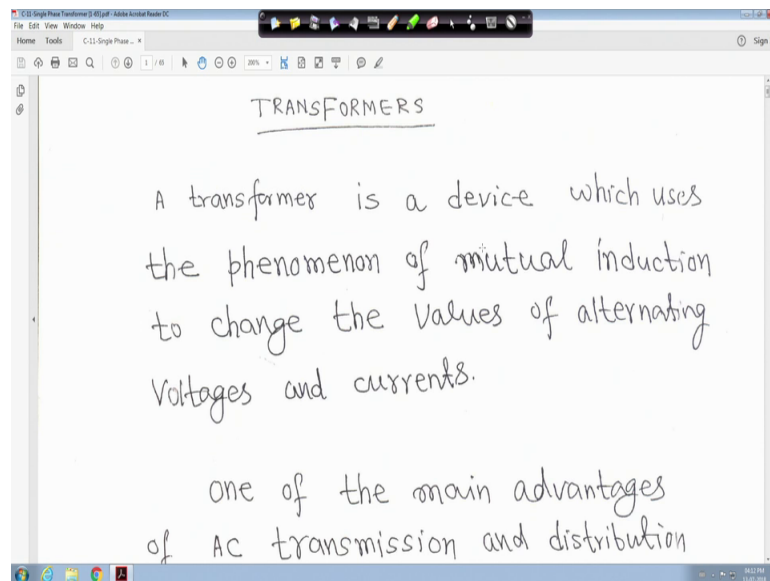


Fundamentals of Electrical Engineering
Prof. Debapriya Das
Department of Electrical Engineering
Indian Institute of Technology, Kharagpur

Lecture – 54
Single Phase Transformer

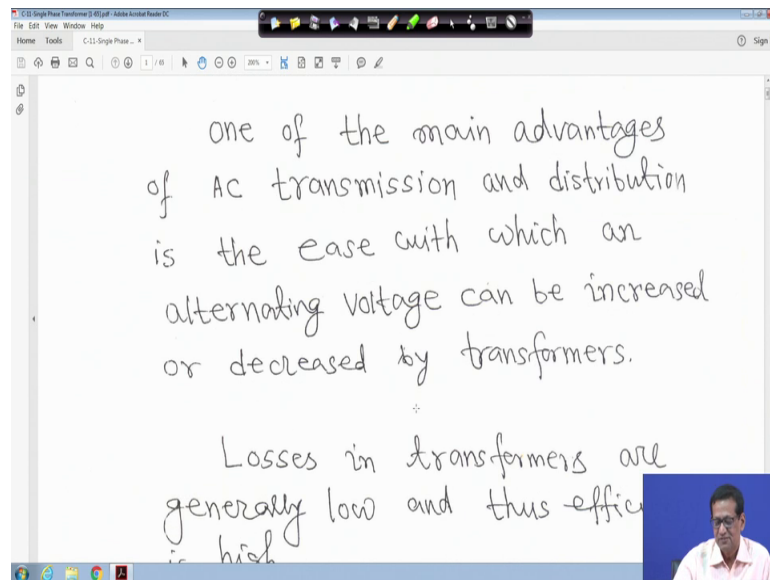
So, now, we will study that single Phase Transformer of the headline it is a transformers.

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That we will study single phase transformers only and after this we will see that your 3 phase induction machine only in brief and then the DC machine will the DC motors right. So, generally if you look at the this thing a transformer is a device which uses the phenomenon of mutual induction to change the values of alternating voltages and current right. So, basically in a transformer that one of the main advantages is that that it can transmit the voltage level that is it can increase the voltage level or it can you what you call decrease the voltage level. So, this is actually what you have the transformer right.

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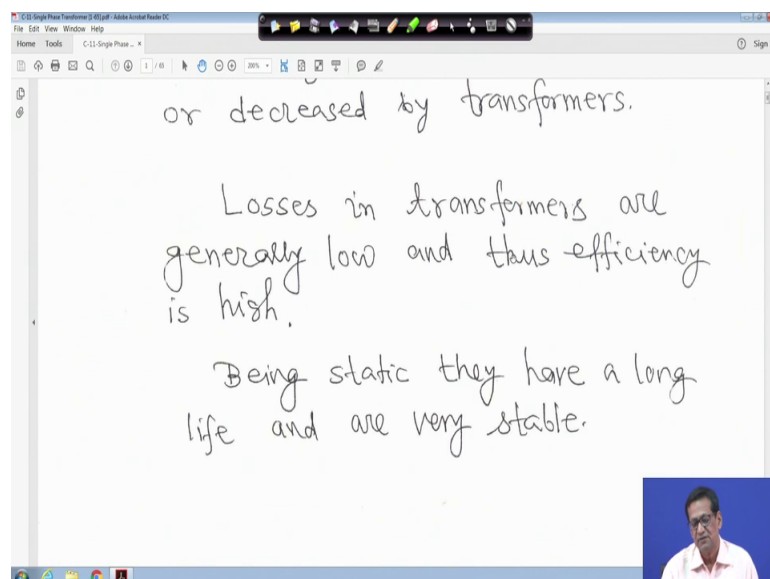
one of the main advantages of AC transmission and distribution is the ease with which an alternating voltage can be increased or decreased by transformers.

Losses in transformers are generally low and thus efficiency is high.

The screenshot shows a digital whiteboard interface with a toolbar at the top and a small video inset of a man in the bottom right corner. The text is written in a cursive, handwritten style.

So, it can your what you call for example, many when you look at the your power station, transmission line, distribution line, there are different voltage level and those voltage steps are or step up or step down only by using your what you call the transformers right. So, that means, therefore, the transformer is a device which uses the phenomenon of mutual inductance mutual induction to change the values of alternating voltage and current right.

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or decreased by transformers.

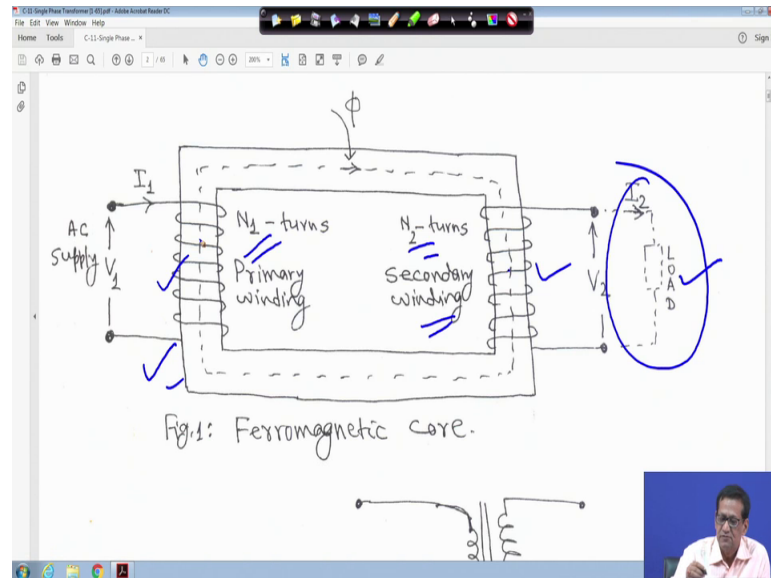
Losses in transformers are generally low and thus efficiency is high.

Being static they have a long life and are very stable.

The screenshot shows a digital whiteboard interface with a toolbar at the top and a small video inset of a man in the bottom right corner. The text is written in a cursive, handwritten style.

So, losses in transformers are your generally low and therefore, efficiency of the transformer is very high, losses we will see later. So, being static they have a long life and are very stable so, the transformer get static device.

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So, now, for example, suppose, if you consider your what you call a ferromagnetic core and you have your primary this side we call primary side say you have N_1 number of turns here, it is N_1 number of turns and you have the secondary you have N_2 number of turns. And in the secondary load is also connected, but shown in dash line; that means, load is not connected.

Now, an alternating supply voltage it is a V_1 is given right. So, when load is actually not connected so, what will happen is very small current right will flow through this your what you call through this primary side of the winding. And we and the flux we will link actually both the primary as well as the secondary winding when this side is your what you call open circuited right that means load is not connected.

So, no current is flowing through the your what you call secondary, but primary side you have applied your small voltage right. So, small current called exciting current will be responsible actually for you are producing the flux. And direction of the flux you will get the magnetic circuit the right hand rule I told you in the direction of the current you graph the your what you call coil and your thumb will put the your what you call the

direction of the flux right. So, let me clear it so, this is actually ferromagnetic core and this is your the your circuit symbol of a transformer.

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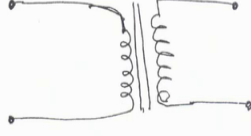



Fig.2: circuit diagram symbol for a transformer.

Primary winding \Rightarrow Connected to AC supply
Secondary winding \Rightarrow May be connected to a load.

PRINCIPLE OF OPERATION

So, primary winding is connected to AC supply I told you and secondary winding may be connected to a load.

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PRINCIPLE OF OPERATION

When the secondary is an open-circuit and an alternating voltage V_1 is applied

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3

to the primary winding, a small current - called the no-load current I_0 - flows, which sets up a magnetic flux in the core. This alternating flux links with both primary and secondary coils

The screenshot shows a digital whiteboard interface with a toolbar at the top and a small video inset of a man in the bottom right corner. The text is written in black ink on a white background.

Now, principles of a principle of operation, when the secondary is an open circuit and an alternating voltage V_1 is applied to the primary winding, a small current called no load that is I_0 flows right, which sets up a magnetic flux in the core. That means, here it will sets up the magnitude suppose a small current here it is showing the I_1 because it is primary side you are putting V_1 voltage I_1 current whenever it is I_0 current when it is at no load right and that time I_1 is equal to say I_0 .

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induces in them emf's of E_1 and E_2 respectively by mutual induction.

The induced emf E in a coil of N -turns is given by

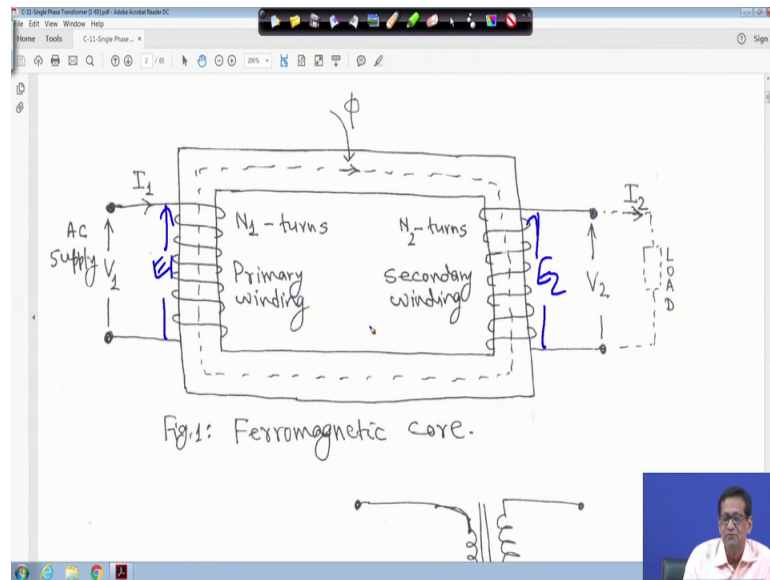
$$E = -N \frac{d\phi}{dt}$$

Following assumptions are made for an ideal transformer.

The screenshot shows a digital whiteboard interface with a toolbar at the top and a small video inset of a man in the bottom right corner. The text is written in black ink on a white background.

And your which sets up in magnetic flux in the core. This alternating flux links with both primary and the secondary coils right that I told you and induces in them an emf's of E_1 and E_2 respectively by mutual induction. That means, here a actually here a volt this is supply voltage anyway for the ideal transformer a voltage will be induced.

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So, if I make it like this it is E_1 right, but at that time you have to see you know different way that this is the winding also has your resistance as well as that your what you call reactance right. So, we will see later so, let me clear it. So, in that case your that your E_1 and E_2 respectively by mutual inductions. So, the induced emf E in a coil if you have N turns is given by E is equal to minus $N d\phi$ by dt . So, from the Faradays law the voltage induced thing is $N d\phi$ by dt and Lenz dI or what you call Lenz's law will give you the your direction of the emf so, that is why minus sign is here. So, following assumptions are made for an ideal transformer.

(Refer Slide Time: 05:19)

Handwritten text on a whiteboard:

$E = -N \frac{d\phi}{dt}$

Following assumptions are made for an ideal transformer:

- (a) Winding resistances are negligible.
- (b) All the flux produced is confined to the core of the transformer

A small video inset of a man is visible in the bottom right corner of the whiteboard frame.

Winding resistance say are negligible, say there is no winding resistance. All the flux produced is confined to the core of the transformer.

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Handwritten text on a whiteboard:

and links fully both the windings.
There is no leakage of the flux.

(c) The permeability of the core

A small video inset of a man is visible in the bottom right corner of the whiteboard frame.

And links fully both the windings there is no leakage of the flux, you are assuming there is no leakage and the flux links both the windings fully.

(Refer Slide Time: 05:40)

There is no leakage of the flux.

(c) The permeability of the core is high so that the magnetising current required to produce the flux and establish it in the core is negligible.

(d) Hysteresis and eddy current

Now number 3, the permeability of the core is very high right so, that the magnetizing current required to produce the flux and establish it in the core is negligible right.

(Refer Slide Time: 05:53)

high so that the magnetising current required to produce the flux and establish it in the core is negligible.

(d) Hysteresis and eddy current losses are negligible.

In an ideal transformer, $\frac{d\phi}{dt}$ is

And number 4 that is d part hysteresis and eddy current losses are negligible, these are the 4 assumptions you have made right. So, these are the 4 assumptions you have made for an ideal transformer.

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In an ideal transformer, $\frac{d\phi}{dt}$ is same for both primary and secondary, thus

$$E_1 = -N_1 \frac{d\phi}{dt}$$

and

$$E_2 = -N_2 \frac{d\phi}{dt}$$

$\therefore \frac{E_1}{N_1} = \frac{E_2}{N_2}$ (i.e. induced emf per turn is constant)

Polarity of the induced emf is given by Lenz's law. It opposes the change and hence is negative.

Now, in an ideal transformer $\frac{d\phi}{dt}$ is same for both primary and secondary winding because the flux ϕ linking both primary and secondary winding. So, E_1 is equal to you can write minus $N_1 \frac{d\phi}{dt}$ that is the induced voltage in the winding, similarly E_2 is equal to minus $N_2 \frac{d\phi}{dt}$ and you are resist you are neglecting your what you call it is the ideal transformer your resistance is neglected.

Now, therefore, if you divide E_1 by E_2 you will get N_1 by N_2 therefore, if you divide these 2 equations E_1 by E_2 you will get N_1 by N_2 therefore, E_1 upon N_1 is equal to E_2 by N_2 that is induced emf per turns is constant that is E_1 by N_1 is equal to E_2 by N_2 . Now, polarity of the induced emf is given by Lenz's law actually it opposes the change. Hence it is actually negative right from your higher secondary physics you have gone all through this right.

(Refer Slide Time: 07:03)

Assuming no losses, ~~and~~ ~~and~~ ~~and~~ ~~and~~

$$\therefore \frac{V_1}{N_1} = \frac{V_2}{N_2}$$
$$\therefore \frac{V_1}{V_2} = \frac{N_1}{N_2} = K$$

$K \Rightarrow$ voltage ratio OR turns ratio
OR transformation ratio

(5)

So, assuming that no losses therefore, we can make V_1 by N_1 is equal to V_2 by N_2 . So, in that case if we assume that there is no loss then we can make V_1 upon V_1 by V_2 is equal to your N_1 upon N_2 here it is E_1 upon E_2 is equal to N_1 upon N_2 right. And if there is no loss we assume there is no loss then we can write that your turn supplied voltage that is V_1 , V_1 by N_1 is equal to V_2 by N_2 this is primary side voltage and V_2 is the secondary side voltage. Therefore, we can make V_1 by V_2 is equal to N_1 by N_2 is equal to K that is called turns ratio therefore, K is the voltage ratio or turns ratio or transformation ratio.

(Refer Slide Time: 07:52)

OR transformation ratio

$$\therefore V_2 = \frac{V_1}{K}$$

$K < 1 \Rightarrow$ step-up transformer
 $K > 1 \Rightarrow$ step-down transformer

When a load is connected across the secondary winding, a current will flow through the secondary winding.

Therefore, V_2 is equal to V_1 upon K , if K less than 1 then this call step - up transformer and if K your greater than one it is called step - down transformer. So, let us go back to that your circuit again here let us go back to the circuit again. So, we are assuming there is no loss right so, and this side is voltage V_1 this side is voltage V_2 ; that means, this is if it is marked that this is my E_1 and here also it is my E_2 we are assuming there is no loss.

Therefore, your V_1 by your V_1 by your E_1 by E_2 is equal to N_1 by N_2 so, is equal to your V_1 by V_2 is equal N_1 by N_2 . Later we will see the relationship between V_1 and E_1 similarly here. So, will be the here only right so, if K less than 1 that is step- up transformer if K greater than 1 that is step - down transformer.

(Refer Slide Time: 09:05)

Handwritten notes on a whiteboard:

$$\frac{V_1}{V_2} = \frac{N_1}{N_2} = K$$

$N_1 = 50$
 $N_2 = 100$

Voltage ratio OR Turns ratio
OR transformation ratio

$$K = \frac{N_1}{N_2} = \frac{50}{100} = \frac{1}{2}$$

$$\therefore V_2 = \frac{V_1}{K}$$

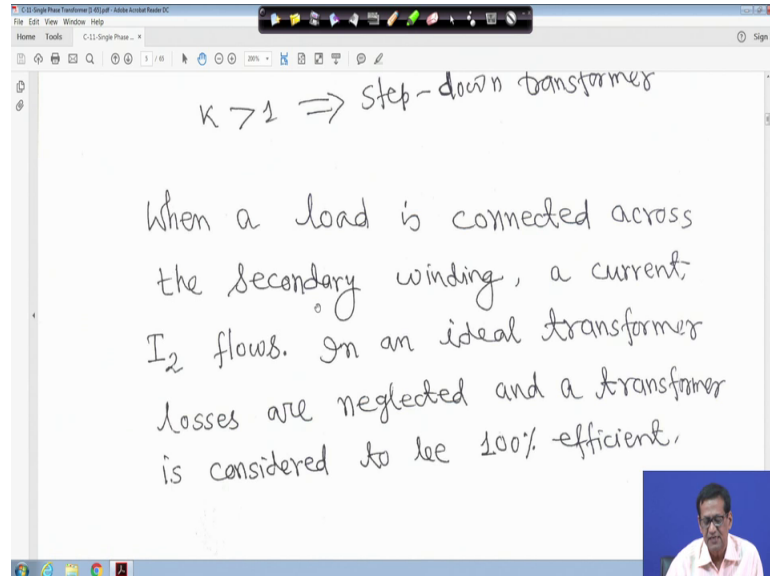
$K < 1 \Rightarrow$ step-up transformer
- step-down transformer

For example, suppose say N_1 is equal to say 50 right and N_2 is equal to say your 100 right, 50 turns and 100 turns. Then K is equal to N_1 by N_2 is equal to 50 by 100 is equal to half; that means, K less than 1 that is your K less than 1 because it is half; that means, it is step- up transformer.

Why it is step - up transformer; that means, here then V_1 upon V_2 is equal to K is equal to half right; that means, V_2 is equal to 2 into V_1 right; that means, it is step-up transformer because primary side voltage if it is V_1 secondary side it is becoming 2 into V_1 . For example, primary side if it is 100 KB then secondary side it is 200 KB so, it is a

step - up transformer if K less than 1. Similarly, for if K greater than 1 then it will be step - down transformer right. So, that is K greater than 1 for step- down transformer.

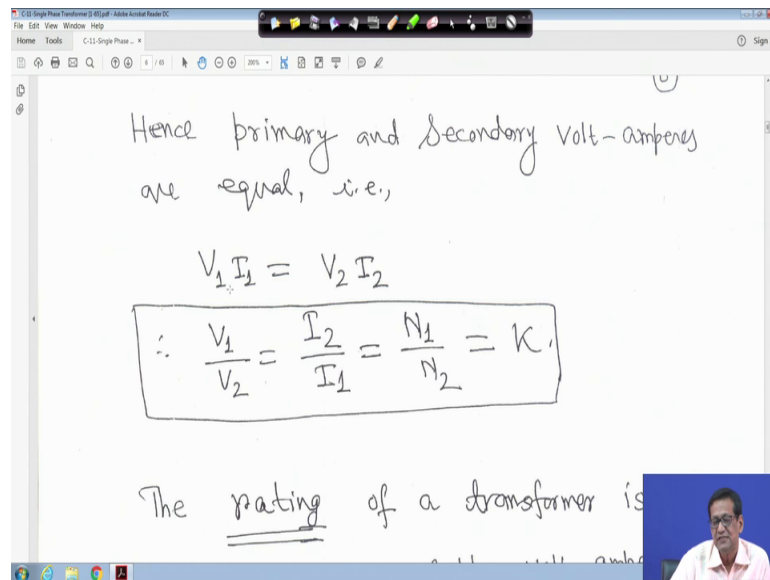
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Now, when a load is connected across the secondary winding a current I_2 flows right. So, in an ideal transformer loss of whenever I am telling this first you draw the circuit diagram in the beginning right the ferromagnetic material the core the winding first you draw it.

Then you see, this when a load is connected across the secondary winding a current I_2 flows in an ideal transformer losses are neglected and a transformer is considered to be 100 percent efficient right, although the reality ideal transformer is not possible, but for the sake of our clarification.

(Refer Slide Time: 10:52)



Hence primary and secondary volt-ampere are equal, i.e.,

$$V_1 I_1 = V_2 I_2$$
$$\therefore \frac{V_1}{V_2} = \frac{I_2}{I_1} = \frac{N_1}{N_2} = K$$

The rating of a transformer is

Now, hence the primary and secondary volt amperes will be equal that is $V_1 I_1$ must be equal to $V_2 I_2$, that is V_1 actually is your primary side voltage and I_1 is the primary side current and V_2 is a secondary side voltage and I_2 is the secondary side current. Therefore, the volt ampere must be same, if $V_1 I_1$ is equal to $V_2 I_2$ therefore, V_1 by V_2 is equal to I_2 by I_1 .

So, V_1 by V_2 is now N_1 by N_2 is equal to I_2 by I_1 is equal to N_1 by N_2 is equal to K . Therefore, either you can write V_1 by V_2 is equal to N_1 by N_2 or in the case of current it will be I_2 by I_1 is equal to N_1 by N_2 that is $N_1 I_1$ is equal to $N_2 I_2$ right. So, that means, emf on the I mean if you later we will see it will be a different way.

(Refer Slide Time: 11:41)

Hence primary and secondary volt-ampere are equal, i.e.,

$$V_1 I_1 = V_2 I_2$$

$$\therefore \frac{V_1}{V_2} = \frac{I_2}{I_1} = \frac{N_1}{N_2} = k$$

$\frac{I_2}{I_1} = \frac{N_1}{N_2}$
 $I_2 N_2 = I_1 N_1$

The rating of a transformer is stated in terms of the volt-ampere

Suppose, if it is I_2 by I_1 is equal to your N_1 by N_2 go for a cross multiplication therefore, $I_2 N_2$ is equal to your $I_1 N_1$ right therefore, emf on the secondary side must be equal to the emf on the primary side right.

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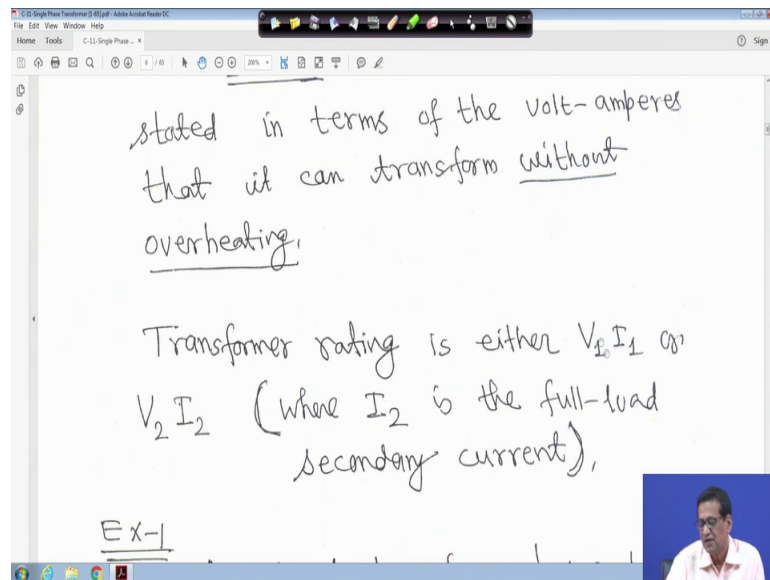
$V_1 I_1 = V_2 I_2$

$$\therefore \frac{V_1}{V_2} = \frac{I_2}{I_1} = \frac{N_1}{N_2} = k$$

The rating of a transformer is stated in terms of the volt-ampere that it can transform without overheating.

So, the rating of a transformer is stated in terms of the volt ampere that it can transform without overheating so, this way we make it then volt ampere.

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stated in terms of the volt-amperes that it can transform without overheating.

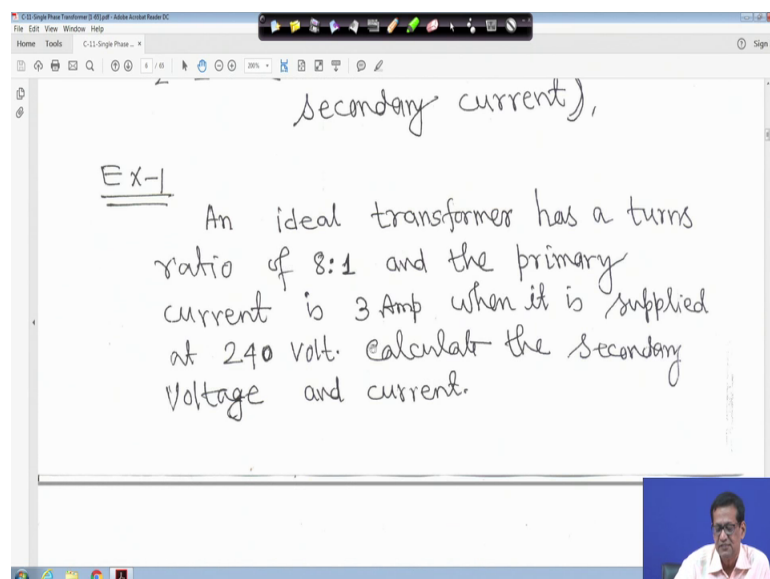
Transformer rating is either $V_1 I_1$ or $V_2 I_2$ (where I_2 is the full-load secondary current),

Ex-1

The screenshot shows a digital whiteboard interface with a toolbar at the top and a small video inset of a person in the bottom right corner. The text is written in black ink on a white background.

Now, transformer rating is either $V_1 I_1$ or $V_2 I_2$ when I_2 is the full load say secondary current. So, this is actually transformer rating generally on the transformer nameplate you will find it is K V a rating will be given right, this frequency will be given for unit impedance will be given all this things will be given. So, just to whatever little bit you have studied we will come to phasor diagram other thing later you take a small example.

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secondary current),

Ex-1

An ideal transformer has a turns ratio of 8:1 and the primary current is 3 Amp when it is supplied at 240 Volt. Calculate the secondary voltage and current.

The screenshot shows a digital whiteboard interface with a toolbar at the top and a small video inset of a person in the bottom right corner. The text is written in black ink on a white background.

An ideal transformer it is turns ratio of 8 is to 1 and the primary current is 3 ampere it is given when it is supplied at 240 volt calculate the secondary voltage and the current right.

(Refer Slide Time: 12:57)

Soln.

$N_1 : N_2 = 8 : 1$ (7)

A turns ratio of 8:1 means

$$\frac{N_1}{N_2} = \frac{8}{1} = K$$

$\therefore K = 8$ (step-down transformer)

$$\therefore \frac{V_1}{V_2} = K$$

240 = 30 Volt.

So, now turns ratio is given 8 is to 1 means it is N 1 is to N 2 I mean whenever it is given that 8 is to 1; that means, it is N 1 is to N 2 is equal to 8 is to 1. So, N 1 by N 2 is equal to 8 by 1 is equal to K. So, K is equal to 8; that means, it is a step down transformer because K greater than 1 right.

(Refer Slide Time: 13:21)

A turns ratio of 8:1

$$\frac{N_1}{N_2} = \frac{8}{1} = K$$

$\therefore K = 8$ (step-down transformer)

$$\therefore \frac{V_1}{V_2} = K$$

$$\therefore V_2 = \frac{V_1}{K} = \frac{240}{8} = 30 \text{ Volt.}$$

$240 \times 3 = 720 \text{ VA}$

Also $I_2 = K$

So, that means V_1 by V_2 is equal to K therefore, V_2 is equal to V_1 upon K so, 240 by 8 so, V_2 will be 30 volt. So, primary side is 240 volt secondary side is 30 volts also we know that I_2 by I_1 is equal to K . So, I_2 is equal to K into I_1 it is given I_1 is equal to 3 ampere. So, I_2 is equal to 24 ampere.

So, interestingly if you see this side it is your 30 volt right full load voltage has low, but at the same time if current has increased because volt ampere has to remain your same. So, if you see the volt ampere primary side 240 volt into 3 ampere current so, 720 volt ampere right. Similarly, for the your secondary side if you look into your second side, the secondary side also has to be 720.

(Refer Slide Time: 14:19)

$\therefore K = 8$ (step-down transformer)
 $\therefore \frac{V_1}{V_2} = K$
 $\therefore V_2 = \frac{V_1}{K} = \frac{240}{8} = 30 \text{ Volt.}$
 Also $\frac{I_2}{I_1} = K$
 $\therefore I_2 = K \cdot I_1 = 8 \times (3) = 24 \text{ Amp.}$
 $30 \times 24 = 720 \text{ VA}$
 $V_1 I_1 = V_2 I_2$

So, if you see this voltage is your V_2 is 30 volt and this is 24 ampere so, that is also 720 volt ampere right. So, that means, $V_1 I_1$ it has to be equal to $V_2 I_2$ right.

(Refer Slide Time: 14:39)

EX-2

A 5 KVA, 1 ϕ transformer has a turns ratio of 10:1 and is fed from a 2.5 KV supply. Neglecting losses, determine

- the full-load secondary current
- the minimum load resistance which can be connected across the secondary winding to give full load KVA
- primary current at full load KVA

Now, another small example so, if 5 KVA, single phase it is 1 phi. So, that will be single phase single phase transformer has a turns ratio 10 is to 1 that is N_1 is to N_2 is equal to 10 is to 1 and is fed from a 2.5 KV supply 2.5 kilovolt right. So, neglecting losses determine, a the full load secondary current, b, the minimum load resistance which can be connected across the secondary winding to give full load KVA and c, is the primary current at full load KVA. So, these are the thing have been asked to and you have to do it.

(Refer Slide Time: 15:18)

Soln.

(a) $\frac{N_1}{N_2} = \frac{10}{1} = 10$,

$V_1 = 2.5 \text{ KV} = 2500 \text{ Volt}$

Since

$$\frac{N_1}{N_2} = \frac{V_1}{V_2}$$

$\therefore V_2 = V_1 \left(\frac{N_2}{N_1} \right) = 2500 \times \frac{1}{10} = 250$

So, first thing is that N_1 by N_2 is equal to 10 is to 1, 10 by 1 is equal to 10. Now, V_1 is given 2.5 KV. So, 2500 volt multiplied by 1000.

(Refer Slide Time: 15:30)

$V_1 = 2.5 \text{ kV} = 2500 \text{ Volt}$
 Since
 $\frac{N_1}{N_2} = \frac{V_1}{V_2}$
 $\therefore V_2 = V_1 \left(\frac{N_2}{N_1} \right) = 2500 \times \frac{1}{10} = 250 \text{ Volt}$
 The transformer rating in Volt-amperes
 $= V_2 I_2$ (at full load)

We know if since N_1 by N_2 is equal to V_1 by V_2 therefore, V_2 is equal to V_1 into N_2 upon N_1 right is equal to V_1 is given 2500 and N_2 by N_1 is 1 upon 10. So, it is 250 volts right so, V_2 is the 250 volt.

(Refer Slide Time: 15:47)

$\therefore V_2 = V_1 \left(\frac{N_2}{N_1} \right) = 2500 \times \frac{1}{10} = 250 \text{ Volt}$
 The transformer rating in Volt-amperes
 $= V_2 I_2$ (at full load)
 $\therefore 5 \times 1000 = 250 \times I_2$
 $\therefore I_2 = 20 \text{ Amp.} = \text{full-load current}$
 (b) Minimum value of load resistance

The transformer rating in volt ampere will be $V_2 I_2$ at full load right. So, it is V_2 is your is equal to your $V_2 I_2$ is that is KVA is given 5000 I mean this is something like this. So, transformer rating at in volt ampere is equal to $V_2 I_2$.

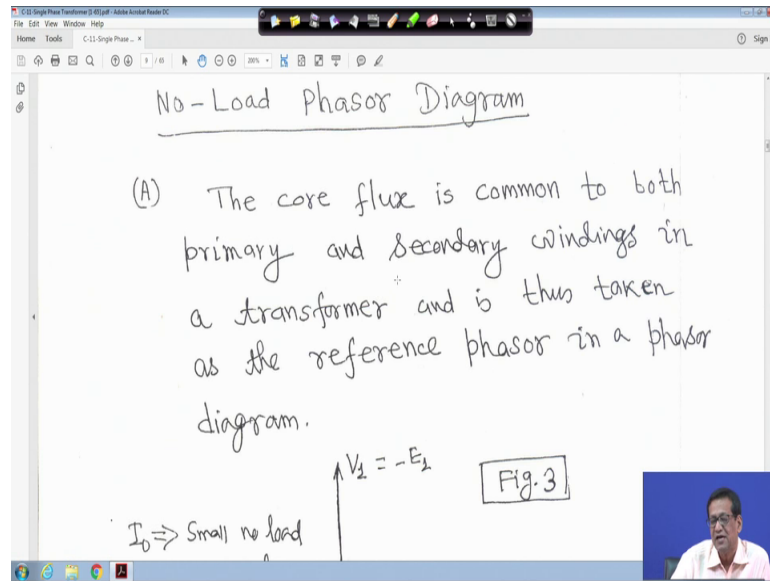
So, this 5 KVA is given so, 5 into 1000 ampere is equal to V_2 is to 250 volt we got V_2 is equal to 250 volt into I_2 prominence if you solve you will get I_2 is equal to 20 ampere the full - load current. So, KVA it is given in the problem it is given 5 KVA; that means, 5000 volt ampere is equal to voltage is 250 volt here and current you have to determine. So, from which you will get the I_2 is equal to 20 ampere.

(Refer Slide Time: 16:36)

$\therefore I_2 = 20 \text{ Amp.} = \text{full-load current}$
 (b) Minimum value of load resistance,
 $R_L = \frac{V_2}{I_2} = \frac{250}{20} = 12.5 \Omega$
 (c) $\frac{N_1}{N_2} = \frac{I_2}{I_1} \quad \therefore I_1 = I_2 \left(\frac{N_2}{N_1} \right)$
 $\therefore I_1 = 20 \times \frac{1}{10} = 2 \text{ Amp.}$

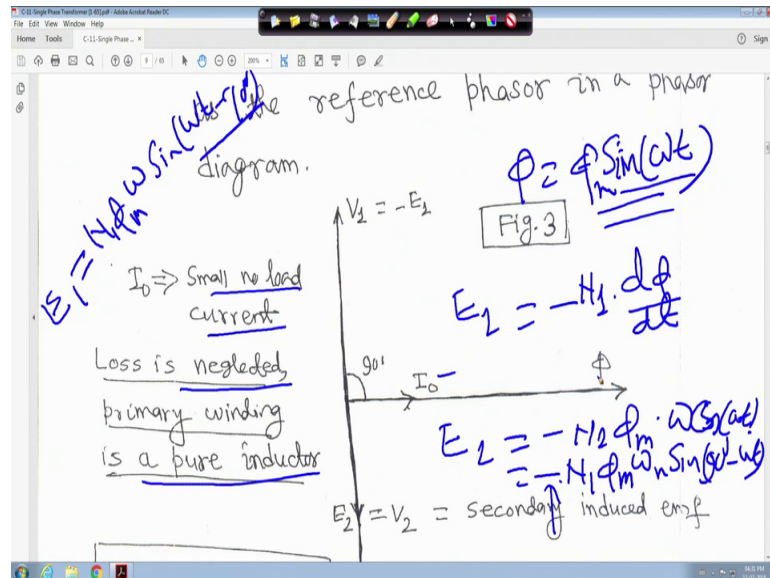
Now, b, minimum value of load resistance so, R_L is equal to just V_2 by I_2 . So, V_2 is given 250 we will get 250 and I_2 got 20 so, it is 12.5 ohm. See, N_1 by N_2 is equal to I_2 by I_1 we know that therefore, I_1 is equal to I_2 in to N_2 by N_1 . So, I_2 we got 20 ampere and N_2 by N_1 is 1 upon 10. So, it is actually 2 ampere right so, very simple.

(Refer Slide Time: 17:07)



Now next is no - load phasor diagram. Now, the core flux actually no load Phasor diagram, the core flux is common to both primary and secondary windings in a transformer that I showed you in the beginning and is thus taken as the reference Phasor in a phasor diagram.

(Refer Slide Time: 17:22)



For example, in a Phasor diagram, this is the flux right, we will assume that phi is equal to so, sinusoidal variation phi M sin omega t right, this is your phi M sin omega t, this is the flux and we are taking the your phi as a reference. Now, I 0 is equally small no load

current and loss is neglected right. So, primary winding then will be a pure inductor because we are giving alternating supply to the primary winding. So, if our loss is neglected it will act like your what you call that is pure inductor.

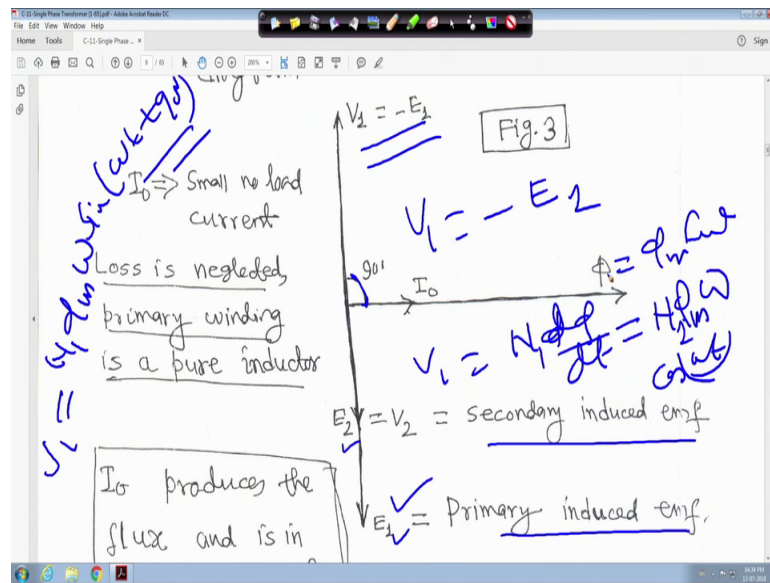
So, in that case what will happen that, whenever you say that as per your, what you call as per Lenz's law right we know that E_1 is equal to minus for the primary winding it is N_1 right. So, into $d\phi$ by dt right, this minus sign comes because of the Lenz's law right. So, this is E_1 is equal to minus $N_1 d\phi$ by dt . Now, we know ϕ is equal to $\phi_{max} \sin \omega t$. So, if you just take the derivative of that then you will get E_1 is equal to minus $N_1 \phi_m \omega \cos \omega t$ right that much that we will get.

So, this one you can write that your minus $N_1 \phi_m \omega \cos \omega t$ this is cosine ωt . So, we can write $\sin 90^\circ$ minus ωt and this minus sign is here this minus sign is here you take minus sign inside that then what we will get that E_1 is equal to your $N_1 \phi_m \omega \sin \omega t$ minus 90° .

So, $\sin \omega t$ minus 90° that is E_1 right; that means, if ϕ is equal to the reference that is your $\sin \omega t$ right and it is a loss is neglected. Therefore, that no load current I_0 also will be in phase with your what you call in your what you call with the flux right and I_0 actually will lagging from your V_1 by your 90° if loss is neglected if it is loss is completely neglected right.

So, in that case I_0 will be in phase with ϕ and your as it is as resistance is neglected. So, generally that your therefore, the I_0 is lagging from the voltage V_1 by 90° , it is because that primary winding is acting as a pure inductor right. And if you take the magnetizing m call magnetizing reactance right X_m then you will see that I_0 is purely I mean loss is neglected then this I_0 and ϕ both are in phase and lagging from V_1 by 90° . So, in this case that E_1 is equal to is coming ωt minus 90° and; that means, ϕ is equal to $\phi_m \sin \omega t$ and here it is $\sin \omega t$ minus 90° that means so, I am clearing it right.

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So, that means, my V_1 will be your what you call lagging from ϕ by 90 degree therefore, this is my E_1 this is my E_1 the primary induced emf. Similarly, E_2 also will be the same way E_2 also will be lagging and E_2 is equal to V_2 because loss your what you call we are we have considering an ideal transformer right. So, this is your secondary induced both will be like this. Now, therefore, the supply voltage from the Lenz's laws it opposes the change right.

So, Lenz's law, Lenz law it is actually V_1 is equal to minus E_1 right. So, an E_1 is equal to minus and $d\psi$ by dt ; that means, my V_1 will be N_1 at in general N_1 your what you call $d\psi$ by dt because E_1 is equal to minus $N_1 d\psi$ by dt so, minus plus it will be $N_1 d\psi$ by dt .

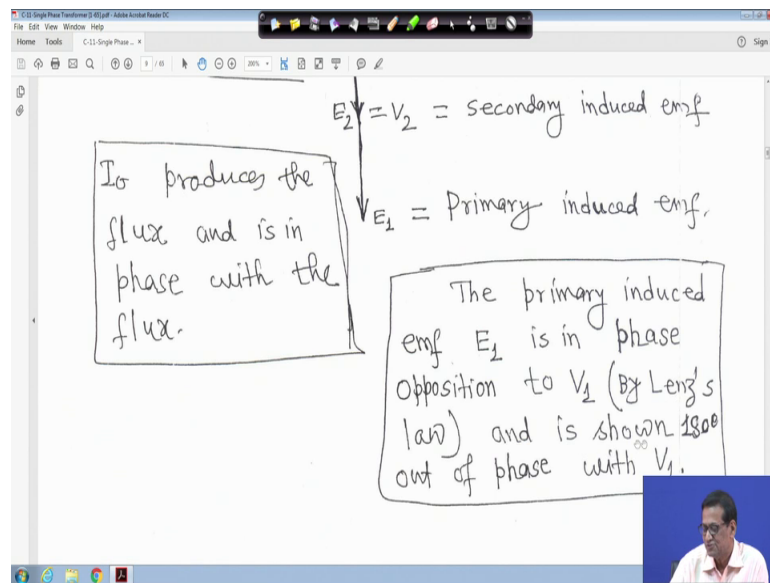
Therefore, my V_1 will be is equal to N_1 , ϕ is equal to ϕ_m your what you call the $\sin \omega t$ if you take the derivative it will be N_1 , then ϕ_m , then ω right, then $\cos \omega t$ right. So, that is that will be your what you call V_1 . So, if you your what you call this $\cos \omega t$ if you write like this for you just misunderstanding if you write like this some where I am writing hope you will be able to read it that your V_1 is equal to your N_1 then ϕ_m .

Then ω and this is $\cos \omega t$ usually you can write one is $\sin 90$ degree minus ωt another is your $\sin 90$ degree plus ωt ; that means, we can write \sin your ωt plus 90 degree right that is by V_1 . That means, this is my ϕ , ϕ is equal to ϕ

$m \sin \omega t$; that means, this V_1 actually leading this ϕ by 90 degree then V_1 is equal to minus E_1 .

So, this is my your E_2 this is E_1 and this is your V_1 is equal to minus E_1 . So, that then E_1 is the primary induced emf and E_2 is the see your E_2 equal to V_2 is equal to secondary induced emf. So, this is actually V_1 is equal to minus E_1 . So, basically your I_0 will be in phase now loss is neglected with the your in phase with your what you call is the flux ϕ , ϕ is the taken as a reference right therefore, let me clear it.

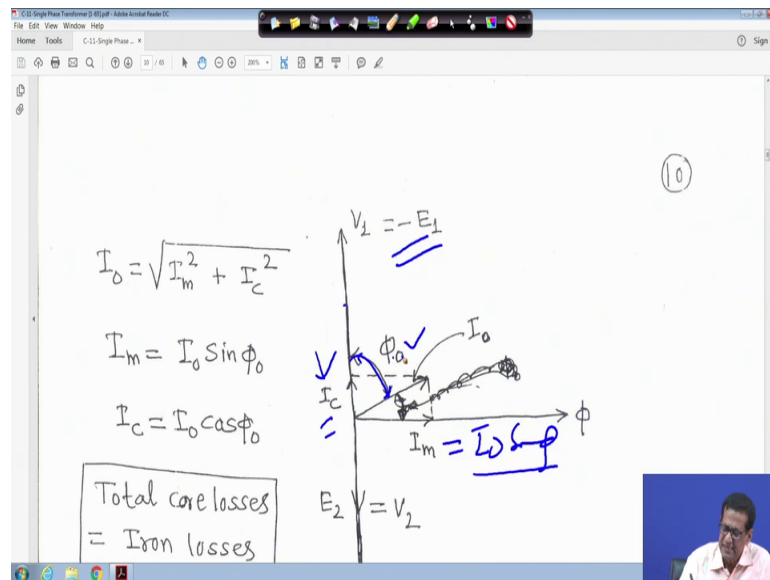
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Therefore, I_0 produces the flux and in the phase with the flux. Now the primary induced emf E_1 is in phase opposition to V_1 by Lenz's law and is shown 180 degree out of phase with V_1 . So, this is V_1 and this is V_1 is equal to minus E_1 so, 180 degree out of phase. So, this is Lenz's law and this Faradays all these things we have studied in your higher secondary physics right. So, this is how that your when we are not considering the losses so, this is the Phasor diagram.

Now, generally what happened in a transformer that heating of the core happens because of your what you call that energy losses due to your hysteresis and eddy currents right shows in the core. So, because of that some loss component will be there, if you consider the loss component then I_0 actually is not exactly lagging 90 degree from V_1 or not exactly is in phase with ϕ_1 there will be some lagging angle of I_0 . So, that is why your whenever you have such thing right that core in this in this case what will happen.

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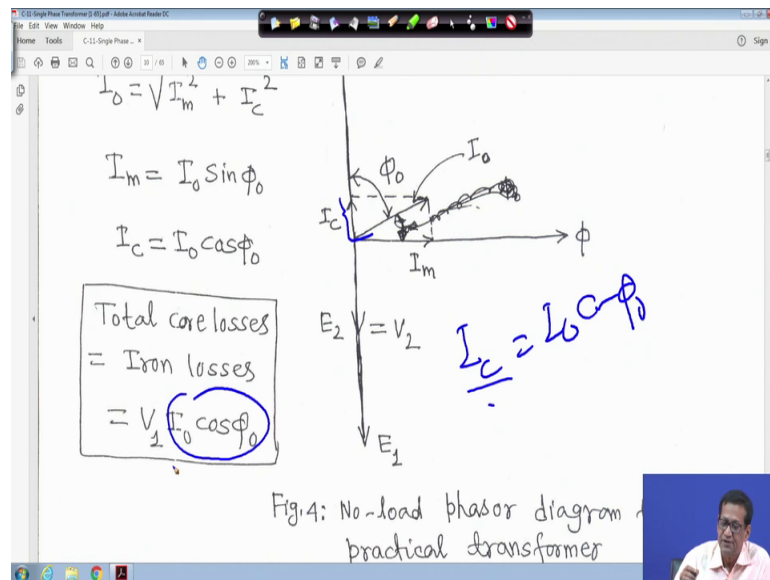


That you are this I_0 actually not exactly in phase in phase with I write because it has some core loss that is iron loss that is eddy current and hysteresis loss. So, because of that your this is V_1 is equal to minus E_1 is ok, but this I_0 actually lagging by an angle ϕ_0 from V_1 .

So, this angle is ϕ_0 and it is your what your call component along ϕ is I_m is equal to your $I_0 \sin \phi_0$, this component is responsible for producing that your no load flux because this is ϕ_0 . So, it is $\cos 90$ your what you call that I_0 is your I_m is equal to I_0 right it will be $\cos 90$ minus ϕ_0 . So, it is $I_0 \sin \phi_0$ and this I_c will be $I_0 \cos \phi_0$ right.

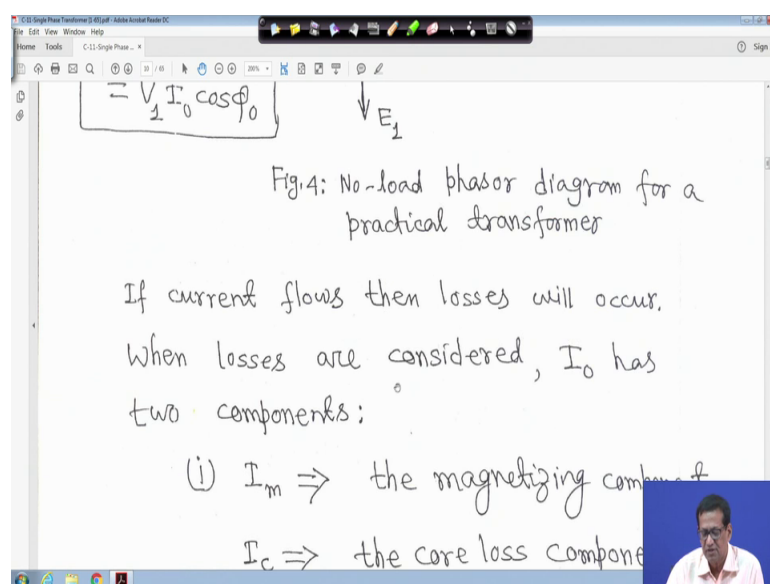
So, this component actually basically it will give your core loss or iron loss and the no load condition right. So, total core losses is equal to basically iron loss is this is the hysteresis and eddy current losses. So, that is why I_0 is not exactly is in phase with ϕ but this angle actually this angle $I \phi_0$ actually quite large so, that is total core loss.

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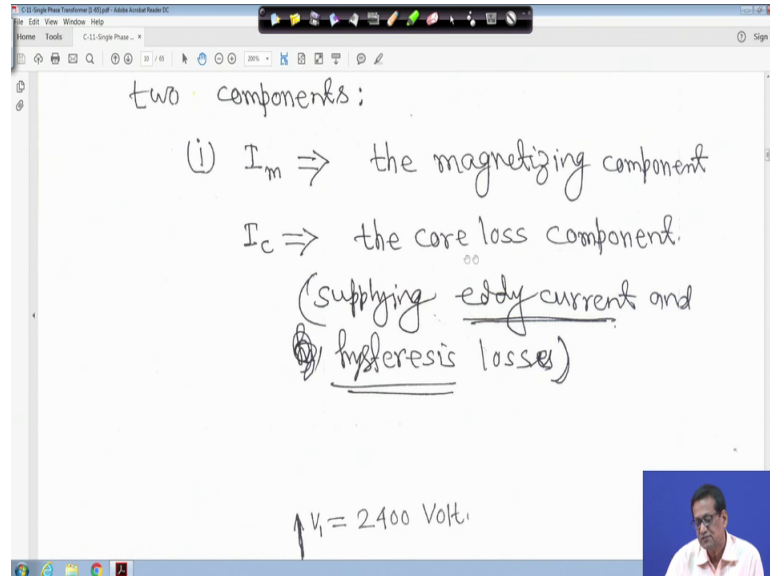
Is equal to iron loss is equal to $V_1 I_0 \cos \phi_0$ right and this and the I told you this $I_0 \cos \phi_0$ that is I_c actually is equal to $I_0 \cos \phi_0$; that means, this component; that means, the $I_0 \cos \phi_0$ actually is equal to your I_c ; that means, V_1 into I_c that is your total core loss or iron loss right. So, this is the no-load phasor diagram for a practical transformer.

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Now, if current flows then losses will occur when losses are considered I_0 has to 2 components I told you everything.

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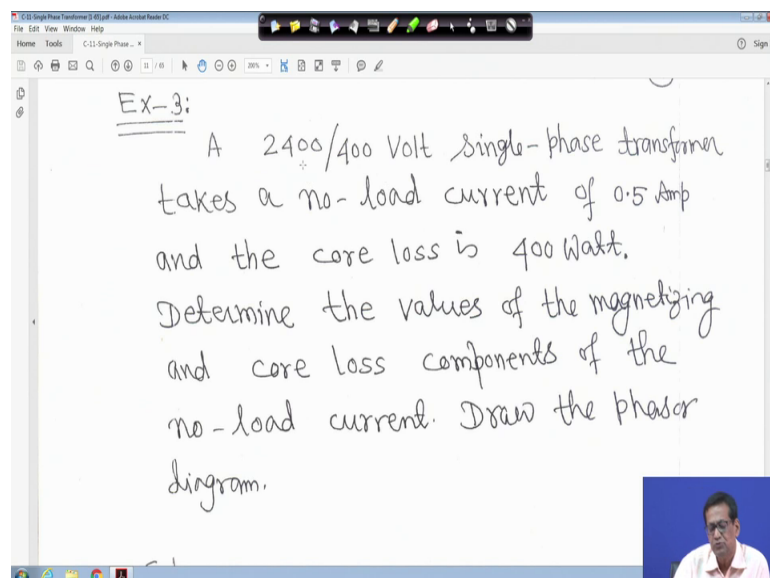
two components:

(i) $I_m \Rightarrow$ the magnetizing component
 $I_c \Rightarrow$ the core loss component.
(supplying eddy current and hysteresis losses)

$V_1 = 2400$ Volt.

I_m we call the magnetizing component and I_c the core loss components this magnetizing component at no load is responsible for producing the flux. So, eddy current loss that is core loss component basically is supplying eddy current and hysteresis losses. This eddy current and hysteresis in the magnetic circuit I have given you those formulas right so, this is nothing, later will come right.

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Ex-3:
A 2400/400 Volt single-phase transformer takes a no-load current of 0.5 Amp and the core loss is 400 Watt. Determine the values of the magnetizing and core loss components of the no-load current. Draw the phasor diagram.

So, now, this is for this numerical a 2400 by 400 volt is a step down transformer because this is primary side 2400 and secondary side 400 volts. So, this is a step down transformer right so, N_1 by N_2 actually is equal to 6 we call V_1 by V_2 . Single phase transformer takes a no load current of 0.5 ampere and the core loss is 400 watt that is core loss is given that is $V_1 I_0 \cos \phi_0$ that is your core loss 400 watt is given. Determine the value of the magnetizing and core loss component of the no load current and draw the phasor diagram.

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Soln.

$$V_1 = 2400 \text{ Volt} ; V_2 = 400 \text{ Volt} .$$

$$I_0 = 0.5 \text{ Amp.}$$

$$\text{Core loss (i.e. iron loss)} = 400 \text{ Watt.}$$

$$\therefore V_1 I_0 \cos \phi_0 = 400$$

$$\therefore 2400 \times 0.5 \cos \phi_0 = 400$$

$$\therefore \cos \phi_0 = \frac{1}{3} \therefore \phi_0 = 70.5^\circ$$

$$\text{Magnetizing component} = I_m = I_0 \sin \phi_0 =$$

So, it is given V_1 is equal to 2400 volt V_2 is given 400 volt I_0 is given 0.5 Ampere. So, core loss that is iron loss is equal to also given 400 watt, therefore, $V_1 I_0 \cos \phi_0$ is equal to 400 so, that is 2400 into 0.5 $\cos \phi_0$ is equal to 400.

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Core loss (w.r. iron loss) —

$$\therefore V_1 I_0 \cos \phi_0 = 400$$
$$\therefore 2400 \times 0.5 \cos \phi_0 = 400$$
$$\therefore \cos \phi_0 = \frac{1}{3} \therefore \phi_0 = 70.5^\circ$$

Magnetizing component = $I_m = I_0 \sin \phi_0 = 0.471 \text{ A}$

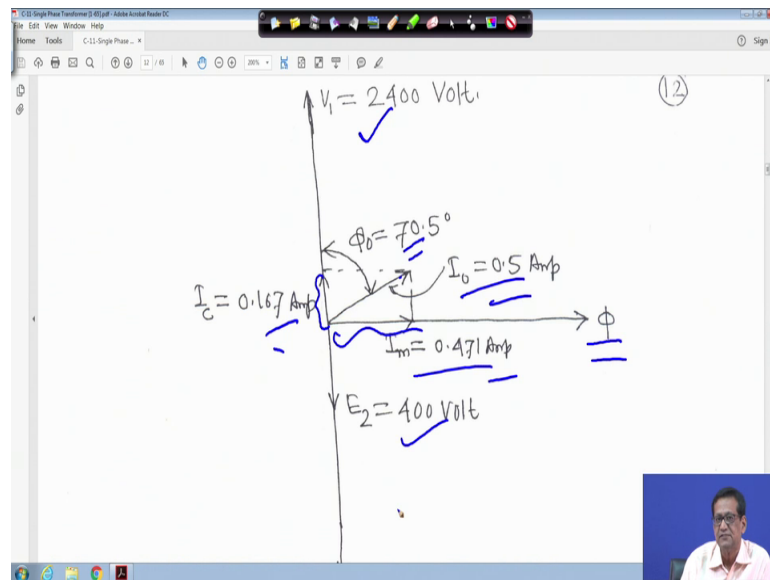
Core loss component = $I_c = I_0 \cos \phi_0 = 0.167 \text{ Amp}$

$$\underline{I_2} = I_c - j I_m = 0.167 - j 0.471$$

Therefore, we will get $\cos \phi_0$ is equal to one third therefore, ϕ_0 is equal to 70.5 degree. Now, magnetizing current I_m will be 0.471 A because ϕ_0 is equal to 70.5 degree and core loss component I_c will be 0.167 ampere. And as this current is lagging if you write in your phasor thing that your I_0 will be is equal to actually $I_c - j I_m$ right. So, I_c is equal to 0.167 and minus your $j 0.471$ right.

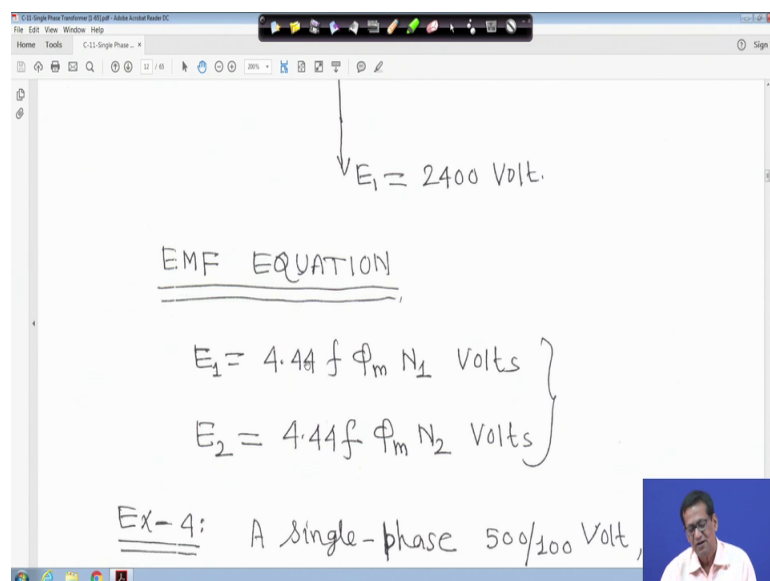
If you take your V_1 as a reference so, this current actually lagging from your what you call the voltage. So, it will be minus sign right this is your real part and this is your imaginary part this is core loss component current and this is your imaginary sorry magnetizing your called the imaginary part in the magnetizing component of the current.

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So, now this is the phasor diagram, this is your V_1 and this is your E_2 is equal to 400 volts, E_1 is also here and this angle is 70.5 degree and this is your this part is I_c and this part is your I_m and this is the resultant current I_0 right. So, this is simply and this is the ϕ the reference phasor right and E_1 is given here.

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E_1 is given here 2400 because it has to be balance ideal case it has to be balanced right so, it is 2400 volt here also it is showing 2400 volts right. Now, EMF equation these 2

equations also in the magnetic circuit in general I have given, E_1 is equal to $4.44 f \phi_m N_1$ volt and the secondary side also $4.44 f \phi_m N_2$ volts right. So, $N_1 N_2$ only trace difference or different, but equations are same right.

So, this emf equation is given actually in that magnetic circuit I have given. And if you take the rmf value we have to divide it what you call that your in the that your what you call in that magnetic circuit the divided by root 2 everything has been done there right.

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$$E_2 = 4.44 f \Phi_m N_2 \text{ Volts}$$

Ex-4: A single-phase 500/100 Volt, 50Hz transformer has a maximum core flux density of 1.5 Wb/m^2 and on effective core cross-sectional area of 50 cm^2 . Determine N_1 and N_2

$$N_1 = \frac{300}{5} = 60$$

$$\frac{V_1}{N_1} = \frac{V_2}{N_2} \Rightarrow \frac{500}{N_1} = \frac{100}{N_2} \Rightarrow N_2 = \frac{100}{500} N_1 = \frac{1}{5} N_1 = \frac{1}{5} \times 60 = 12$$

So, now if you take this example single phase 500 by 1000 volt 50 hertz then it will also a step down transformer because voltage is getting reduced on the secondary side has a maximum core flux density is 1.5 Weber per meter square and on effective core your cross sectional area of 50 centimeter square. Determine N_1 and N_2 , a very simple one.

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The screenshot shows a handwritten solution on a whiteboard. It starts with the word "Soln." underlined. The first equation is $\Phi_m = B \times A$. Below it, the values are given: $B = 1.5 \text{ Wb/m}^2$ and $A = 50 \text{ cm}^2 = 50 \times 10^{-4} \text{ m}^2$. The next line shows the calculation: $\therefore \Phi_m = (1.5)(50 \times 10^{-4}) = 75 \times 10^{-4} \text{ Wb}$. Then, it says "Since" followed by the equation $E_1 = 4.44 f \Phi_m N_1$. The final line shows the calculation for N_2 : $\therefore N_2 = \frac{E_2}{4.44 f \Phi_m} = \frac{500}{4.44 \times 50 \times 75}$. A small video inset of a man is visible in the bottom right corner of the whiteboard area.

You know flux is equal to B into A you have seen in a magnetic circuit this is B is the flux density and A is the cross sectional area. So, B is given 1.5 Weber per meter square and A is 50 centimeter square so, 50 into 10 to the power minus 4 meter square. Therefore, phi m is equal to 1.5 in to this your area is equal to 75 into 10 to the power minus 4 Weber. Since, E 1 is equal to 4.44 phi m N 1 you know that therefore, N 1 will be E 1 upon 4.44 f phi m that will be 500 divided by you substitute and the if even it is not mentioned; even if it is not mentioned right.

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The screenshot shows a handwritten solution on a whiteboard. It starts with the calculation: $\therefore \Phi_m = (1.5)(50 \times 10^{-4}) = 75 \times 10^{-4} \text{ Wb}$. Then, it says "Since" followed by the equation $E_1 = 4.44 f \Phi_m N_1$. A handwritten note in blue ink says $f = 50 \text{ Hz}$. The next line shows the calculation for N_2 : $\therefore N_2 = \frac{E_2}{4.44 f \Phi_m} = \frac{500}{4.44 \times 50 \times 75 \times 10^{-4}}$. An arrow points to the 50 in the denominator, and there is a double underline under the 75. The final line shows the calculation for N_2 : $\therefore N_2 = \frac{E_2}{4.44 f \Phi_m} = \frac{100}{4.44 \times 50 \times 75 \times 10^{-4}}$. A double underline is under the 300 in the previous line.

Generally, you take it is a 50 hertz system f it is equal to 50 hertz. So, that is f is equal to 50 hertz is taken and this is the phi m right you will get N 1 is equal to 300. Similarly, N 2 is equal to E 2 upon 4.44 f phi m that is 100 upon 4.44 50 hertz f is 50 hertz and this one you will get 60.

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The image shows a digital whiteboard with handwritten mathematical derivations for transformer turns ratios. The derivations are as follows:

$$\therefore N_1 = \frac{E_1}{4.44 f \phi_m} = \frac{4500}{4.44 \times 50 \times 75 \times 10^{-4}}$$

$$\therefore N_1 = 300$$

$$N_2 = \frac{E_2}{4.44 f \phi_m} = \frac{100}{4.44 \times 50 \times 75 \times 10^{-4}}$$

$$\therefore N_2 = 60$$

Ex-5: A 4500/225 Volt, 50 Hz single-phase transformer is to have an

So, basically you will get N 1 is equal to 300 and N 2 is equal to 60 in your what you call even without using this the voltage ratio is given your what you call V 1 upon V 2 is given your this is your V 1 upon V 2 is equal to say N 1 upon N 2 right and N and this is given actually 500 by 100 actually will 5. So, we have got N 1 we got is 300 therefore, N 2 is equal to your 300 by 5 here from here also we can get it N 2 is equal to 60 right. So, this is your N 2 is equal to 60.

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EX-5: A 4500/225 Volt, 50 Hz single-phase transformer is to have an approximate emf per turn of 15 Volt and operate with a maximum flux of 1.4 Wb/m². Calculate (a) the number of primary and secondary turns (b) cross-sectional area of the core.

So, thank you very much we will be back again.