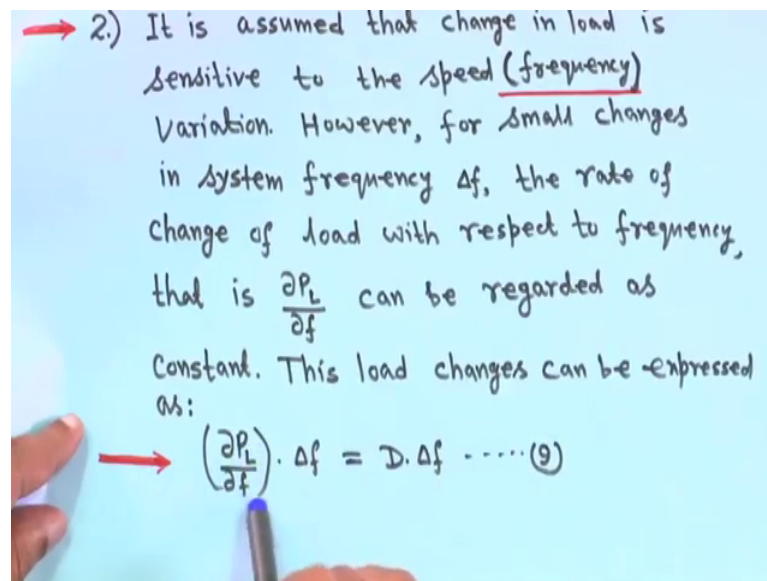


Power System Engineering
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Lecture - 48
Load frequency control (Contd.)

So this equation we have seen this is equation 8. Now another thing is that it is assumed that change in load is sensitive with the speed at frequency variation, we are assuming the load is frequency sensitive it is not insensitive to the frequency, we are assuming that load is frequency sensitive right. However, for small changes in system frequency Δf because, Δf change is very small right that. The rate of change of load with respect to frequency that is your ΔP_L upon Δf can be regarded as constant right, then ΔP_L Δf will be regarded as a it can be regarded as a constant.

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Although we are, but we are assuming that load is sensitive to the change in frequency therefore, this load changes can be expressed as your ΔP_L upon Δf into Δf this we are taking as a constant and, we are assuming that due to this is due to the your very small change in Δf , this is very small into Δf and, these we define actually D into Δf this is equation 9. If you do not consider that D is equal to 0 later we will see, but we will assume that load is sensitive. So, change in frequency.

So, in that case ΔP_L upon Δf can be regarded as a constant right how we will take that later will come later, we will take numerical small example will come right.

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Therefore, the power balance equation can be written as:

$$\rightarrow \Delta P_g - \Delta P_L = \frac{2H P_r}{f_0} \frac{d}{dt}(\Delta f) + D \Delta f$$

$$\therefore \frac{\Delta P_g}{P_r} - \frac{\Delta P_L}{P_r} = \frac{2H}{f_0} \frac{d}{dt}(\Delta f) + \frac{D}{P_r} \Delta f$$

$$\rightarrow \therefore \Delta P_g(pu) - \Delta P_L(pu) = \frac{2H}{f_0} \frac{d}{dt}(\Delta f) + D(pu) \Delta f \quad \dots(10)$$

So, this is your D into Δf therefore, the power balance equation therefore, the power balance equation this one ΔP_g minus ΔP_L it has 2 terms, 1 is the rate of change of kinetic energy that is $2H$, you know rate of change of kinetic energy means $\frac{d}{dt}$ or what we will call the power. So, $2H P_r$ upon $f_0 \frac{d}{dt}$ upon Δf plus that D into Δf term the previous equation; that means, this term this term right.

So, look we will take Laplace transform on both sides later, but except using S in that your (Refer Time: 02:07) time constant. Nowhere I will put $\Delta P_g S$ or $\Delta P_L S$ or your $\Delta f s$, it is understandable to you see. If we put everywhere S it will be you know little bit clumsy; so, I do not want that. Now what do you do this equation both side you divide by P_r right both side P_r . So, this is ΔP_g upon R minus ΔP_L upon R this P_r you divide is gone. So, it is $2H$ upon $f_0 \frac{d}{dt}$ upon Δf plus D upon P_r into Δf .

So, if you assume this is a base value then ΔP_g upon it is megawatt of course, ΔP_g upon Δf it is in per unit minus ΔP_L it is also per unit then $2H$ upon $f_0 \frac{d}{dt}$ upon this Δf is in hertz right this Δf remember hertz f_0 is hertz 18 second here no unit change it is in hertz. And D will be your what you call in per unit because this D is equal to your ΔP_L upon Δf and you are dividing it by P_r .

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$$D = \frac{\partial P_L}{\partial f}$$

$$\therefore \frac{D}{P_r} = \frac{(\frac{\partial P_L}{\partial f})}{P_r}$$

$$= W_{ke} \left(\frac{f_0^2 + 2f_0 \cdot \Delta f}{f_0^2} \right)$$

$$= W_{ke} \left(1 + \frac{2}{f_0} \cdot \Delta f \right)$$

$$= W_{ke} \left(1 + \frac{2\Delta f}{f_0} \right)$$

There

So, delta P R will be delta P L upon your P R delta P L upon delta f right into 1 upon P r. So, delta P L upon this P L delta P L P R it will become per unit that is why this and this, but this will remain hertz frequency will be hertz right; that means, unit of D will be per unit megawatt per hertz. So, that is why this D here is written in per unit; so, d is also per unit into delta f this is written right this is equation 10.

So, next is your that; that means, your next one just hold on therefore, if you if you take the Laplace transform both this after this; this delta P g, delta P L D all is in per unit. So, again and again this per unit will not be writternable, but equation 10 onwards; all these values unless and until I mention all are in per unit only right.

But again and again I will not write per unit then things will become clumsy; I do not want that, but equation 10 onwards, everything is in per unit and frequency of course, is in hertz, H will remain second, f 0 also will remain in hertz right, but this delta P g value delta delta P L value D all are in per unit right. So, again and again I will not write, but understandable.

So, if you and every time I will not put delta P g S delta P L S or delta fs right because it is Laplace transform understandable; such that in mathematics writing will be easier right so, but it is understandable. So, you take the Laplace transform of this equation both side you take the Laplace transform; if you can simplify you take the Laplace transform and then you simplify if you if you if you do so.

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Taking the Laplace transform of Eqn. (20), we get,

$$\rightarrow \Delta f = \frac{\Delta P_g - \Delta P_L}{D + \frac{2H}{f_0} s}$$
$$\rightarrow \therefore \Delta f = [\Delta P_g - \Delta P_L] \times \frac{K_p}{(1 + sT_p)} \dots\dots (21)$$

Where

$$\rightarrow T_p = \frac{2H}{Df_0} = \text{power system time constant}$$
$$\rightarrow K_p = \frac{1}{D} = \text{Gain of power system.}$$

If you do so, then you will get Δf is equal to ΔP_g minus ΔP_L upon D plus $2H$ upon f_0 into S this you know now right. So, because if you take that this equation that this is a Laplace transform it will be S into initial conditions are 0 you assume right; S into your Δf s, but S I mean bracket you are what to call not considering then again and again for all the variables I have to put; so, you do not want that right. So, it is your $2H$ upon f_0 S into Δf and this will be D into this thing all these things in take the Laplace transform and simplify right.

So, if you do so, it will become Δf will become ΔP_g minus ΔP_L divided by D plus $2H$ upon f_0 into S ; this way it will come. Or you can what you can do is this one you further simplify; that means, this how this thing is coming that Δf is equal to ΔP_g minus ΔP_L into K_p upon $1 + sT_p$ how things are coming from this equation. Numerator and denominator you divide it by D right if you I mean let me write for you.

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$$\Delta f = \frac{(\Delta P_g - \Delta P_L)}{\left(D + \frac{2H}{f_0} s\right)}$$

$$\therefore \Delta f = \frac{(\Delta P_g - \Delta P_L) \times \frac{1}{D}}{\left(1 + \frac{2H}{D f_0} s\right)} = \frac{K_p}{(1 + s T_p)} (\Delta P_g - \Delta P_L)$$

$$K_p = \frac{1}{D}$$

$$T_p = \frac{2H}{D f_0} \text{ sec.}$$

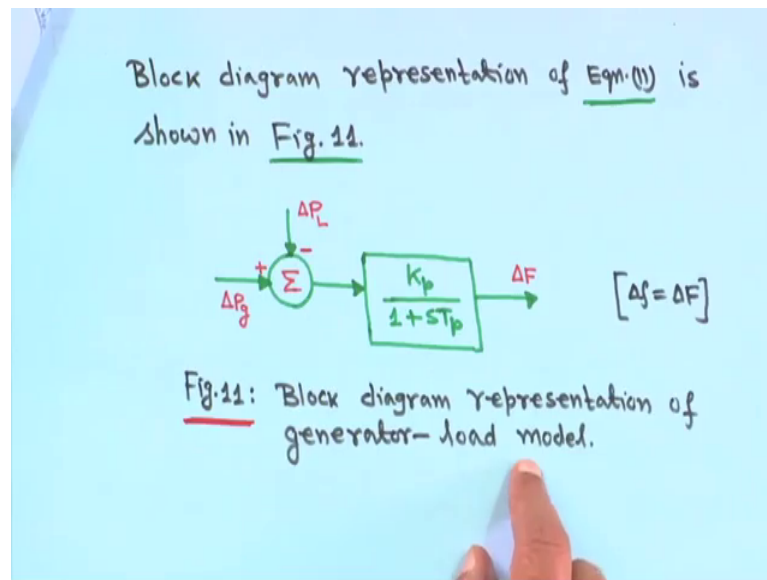
This is actually the equation Δf is equal to ΔP_g minus ΔP_L divided by D plus $2H$ upon $f_0 S$ this is the equation. Numerator and denominator you divided by D then Δf will be is equal to ΔP_g minus ΔP_L into 1 by D right divided by D divide it will be 1 plus $2H$ divided by your $D f_0$ into S right. You define K_p is equal to 1 upon D and T_p , you call T_p is the power system time constant it is $2H$ upon $D f_0$ this will be in second right.

So, if you define this then this equation will become K_p upon 1 plus $S T_p$ into ΔP_g minus ΔP_L ; just hold on this is your K_p upon 1 plus $S T_p$ into ΔP_g minus ΔP_L right. So, same thing just I have written left hand side here it is your right hand side. So, this Δf is equal to ΔP_g minus ΔP_L into K_p upon 1 plus $S T_p$; this is equation 11.

So, here T_p is equal to your power system time constant $2H$ upon $D f_0$ and K_p is equal to 1 upon D is equal to we call sometimes gain of power system. So, with this governor transfer function we got, turbine got and this generator we got right. This is actually sometimes we call this is power system transfer function or generator transfer function right.

Once you get it; then you combine governor turbine and generator because here we have also related everything ΔP_g we have related to Δf of course, ΔP_L is there right. So, this one; this one if you represent in a small block diagram; so, this is ΔP_g .

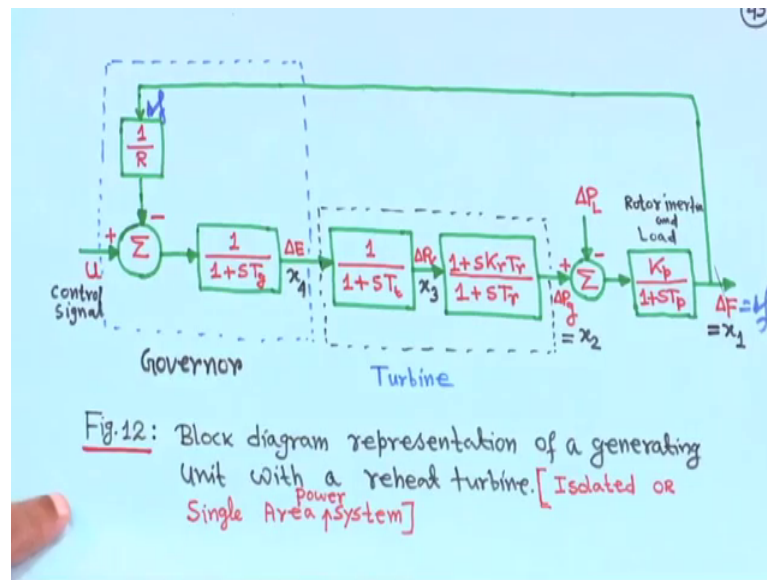
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And this is ΔP_L ΔP_L is minus sign ΔP_g plus because ΔP is minus into this one then the block diagram $\frac{K_p}{1 + sT_p}$ that is Δf ; small Δf capital they are same; I have written here right.

This is the block diagram represent our generator load model; sometimes we call this part we call sometimes power system model also right; so, this part. So, ΔP_g we have related with the turbine your what you call turbine power output right ΔP_g ; then that one also related to ΔE governor output. And then finally, Δf was the input and u write; so, all these things we have made it.

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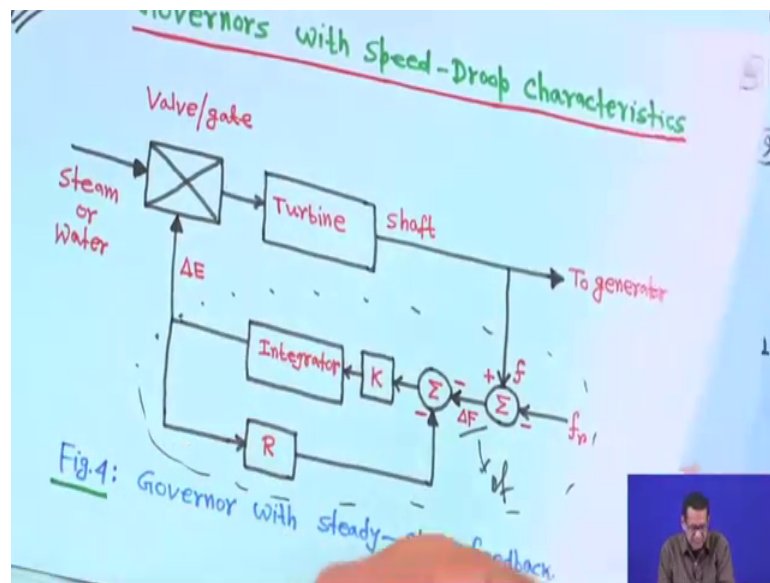
Now if you combine; now, it will be like this because this block this governor one you got it know u minus $\Delta f R$ upon this one this is ΔE . Let me just one minute just you go now one after another right. Then just see this part this is the governor part, this we have made it just a hold on I will show you I will show you just hold on.

This is this is your speed regulation parameter R just hold on these such that you will have a good feeling about this that how we actually develop the model right just hold on if just if I can make it once again here right. So, this is your turbine part first let me show you, this is your turbine part this is your turbine part 1 plus $S K S K r$ upon 1 plus $S T T$ into 1 plus $S T r$ $\Delta P g$ and ΔE E is the input $\Delta P g$ is the output. So, this is $\Delta P g$ is the output, ΔE is the input and this term is added here right.

So, these 2 terms are there; so, you have broken it right because of that state variable form. So, this is actually in between one variable is added $\Delta P g$ right, but this is the 2 and ΔE and this one just now we have made it no Δf smaller or capital does not matter $\Delta P g$ minus $\Delta P L$ into this one just now we have made it. And this one already we have made it no ΔE into u minus 1 upon R 1 upon 1 plus $S T g$ and this is input was Δf also in that block diagram it was shown you write all these things you just make it and just add it no it is completing a closed loop frequency or closed loop your what you call transfer function.

So, just 1 minute if I get it to immediately I will show you just 1 minute if it is here or not just 1 minute if I get it I will show you this is your turbine model; this is just hold on if I get it I will show you again just hold on. Here this speed this one we took that speed changer was not shown were speed changer was not shown here.

(Refer Slide Time: 11:15)



But somewhere I made a speed changer also and this one is a final block diagram; somehow it has been missed somewhere here right.

But this already we have derived u minus I derived for u also here I derived for u this one this one I have derived for u ΔE is equal to u minus Δf it is in front of me actually right into 1 upon this one also derived this one also derived. So, this was also clubbed together and its input was Δf now, in the input was Δf .

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$$\begin{aligned}
 \therefore s \Delta E &= -K \Delta F \\
 s \Delta E + RK \Delta E &= R \cdot K U - K \cdot \Delta F \\
 (s + RK) \Delta E &= (R \cdot K) U - K \cdot \Delta F \\
 \therefore \left(1 + \frac{s}{RK}\right) \Delta E &= \frac{RK}{RK} U - \frac{K}{RK} \Delta F \\
 \therefore (1 + sT_2) \cdot \Delta E &= U - \frac{1}{R} \Delta F \\
 \therefore \Delta E &= \frac{U}{(1 + sT_2)} - \frac{1}{R(1 + sT_2)} \Delta F \\
 \therefore \Delta E &= \left(U - \frac{\Delta F}{R} \right) \times \frac{1}{(1 + sT_2)}
 \end{aligned}$$

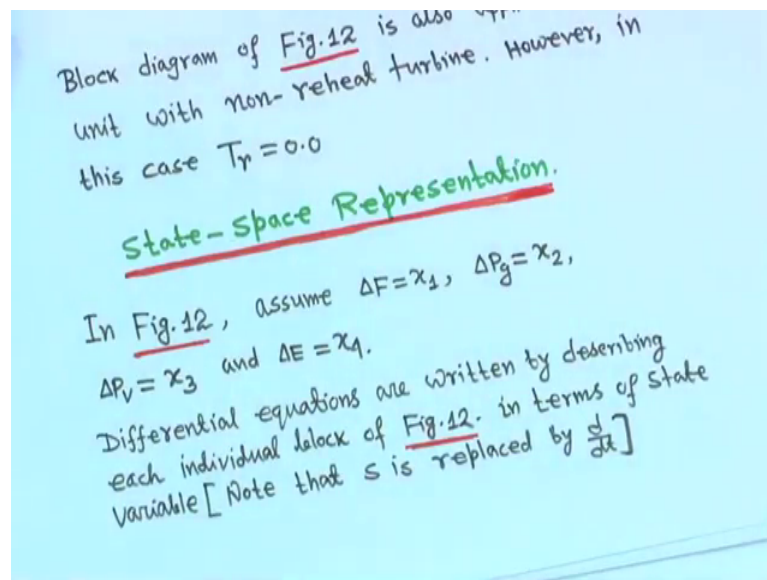
So, this delta f; this delta f is equal to same thing small delta f right. So, this is your delta f same thing; so, this is coming here this delta f actually coming from here. So, this is a closed loop system; so, with this is a block diagram representation of a generating unit with a reheat turbine it is isolated or single area power system what is area will come later.

So, this is actually what you call that isolated power system; this is governor, this is turbine and this is your power system. So, this is actually I have written rotor inertia load right, this is this dashed portion is turbine and this portion is governor and this is u is your control signal actually. So, now, what we will do this with this one we have got this block diagram. Now what we will do is that we have to what you call we have to go for state press representation and then we will see the steady state error and other things.

So, what you do? This we have to make it in the form of \dot{x} is equal to ax plus bu right that way you have to make it. So, this one we have taken out this output is taken as x_1 right, this delta P g is taken as x_2 in between because you have to make it a state variable this output of this one you have taken as x_3 and this one output of this governor time (Refer Time: 13:15) this is x_4 right and this is u this thing. So, we have to write down and assuming that all the initial conditions are 0. So, we have to write down \dot{x}_1 , \dot{x}_2 , \dot{x}_3 and \dot{x}_4 .

And I have to put we have to put it in the state variable form right. So, what we will do is that in the state place representation this all these things are shown here. Delta has been taken as x_1 , delta P g taken as x_2 this I have given a name delta P V x_3 and delta E as x_4 this 4 state variables right.

(Refer Slide Time: 13:45)



So, all these things are given here delta f x_1 , delta P g is actually x_2 delta P V x_3 and delta E x_4 . So, differential equation are written by your describing each individual block of figure 12, this is figure 12, this is figure 12 right in terms of state variable note that s is replaced by d/dt because it is in a Laplace transform. So, what will do that you write all the equations \dot{x}_1 , \dot{x}_2 all I have written here \dot{x}_1 , \dot{x}_2 , \dot{x}_3 , \dot{x}_4 .

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$$\begin{aligned} \rightarrow \dot{x}_1 &= \frac{-1}{T_p} x_1 + \frac{k_p}{T_p} x_2 - \frac{k_p}{T_p} \Delta P_L \dots (12) \\ \rightarrow \dot{x}_2 &= \frac{-1}{T_r} x_2 + \left(\frac{1}{T_r} - \frac{k_r}{T_e} \right) x_3 + \frac{k_r}{T_e} x_4 \dots (13) \\ \rightarrow \dot{x}_3 &= \frac{-1}{T_e} x_3 + \frac{1}{T_e} x_4 \dots (14) \\ \rightarrow \dot{y} &= \frac{-1}{RT_g} x_1 - \frac{1}{T_g} x_4 + \frac{1}{T_g} u \dots (15) \end{aligned}$$

But that is I have written here, but I am writing here for you write such that things will be understandable. So, just see how we are writing first you write down the equation for your x_1 ; this is your x_1 right. So, how we will do this? Just 1 minute here one or two small thing you have what you call you have to understand right first you see this x_1 ; this x_1 .

(Refer Slide Time: 14:48)

$$\begin{aligned} x_1 &= \frac{(x_2 - \Delta P_L) \times k_p}{(1 + s T_p)} \\ \therefore x_1 + (s x_1) T_p &= k_p x_2 - k_p \Delta P_L \\ \therefore x_1 + \dot{x}_1 T_p &= k_p x_2 - k_p \Delta P_L \quad \left(s \rightarrow \frac{d}{dt} \right) \\ \therefore \dot{x}_1 T_p &= -x_1 + k_p x_2 - k_p \Delta P_L \\ \therefore \dot{x}_1 &= -\frac{1}{T_p} x_1 + \frac{k_p}{T_p} x_2 - \frac{k_p}{T_p} \Delta P_L \end{aligned}$$

So, x_1 is equal to I will write little bit slowly such that handwriting will be better right because this is a pen and paper. So, this is your x_1 is equal to this ΔP_g actually your

x_2 . So, basically it will be x_2 minus say $\Delta P L$ because $\Delta P g$ you have taken x_2 that is your x_2 minus $\Delta P L$ right into $K p$ upon 1 plus $S T p$ right.

So, that is your x_1 you cross multiply you cross multiply; that means, it will be x_1 then $S x_1 T p$ we are taking x and x_1 together is equal to $K p x_2$ minus $K p$ into $\Delta P L$ right; that means, this $S x_1$ actually S is ddt . So, $S x_1$ will be $x_1 \text{ dot}$. Therefore, because S actually is ddt therefore, it will be $x_1 \text{ dot}$; that means, your $x_1 x_1 \text{ dot}$ into $T p$ is equal to $K p x_2$ minus $K p$ into $\Delta P L$ right.

That means, just hold on; that means, this $x_1 \text{ dot } T p$ is equal to minus x_1 plus $K p x_2$ minus $K p$ into $\Delta P L$. Therefore, $x_1 \text{ dot}$ is equal to minus 1 upon $T p x_1$ plus $K p$ upon $T p x_2$ minus $K p$ upon $T p \Delta P L$. So, this is actually this is what I have written here this equation; this is equation 12 minus 1 upon $T p x_1$ plus $K p$ upon $T p x_2$ minus $K p$ upon $T p \Delta P L$; this is equation 12.

So, this is what I have written here this is actually your equation 12. So, this I have written here directly instead of writing so, many step, but here I showed you what is $x_1 \text{ dot}$ is equal to right. Next we will write your other equations now before writing $x_2 \text{ dot}$; I will write $x_3 \text{ dot}$ for you; why? Now we will know right first I will write $x_3 \text{ dot}$. So, you come to the come to your diagram these x_3 first I write $x_3 \text{ dot}$ and then I will come to $x_2 \text{ dot}$.

(Refer Slide Time: 17:36)

$$x_3 = \frac{x_4}{(1 + sT_t)}$$

$$\therefore x_3 + (sx_3)T_t = x_4$$

$$\therefore x_3 + x_3' T_t = x_4$$

$$\therefore x_3' T_t = -x_3 + x_4$$

$$\therefore x_3' = \frac{-1}{T_t} x_3 + \frac{1}{T_t} x_4$$

So, if you look at the diagram that x_3 will be equal to x_4 in 1 upon $1 + S T t$. So, from this diagram only x_3 is equal to x_4 divided by $1 + S T t$; then go for cross multiplication again it will be x_3 plus your $S \times x_3$ into $T t$ is equal to x_4 right; that means, x_3 is x_3 dot. So, it is x_3 plus x_3 dot $T t$ is equal to x_4 .

That means, your x_3 dot $T t$ is equal to your minus x_3 plus x_4 ; that means, your x_3 dot is equal to minus 1 upon $T t \times x_3$ plus 1 upon $T t \times x_4$. So; that means, this equation your this equation x_3 it is x_3 dot is equal to minus 1 upon $T t \times x_3$ plus 1 upon $T t \times x_4$ this one we write next right why I wrote this one first you know now.

This is actually equation 14; this is your equation x_3 dot. Now we will come to x_2 because in the x_2 dot equation this x_3 dot is required; that is why x_3 dot is obtained first right. Next you come to your x_2 dot right this x_2 dot; so, this x_2 is equal to x_3 into whole all of this thing.

(Refer Slide Time: 19:12)

$$\begin{aligned}
 x_2 &= \left(\frac{1 + S K_r T_r}{1 + S T_r} \right) \cdot x_3 \\
 (1 + S T_r) x_2 &= x_3 + (S x_3) \cdot K_r T_r \\
 x_2 + (S x_2) T_r &= x_3 + \dot{x}_3 K_r T_r \\
 \therefore x_2 + \dot{x}_2 T_r &= x_3 + K_r T_r \left(-\frac{1}{T_L} x_3 + \frac{1}{T_L} x_4 \right) \\
 \therefore \dot{x}_2 T_r &= -x_2 + x_3 + \frac{-K_r T_r}{T_L} x_3
 \end{aligned}$$

Therefore, your x_2 is equal to this is x_2 ; this is x_2 is equal to 1 plus $S K_r T_r$ divided by $1 + S T_r$ into your this x_3 this x_3 right. Now when you now multiply with this one cross multiplication; so $1 + S T_r \times x_2$ is equal to multiply this one; it will be x_3 plus $S \times x_3$ because S is here into K_r into T_r right.

So, if you multiply this one then it will be x_2 plus $S \times x_2 T_r$ is equal to x_3 it is $S \times x_3$ means x_3 dot $K_r T_r$ because x_3 dot is coming because x_3 dot you have to substitute

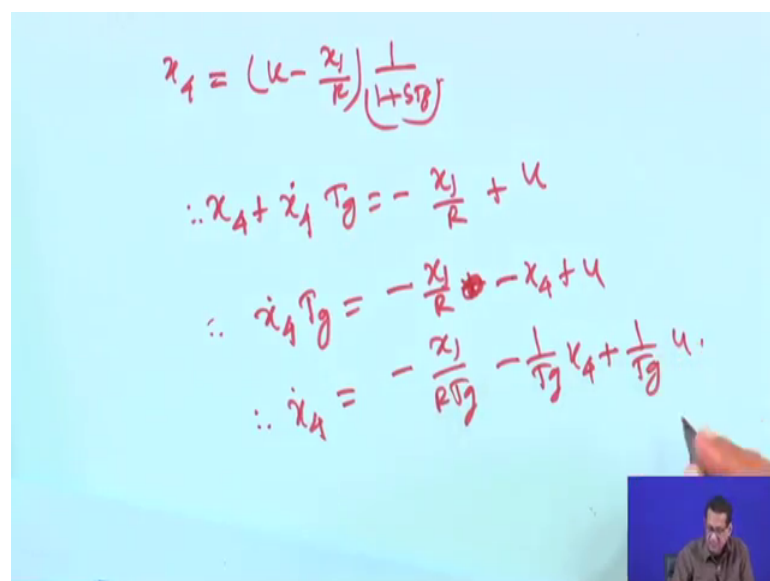
from that equation. This x_3 dot you have to this S x dot value you have to substitute here otherwise you cannot that is why I wrote that equation 3 first right.

. So, the way I have chosen the state variable; so, this one actually is x_2 is x_2 dot. So, it is x_2 plus x_2 dot into T_r is equal to x_3 plus K_r into T_r and this x_3 dot this 1 minus 1 upon $T_t \times 3$ plus 1 upon $T_t \times 4$; you substitute it will minus 1 upon $T_t \times 3$ plus 1 upon $T_t \times 4$ u substitute right; that means, my x_2 dot T_r is equal to minus x_2 right, plus x_3 plus you multiply sorry it will be minus minus $K_r T_r$ upon $T_t \times 3$ right.

Then it is plus $K_r T_r$ upon $T_t \times 4$ right just hold on I have to go a little bit up otherwise you cannot see this right this one right. Then both side you divide by T_r and simplify then you will get this equation then will get equation 13 then you will get equation 13 right the both side you divide by T_r and simplify then you will get your x_2 dot is equal to minus 1 upon $T_r \times 2$ plus 1 upon T_r minus K_r upon $T_t \times 3$ plus K_r upon $T_t \times 4$ this is equation 13 right.

So, x_1 dot, x_3 dot, x_2 dot all I showed just to make it right just to save some time I did not do further, but you make this thing. Next your x_4 dot right just see the x_4 dot; now for x_4 look at this diagram; look at this diagram right this is your x_4 ; this is your x_4 . So, you can write x_4 is equal to x_4 is equal to this is u and this Δf means x_1 this means x_1 .

(Refer Slide Time: 22:17)



$$x_1 = \left(u - \frac{x_1}{R}\right) \frac{1}{(1+sT)}$$

$$\therefore x_4 + x_1 T_g = -\frac{x_1}{R} + u$$

$$\therefore x_4 T_g = -\frac{x_1}{R} - x_4 + u$$

$$\therefore x_4 = -\frac{x_1}{R T_g} - \frac{1}{T_g} x_4 + \frac{1}{T_g} u$$

So, it is plus u minus x 1 in by all R right. So, it will be u minus x 1 by R right into 1 by 1 plus S T g right that is the x 4 is equal to right. So, let cross multiplication again; so, writing directly it is x 4 and S x 4 T g x S 4 means x 4 dot. So, it is x 4 dot then T g is equal to this term writing first minus x 1 upon R plus u or x 4 dot T g is equal to this we are writing first minus x 1 R right.

Minus x 4 plus u write or x 4 dot is equal to minus x 1 upon R T g minus 1 upon T g x 4 plus 1 upon T g u write; this is actually your equation number 15 this is equation 15 that is x 4 dot minus 1 upon R T g x 1 minus 1 upon T g x 4 plus 1 upon T g u; this is equation 15. I think up to this it is your what you call it is understandable that how to obtain all state variable equation x 1 dot, x 2 dot, x 3 dot they are 4 state variables right.

So, I have taken state variable like this you are what you call here x 1, x 1, x 2, x 3, x 4. If you can take this is x 1, x 2, x 3, x 4 also no problem the way what you can take this way right. So, this is all this thing after that we have to put this equation in x dot is equal to x plus B u form right.

(Refer Slide Time: 24:16)

$$\dot{x} = Ax + Bu + \gamma p$$

$p = \Delta P_L$

Eqns. (32)-(35) can be written in matrix form:

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} -\frac{1}{T_p} & \frac{K_p}{T_p} & 0 & 0 \\ 0 & -\frac{1}{T_i} & (\frac{1}{T_i} - \frac{K_r}{T_i}) & \frac{K_r}{T_i} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \end{bmatrix} + \begin{bmatrix} -\frac{K_p}{T_p} \\ 0 \end{bmatrix} p$$

That means, this equation we have to write that you are in this form x dot is equal to A x plus B u plus gamma p this gamma p from this way you have to write this equation. Now if you do; so, then what we will get right.

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Eqs. (12)–(15) can be written in matrix form:

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \\ \dot{x}_4 \end{bmatrix} = \begin{bmatrix} -\frac{1}{T_p} & \frac{K_p}{T_p} & 0 & 0 \\ 0 & -\frac{1}{T_r} & \left(\frac{1}{T_r} - \frac{K_r}{T_k}\right) & \frac{K_r}{T_k} \\ 0 & 0 & -\frac{1}{T_k} & \frac{1}{T_k} \\ -\frac{1}{RT_g} & 0 & 0 & -\frac{1}{T_g} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \\ \frac{1}{T_g} \end{bmatrix} u + \begin{bmatrix} -\frac{K_p}{T_p} \\ 0 \\ 0 \\ 0 \end{bmatrix} \Delta P_L$$

(16)

So, when you make it \dot{x} is equal to $Ax + Bu + \gamma p$ right. So, this is actually your this one your a matrix right and Bu this is u this is actually this one will be B and this is ΔP_L . γp means it is your what you call γp means this p actually is equal to your P_L right I made ΔP_L because change in the load; so, ΔP_L .

So, u and ΔP_L , but if you look at this equation just hold on just hold on this is also we have taken ΔP_L . So, this is I have also written ΔP_L . So, p is equal to actually ΔP_L right. So, if you put in this form \dot{x} is equal to $Ax + Bu + \gamma p$ just hold on right just hold on.

So, this A is actually state transition matrix right B is equal to your control transition matrix and γ is equal to disturbance transition matrix. This is actually this one this one actually your γ right this is actually is your γ this is γ and this is B ; this is A ; A B and γ right an x_1, x_2, x_3, x_4 are the state variables u is the control variable and ΔP_L basically is a disturbance in the system right.

So, this one if you write then if you look at this those equations that equation 12 13, 14 and 16 this \dot{x}_1 is equal to actually minus 1 upon $T_p \times x_1$. So, minus 1 upon $T_p \times x_1$ plus K_p upon $T_p \times x_2$ plus K_p upon $T_p \times x_2$ right; no x_3, x_4 term is involved in this equation. So, their coefficients are 0; so, it is 0 0 right because x_1, x_2, x_3, x_4 no u term is your involved in this equation.

Therefore, all this is 0 right and then disturbance term is there minus K_p upon ΔP_L . So, in a very first row this is minus K_p upon T_p into ΔP_L is here; this is \dot{x}_1 dot is written I think you know this. Similarly \dot{x}_2 dot \dot{x}_2 dot is equal to your \dot{x}_1 is not involved here. So, it is 0 right then this one your \dot{x}_2 dot that is minus 1 upon T_r ; so minus 1 upon T_r is here right. Then this one 1 upon T_r minus K_r upon T_t is \dot{x}_3 so 1 upon T_r minus K_r minus T_t \dot{x}_3 in the third term and fourth term K_r upon T_t \dot{x}_4 . So K_r upon T_t \dot{x}_4 so K_r upon T_t \dot{x}_4 right and there is no u term, no disturbance term so corresponding this is 0, this is 0.

Now third term only minus \dot{x}_3 and \dot{x}_4 are involved others everything is 0 so \dot{x}_1 is 0, \dot{x}_2 is 0 it is minus 1 upon T_t and it 1 upon T_t is \dot{x}_3 , this is 0, this is 0 right. And last term \dot{x}_4 ; \dot{x}_1 and \dot{x}_4 is involved \dot{x}_2 , \dot{x}_3 is not there both are minus sign so minus 1 upon $R T_g$ 0 0 and \dot{x}_4 is this minus 1 upon T_g this one \dot{x}_4 and it is u 1 upon T_g so 1 upon T_g is here because this is u but here it is 0 right. So, this is actually written in this form \dot{x} dot is equal to actually \dot{x}_1 dot, \dot{x}_2 dot, \dot{x}_3 dot, \dot{x}_4 dot capital \dot{X} dot any one is equal to A into x plus B into u plus γ into P this way we have written this equation.

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Eqn. (26) can be written as:

$$\dot{X} = AX + BU + \Gamma p \dots (27)$$

Where

$$X' = [x_1 \ x_2 \ x_3 \ x_4]$$

$$A = \begin{bmatrix} -\frac{1}{T_p} & \frac{K_p}{T_p} & 0 & 0 \\ 0 & -\frac{1}{T_r} & \left(\frac{1}{T_r} - \frac{K_p}{T_t}\right) & \frac{K_r}{T_t} \\ 0 & 0 & -\frac{1}{T_t} & \frac{1}{T_t} \\ -\frac{1}{R T_g} & 0 & 0 & -\frac{1}{T_g} \end{bmatrix}, B' = \begin{bmatrix} 0 & 0 & 0 & \frac{1}{T_g} \end{bmatrix}$$

$$\Gamma' = \begin{bmatrix} -\frac{K_p}{T_p} & 0 & 0 & 0 \end{bmatrix}, p = \Delta P_L$$

So, it can be written as \dot{X} is equal to Ax plus Bu plus γp where X transpose I have taken state variable x_1, x_2, x_3, x_4 A matrix is this matrix, this matrix is A matrix right. And it is B matrix $0 \ 0 \ 0 \ 1$ T_g , but I have written be transpose dash is transpose as a space can be accommodated. So, $0 \ 0 \ 0 \ 1$ upon this is B transpose that is why it is written

that this is A actually and similarly that γ actually minus $K p$ upon $T p 0 0 0 0$, but taken as a transpose as that space can be saved here. So, γ dash is equal to minus $K p$ upon $T p 0 0 0$ and this p is the disturbance that is your $\delta P L$ right. I hope you have understood this state variable.

Thank you very much.