

Principles of Communication- Part I
Professor Aditya K. Jagannathan
Department of Electrical Engineering
Indian Institute of Technology Kanpur

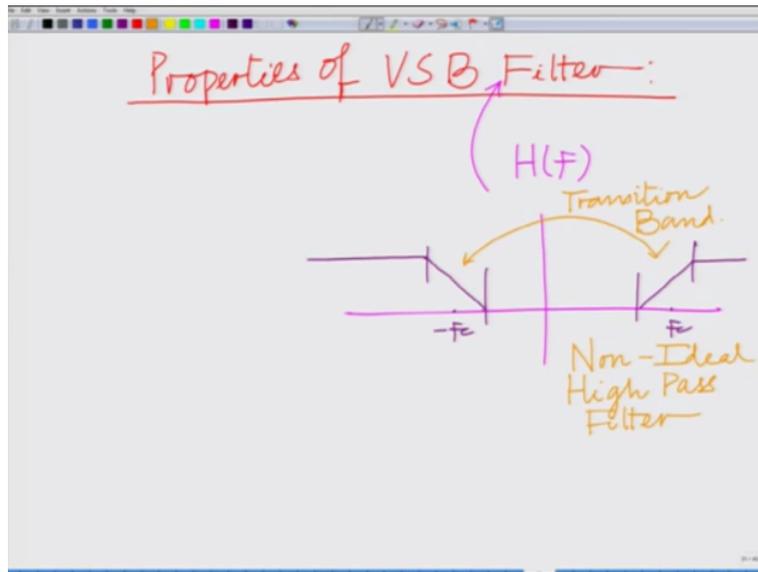
Module No 5

Lecture 27

Properties of Vestigial Side Band Filter of Reconstruction of Message Signal without Distortion

Hello welcome to another module in this massive open online course. So we are looking at vestigial sideband modulation which is basically a form of upper sideband or single sideband modulation and which the filter is non-ideal and let us look at the properties of this non-ideal VSB filters.

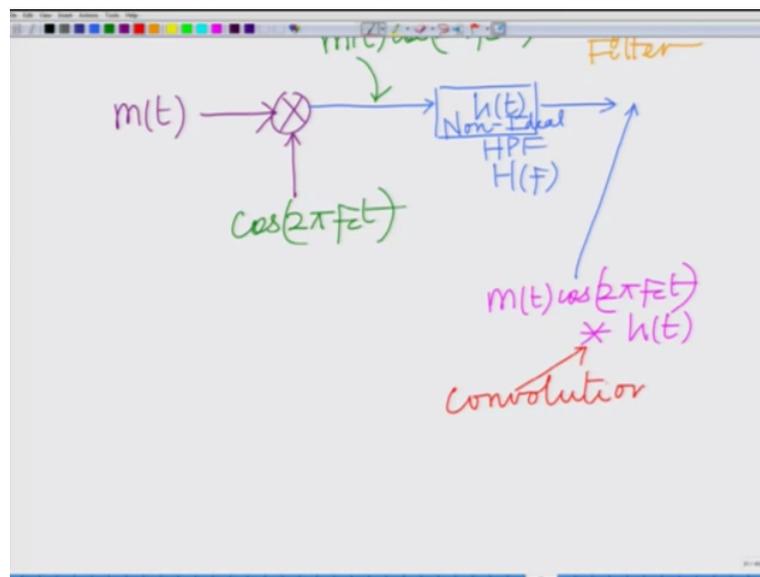
(Refer Slide Time: 0:40)



So we are looking at the property of this VSB filter and let us say this has impulse this has spectrum HF, correct? This non-ideal VSB filter has spectrum HF which as we already said it has it is a high pass filter but it is not an ideal high pass filter, so it has a finite transition band, correct? So this is minus f_c and this band these 2 bands these are your transition bands, correct? Where it is rising from where the impulse where the responses lies between 0 and 1 that it is rising from 0 to 1 that is known as the transition band and this is a non-ideal high pass filter, correct?

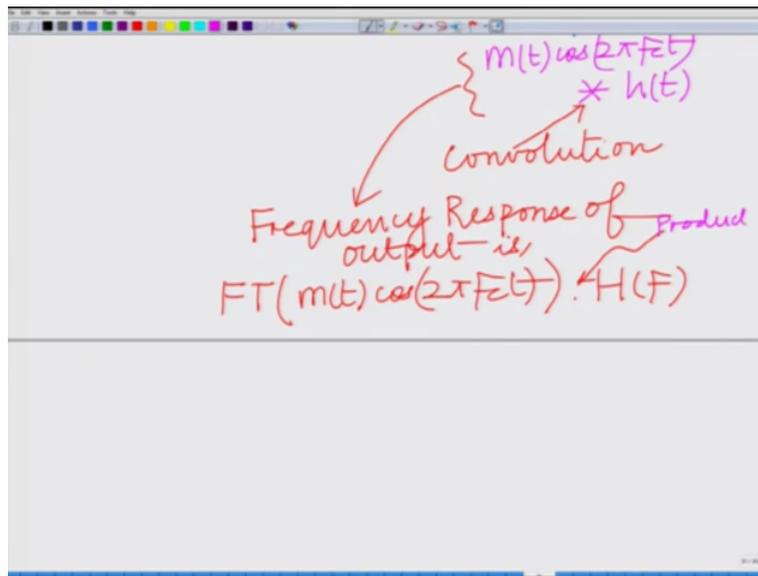
Non-ideal high pass filter at with cut-off frequency F_c this is a let me just write it again clearly this is a non-ideal high pass filter. As we already said we prefer this non-ideal high pass filter we prefer this because designing I Ideal high pass filters or implementing ideal high pass filters as a very high complexity, okay. Require a large number of stages to implement the ideal high pass filter that's one where is this non-ideal high pass filter can be implemented with relatively lower complexity, alright. So this is preferred in a practical implementation, okay. So let us look at a schematic for vestigial sideband modulation, okay.

(Refer Slide Time: 2:51)



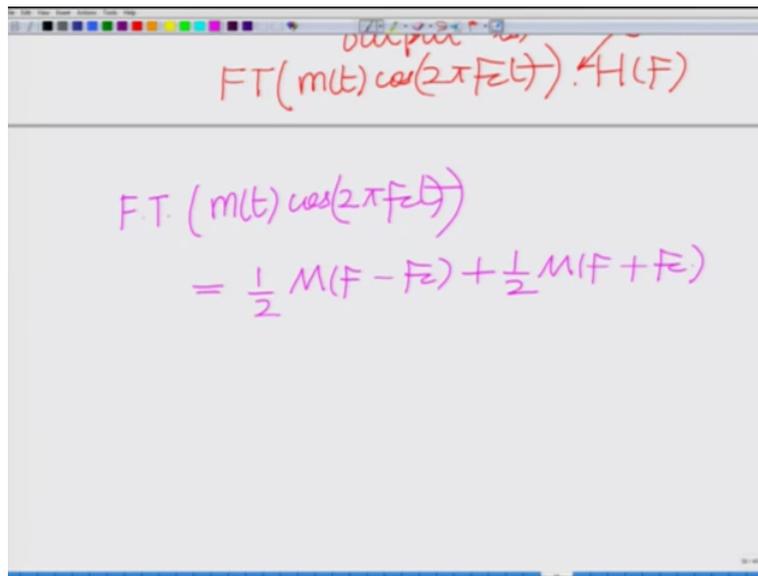
So we have our signal $m(t)$ which is as usual modulated with cosine $2\pi F_c t$ first because remember we are using the frequency discrimination, okay. Frequency discrimination technique except that we are using non-ideal so it is modulated cosine $2\pi F_c t$ let us write this over here that is cosine $2\pi F_c t$ to generate $m(t)\cos(2\pi F_c t)$ and that is pass through your linear time invariant system with impulse response $h(t)$ or that is your non-ideal high pass filter impulse response $h(t)$ and spectrum $H(F)$ and this is basically the output. So naturally the output here will be this is basically your $m(t)\cos(2\pi F_c t)$ convolved with $h(t)$ because modulated signal $m(t)\cos(2\pi F_c t)$ is passing through the non-ideal high pass filter with impulse response $h(t)$ therefore the output is $m(t)\cos(2\pi F_c t)$ convolved with the impulse response, okay. So this is the convolution, okay.

(Refer Slide Time: 4:48)



So that should be clear this is your convolution operation, okay which in the frequency domain means and then for the frequency response of this of the output frequency response of the output is that is the Fourier transform in the frequency domain it is the Fourier transform of $m(t) \cos(2\pi Fct)$ with multiplication because convolution in time domain this becomes your multiplication, okay. So that is also something that you must be very familiar with at this point. So this is this becomes a, your simple product. Let us write product instead of multiplication, okay.

(Refer Slide Time: 6:00)

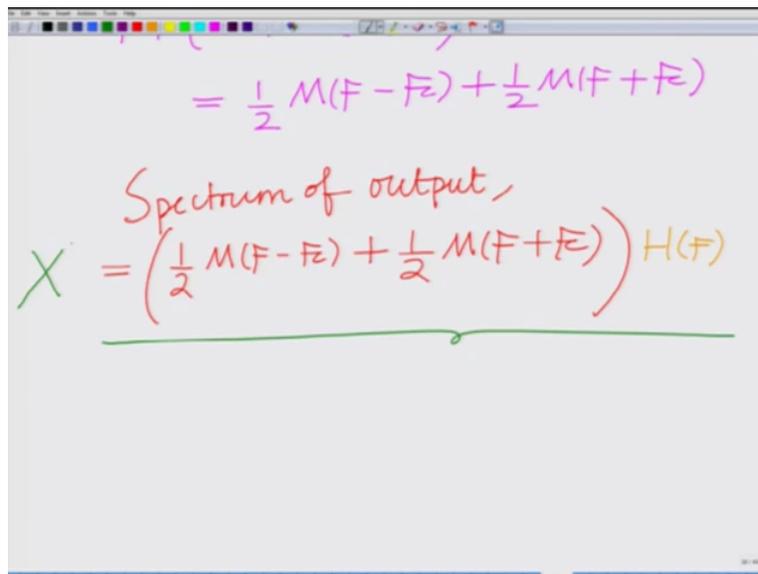


Handwritten notes on a whiteboard. At the top, it says "output" and "FT(m(t) cos(2πF_ct)) * H(f)". Below that, the main equation is written in purple: "F.T. (m(t) cos(2πF_ct)) = 1/2 M(f - F_c) + 1/2 M(f + F_c)".

$$\text{FT}(m(t) \cos(2\pi F_c t)) \cdot H(f)$$
$$\text{F.T. } (m(t) \cos(2\pi F_c t)) = \frac{1}{2} M(f - F_c) + \frac{1}{2} M(f + F_c)$$

And now the Fourier transform of $m(t) \cos 2\pi F_c t$ that is also something that we are very familiar with that is half $M(f - F_c)$ and half $M(f + F_c)$. So the Fourier transform of $m(t) \cos 2\pi F_c t$ this is equal to half $M(f - F_c)$ plus half $M(f + F_c)$.

(Refer Slide Time: 7:02)



Handwritten notes on a whiteboard. It shows the equation from the previous slide: "1/2 M(f - F_c) + 1/2 M(f + F_c)". Below that, it says "Spectrum of output," and then the final equation: "X = (1/2 M(f - F_c) + 1/2 M(f + F_c)) H(f)". The entire expression is underlined in green.

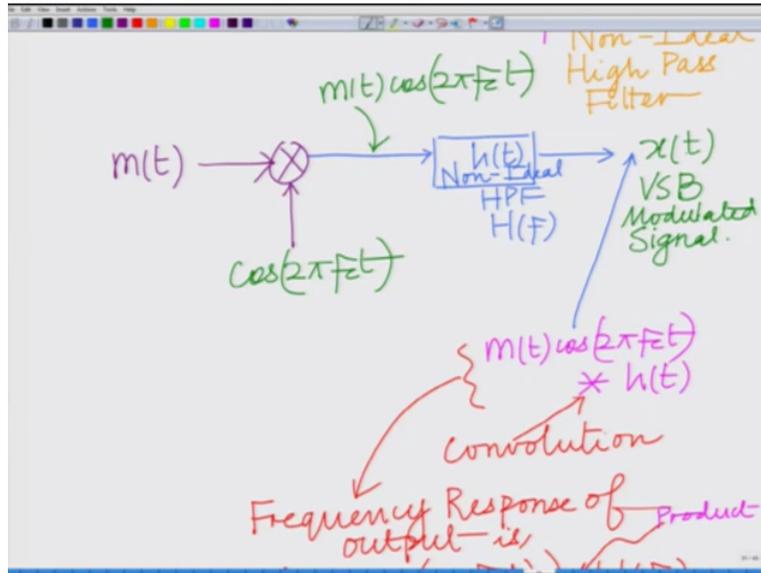
$$= \frac{1}{2} M(f - F_c) + \frac{1}{2} M(f + F_c)$$

Spectrum of output,

$$X = \left(\frac{1}{2} M(f - F_c) + \frac{1}{2} M(f + F_c) \right) H(f)$$

So the net Fourier spectrum of the output, so spectrum of the output of the VSB modulated signal that is spectrum of the VSB modulated signal is half MF minus Fc plus half MF plus Fc times HF, okay. So this is basically the spectrum let us call this as X(F).

(Refer Slide Time: 7:24)



If we call the signal as $x(t)$ here the VSB modulated signal as $x(t)$ this is our VSB vestigial sideband modulated if $x(t)$ is the vestigial sideband modulated signal let say it has spectrum $X(F)$ that is this $x(t)$ has spectrum $X(F)$.

(Refer Slide Time: 7:40)

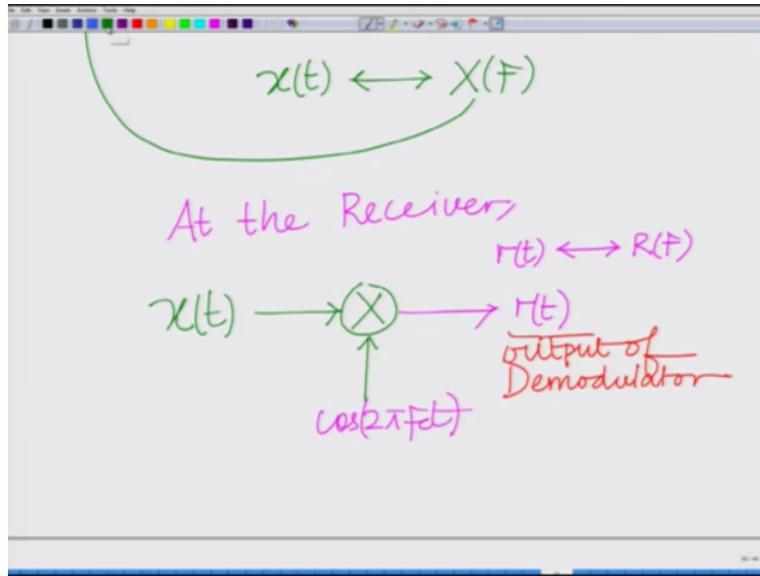
A hand-drawn equation defining the spectrum of the output signal. The equation is:

$$X(F) = \left(\frac{1}{2} M(F - F_c) + \frac{1}{2} M(F + F_c) \right) H(F)$$
 Below the equation, a horizontal line separates it from the Fourier transform pair:

$$x(t) \leftrightarrow X(F)$$
 A green arrow points from the $x(t)$ term in the transform pair up to the $X(F)$ term in the equation above.

So output signal $x(t)$ VSB modulated signal $x(t)$ where $X(F)$ $x(t)$ has spectrum $X(F)$ and that $X(F)$ is given by this that $X(F)$ is given by this that is half MF minus F_c plus half MF plus F_c that is the spectrum of $m(t)$ cosine $2\pi F_c t$ multiplied by HF which is the spectrum of the non-ideal high pass filter, okay which has a transition band around F_c , okay.

(Refer Slide Time: 8:15)



Now at the receiver consider demodulation at the receiver we have your $x(t)$ which is the received signal this is again demodulated by passing through by demodulating with your cosine $2\pi F_c t$ and that gives rise to the output signal, okay. So let us call this output signal as $r(t)$ with spectrum let us say $r(t)$ is the output of the demodulator that has spectrum $R(F)$, okay. So $r(t)$ this is the output of this is the output of the demodulator, okay.

(Refer Slide Time: 9:23)

$$\begin{aligned} r(t) &= x(t) \cdot \cos(2\pi f_c t) \\ &= \frac{1}{2} X(F - F_c) + \frac{1}{2} X(F + F_c) \end{aligned}$$

So this is basically $r(t)$ and see $r(t)$ is basically your $x(t)$ times cosine $2\pi f_c t$ and therefore $r(t)$ is basically demodulated $x(t)$ times cosine $2\pi f_c t$ therefore its spectrum is naturally half $X(F)$ minus F_c plus half $X(F)$ plus F_c , okay. So this so $x(t)$ cosine $2\pi f_c t$ it's spectrum is half $X(F)$ minus F_c plus half $X(F)$ plus F_c , now substitute for $X(F)$.

(Refer Slide Time: 10:22)

$$= \frac{1}{2} M(F - F_c) + \frac{1}{2} M(F + F_c)$$

Spectrum of output, $X(F)$

$$X(F) = \left(\frac{1}{2} M(F - F_c) + \frac{1}{2} M(F + F_c) \right) H(F) \quad \text{Eqn 1}$$

$x(t) \leftrightarrow X(F)$

At the Receivers
 $r(t) \leftrightarrow R(F)$

Now in this what we are going to do is substitute, so if we call this is a spectrum for $X(F)$, okay spectrum of output that is $X(F)$. So if you call this as equation 1, now what we are going to do is

substitute for that is equation 1 tells us that $X(f)$ is half $M(f - f_c)$ plus half $M(f + f_c)$ into $H(f)$ substitute that spectrum expression for the spectrum $X(f)$ in this expression for the spectrum $r(t)$, okay.

(Refer Slide Time: 10:42)

The image shows a whiteboard with the following handwritten equations:

$$r(t) = x(t) \cdot \cos(2\pi f_c t)$$

$$R(f) = \frac{1}{2} X(f - f_c) + \frac{1}{2} X(f + f_c)$$

Below the second equation, there is a bracket and the text "Spectrum of output of Demodulator".

$$= \frac{1}{2} \left\{ \frac{1}{2} M(f - 2f_c) + \frac{1}{2} M(f) \right\} H(f - f_c)$$

By the way, this is $R(f)$ that is the spectrum of output, okay. This is a spectrum of output of spectrum of output of spectrum of the output of the demodulator that is equal to half, okay. And instead of $X(f)$ minus f_c I am going to substitute that expression, so $X(f)$ minus f_c so we have half $X(f)$ minus f_c is half $M(f - 2f_c)$ plus half $M(f)$, so this is half so $X(f)$ minus f_c is half $M(f - 2f_c)$ plus f_c minus f_c that is half $M(f)$ times $H(f - f_c)$, okay.

(Refer Slide Time: 12:21)

$$\begin{aligned}
 \text{Demodulator} &= \frac{1}{2} \left\{ \left(\frac{1}{2} M(F-2F_c) + \frac{1}{2} M(F) \right) H(F-F_c) \right\} \\
 &+ \frac{1}{2} \left\{ \left(\frac{1}{2} M(F) + \frac{1}{2} M(F+2F_c) \right) H(F+F_c) \right\} \\
 &= \frac{1}{4} M(F-2F_c) H(F-F_c) + \frac{1}{4} M(F) H(F-F_c) \\
 &+ \frac{1}{4} M(F) H(F+F_c) + \frac{1}{4} M(F+2F_c) H(F+F_c)
 \end{aligned}$$

So this is your basically half $X(F)$ minus F_c plus half now $X(F)$ plus F_c , so that will be half $M(F)$ minus F_c plus F_c so half $M(F)$ plus half $M(F)$ plus F_c plus F_c $M(F)$ plus $2F_c$ into $H(F)$ plus F_c , okay. So this is the net expression. Now if you look at this now let us write this term by term so this is $\frac{1}{4} M(F)$ minus $2F_c$ into $H(F)$ minus F_c plus $\frac{1}{4} M(F)$ into $H(F)$ minus F_c plus $\frac{1}{4} M(F)$ into $H(F)$ plus F_c plus $\frac{1}{4} M(F)$ plus $2F_c$ into $H(F)$ plus F_c , okay. So these are the 4 terms you get from the Expansion of the output of the demodulator. So this is still we are talking about the spectrum of the output signal of the demodulator that is we are talking about the spectrum R_F .

(Refer Slide Time: 14:10)

$$= \frac{1}{4} M(F-2F_c) H(F-F_c) + \frac{1}{4} M(F) H(F-F_c) + \frac{1}{4} M(F) H(F+F_c) + \frac{1}{4} M(F+2F_c) H(F+F_c)$$

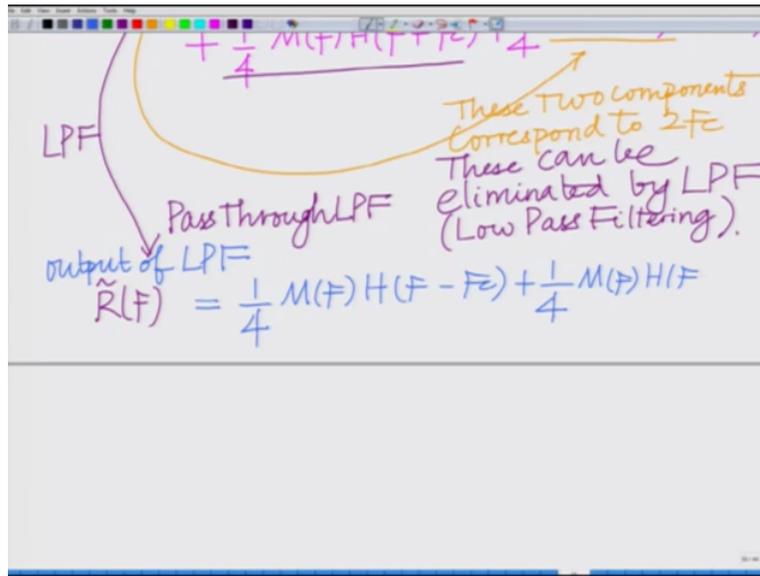
Pass through LPF

These two components correspond to $2F_c$. These can be eliminated by LPF (Low Pass Filtering).

Now if you look at this spectrum which we have simplified by substituting the expression for the spectrum of $X(F)$ that is the spectrum of the $X(F)$ which is the spectrum of the VSB modulated signal $x(t)$, now you can see that MF minus F_c look at these $2MF$ minus F_c and MF plus $2F_c$, so these 2 components correspond to $2F_c$ are centered at $2F_c$ MF minus F_c MF minus $2F_c$ is MF shifted to $2F_c$ and MF plus $2F_c$ is MF shifted to minus $2F_c$, so these 2 are centered at $2F_c$. So these can be eliminated by low pass filtering, hence these can be eliminated by low pass filter.

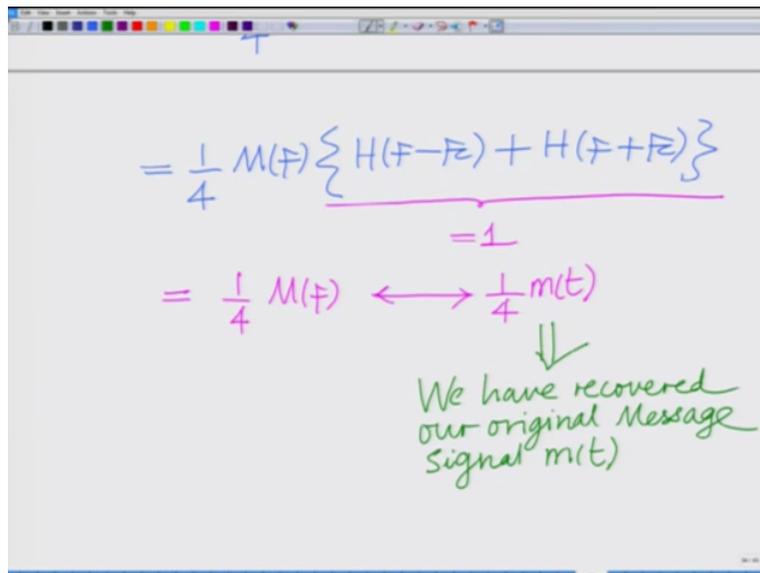
So when we eliminate these by low pass filtering only the 2 other components are going to remain, so that is the central idea. So now we are going to low pass filter it, now these can be eliminated by LPF, okay. That is your, hence now if you pass this through a low pass filter pass that is pass RT through LPF's only these components are going to remain that is $\frac{1}{4} MF$ into HF minus F_c into $\frac{1}{4}$ into HF plus F_c .

(Refer Slide Time: 15:32)



So once you pass this you LPF and let us say you get $\tilde{R}(f)$ that is output of LPF. So you are $\tilde{R}(f)$ is output of LPF which is $\frac{1}{4} M(f) H(f - f_c) + \frac{1}{4} M(f) H(f) + f_c$, okay. So $\frac{1}{4} M(f) H(f) + f_c$.

(Refer Slide Time: 17:28)

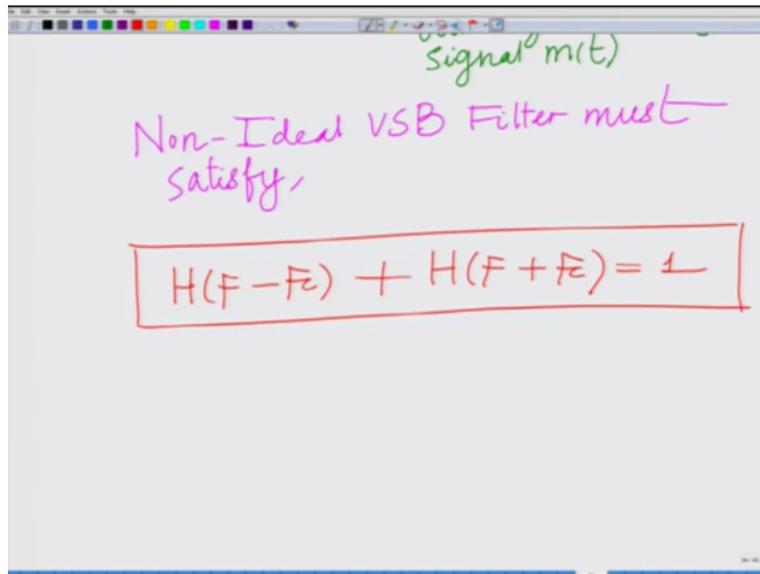


And now if you take $M(f)$ common you can see this is $\frac{1}{4} M(f) H(f - f_c) + \frac{1}{4} M(f) H(f) + f_c$. Now therefore if we can set these 2 a constant $H(f - f_c)$, so you can see the net output spectrum after low pass filtering is $\frac{1}{4} M(f) H(f - f_c) + \frac{1}{4} M(f) H(f) + f_c$. Now if you can

set this $H(f - f_c) + H(f + f_c)$ equal to sum constant in particular let us say this is one then the output spectrum will be $\frac{1}{4} M(f)$ which is basically proportional to the spectrum of $m(t)$ that is in fact the output signal will be $\frac{1}{4} m(t)$.

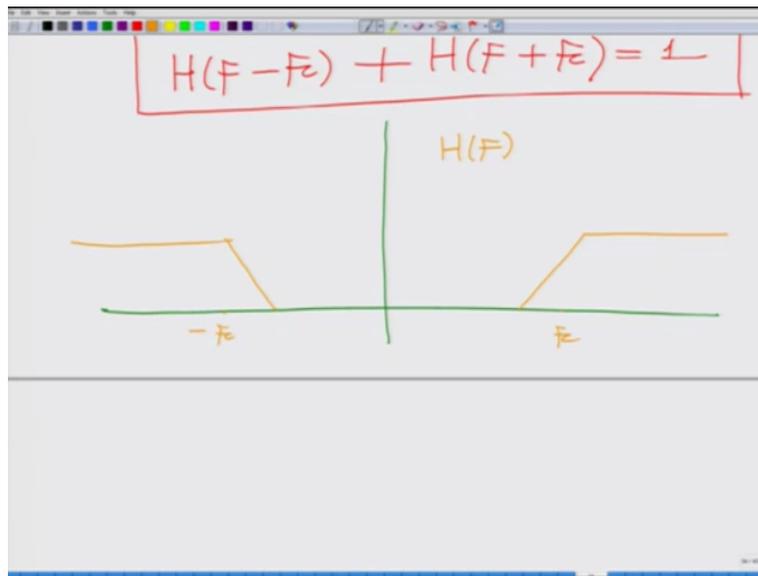
So if this is equal to one then this is simply $\frac{1}{4} M(f)$ which in the time domain corresponds to $\frac{1}{4} m(t)$ and therefore we would have recovered our which implies that we have recovered our original we have recovered our original signal $m(t)$. But note that the requirement is $H(f - f_c) + H(f + f_c)$ should be equal to one, so that is the property that the VSB filter that the non-ideal VSB filter must satisfy, okay. So let us look at that property, so we have $H(f - f_c)$.

(Refer Slide Time: 17:50)



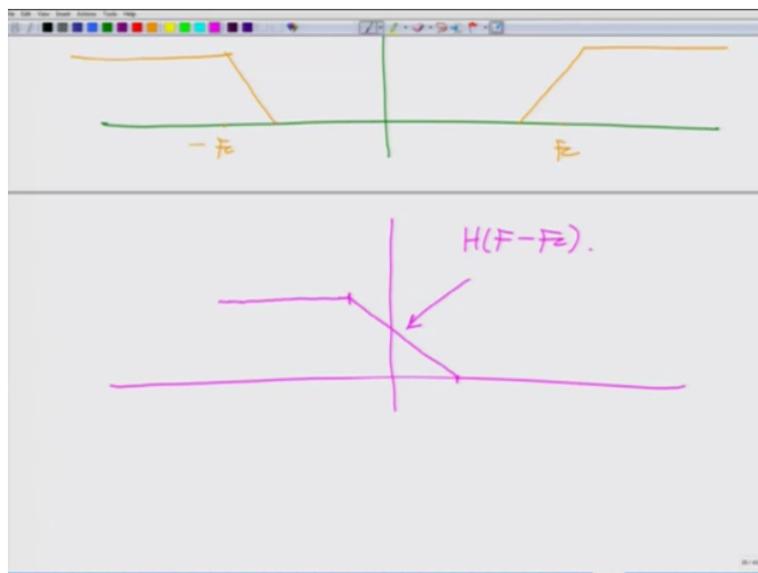
So VSB filter must satisfy so the non-ideal VSB filter must satisfy for recovery distortion-less recovery non-ideal VSB filter must satisfy the property $H(f - f_c) + H(f + f_c)$ equal to one non-ideal this is the property that your non-ideal VSB filter must satisfy, okay.

(Refer Slide Time: 18:38)



So let us look at this property that the non-ideal VSB filter must satisfy, so this is your HF, correct? And let us look at this; this is minus f_c so this is your HF, okay.

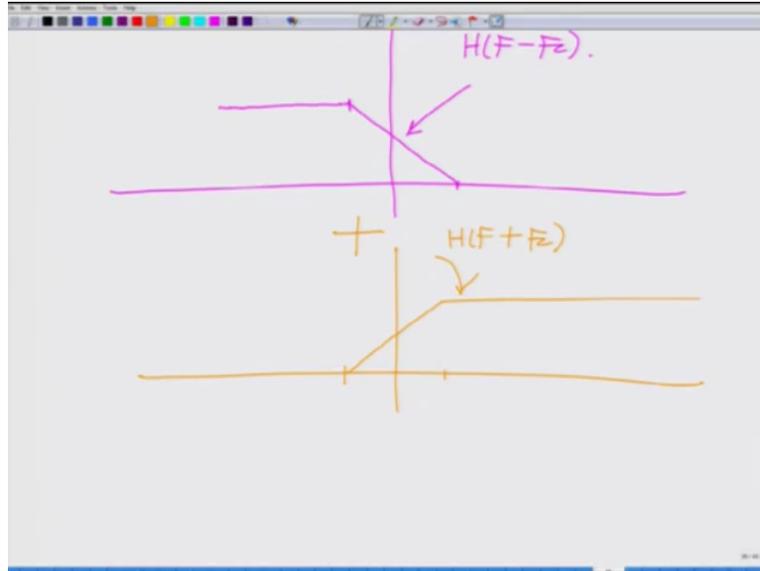
(Refer Slide Time: 19:12)



And now what we are going to do is $H(f - f_c)$ is basically $H(f)$ shifted by f_c so $H(f - f_c)$ is (shi) $H(f)$ shifted that is advance by f_c , so we have $H(f - f_c)$ so the band, okay. So this is basically your $H(f - f_c)$ and plus there will be some other components at $2f_c$ we are not

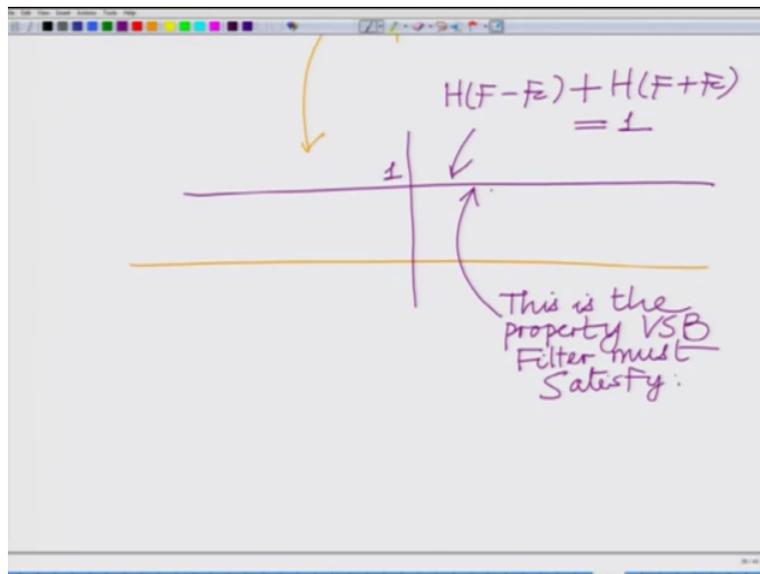
worried about that, alright. So we are only worried about this component which is in the baseband that is HF minus Fc.

(Refer Slide Time: 19:59)



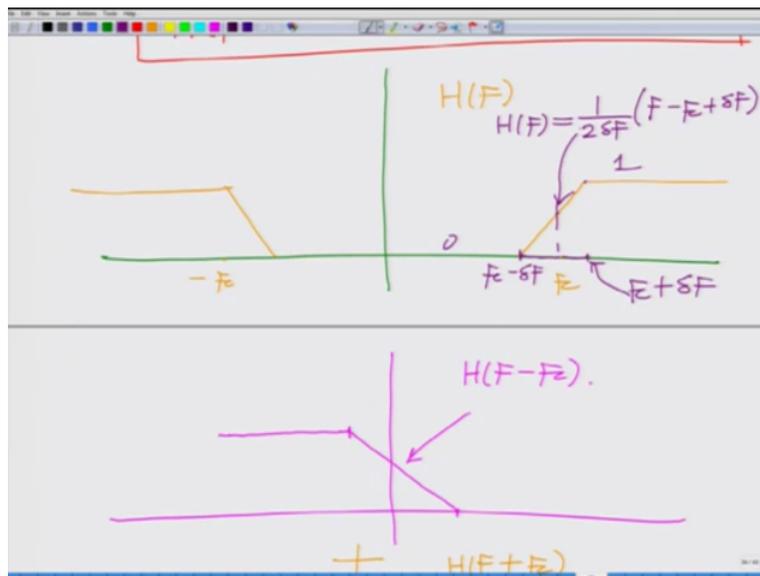
Now let us look at HF plus Fc and if you look at HF plus Fc that looks something like this. So this is your HF plus Fc that is basically your component that is at Fc the shifted backward to the 0 frequency that is HF plus Fc that is shifted by minus Fc that is shifted by Fc to the left.

(Refer Slide Time: 20:39)



Now when you add these 2 that is HF minus FC plus HF plus FC the VSB (property) the VSB filter should obey the property that VSB filter must satisfy the property that when you add these 2 you get you get unity that is you should get unity that is HF minus FC plus HF plus FC equal to one. So this is the property that the VSB filter must satisfy. So this is equal to one this is the property that the VSB filter must satisfy and you can see this property is satisfied if the VSB filter is symmetric about F_c .

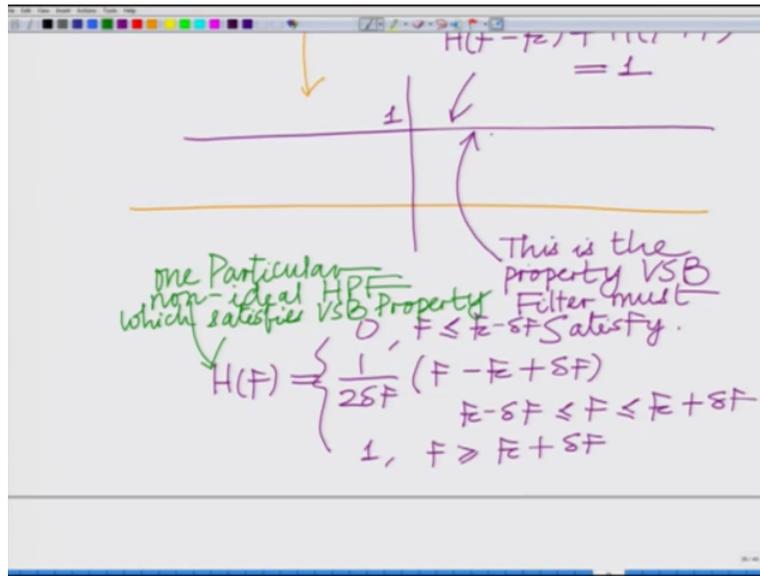
(Refer Slide Time: 21:40)



That is if you can see if these VSB filter is symmetric about F_c that is basically if this is symmetric about F_c that is this is let us say F_c minus δF this point is let us say F_c plus δF and then if its symmetric about F_c then you can see that symmetric about F_c in the sense that you can see that this is linear linearly increasing between F_c minus δF to F_c plus δF the midpoint is at F_c . So if this is symmetric about F_c then this property is satisfied or in other words between F_c minus δF to F_c plus δF this has to be $H(F)$ equals 1 over you can see this linear part corresponds to 1 over the slope is 1 over that is it is rising.

So this is one this is 0 so slope is 1 over it is rising to 1 in interval of $2\delta F$ 1 over $2\delta F$ times F minus F_c plus δF . So if this property satisfied that is if this filter $H(F)$ is symmetric about F_c that is starts from F_c minus δF to F_c plus δF and rises from 0 to 1 linearly then you can see that when you shift $H(F)$ to so when you consider $H(F + F_c)$ and $H(F - F_c)$ and superimpose them or add them in the baseband they will sum up to 1.

(Refer Slide Time: 23:35)



So the property that you can see the this is the property that the VSB (filter) filter must satisfy $H(f - F_c) + H(f + F_c) = 1$, one such filter has the response $H(f)$ equals 1 over twice Δf in $F - F_c + \Delta f$ for $F_c - \Delta f \leq F \leq F_c + \Delta f$ and $H(f)$, so $H(f)$ equal to this equal to 0. So for F less than or equal to $F_c - \Delta f$ equal to 1 for F greater than or equal to $F_c + \Delta f$. So this is one particular filter one particular VSB filter.

So this is one particular filter non-ideal one particular ideal filter non-ideal HPF non-ideal HPF which satisfies VSB property, okay. This is one particular non-ideal high pass filter which satisfies the VSB property, alright. So what we have seen in this module what we have seen is basically we require that is one can implement a non-ideal version of single sideband modulation, alright. In this particular place we have chosen upper side band modulation and non-ideal version of upper sideband modulation which is termed as vestigial sideband modulation with a non-ideal high pass filter, alright.

And we have shown if the high pass filter satisfies certain property that is $H(f - F_c) + H(f + F_c) = 1$ then you can reconstruct, correct? You can reconstruct this VSB you can reconstruct the transmitted message signal again $m(t)$ without any distortion by again passing through the demodulator that is demodulating with $\cos(2\pi F_c t)$ at the receiver. However the disadvantage of the VSB modulation still remains that it requires a slightly larger bandwidth in

this particular place you can see that the transition bandwidth is $f_c - \Delta f$ to $f_c + \Delta f$. So requires a (addi) additional bandwidth of Δf , alright which the previous upper side modulation upper sideband modulation scheme did not require, alright.

So requires a slightly (addi) slightly larger bandwidth that is $f_m + \Delta f$ where f_m is the maximum frequency, so previously upper sideband modulation upper sideband modulation required only f_m , correct? Now this requires $f_m + f_c$ which is slightly larger than f_m but of course it is a trade-off it allows for a lower complexity the design of the non-ideal high pass filter and if this non-ideal high pass filter satisfies this property $H(f_c - f)$ $H(f_c + f)$ equal to unity then that allows the reconstruction of the message signal $m(t)$ without any distortion by simply demodulating with $\cos(2\pi f_c t)$.

Now similar condition can also be derived for the vestigial sideband modulation with the lower sideband that is non-ideal low pass filter, alright. I will let you explore that, alright. So we will stop this module here and continue with other aspects in the subsequent modules, thank you.