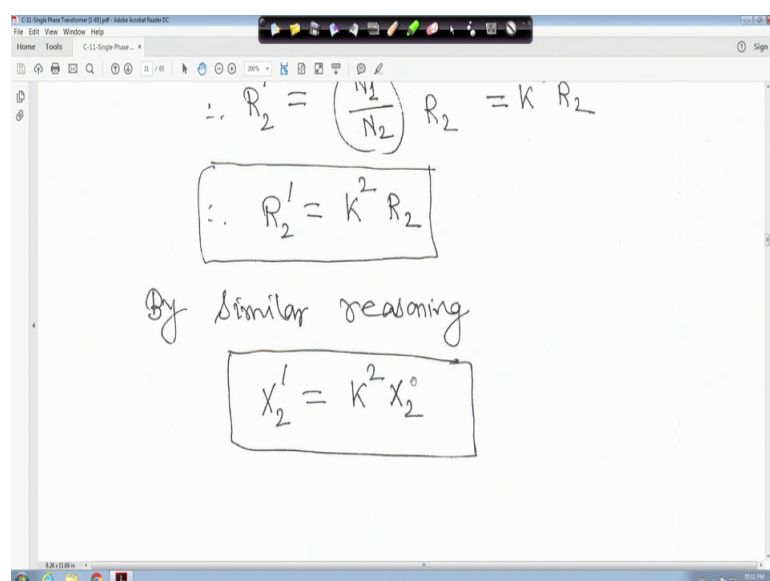
$$\therefore R_2' = \frac{I_2^2}{I_2'^2} R_2 = \left(\frac{I_2}{I_2'}\right)^2 R_2$$

$$\therefore R_2' = \left(\frac{N_1}{N_2}\right)^2 R_2 = k^2 R_2$$

The final result is boxed: $\therefore R_2' = k^2 R_2$. To the right, the transformation ratio is noted as $k = \frac{N_1}{N_2}$. Below the equations, it says "By similar reasoning".

But we have seen earlier that K is equal to we have seen earlier the K trans ratio is equal to N_1 upon N_2 therefore, R_2 dash will be K square into R_2 , right.

(Refer Slide Time: 26:31)



A screenshot of a digital whiteboard showing the derivation of the relationship between primary and secondary resistances in a transformer. The equations are written in black ink:

$$\therefore R_2' = \left(\frac{N_1}{N_2}\right)^2 R_2 = k^2 R_2$$

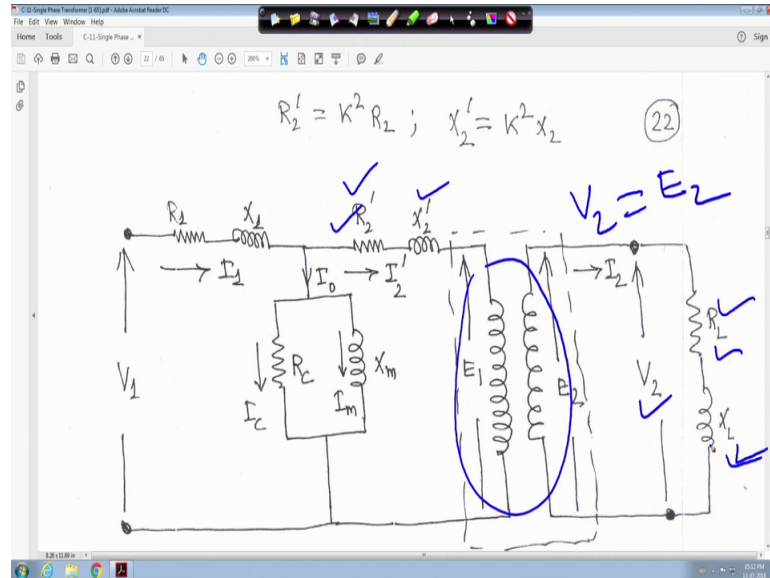
The final result is boxed: $\therefore R_2' = k^2 R_2$. Below the equations, it says "By similar reasoning".

$$\therefore X_2' = k^2 X_2$$

The final result is boxed: $X_2' = k^2 X_2$.

By similar way that reactance also can be transferred to that, so X_2 dash also will be K^2 into X_2 , right.

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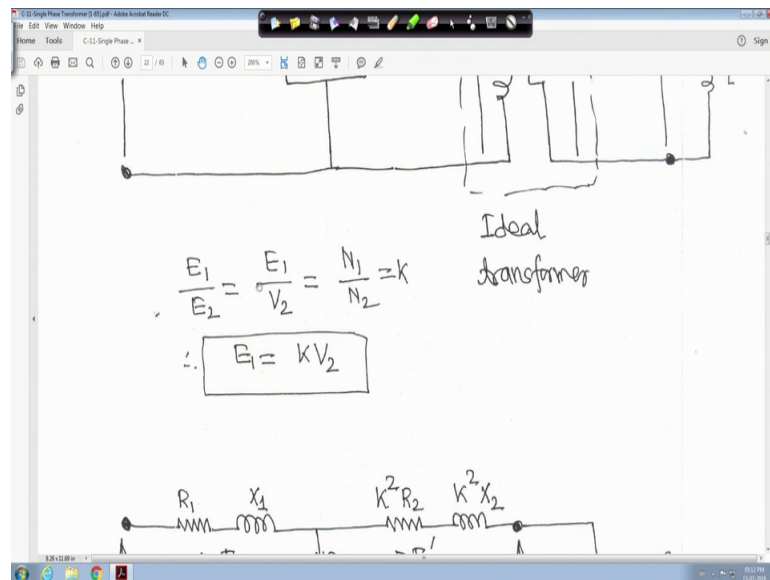


So, if it is so, therefore, R_2 dash is equal to $K^2 R_2$ and X_2 dash is equal to $K^2 X_2$. So, now this side your what you call the secondary side a resistance and reactance the equivalent one transferred to the primary side, right. but this is an your what you call, but this is an ideal transformer but load R_L , X_L is there V_2 is also there.

So, in that case what will happen at all this thing transferred to here. So, your primary or your secondary side my V_2 now is equal to E_2 , right my V_2 is equal V_2 is equal to E_2 , right. So, V_2 is V_2 is equal to your E_2 therefore, your because all this thing transfer here V_2 is the voltage across R_L and X_L to what one can your do is a primary side or equivalent one then what will be the equivalent voltage of your this V_2 to the primary side it will be nothing, but you are what you call that K into your V_2 will come to the primary side.

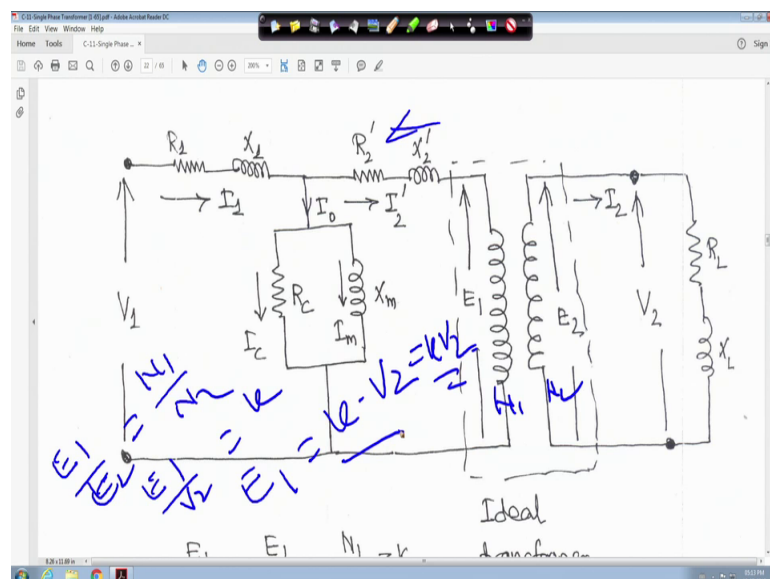
So, in that case and this R_L and X_L in similar way you can bring it to the primary side. R_L also you can make R_L dash X_L will be X_L dash that also can be transferred to the primary side, right.

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If it is so, similar way if it is so, then if you look into this that E_1 by E_2 is equal to you know N_1 by N_2 and E_2 is equal to V_2 . So, E_1 by V_2 is equal to your K therefore, E_1 is equal to K into V_2 .

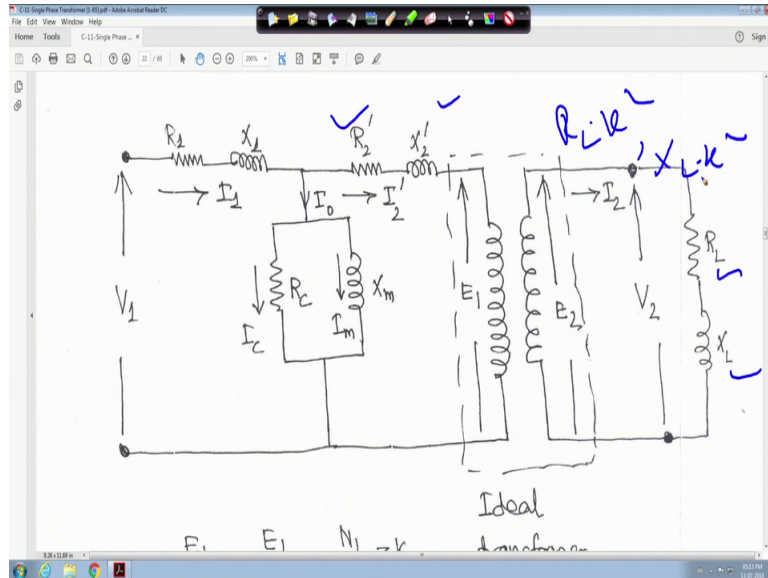
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That means this side that means, this side voltage transformation it will be K into V_2 because it is ideal transfer this trans ratio is N_1 this is N_2 E_1 upon E_2 is equal to N_1 upon N_2 that is your E_1 upon E_2 is equal to your N_1 upon N_2 , right. But E_2 is equal to V_2 because this thing is transformed to this side, right E_2 is equal to V_2 that means,

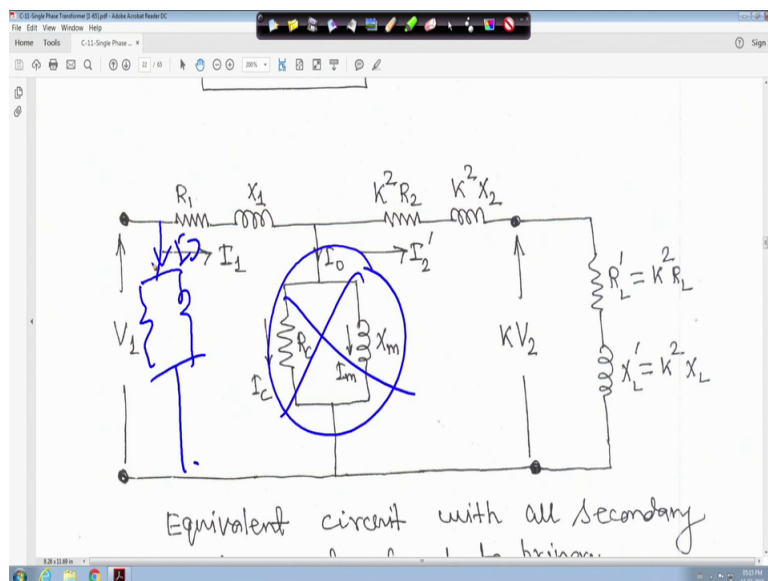
your 1 upon V 2 is equal to K, right N 1 upon N 2 is equal to K therefore, E 1 is equal to K into V 2, right. And let me clear it.

(Refer Slide Time: 28:49)



And when you transform this R L and X L to this side it will be then your R L into your K square. Similarly, it will be X L into K square the way you have transformed this, that is you R L dash and that will your X L dash. So, let me clear it.

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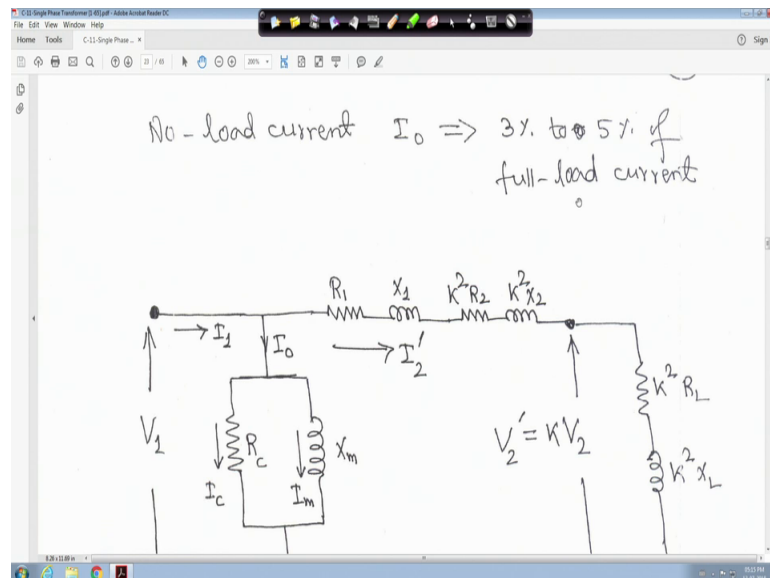


So, in this case your this R L dash is equal to K square your R L and X L dash is equal to K square into X L. I told you and your E 1 can be represent by K V 2. This is your E 1 it

can be represent by $K V_2$ voltage across the load. So, this is actually equivalent circuit of the transformer, then what we did? We transform all the secondary parameters to the primary side, right and this is my V_1 , this is my this one my primary is your what you call the parasite parameter this one also primary side parameters. And secondary side you have transform by multiplying your what you call just square of the trans ratio or transformation ratio that is $K^2 R_2$, $K^2 X_2$ and this is K^2 all that means, all the parameters resistance and reactance you have to multiply by K^2 and this should be $K V_2$.

So, this from the numerical point of view this you have to keep it in mind. But question is that this I_0 current actually this I_0 current is very small compared to the full load current, right. Generally your 3 to 5 percent, right. So, if you make this kind of series parallel circuit it will be not easy it will take time for your, what you call for solving numerical for computation. So, in that case what we will do what we will do this branch actually without your loosing much accuracy this branch will put somewhere here we will put somewhere here, right we will put somewhere here and this branch will remove from here and this will be my I_0 . So, error will be very less, right for easy computation.

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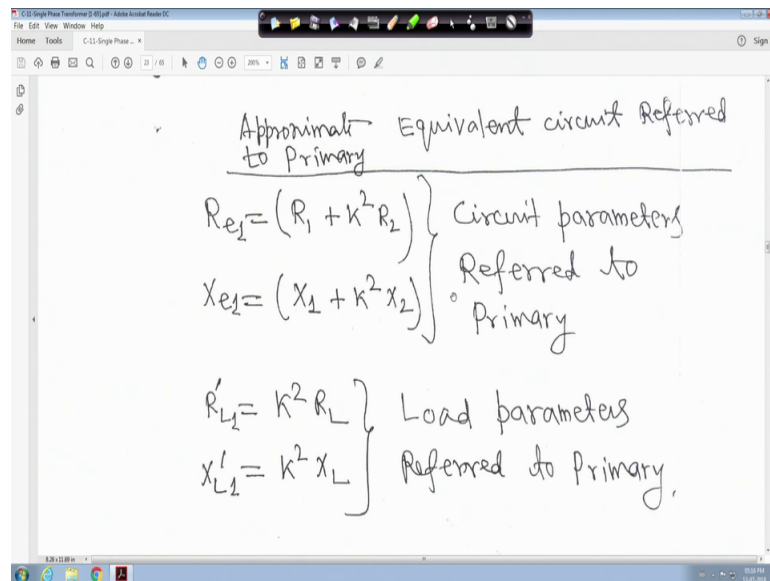


If we do so then this circuit that your I_0 is 3 to 5 percent of the full load current where circuits looks like this. So that means, you brought that one that means, of the beginning this is my I_1 and this is I_0 is going in that case I_1 is equal to your I_0 plus I_2 dash,

right. So, R_1 and this is the total resistance $R_1 + K^2 R_2$ the total resistance load we are not considering the load keep it separate then $X_1 + K^2 X_2$ is very primary and secondary equivalent resistance, right, so R_e is equal to R_1 rather is equal to $R_1 + K^2 R_2$ X_{e1} is equal to $X_1 + K^2 X_2$, right.

So, this is an approximate equivalent circuit and this side voltage will be V_2 that is equal to say K into V_1 , right and this is the supply voltage.

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So, if it is so, then this is approximate equivalent your circuit referred to primary, right R_{e1} is this one X_{e1} is this one. This value called referred to the primary side because everything we have brought it to the primary side, right.

And similarly R_{L1} dash is equal to $K^2 R_L$ and X_{L1} dash is equal to $K^2 X_L$ that is the load parameters referred to primary. If you bring that other things suppose I want to take it to the secondary side the primary parameters that many things will change including your r_p x_m everything. So, in that case you should have been R_2 plus R_1 upon K^2 it should have been X_2 plus your X_1 upon K^2 . Similarly you should have been your R_L upon K^2 and you should have been X_L upon K^2 if it is refer to the your secondary side, similarly voltage also would have been changed, right you should have been you are divided by K instead of multiplication of K , right. So, what I will solve the numericals.

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Ex-6
A single-phase transformer has 2000 turns on the primary and 800 turns on the secondary. Its no-load current is 5 Amp at a power factor of 0.20 lagging. Assuming the volt-drop in the windings is negligible, determine the primary current and power factor

So, take a one small take a simple example. A single phase transformer has 2000 turns on the primary and 800 turns on the secondary side. Its no load current is 5 ampere at a power factor of 0.2 lagging, right because a no load power factor is very poor. So, assuming the Volt drop in the windings is negligible.

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on the secondary. Its no-load current is 5 Amp at a power factor of 0.20 lagging. Assuming the volt-drop in the windings is negligible, determine the primary current and power factor when the secondary current is 100amp at a power factor of 0.85 lagging.

Soln.

So, neglecting the drop determine the primary current and power factor when the secondary current is 100 ampere at a power factor of 0.85 lagging, right. So, this is the problem, right.

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The image shows a software application window titled "C-11: Single Phase Transformer [2] (1).ippt - Adobe Acrobat Reader DC". The window contains handwritten mathematical work on a whiteboard background. The work is as follows:

Soln.

$$I_2' N_1 = I_2 N_2$$
$$\therefore I_2' = \frac{N_2}{N_1} \cdot I_2$$
$$\therefore I_2' = \frac{800}{2000} \times 100 = 40 \text{ amp, at } 0.85 \text{ pf lagging.}$$

Secondary pf = 0.85

$$\cos \phi_2 = 0.85$$
$$\therefore \phi = 31.8^\circ$$

There is a small video inset in the bottom right corner of the window showing a man speaking.

So, now we know $I_2' N_1$ is equal to $I_2 N_2$. Now, all formulas and known to you I_2 is 100 ampere at 0.85 power factor lagging, right therefore, I_2' is equal to N_2 upon and I_2 all the data are given. So, I_2' is compute 40 ampere and it is 0.85 lagging that is a I_2' dash.

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The image shows a software application window titled "C-11: Single Phase Transformer [2] (1).ippt - Adobe Acrobat Reader DC". The window contains handwritten mathematical work on a whiteboard background. The work is as follows:

$$\therefore I_2' = \frac{N_2}{N_1} \cdot I_2$$
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Secondary pf = 0.85

$$\cos \phi_2 = 0.85$$
$$\therefore \phi = 31.8^\circ$$

There is a small video inset in the bottom right corner of the window showing a man speaking.

Now, secondary side power factor is power factor is 0.85. So, ϕ_2 is equal to 31.8 degree, right. So, this is your what you call that secondary side power factor that given,

right it is the problem it is given, that your when the secondary current is hundred ampere at a power factor of 0.85 lagging.

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25

$$I_0 = 5 \text{ Amp}, \cos \phi_0 = 0.20$$

$$\therefore \phi_0 = 78.5^\circ$$

V_1 ↑

Now, I_0 is given 5 ampere and $\cos \phi_0$ is 0.2 is given. So, ϕ_0 is equal to 78.5 degree.

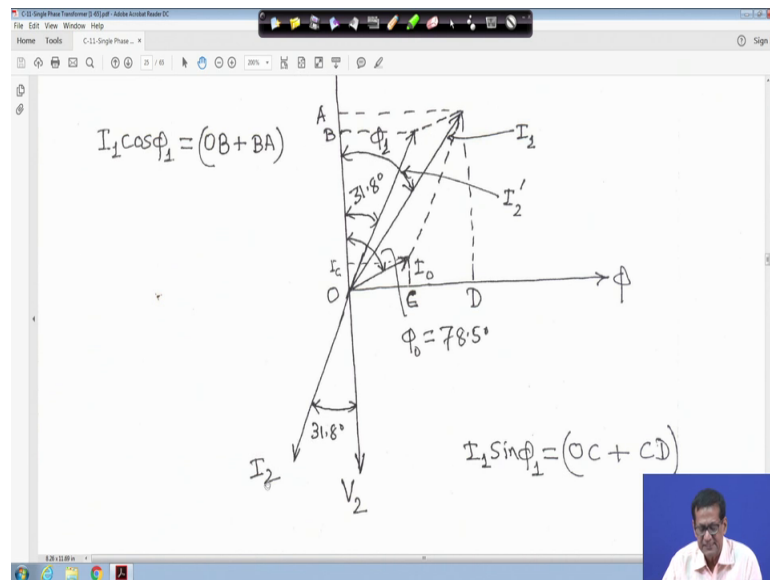
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$$I_1 \cos \phi_1 = (OB + BA)$$

$\phi_0 = 78.5^\circ$

Now, if you draw the phasor diagram that ϕ as a reference and this is your V_1 at this is I_1 , I_1 is equal to your I_0 plus your I_2 dash. And you and this is I_2 .

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And I_2 and I_2' are in anti phase I told you that is why this is I_2 and this is your I_2' dash. So, this is look at the look at this your what you call cursor and making it, right this is I_2' dash and this is my I_1 is equal to I_0 plus this thing and this ϕ_0 , the angle ϕ_0 it is given that is 78.5 degree, right. So, that means, your $I_1 \cos \phi_1$ that is this is my I_1 , and this is my your what you call that your $\cos \phi_1$ that is this OA , that OA is equal to actually OB plus BA . I am not writing here it is understandable just make it your projection on this your what you call on this y axis vertical axis say your V_1 , right, so OB plus BA .

Similarly this side is if you make $I_1 \sin \phi_1$ is basically $I_1 \sin \phi_1$ is equal to OD that is nothing, but OC plus CD , right. So, all the angles are marked and your currents are also computed, right.

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$$V_2$$

$$\therefore I_1 \cos \phi_1 = I_2 \cos(31.8^\circ) + I_0 \cos \phi_0 = 40 \times 0.85 + 5 \times 0.2$$

$$\therefore I_1 \cos \phi_1 = 35.0$$

$$I_1 \sin \phi_1 = I_0 \sin \phi_0 + I_2 \sin(31.8^\circ) = 5 \sin(78.5^\circ) + 40 \sin(31.8^\circ)$$

$$\therefore I_1 \sin \phi_1 = 25.98$$

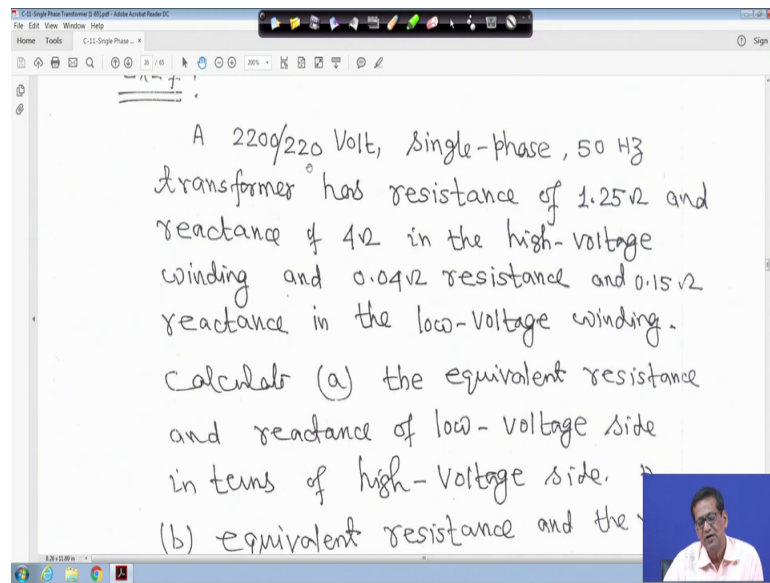
$$\therefore I_1 = \sqrt{(35)^2 + (25.98)^2} = 43.6 \text{ Amp}$$

$$\phi_1 = 36.6^\circ \quad \cos \phi_1 = 0.80$$

So, you can make it $I_1 \cos \phi_1$ is equal to $I_2 \cos 31.8$ degree plus $I_0 \cos \phi_0$, right. Whatever it come, so $I_1 \cos \phi_1$ coming actually 35, right. So, if you make it this AB actually is nothing, but this component. Just do it little bit yourself you will get it very simple, right, but everything I am marked for you.

And similarly your $I_1 \sin \phi_1$ is equal to $I_0 \sin \phi_0$ plus $I_2 \sin$ are 31.8 degree. you will get your $I_1 \sin \phi_1$ is equal to 25.98. So, this $I_1 \cos \phi_1$ $I_1 \sin \phi_1$ you square and add it, right if you do so, you will get I_1 is equal to 43.6 ampere because $\sin^2 \phi_1 + \cos^2 \phi_1$ is equal to 1. And if you divide this $I_1 \cos \phi_1$, and $I_1 \sin \phi_1$ $I_1 \sin \phi_1$ by $I_1 \cos \phi_1$ you will get you divide it and get it ϕ_1 . You will get $\tan \phi_1$ is equal to something, so ϕ_1 is equal to 36.6 degree. So, $\cos \phi_1$ will come you are what you call 0.8, right. So, this is the answer.

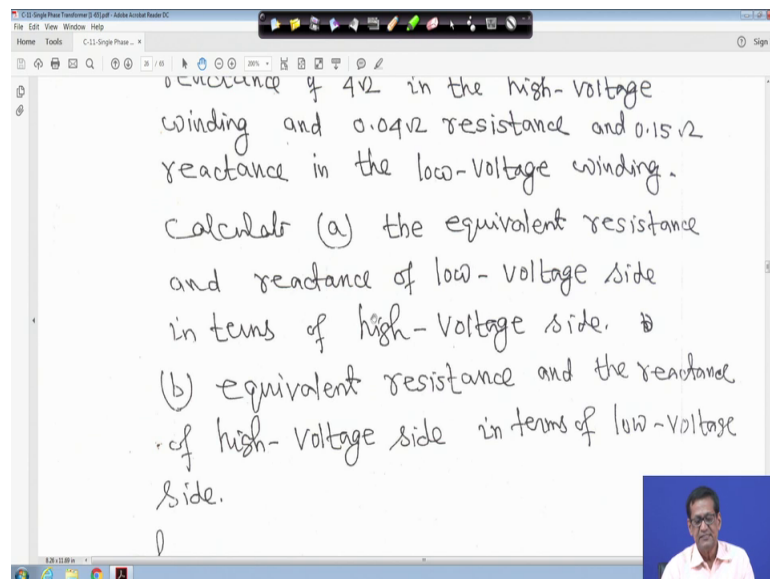
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A 2200/220 Volt, single-phase, 50 Hz transformer has resistance of $1.25\ \Omega$ and reactance of $4\ \Omega$ in the high-voltage winding and $0.04\ \Omega$ resistance and $0.15\ \Omega$ reactance in the low-voltage winding. Calculate (a) the equivalent resistance and reactance of low-voltage side in terms of high-voltage side. (b) equivalent resistance and the

Another one is a 2200/220 Volt primary side this Volt secondary side this Volt step down transformer single phase 50 Hertz frequency is 50 Hertz are resistance $1.25\ \Omega$, and reactance of $4\ \Omega$ in the high voltage winding. And $0.04\ \Omega$ resistance and $0.15\ \Omega$ reactance in the low voltage winding, it is primary side is this much and secondary side is this much is given, right.

(Refer Slide Time: 37:06)



reactance of $4\ \Omega$ in the high-voltage winding and $0.04\ \Omega$ resistance and $0.15\ \Omega$ reactance in the low-voltage winding. Calculate (a) the equivalent resistance and reactance of low-voltage side in terms of high-voltage side. (b) equivalent resistance and the reactance of high-voltage side in terms of low-voltage side.

So, calculate the equivalent resistance and reactance of low voltage side in terms of high voltage side; b, equivalent resistance and reactance of high voltage side in terms of low voltage side both side you have to get it, right.

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$R_1 = 1.25 \Omega$, $X_1 = 4 \Omega$
 $R_2 = 0.04 \Omega$, $X_2 = 0.15 \Omega$
 $K = \frac{N_1}{N_2} = \frac{V_1}{V_2} = \frac{2200}{220} = 10$
 (a) $R_2' = K^2 R_2 = (10)^2 \times 0.04 = 4 \Omega$
 $X_2' = K^2 X_2 = (10)^2 \times 0.15 = 15 \Omega$
 In terms of high-voltage side
 $R_{e1} = R_1 + R_2' = (1.25 + 4) = 5.25 \Omega$
 $X_{e1} = X_1 + X_2' = (4 + 15) = 19 \Omega$

So, R_1 is given R_2 is given, X_1 is given X_2 X_2 is given. R_1 X_1 for primary side, R_2 X_2 for secondary side. K is also given N_1 by N_2 is equal to V_1 by V_2 is equal to this much is equal to 10, right. So, R_2 dash for the referred to the your what you call primary side R_2 dash will be K square R_2 that is 4 ohm, right all data you put, right and X_2 dash will be K square X_2 . So, 10 square into 0.5, 15 ohm.

Therefore, in terms of high voltage side that is a primary winding, right, high voltage means here primary side the way we are made it, right here you are primary side is the high voltage side, right. Here it is high voltage side just this side your making primary side so, high voltage side.

So, in this case your what you call R_{e1} will be R_1 plus R_2 dash you add will get 5.52 ohm. Similarly X_{e1} will be X_1 plus X_2 dash you add will get 19 ohm, right.

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(b) $R_1' = \frac{R_1}{k^2} = \frac{1.25}{(10)^2} = 0.0125 \Omega$

$X_1' = \frac{X_1}{k^2} = \frac{4}{(10)^2} = 0.04 \Omega$

In terms of low voltage side,

$R_{e2} = R_2 + R_1' = (0.04 + 0.0125) = 0.0525 \Omega$

$X_{e2} = X_2 + X_1' = (0.15 + 0.04) = 0.19 \Omega$

Now, B part is referred to the secondary side. In this case it will be divided that is R 1 dash will be that is because R 1 X 1 you have to transform to the secondary side not R 2 X 2, R 2 X 2 will remaining the secondary side all the in primary side your transforming the secondary side there is high voltage side you are taking the low voltage side. So, in that time high your high voltage side resistance reactance it has to be divided by your K square, so that is why R 1 upon K square. So, it is 1.25 over 10 square 0.125 ohm and X 1 will be X 1 dash will be X 1 upon K square it is 10.04 ohm.

So, in terms of low voltage side now that is your secondary side, right it is Re 2 is equal to R 2 plus R 1 dash you add it is 0.0525 ohm, right.

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The screenshot shows a digital whiteboard with the following handwritten content:

$$X_1' = \frac{X_1}{k^2} = \frac{4}{(10)^2} = 0.04 \Omega$$

On terms of low voltage side.

$$R_{e2} = R_2 + R_1' = (0.04 + 0.0125) = 0.0525 \Omega$$
$$X_{e2} = X_2 + X_1' = (0.15 + 0.04) = 0.19 \Omega$$

Ex-8

For above the equivalent circuit

A small video inset in the bottom right corner shows a man in a white shirt speaking.

And X_2 dash if you add it will be your find your 0.19 ohm, right. But one thing look here it is 5.25 ohm, it is 19 ohm and secondary side it is 0.0525 ohm and if you want to bring whole thing to the your what you call your to the your primary your what you call primary side, if you multiply this by 100, 10 square it will be 5.25 ohm. And this one if you multiply by 10 square that is 100 you will get 19 ohm or vice versa, right from that you can check whether calculation is correct or not, right. So, this is one.

Thank you very much. We will be back again.