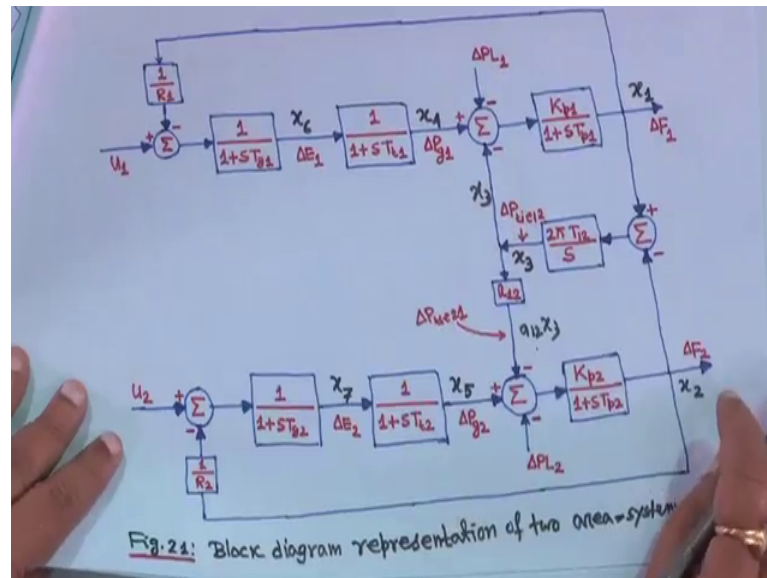


Power System Engineering
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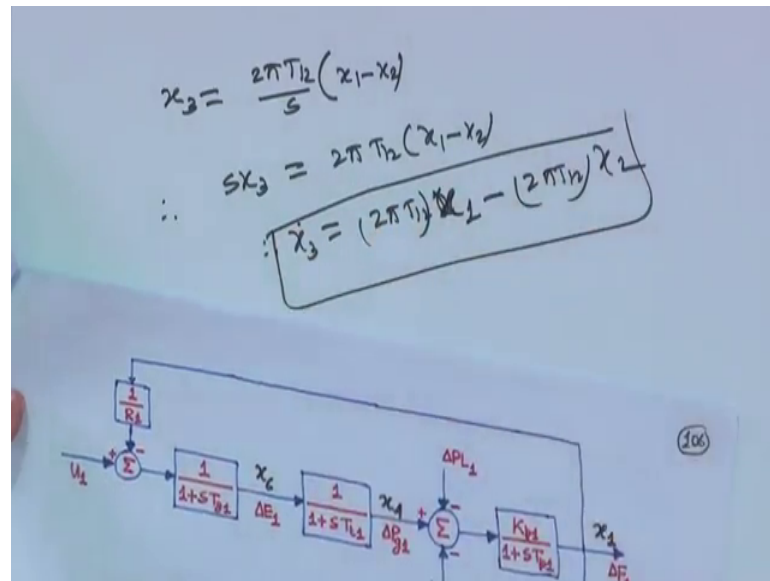
Lecture - 55
Load frequency control (Contd.)

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Next look all these things I am making it for you such that when you will go through you know it will be very easy for you to this thing even without looking into the book you can make it of your own right. So, now, next is x 3 next is x 3 this one right.

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So, in this case if you look in the block diagram it that x_3 is equal to x_3 is equal to $2\pi T_{12}$ upon s $2\pi T_{12}$ upon s into this is actually x_1 . So, this is x_1 and this is x_2 ; so into x_1 minus x_2 right. So, it is a plus x_1 it is minus x_2 x_1 minus x_2 right; that means, $s x_3$ is equal to $2\pi T_{12} x_1$ minus x_2 ; that means, x_3 dot is equal to $2\pi T_{12}$ x_1 minus $2\pi T_{12}$ into x_2 . So, this is your what you call x_3 dot. So, if you this is a third equation.

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From Fig. 2.1, state-variable equations can be written as:

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \\ \dot{x}_4 \\ \dot{x}_5 \\ \dot{x}_6 \\ \dot{x}_7 \end{bmatrix} = \begin{bmatrix} -\frac{1}{T_{p1}} & 0 & -\frac{K_{p2}}{T_{p1}} & \frac{K_{p2}}{T_{p1}} & 0 & 0 & 0 \\ 0 & -\frac{1}{T_{p2}} & -\frac{a_{12} K_{p2}}{T_{p2}} & 0 & \frac{K_{p2}}{T_{p2}} & 0 & 0 \\ 2\pi T_{12} & -2\pi T_{12} & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & -\frac{1}{T_{i2}} & 0 & \frac{1}{T_{i2}} & 0 \\ 0 & 0 & 0 & 0 & -\frac{1}{T_{i2}} & 0 & \frac{1}{T_{i2}} \\ -\frac{1}{R_1 T_{g2}} & 0 & 0 & 0 & 0 & -\frac{1}{T_{g2}} & 0 \\ 0 & -\frac{1}{R_2 T_{g2}} & 0 & 0 & 0 & 0 & -\frac{1}{T_{g2}} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \\ x_5 \\ x_6 \\ x_7 \end{bmatrix}$$

If you look at the third equation $\dot{x}_3$ is equal to $2\pi \times 12 \times 1$ minus $2\pi \times 1$ to x_2 rest of the your what you call elements are 0 right this is the third equation.

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$$\begin{bmatrix} 0 & 0 \\ 0 & 0 \\ \frac{1}{T_{p1}} & \frac{1}{T_{p2}} \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix} + \begin{bmatrix} -\frac{K_{p1}}{T_{p1}} \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} -\frac{K_{p2}}{T_{p2}} \\ 0 \\ 0 \end{bmatrix} \begin{bmatrix} \Delta PL_1 \\ \Delta PL_2 \end{bmatrix} \dots (31)$$

And similarly for the third row both your this is B matrix this is gamma matrix third row this is 0 this is also 0 right because no u are ΔPL is involved there next is your $\dot{x}_4$. So, this is my $\dot{x}_4$ this is my $\dot{x}_4$. So, $\dot{x}_4$ is equal to actually $\dot{x}_6$ upon 1 plus $s \tau_1$ right. So, this is $\dot{x}_4$.

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$$z_4 = \frac{x_6}{(1 + sT_{b1})}$$

$$\therefore x_4 + (sT_{b1})T_{b1} = x_6$$

$$\therefore \dot{x}_4 T_{b1} = -x_4 + x_6$$

$$\therefore \dot{x}_4 = -\frac{1}{T_{b1}} x_4 + \frac{1}{T_{b1}} x_6$$

So, I am making it this way if they look x_4 is equal to your x_6 divided by $1 + ST_{t1}$ right; that means, x_4 plus $s x_4$ into $Tt1$ is equal to x_6 .

That means this is actually x_4 dot therefore, x_4 dot is equal to minus x_4 x_4 dot $Tt1$ is equal to minus x_4 plus x_6 right; that means, here I am making it; that means, x_4 dot is equal to your minus 1 upon $Tt1$ x_4 plus 1 upon $Tt1$ x_6 . So, here also know you involve this is this is your x_4 dot here also know you involve low $\Delta p1$ is involve already these two elements will be there in that a matrix right. So, if you see the x_4 dot it is minus 1 upon $Tt1$ x_4 plus 1 upon $Tt1$ x_6 it will look minus all are 0, first three minus 1 upon $Tt1$ this into x_4 it fifth one is not there then one upon $Tt1$ your x_6 right 0 and similarly on the fourth row because know you know $\Delta p1$ is there. So, here it is 00 here also it is 00.

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$$x_5 = \frac{x_7}{(1 + ST_{t1})}$$

$$\therefore x_5 + (Sx_5)T_{t1} = x_7$$

$$\therefore \cancel{x_5} \therefore x_5 T_{t1} = -x_5 + x_7$$

$$\therefore x_5 = -\frac{1}{T_{t1}}x_5 + \frac{1}{T_{t1}}x_7$$

Next you consider that x_5 right that is your this one x_5 this one. So, similarly you can write x_5 is equal to x_7 upon $1 + ST_{t2}$; that means, we can write x_5 is equal to x_7 divided by one plus ST_{t2} then cross multiply. So, it will be x_5 plus Sx_5 $Tt2$ is equal to x_7 ; that means, this is your x_5 dot is equal to you know I let me make $Tt2$ here also x_5 dot $Tt2$ is equal to minus x_5 plus x_7 right therefore, x_5 dot is equal to minus 1 upon $Tt2$ x_5 plus one upon $Tt2$ x_7 right.

So, here also no you know ΔPL is involve only a matrix has to be filled a fifth element and the seventh one there is the if you look at the fifth row. So, first four as zero

it is minus 1 upon $T_t 2 \times 5$ minus one upon $T_t 2 \times 5$ this 1 minus 1 upon $T_t 2 \times 5$ plus sixth element is zero one upon $T_t 2 \times 7$. So, one upon $T_t 2 \times 7$ this is your fifth row and here also fifth one is here it is 00 because no u is involved and here also it is 00 because no disturbance thing is involved right. So, this is your x_5 then if you come to x_6 this one this one if you come right then just it will be like this rather than the writing on the notebook you are making note of this thing I thought I i will make it here such that it will be easy for you to understand right.

So, now $x_6 \times 6$ will be look this u_1 will be there it is plus minus this x_1 is coming here. So, this is your x_1 .

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$$x_6 = \left(u_1 - \frac{x_1}{r_1}\right) \times \frac{1}{(1+sT_{g1})}$$

$$\therefore x_6 + (sT_{g1})x_6 = -\frac{x_1}{r_1} + u_1$$

$$\therefore x_6 T_{g1} = -\frac{x_1}{r_1} - x_6 + u_1$$

$$\therefore x_6 = -\frac{x_1}{r_1 T_{g1}} - \frac{1}{T_{g1}} + \frac{1}{T_{g1}} u_1$$

So, basically it will be x_6 is equal to u_1 minus x_1 upon r_1 into 1 upon 1 plus $s t g_1$ right; that means, we can write that x_6 is equal to we can write x_6 is equal to u_1 minus your x_1 upon r_1 into your 1 upon 1 plus $s t g_1$ right. So, if you go for cross multiplication it will be x_6 plus your $s x_6$ into T_{g1} this one writing first minus x_1 upon r_1 plus u_1 right.

That means we can write $s x_6$ is x_6 dot right T_{g1} is equal to this one writing first minus x_1 by r_1 minus this one we are writing first x_6 plus u_1 therefore, your x_6 dot is equal to minus x_1 upon $r_1 T_{g1}$ minus 1 upon T_{g1} plus 1 upon minus 1 upon $T_{g1} \times 6$ then one upon $T_{g1} u_1$ right. So, this is the equation where I am making all sort of things by chance this is a recording thing right and continuously you have to move right if I make

any mistake anywhere if you observe throughout this course because many places I have tried to derive hope hoping that things are ok.

But if you see that any point or anything I have missed or something written you know incorrectly, but later hopefully it has been corrected right, but still you point out to me hopefully things are hopefully things are right. So, because in the nobody is sitting in front of me then they can rectify cell on the blackboard when you write if we miss any term immediately they point out sir you have missed the term right, but here nobody is there in front of me right. So, anyway. So, this x_6 dot will be your then this if you come to the sixth element then it will be a 6_1 will be minus 1 upon r_1 Tg_1 . So, if you come to that that it is x_1 . So, minus 1 upon r_1 Tg_1 .

Then you are directly come to the sixth element of that sixth row right because rest and between all that for your what you calls six two six three six four six five a six three six four your a 6_1 a 6_2 a 6_3 a 6_4 a 6_5 all are 0. So, all are actually 0 right these are 0 then sixth element is coming your minus 1 upon Tg_1 here minus 1 upon Tg_1 into x_6 and in the u that sixth element one upon Tg_1 u 1 is there. So, will go to the B matrix that sixth row B matrix this is a sixth row. So, here it is 1 upon Tg_1 it is 0 node delta PL is involve here. So, it is 0, but it is 1 upon Tg_1 right.

So, similarly if you write your last equation that is your x_7 right if you write the last equation x_7 look at here last equation if you write here x_7 . So, this is actually your x_2 this is x_2 . So, it is u_2 minus x_2 upon r_2 into 1 upon 1 plus Stg_2 is equal to x_7 . So, this one we can write that your x_7 is equal to from this from here.

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$$\begin{aligned}
 x_7 &= \left(u_2 - \frac{x_2}{R_2} \right) \times \frac{1}{(1+sT_{g2})} \\
 \therefore x_7 + (sT_{g2})x_7 &= -\frac{x_2}{R_2} + u_2 \\
 \therefore \dot{x}_7 T_{g2} &= -\frac{x_2}{R_2} - x_7 + u_2 \\
 \therefore \dot{x}_7 &= -\frac{x_2}{R_2 T_{g2}} - \frac{1}{T_{g2}} x_7 + \frac{1}{T_{g2}} u_2
 \end{aligned}$$

Only from here only right it is u_2 minus your x_2 upon R_2 into your one upon one plus sT_{g2} go for a cross multiplication it will be then x_7 plus $sT_{g2}x_7$ then T_{g2} writing this one first minus x_2 upon R_2 then we are writing u_2 right or $sT_{g2}x_7$ is equal to your $\dot{x}_7$ then T_{g2} is equal to this one writing first minus x_2 upon R_2 then after that this minus x_7 this one and plus u_2 right.

Or $\dot{x}_7$ is equal to minus x_2 upon $R_2 T_{g2}$ minus 1 upon T_{g2} times x_7 plus 1 upon T_{g2} times u_2 right this is your $\dot{x}_7$. So, u_2 is involved here u_2 is involved here other things is only a 72 and your what you call a 77 these two elements are there in the A matrix right. So, a 72 is minus one upon $R_2 T_{g2}$ and then this one a 77 minus 1 upon T_{g2} and last one is that it is your u_2 it is 1 upon T_{g2} u_2 is there. So, here it is 1 upon T_{g2} u_2 is there right therefore, it is 0 first one then 1 upon T_{g2} u_2 and here it is 00 and this is ΔPL_1 ΔPL_2 u_1 u_2 right.

So, this is equation 31 equation 31 means all together this one this is left hand side. It is $\dot{x}$ dot this matrix is x right and this one your Bu and this is γ if you observe one thing you will see because of this tie line power flow this one diagonal element is actually 0, but rest all are your what you call have a negative sign at least in the diagonal and because of this tie line that this one element is here is 0. So, this is a 7 into 7 matrix right and this is your 7 into 2 b matrix and this is γ matrix. So, this is say your 7 into 2

again. So, this is what you call that that you can write now $\dot{x}$ is equal to x plus Bu plus γp .

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Above equation can be written as:

$$\rightarrow \dot{X} = AX + BU + \Gamma p \dots (32)$$
$$\rightarrow U = \begin{bmatrix} u_1 \\ u_2 \end{bmatrix}; \quad p = \begin{bmatrix} \Delta PL_1 \\ \Delta PL_2 \end{bmatrix} \dots (33)$$

Where A is 7x7 matrix, B and Γ are 7x2 matrices, X , U and p are the state, control and disturbance vectors.

Now, that means, this equation is written as $\dot{x}$ is equal to x plus Bu plus γp in this form this is equation 32 where u is equal to u_1 u_2 and p is the disturbance vector ΔPL_1 upon ΔPL_2 where a is a seven into seven matrix I told you B and γ are 7×7 into 2 matrices x , u and p are the state control and disturbance vector right our state variable whatever we have chosen you can you alternate also or even interchange also this way that way no problem, but you will get the same result you will get the same result right. So, suppose if we want this equation is equal to $\dot{x}$ is equal to x plus Bu plus γp suppose it is uncontrolled.

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$$\begin{aligned}
 u &= 0 = \begin{bmatrix} u_1 = 0 \\ u_2 = 0 \end{bmatrix} \\
 \dot{x} &= Ax + Bu + \Gamma p. \\
 \therefore \dot{x} &= Ax + \Gamma p \\
 x' &= [x_1 \ x_2 \ x_3 \ x_4 \ x_5 \ x_6 \ x_7] \\
 \therefore x'_{ss} &= [x_{1ss} \ x_{2ss} \ x_{3ss} \ x_{4ss} \ x_{5ss} \ x_{6ss} \ x_{7ss}]
 \end{aligned}$$

Suppose u is 0 u is 0 means actually is equal to u_1 is equal to 0 u_2 is equal to 0 it is uncontrolled mode therefore, this equation $\dot{x}$ is equal to $Ax + Bu + \Gamma p$ right as u is 0; that means, this equation can be written as $\dot{x}$ is equal to say uncontrolled mode uncontrolled mode plus Γp it is uncontrolled mode when u is equal to 0 now at steady state I told you suppose steady state means suppose you are x I am making it as a transpose say x' x transpose your $x_1 \ x_2 \ x_3 \ x_4 \ x_5 \ x_6$ and x_7 right now this is transpose. So, it is steady state actually a steady state if you put this transpose this all will be $x_{1ss} \ x_{2ss} \ x_{3ss}$ all the steady state value x_{4ss} these were also you have seen for single area x_{6ss} and x_{7ss} right.

So, these are all the your what you call the steady state value. So, when all these things all these state variable reaches to a steady state the derivative is 0 the derivative is 0 right.

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$$\dot{x}_{ss} = \begin{bmatrix} \dot{x}_{1ss} \\ \dot{x}_{2ss} \\ \dot{x}_{3ss} \\ \dot{x}_{4ss} \\ \dot{x}_{5ss} \\ \dot{x}_{6ss} \\ \dot{x}_{7ss} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix} = 0$$

So; that means, I mean; that means, if you take I mean if I put like this rather than transpose now suppose if I make it like this x_{ss} is equal to your $x_{1ss} \times x_{2ss} \times x_{3ss} \times x_{4ss} \times x_{5ss} \times x_{6ss} \times x_{7ss}$ right these are the thing x_{ss} means steady state right $x_{1ss} \times x_{2ss} \times x_{3ss} \times x_{4ss} \times x_{5ss} \times x_{6ss} \times x_{7ss}$ right these are the thing x_{ss} means steady state if you make their dot suppose $\dot{x}_{ss}$ then if you $\dot{x}_{ss}$ then $\dot{x}_{1ss}$ steady state dot $\dot{x}_{2ss}$ dot dot dot dot dot all the steady state dot.

So, at steady state when all the state variables reach to a steady state means it will be 0000000 right all seven zeros are there. So, it will resist to restore to the steady state therefore, in this equation when you put x is equal to your x_{ss} ; that means, your writing on the next page.

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$$\begin{aligned}\dot{X}_{ss} &= AX_{ss} + \Gamma p. \\ \therefore 0 &= AX_{ss} + \Gamma p \\ \therefore AX_{ss} &= -\Gamma p. \\ \therefore X_{ss} &= -A^{-1}\Gamma p = 7 \times 1 \\ \begin{matrix} x_{1ss} \\ x_{2ss} \\ \vdots \\ x_{7ss} \end{matrix} &= \begin{bmatrix} 1 \\ 1 \end{bmatrix}\end{aligned}$$

That means your $\dot{X}_{ss}$ is equal to $s s$ plus γp ; that means, my this one actually this is 0 X_{ss} is steady state I told you that all the steady state values this will be actually is equal to 0 right. So, all $\dot{X}_{ss}$ will be 0 therefore, this 0 is equal to $A x_{ss}$ plus γp .

That means $A x_{ss}$ is equal to minus γp multiplied both sides by A inverse; that means, x_{ss} which will minus A inverse γp right only thing is that A inverse has to exist, but for this kind of system let me tell you A inverse exists; that means, you know A inverse it is a 7×7 matrix γ matrix is also known to you right and because they are p load disturbance is also known to you $p_1 p_2$ everything is known to you parameters are known to a matrix parameters are known to you; that means, if the this one actually it will be this will become a your what you call 7×1 right.

So, in that case your what you call this all the steady state values $x_1 x_2$ everything you everything will get I mean all the seven state variables whatever I have shown right all this your this thing your steady state values you will get. So, all these steadies, but at steady state this is actually $\dot{x}$ this is steady state values of all $x_1 x_2$ all.

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$$\dot{x}_{ss} = \begin{bmatrix} \dot{x}_{1ss} \\ \dot{x}_{2ss} \\ \dot{x}_{3ss} \\ \dot{x}_{4ss} \\ \dot{x}_{5ss} \\ \dot{x}_{6ss} \\ \dot{x}_{7ss} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix} = 0$$

$x_{1ss} \quad x_{2ss}$

You will get and; that means, the steady state values of all the values you will get all the seven state variables in MATLAB you can easily verify if you know the MATLAB take some parameter and just check you will get all these values right.

So, that is why what you call that this is easy way to find out the steady state value of course, that a inverse has to exist right it has to exist then only it is your only it is possible otherwise it is not possible right. So anyway, this will be a 7 into 7; that means, all the values whatever will get first one will become X_{ss} when X_{ss} second one x_{2ss} up to x_{7ss} whatever we will get this side all the steady state values will get you can easily verify in the MATLAB also right.

So, that is why this is your what we told that about $\dot{x}$ is equal to x plus Bu plus γp .

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The steady-state frequency deviation is the same for the two areas. At steady-state, $[u_1 = u_2 = 0, \text{Uncontrolled mode}]$

→ $\Delta F_1 = \Delta F_2 = \Delta F_{ss}$

and

→ $\Delta P_{g1}^{ss} - \Delta P_{tie,12}^{ss} - \Delta P_{L1} = D_1 \Delta F_{ss} \dots (34)$

→ $\Delta P_{g2}^{ss} - a_{12} \Delta P_{tie,12}^{ss} - \Delta P_{L2} = D_2 \Delta F_{ss} \dots (35)$

→ $\Delta P_{g1}^{ss} = \frac{-\Delta F_{ss}}{R_1} \dots (36)$

→ $\Delta P_{g2}^{ss} = \frac{-\Delta F_{ss}}{R_2} \dots (37)$

Now, now we have to go for this that is how told you how to go first steady state analysis for all the variables now mathematically we will see also from here same as before will proceed that the steady state frequency deviation is, but they are here you are getting you are what you call this steady state value whatever you are getting here directly all the numerical values, but we have to obtain some mathematical expression for that so; that means, at the steady state actually even it is a two area system as steady state that your delta F 1 actually is equal to delta F 2 is equal to delta F SS and we are considering this is uncontrolled mode that is I told you u_1 is equal to u_2 is equal to 0 uncontrolled mode written here in reading right.

So, this delta F 1 is equal to delta F 2 is equal to delta F SS, this is a steady state at steady state both the area steady state error is same therefore, for power balance equation that.

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$$\therefore \Delta P_{tie21} = a_{12} \Delta P_{tie12} \quad \text{--- (26)}$$

With reference to Eqn(20), incremental power balance equation for area-1 can be written as:

$$\Delta P_{g1} - \Delta P_{L1} - \Delta P_{tie12} = \frac{2H_1}{F_0} \frac{d}{dt} (\Delta F_1) + D_1 \Delta F_1 \quad \left[\begin{matrix} F_0 = f_0 \\ \Delta F_1 = \Delta f_1 \end{matrix} \right] \quad \text{--- (27)}$$

What you call that earlier this equation for power balance equation now look at that that at steady state it will be ΔP_{g1} s s do not disturbance will be there as it is it will be ΔP_{tie12} s s right from our general knowledge only we are trying to make it as steady state I told you that any derivative of any state will become 0. So, at d/dt of ΔF_1 one will be zero because it has these two the steady state and this will be actually ΔF_1 into ΔF_1 s s right.

A steady state this term will vanish because its derivative will become 0; that means, this equation ΔP_{g1} s s instead of P_{g1} you are making s s the steady state ΔP_{g1} s s minus ΔP_{tie12} s s minus ΔP_{L1} one is equal to d/dt of ΔF_1 SS right. This is actually coming from equation 27 similarly your this thing only this part will be vanished right.

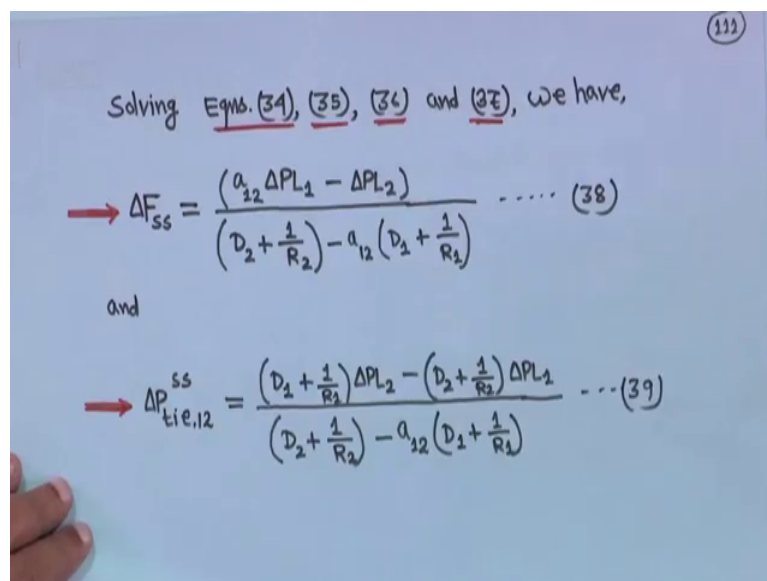
So, similarly what you call similarly for the area two if you write I told you that area two in the case of area two equation will remain same. It will be it will I did not write that one, but understandable it will be ΔP_{g2} minus ΔP_{L2} minus it will be ΔP_{tie21} . Hence it will be minus a_{12} into ΔP_{tie12} is equal to it will be $2H_2$ upon F_0 into d/dt of ΔF_2 plus D_2 into ΔF_2 for the area two understandable and again this part will be vanish for the area two and in that case it will become ΔP_{g2} s s minus ΔP_{tie21} s s actual is equal to minus a_{12} ΔP_{tie12} s s steady state error.

Here also for area two I told you how I will make it using minus delta PL 2 is equal to d 2 into delta F SS this is actually equation 35 right and we also know from isolated system same philosophy will be applied here the delta P g 1 steady state actually minus delta F SS upon R 1 in this in the case of your isolated case we have seen that delta P g s s actually is equal to minus delta F SS upon R, but here two area systematics. So, for area one delta P g 1 s s will be minus delta F SS upon r one and delta P g two s s is equal to minus delta F SS upon R 2 this is equation 36 this is equation 37.

Now, this delta P g 1 s s and delta P g 2 s s you substitute here that mean this equation will be function of delta F SS and delta P tie 12 s s s similarly delta P g 2 s s is equal to minus delta F SS upon R 2 this you substitute here here you will substitute then this equation will become function of your what you call delta P a your this you know it is in that in terms of delta P tie 12 s s and delta F SS. So, this equation also in terms of delta F SS and delta P tie 12 s s this equation also will become in terms of your delta F SS and delta P tie 12 s s they solve these two equations solve these two equations right.

So, I am not putting and showing it here it is understandable delta P g 1 s s you put it here right and make one equation and here also delta P g 2 s s you make it here make this a another equation and solve this right. So, if you solved it.

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(111)

Solving Eqs. (34), (35), (36) and (37), we have,

$$\rightarrow \Delta F_{ss} = \frac{(a_{12} \Delta PL_1 - \Delta PL_2)}{\left(D_2 + \frac{1}{R_2}\right) - a_{12} \left(D_1 + \frac{1}{R_1}\right)} \dots (38)$$

and

$$\rightarrow \Delta P_{tie,12}^{ss} = \frac{\left(D_1 + \frac{1}{R_1}\right) \Delta PL_2 - \left(D_2 + \frac{1}{R_2}\right) \Delta PL_1}{\left(D_2 + \frac{1}{R_2}\right) - a_{12} \left(D_1 + \frac{1}{R_1}\right)} \dots (39)$$

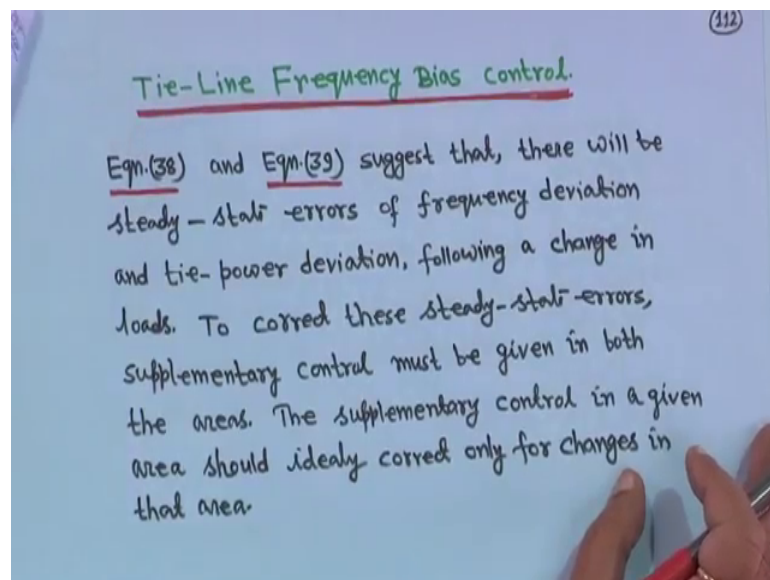
Because it is a linear equation solving. So, no need to do it you will be able to do it right. So, if you do. So, and solve it then that is why I am writing solving equation 34, 35, 36,

and 37 the way I told you will get ΔF_{SS} is equal to $\frac{1}{D_2 + 1} \Delta P_1 - \frac{1}{D_1 + 1} \Delta P_2$ right divided by $\frac{1}{R_2} - \frac{1}{R_1}$ this is equation 38.

That means at steady state uncontrolled mode two area system actually frequency deviation of both the areas are same right it is not ΔF_1 or ΔF_2 it will be same and type and ΔP_{tie} after solving those 2 equations you will get $\frac{1}{D_1 + 1} \Delta P_1 - \frac{1}{D_2 + 1} \Delta P_2$ divided by $\frac{1}{R_2} - \frac{1}{R_1}$. So, numerators are different, but denominator both cases it is same $\frac{1}{D_2 + 1} \Delta P_2 - \frac{1}{D_1 + 1} \Delta P_1$. This is equation 39; that means, uncontrolled mode at least these expressions are known to us right and if this expression is known to us means that is your ΔP_1 is equal to $-\Delta F_{SS} R_1$. So, you know the ΔF_{SS} you can easily find out ΔP_1 and ΔP_2 .

But this is the expression right you can solve it you please solve it of your own.

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And just get in this is simple thing right now once this is done ΔF_{SS} and ΔP_{tie} .

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(11)

Solving Eqs. (34), (35), (36) and (37), we have,

$$\rightarrow \Delta F_{ss} = \frac{(a_{12} \Delta PL_1 - \Delta PL_2)}{\left(D_2 + \frac{1}{R_2}\right) - a_{12} \left(D_1 + \frac{1}{R_1}\right)} \dots (38)$$

and

$$\rightarrow \Delta P_{tie,12}^{ss} = \frac{\left(D_1 + \frac{1}{R_1}\right) \Delta PL_2 - \left(D_2 + \frac{1}{R_2}\right) \Delta PL_1}{\left(D_2 + \frac{1}{R_2}\right) - a_{12} \left(D_1 + \frac{1}{R_1}\right)} \dots (39)$$

And just before moving further from this equation only suppose in area one disturbance is only there in area one this disturbance is there in area one and area two suppose disturbance ΔP_2 is equal to 0 there is no disturbance in the area one.

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$$\Delta PL_1, \Delta PL_2 = 0$$

$$\Delta F_{ss} = \frac{a_{12} \Delta PL_1}{\left(D_2 + \frac{1}{R_2}\right) - a_{12} \left(D_1 + \frac{1}{R_1}\right)}$$

$$\Delta P_{tie,12}^{ss} = \frac{-\left(D_2 + \frac{1}{R_2}\right) \Delta PL_1}{\left(D_2 + \frac{1}{R_2}\right) - a_{12} \left(D_1 + \frac{1}{R_1}\right)}$$

So, in that case this equation this equation will become ΔF_{ss} is equal to $a_{12} \Delta PL_1$ divided by d_2 plus 1 upon R_2 minus $a_{12} d_1$ plus 1 upon R_1 .

Similarly, in the tie power equation if your what you call ΔP_1 is your ΔP_2 is equal to 0 if ΔP_2 is equal to 0 in the tie power equation then it will be it ΔP_{tie}

12 steady state is equal to right delta P 1 2 is 0. So, this term will not be there it is minus your d 2 plus 1 upon R 2 delta P 1 1 divided by same thing same denominator minus a 12 d 1 plus 1 upon R 1 right. So, this is your what you call a expression for this one.

Now, we know we know for example, everything we are talk this is in hertz this is this is actually in hertz and this is in per unit megawatt right this is not in per unit this is in hertz and this is in per unit megawatt now if we know.

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The image shows handwritten mathematical derivations on a whiteboard. The first equation is:

$$\Delta F_{ss} = \frac{a_{12} \Delta P_{12}}{(D_2 + \frac{1}{R_2}) - a_{12} (D_1 + \frac{1}{R_1})}$$

The second equation is:

$$\Delta P_{12}^{ss} = \frac{-(D_2 + \frac{1}{R_2}) \Delta P_{11}}{(D_2 + \frac{1}{R_2}) - a_{12} (D_1 + \frac{1}{R_1})}$$

The third equation is:

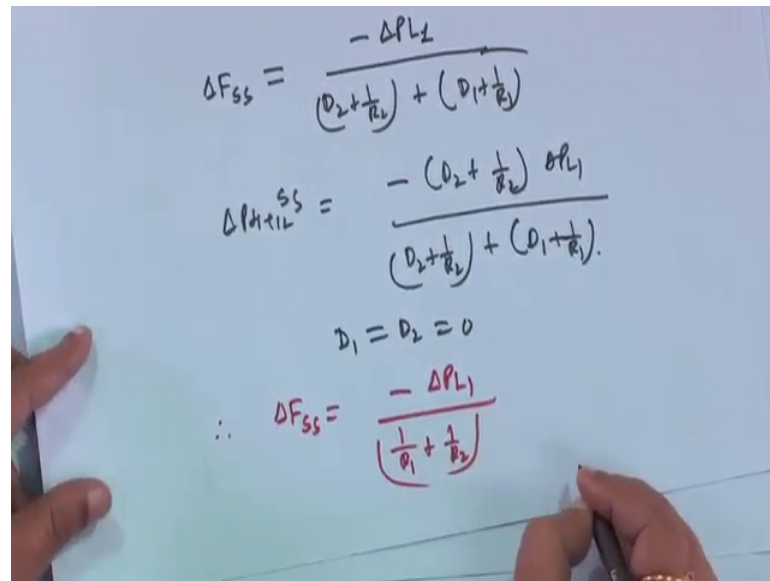
$$a_{12} = -\frac{P_{r1}}{P_{r2}} \quad \left| \quad P_{r1} = P_{r2} \right.$$

The final conclusion is:

$$\therefore a_{12} = -1.$$

We have seen know a 12 is equal to minus P r 1 upon P r 2 right; that means, if we assume let assume area capacity ratio P r 1 P r 2 is equal to 1 there is P r 1 is equal to P r two that is their same; that means, a 12 is equal to minus 1. So, if we put here a 12 is equal to minus 1 here you put in this here, here, here, also here you put minus 1.

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$$\Delta F_{ss} = \frac{-\Delta P_{L1}}{(D_2 + \frac{1}{R_2}) + (D_1 + \frac{1}{R_1})}$$

$$\Delta P_{12}^{ss} = \frac{-(D_2 + \frac{1}{R_2}) \Delta P_{L1}}{(D_2 + \frac{1}{R_2}) + (D_1 + \frac{1}{R_1})}$$

$$D_1 = D_2 = 0$$

$$\therefore \Delta F_{ss} = \frac{-\Delta P_{L1}}{(\frac{1}{R_1} + \frac{1}{R_2})}$$

If you do. So, then you will get delta F steady state is equal to minus delta P 1 one divided by D 2 plus one upon R 2 and a 12 is minus 1 it will be then plus right. So, it will be plus D 1 plus 1 upon R 1 similarly delta P tie 12 s s here only it will be minus 1. So, it will be plus right therefore, delta P tie 12 steady state is equal to your minus D 2 plus 1 upon R 2 right then into delta P 1 1 divided by D 2 plus 1 upon R 2 plus your D 1 plus 1 upon R 1 right now suppose you assume load is insensitive to the changes in frequency; that means, just for the sake of clarification some understanding say D 1 is equal to d 2 is equal to 0 say load is insensitive to changes in frequency.

If D 1 is equal to D 2 is equal to your 0 right then your delta F SS will be minus delta P 1 1 as D 1 D 2 is equal to 0 it will be one upon R 1 plus 1 upon R 2 right similarly here also if D 2 is 0 D 1 D 2 both are 0.

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$$\Delta P_{tie12}^{ss} = \frac{-\Delta P_1}{\left(\frac{1}{R_2} + \frac{1}{R_1}\right)}$$

$$R_1 = R_2 = R$$

$$\Delta F_{ss} = - \frac{2\Delta P_1 \cdot R}{2}$$

Then ΔP_{tie12} steady state ΔP_{tie12} here ΔP_{tie12} will be minus ΔP_1 divided by R_2 and here it will be $\frac{1}{R_2} + \frac{1}{R_1}$ this is ΔP_{tie12} and this is ΔF_{ss} right.

So, if you take if you take say R_1 is equal to R_2 is equal to R same value if you take right so; that means, ΔF_{ss} will become minus 2 ΔP_1 sorry minus your R into ΔP_1 right divided by two right you take R_1 is equal to R_2 is equal to R . So, it will be your minus R into ΔP_1 upon two similarly for tie power similarly for tie power if you take their same.

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$$\begin{aligned}
 R_1 &= R_2 = R, \\
 \Delta F_{ss} &= - \frac{2 \Delta L_1}{2} \cdot \frac{R \cdot \Delta L_1}{2} \\
 \therefore \Delta F_{ss}^{ss} &= \frac{- \frac{\Delta L_1}{R}}{\frac{2}{R}} \\
 &= - \frac{\Delta L_1}{R} \times \frac{R}{2} = - \frac{\Delta L_1}{2}
 \end{aligned}$$

Then delta P tie one two s s steady state is equal to it is minus delta PL 1 divided by R we have taken both are same it will be two by R right; that means, minus delta PL 1 upon R right into R by 2.

So, it will be minus delta PL 1 by 2 right; that means, when D 1 D 2 is equal to 0 and both are your what you call R 1 is equal to R 2 is equal to R. So, if we write and separately then what will happen.

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$$\begin{aligned}
 D_1 &= D_2 = 0 & P_{Y1} &= P_{Y2} \\
 R_1 &= R_2 = R & q_{12} &= -1 \\
 \Delta F_{ss} &= - \frac{R \cdot \Delta L_1}{2} \\
 \Delta F_{ss}^{ss} &= - \frac{\Delta L_1}{2} \\
 \Delta L_1 &= 0.01 \\
 R &= 2.4 \\
 \Delta F_{ss} &= - \frac{2.4}{2} \times 0.01 = -1.2 \times 0.01 \\
 &= -0.012 \text{ Hz}
 \end{aligned}$$

That steady state error ΔF_{SS} is equal to you will get here minus minus sign is here right here it is minus r into ΔP_{L1} upon 2 and for tie line power ΔP_{tie12} steady state is equal to minus ΔP_{L1} upon 2 this is actually this will be very helpful for the numerical point of view. So, what we have done is conditioned here what we have taken we have taken D_1 is equal to D_2 is equal to 0. We have taken R_1 is equal to R_2 is equal to R in addition to that P_{r1} is equal to P_{r2} .

Such that a 12 is equal to minus 1 right now for example, if ΔP_{L1} is equal to say 0.01 right and R is equal to 2.4 hertz per unit megawatt right therefore, your steady state value ΔF_{SS} will be minus 2.4 by 2 into 0.01 right. So, you will get it is your minus is equal to minus 1.2 into 0.01. So, minus 0.012 hertz right. So, this is the steady state value.

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Handwritten notes on a blue background showing the calculation of steady state frequency error and tie line power. The notes include the following equations and values:

$$D_1 = D_2 = 0$$

$$R_1 = R_2 = R$$

$$P_{r1} = P_{r2}$$

$$\Delta F_{SS} = -\frac{R \cdot \Delta P_{L1}}{2}$$

$$\Delta P_{tie12}^{SS} = -\frac{\Delta P_{L1}}{2}$$

$$D_1 = D_2 = \frac{1}{K_D} = \frac{1}{120}$$

$$\Delta P_{L1} = 0.01$$

$$R = 2.4$$

$$\Delta F_{SS} = -\frac{2.4 \times 0.01}{2} = -1.2 \times 0.01 = -0.012 \text{ Hz}$$

$$\Delta P_{tie12}^{SS} = -\frac{0.01}{2} = -0.005 \text{ pu MW}$$

And for tie power making it here for tie power it will be ΔP_{tie12} steady state is equal to minus 0.01 by 2 per unit megawatt is equal to minus 0.005 per unit megawatt.

So, this will be very helpful for your numerical point of view just have a have some your this thing and if you consider that a D value D value I mean D_1 D_2 is equal to 1 upon your what you call K_P is 121 upon K_P . So, 1 upon 120 if you take D_1 is equal to D_2 is equal to 1 upon K_P and K_P is 120 means 1 upon 120 then you will get this value is slightly less. It will become minus 0.0117 hertz or if I recall correctly right, but this is a good approximation I mean very close actually and this is also.

Thank you very much, we will be back.