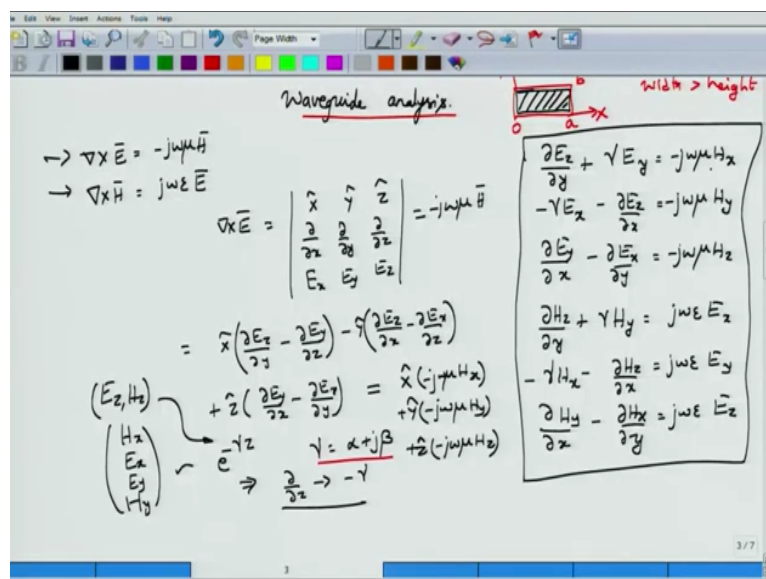


Electromagnetic Theory
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Lecture - 69
Waveguide Analysis

So in this module, we will begin analyzing waveguides that we discussed in the previous module. For the sake of simplicity, we will consider only rectangular waveguides, which means that they have this cross section which is rectangular.

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So, if you look at the cross section this is how they would look probably let us make it more rectangular rather than square. So, along x axis, along y axis, the width of the waveguide is a and the height of the waveguide is b, okay. In the traditional notation, the width is actually taken to be larger than the height, okay. And, we will see why that has to be done. Although in principle there is no difference between width and height.

I mean you can consider b as width and a as height and that does not really matter, okay. We will make one important assumption that is all the field quantities, electric fields that are there and magnetic fields, they would all have to propagate along z axis, okay. So, they would be propagating along z axis, but they could be varying with respect to x, y and in the other case they might also vary with respect to z.

For the rectangular waveguides though, we can assume that the electric fields would vary along, I mean vary with respect to x and y , but they would also propagate along z . Now, what sort of propagation should we assume about this one. Should we assume about this one sine propagation, sine propagation, a pulse propagation.

Well, what we will do is, we will assume that these waves are of a particular frequency, okay and they are propagating in the medium in which they can suffer both attenuation as well as just a propagation, so, there can suffer attenuation as well, okay. So, we capture that by writing down the propagation constant to be a complex number consisting of α and β as real and imaginary parts.

As we have seen even for the transmission line case scenario. α corresponds to attenuation, β corresponds to propagation constant and the propagation of all these fields this should have been H_y , okay, so I forgot H_y . So, all these field components would be varying along $e^{-\gamma z}$. And even the components E_z and H_z , they both would be varying as a function $e^{-\gamma z}$.

Now, the advantage for assuming this type of propagation is that I can replace the derivatives of any of these field quantities with respect to z by $-\gamma$ times the field quantities. In other words, I can replace the differential operation by a simple multiplication operation with $-\gamma$, okay. The starting point for analysis would be that two Maxwell's equation, which relate the curl of electric field and curl of magnetic field to each other, okay.

In the second expression, in the curl for H , we have ignored whatever the conduction current is because we are going to assume that the region of interest for us to look at the waves is inside the waveguide. And inside waveguide, there is no conductor and there is no possibility of having a conducting current, okay. Well, if there is no current and how are these fields generated?

And the answer is that the currents are there, but they are not there inside the waveguide, but they are there on the waveguide walls. We will also of course assume that the material that fills this waveguide is all completely perfect in the sense that there are no leakage currents. Therefore, we can assume safely that there is no currents inside the waveguide and anyway these are you know hollow cavities.

And for the voltage range that one chooses there would essentially be no leakage inside the air dielectric and hence there will not be any current inside, the conduction current will not be there. So, whatever the current that would be there that would be displacement current and I have also replaced or I am actually using without telling you that these are phasor quantities, right.

So, I am not explicitly indicating the time dependence, we are only interested in the spatial dependence because time dependence is taken to be the phasor form. So, $\text{del by del } t$ become $j \omega$, integral becomes 1 by $j \omega$ and because of that reason we have changed, we have written this as $j \omega$. We will also assume that μ and ϵ are constants, okay, unless we specify them to be non constant, okay.

We also know how to obtain curl of electric field. You know this is simple determinant of this 3 by 3 metrics and fortunately this works only for, I mean unfortunately this works only for the rectangular waveguides and that is probably the reason why we are choosing to work in the rectangular field, waveguide. Because the formulas are little tractable compared to the rectangular waveguide.

Although there is nothing specific, there is nothing special about a rectangular cross section. In fact, circular cross sections are much more widely used than rectangular cross section in several applications, okay. So, going back to the rectangular cross section, we have this curl of electric field consisting of three different components x component, y component and z component and this should be equated to the right hand side.

The right hand side also contains three components H_x , H_y and H_z . All these components getting multiplied by minus $j \omega \mu$, right. So, this curl of e must actually be equal to minus $j \omega \mu H$, so which means that it should be $\hat{x} \text{ minus } j \omega \mu H_x$ plus $\hat{y} \text{ minus } j \omega \mu H_y$ plus $\hat{z} \text{ minus } j \omega \mu H_z$, okay. Unlike the plane wave situation, none of these H_x , H_y are going to be - I mean none of these H_z will not be zero.

E_z will not be zero in general and moreover H_x and H_y will not be independent of x and y , so you cannot just remove them out like that. They do depend on x and y , okay because there are bounding boxes, if you think of this along x direction as well as along y direction. There

are conductors, if you go along x, there are two conductors, if you go along y, there are two conductors, of course they are not really two conductor.

But there is a single conductor, but there is a sort of you know imagination that there are two conductors out there, okay, you can think of that way in that. Okay, now here are a set of equations, which I have written, okay. This set of equations are obtained by equating the appropriate or writing down the curl expression for electric field as well as curl for the magnetic field.

And then equating them correctly, okay, so, equating them to the corresponding components. So you can see that the first three set of equations are simply, this equation, curl of E is equal to minus j omega mu, because minus j omega mu H x must be equal to del E z by del y, you can see here, minus del E y by del z. But, I already know what is del by del z. Del by del z is minus gamma and there is a minus sign already present here, so that becomes plus gamma E y.

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The image shows a whiteboard with handwritten mathematical derivations. At the top left, it states:

$$\nabla \times \vec{E} = -j\omega\mu\vec{H}$$

$$\nabla \times \vec{H} = j\omega\epsilon\vec{E}$$
 Below this, the curl of E is expanded using a determinant:

$$\nabla \times \vec{E} = \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ E_x & E_y & E_z \end{vmatrix} = -j\omega\mu\vec{H}$$
 A diagram shows a 3D coordinate system with x, y, and z axes. A vector \vec{E} is shown in the xy-plane, and a vector \vec{H} is shown along the z-axis. The text below the diagram says:

$$\vec{E} = \vec{E}_T + \vec{E}_L$$

$$\vec{H} = \vec{H}_T + \vec{H}_L$$

$$\vec{E}_T \propto f(E_x, E_y)$$

$$\vec{H}_T \propto g(E_x, E_y)$$
 The main derivation continues with the expansion of the curl of E:

$$= \hat{x} \left(\frac{\partial E_z}{\partial y} - \frac{\partial E_y}{\partial z} \right) - \hat{y} \left(\frac{\partial E_z}{\partial x} - \frac{\partial E_x}{\partial z} \right) + \hat{z} \left(\frac{\partial E_y}{\partial x} - \frac{\partial E_x}{\partial y} \right)$$
 This is equated to $-j\omega\mu\vec{H}$. The final result is:

$$\hat{x} (-j\omega\mu H_x) + \hat{y} (-j\omega\mu H_y) + \hat{z} (-j\omega\mu H_z)$$
 On the right side of the whiteboard, a box contains the following equations:

$$\frac{\partial E_z}{\partial y} + \gamma E_y = -j\omega\mu H_x$$

$$-\gamma E_x - \frac{\partial E_z}{\partial x} = -j\omega\mu H_y$$

$$\frac{\partial E_y}{\partial x} - \frac{\partial E_x}{\partial y} = -j\omega\mu H_z$$

$$\frac{\partial H_z}{\partial y} + \gamma H_y = j\omega\epsilon E_z$$

$$-\gamma H_x - \frac{\partial H_z}{\partial x} = j\omega\epsilon E_y$$

$$\frac{\partial H_y}{\partial x} - \frac{\partial H_x}{\partial y} = j\omega\epsilon E_z$$

I hope you understand this first equation, carefully look at this two so, maybe I can help you in that one by erasing off this part, hope you can rewrite that one, minus j omega H z. Now consider each component, okay, so, consider for example this component and then equate that to this one, okay and then replace del by del z by minus gamma and you will actually get the first three equations.

Similarly, writing down curl of H , you will get the next three equations. I really urge you to write down these equations you know without looking at the answers first, and then write down them and convince yourself that this is alright. Now, you may ask, why am I doing this. I mean what is the need for doing this? The terms of that, I can actually solve for the electric and magnetic field by expressing all of them, you know the transverse components.

What are the transverse components? Transverse components are x and y components for the electric field in terms of E_z and H_z . This E_z and H_z are called as the longitudinal components, okay. So, you have three axis, right? So, this is the z axis, this the x and y . Do not worry if my notations are not really consistent. What I want to show you is that there are three axis out there.

And the electric field components in the x and y axis together are called as the transverse components and the component of the electric field along this one is called as the longitudinal component. So, in the plane, okay, so the electric field that you will have will be called as the transverse component and therefore the total electric field can actually be split into transverse and longitudinal components, okay. Longitudinal only E_z is there.

Similarly, you can split H as well as into its transverse and longitudinal components, okay. So, I want to express E_x and E_y and in terms of E_z and H_z . I also want to express H_x and H_y transverse components as some function of E_z and H_z , okay. Some function let us say this is g , function g , okay. So, if I express them then if I know how E_z and H_z are to solved then once I have that I can find out the expression for E_x , E_y , H_x and H_y from these two solutions, right.

So, only two variables, E_z and H_z need to be known in order to completely specify E_x , E_y , H_x and H_y . Again, there is no specific reason, why one has to choose the horizontal components, expect that for the more nomenclature, it becomes easier for us to talk of TE or TM modes, if I know E_z and H_z , right. So, for a TE mode, there will not be any component of the electric field along the longitudinal.

So E_z will be equal to zero, then you are left to solve only for H_z and use that obtain the transverse electric and magnetic field components, okay.

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$\nabla \times \vec{E} = -j\omega\mu\vec{H}$
 $\nabla \times \vec{H} = j\omega\epsilon\vec{E}$

$$\nabla \times \vec{E} = \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ E_x & E_y & E_z \end{vmatrix} = -j\omega\mu\vec{H}$$

$$= \hat{x} \left(\frac{\partial E_z}{\partial y} - \frac{\partial E_y}{\partial z} \right) - \hat{y} \left(\frac{\partial E_z}{\partial x} - \frac{\partial E_x}{\partial z} \right) + \hat{z} \left(\frac{\partial E_y}{\partial x} - \frac{\partial E_x}{\partial y} \right) = \hat{x}(-j\omega\mu H_x) + \hat{y}(-j\omega\mu H_y) + \hat{z}(-j\omega\mu H_z)$$

$\vec{E} = \vec{E}_T + \vec{E}_L$
 $\vec{H} = \vec{H}_T + \vec{H}_L$
 $\vec{E}_T \propto f(E_z, H_z)$
 $\vec{H}_T \propto g(E_z, H_z)$

$$H_y = \frac{\gamma}{j\omega\mu} E_x + \frac{1}{j\omega\mu} \frac{\partial E_z}{\partial x}$$

$$\frac{\partial E_z}{\partial y} + \gamma E_y = -j\omega\mu H_x$$

$$-\gamma E_x - \frac{\partial E_z}{\partial z} = -j\omega\mu H_y$$

$$\frac{\partial E_y}{\partial x} - \frac{\partial E_x}{\partial y} = -j\omega\mu H_z$$

$$\frac{\partial H_z}{\partial y} + \gamma H_y = j\omega\epsilon E_x$$

$$-\gamma H_x - \frac{\partial H_z}{\partial x} = j\omega\epsilon E_y$$

$$\frac{\partial H_y}{\partial x} - \frac{\partial H_x}{\partial y} = j\omega\epsilon E_z$$

Now, how do we do that? Consider for example, the second equation, okay. So, let me highlight that equation, okay. I use this equation to solve for H y. What do I mean by that? I simply take this minus j omega mu on to the left hand side and then write down what is H y, okay. So, you can see H y is actually equal to gamma by j omega mu E x, okay, by taking minus one by j omega mu down and you have also plus one by j omega mu del E z by del x.

I do not know how E z varies with x. I only know how E z varies with z. I also know how E z varies with the other, I mean I only know all the other components varying only with z. I do not know how they vary with x or y, okay, but it does not matter. Now, I know what is H y. Is there H y in the other group of equations, right? So, there is H y in this equation wherein you have del H z by del y plus gamma H y is equal to j omega epsilon E x, okay.

And, if you look at H y, H y is expressed in terms of E x and H, E x and E z. So, if I can write down this, you know substitute for H y into this expression and rearrange it and pull this gamma by j omega E x to the right hand side then I will have E x solely in terms of E z and H z, okay. So, I can do that, I mean let me try doing that one. I cannot use this second equation because I do not know how H y would vary with x.

If I try doing that one by taking the derivative with respect x and I will also have to write down del E x by del x and this becomes the second order equation del square E z by del x square, so, I do not know how to do that. Therefore, I do not use this equation and there is no H y in the second equation and there is only H y in this equation, which I can use, okay.

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$$H_y = \frac{1}{j\omega\mu} E_x + \frac{\gamma}{j\omega\mu} \frac{\partial E_z}{\partial x}$$

$$\frac{\partial H_z}{\partial y} + \frac{\gamma^2}{j\omega\mu} E_x + \frac{\gamma}{j\omega\mu} \frac{\partial E_z}{\partial x} = j\omega\epsilon E_x$$

$$(j\omega\epsilon - \frac{\gamma^2}{j\omega\mu}) E_x = \frac{\gamma}{j\omega\mu} \frac{\partial E_z}{\partial x} + \frac{\partial H_z}{\partial y}$$

$$-(\omega^2\mu\epsilon + \gamma^2) E_x = \gamma \frac{\partial E_z}{\partial x} + j\omega\mu \frac{\partial H_z}{\partial y}$$

$$h^2 = \gamma^2 + \omega^2\mu\epsilon$$

$$E_x = -\frac{1}{h^2} \left(\gamma \frac{\partial E_z}{\partial x} + j\omega\mu \frac{\partial H_z}{\partial y} \right)$$

$$\propto f(E_z, H_z)$$

So, let me use that equation and write down substitute for H_y , so what do I get. I have $\frac{\partial H_z}{\partial y}$ that hasn't changed, right, plus $\frac{\gamma^2}{j\omega\mu} E_x$ plus $\frac{\gamma}{j\omega\mu} \frac{\partial E_z}{\partial x}$ must be equal to $j\omega\epsilon E_x$, right. So, with this I can actually pull this $\frac{\gamma^2}{j\omega\mu} E_x$ to the, sorry, this is actually E_x , right. So, this is E_x not E_y , okay.

So, I can pull this on to the right hand side and then pull everything on to the left hand side, rearrange the two equations. What I get is $j\omega\epsilon E_x - \frac{\gamma^2}{j\omega\mu} E_x = \frac{\gamma}{j\omega\mu} \frac{\partial E_z}{\partial x} + \frac{\partial H_z}{\partial y}$. I can rearrange this equation in the brackets, I mean expression in this brackets.

So, I get $-(\omega^2\mu\epsilon + \gamma^2) E_x = \gamma \frac{\partial E_z}{\partial x} + j\omega\mu \frac{\partial H_z}{\partial y}$, okay times E_x must be equal to $j\omega\mu \frac{\partial H_z}{\partial y} + \gamma \frac{\partial E_z}{\partial x}$, okay. Call this $\omega^2\mu\epsilon + \gamma^2$ as h^2 , okay. So, h^2 is equal to $\gamma^2 + \omega^2\mu\epsilon$, okay. So, if I call this as h^2 .

Then E_x will become $-\frac{1}{h^2} \left(\gamma \frac{\partial E_z}{\partial x} + j\omega\mu \frac{\partial H_z}{\partial y} \right)$, this is h^2 times $\frac{\partial H_z}{\partial y}$, okay. I can of course pull this minus sign outside and then call this h^2 as a common factor. So, what I get is $-\frac{1}{h^2} \left(\gamma \frac{\partial E_z}{\partial x} + j\omega\mu \frac{\partial H_z}{\partial y} \right)$. So, this is what I get for E_x . So, it is very clear that E_x has been expressed in terms of, you know proportional to some functions of E_z and this is H_z , right.

So, our objective has been achieved for E_x . Now, you have to do this procedure for E_y , H_x , H_y . Rather than doing all of that, I will simply give you the values, you can actually check for yourself you know, all you need to do is to find a corresponding component and then find another equation, substitute, rearrange all that equations and you will be able to obtain what is E_y , okay.

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$$E_y = -\frac{1}{h^2} \left(\gamma \frac{\partial E_z}{\partial y} - j\omega\mu \frac{\partial H_z}{\partial x} \right) \quad f(E_z, H_z)$$

$$H_x = -\frac{1}{h^2} \left(-j\omega\epsilon \frac{\partial E_z}{\partial y} + \gamma \frac{\partial H_z}{\partial x} \right)$$

$$H_y = -\frac{1}{h^2} \left(j\omega\epsilon \frac{\partial E_z}{\partial x} + \gamma \frac{\partial H_z}{\partial y} \right)$$

~~TEM mode?~~
 $E_z = 0, H_z = 0 \Rightarrow h^2 = 0 \Rightarrow k = 0$
 E_x, E_y, H_x, H_z
 $\gamma^2 = -\omega^2\mu\epsilon \Rightarrow \gamma = j\omega\sqrt{\mu\epsilon} = \alpha + j\beta$
 $\Rightarrow \alpha = 0, \beta = \omega\sqrt{\mu\epsilon} = \omega/v$

TE modes
 $E_z = 0$
 $E_x = -\frac{j\omega\mu}{h^2} \frac{\partial H_z}{\partial x}$
 $E_y =$
 $H_z =$
 $\rightarrow H_y!$

You will be able to obtain what are, all the different terms, but I will just write down for E_y , okay that would be $\gamma \frac{\partial E_z}{\partial y} - j\omega\mu \frac{\partial H_z}{\partial x}$, okay. So, this is one expression for E_y , similarly I have expression for H_x as well as H_z . These are given in the text book, so you can refer to that minus one by h^2 minus $j\omega\epsilon \frac{\partial E_z}{\partial y}$, okay plus $\gamma \frac{\partial H_z}{\partial x}$.

Finally, you have H_y right. H_y is minus one by h^2 $j\omega\epsilon \frac{\partial E_z}{\partial x} + \gamma \frac{\partial H_z}{\partial y}$, okay. So, with all these things known to us, right, so with all these fellows expressed some function of E_z and H_z . Let us actually write down the wave equation of E_z , write down the wave equation for H_z , solve them and then use those expressions in this expression for E_x , E_y , H_x and H_y , okay.

To obtain, right, so once you have done that one, all you have to is to substitute for E_z and H_z after calculating them and substitute and obtain the value for E_x , E_y , H_x and H_y . So, the objective of getting the transverse components in terms of longitudinal components and you

know the relation between the two has been achieved, okay. What do we do from here? Where do we go from here?

First of all, let us see what possible modes that we can obtain, okay. So, let us first try if any wave we can obtain TEM mode. Well, what do we need to obtain a TEM mode? In TEM mode, you have E_z equal to zero, H_z is also equal to zero, right, so this is the TEM mode, right. For this mode in which both E_z and H_z is equal to zero, what will happen to $\text{del } E_z$ by $\text{del } x$ or E_z by $\text{del } y$? What will happen to these components? They would all go to zero.

So, all the components that are mentioned in this brackets will have to be equal to zero and if you want a non-zero value of E_x , E_y , H_x and H_y , the only way you can obtain that is to make h^2 is also equal to zero, okay. Because you now have zero by zero and that zero by zero will make you know a small quantity by small quantity. We will keep everything to be finite.

So, if you want E_x , E_y , H_x and H_z and all of them to be independent of x and y and propagating along z which forms the TEM mode then the condition is that h^2 should be equal to zero or equivalently h is equal to zero. Now, h equal to zero means, γ^2 must be equal to minus $\omega^2 \mu \epsilon$, which also means that γ must be equal to $j \omega \sqrt{\mu \epsilon}$.

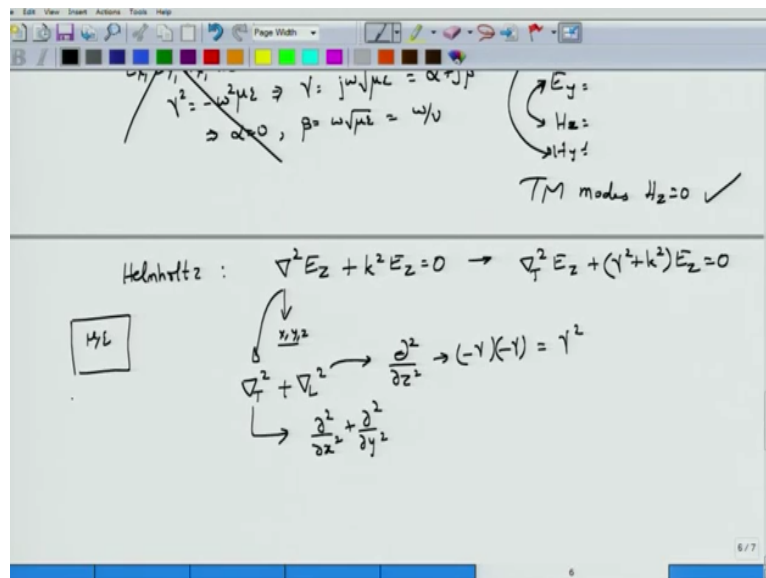
We know that this is $\alpha + j \beta$. This simply implies that α is equal to zero, β is equal to $\omega \sqrt{\mu \epsilon}$ or ωv , okay. So, we have seen this condition, you know for a TEM mode, this is what you need to have a lossless TEM mode condition is required for the waves to be existing. Of course this does not really happen for a waveguide, so, you can conveniently and safely scratch this off from your list of allowed modes.

So, then what about other modes? Can I have TE modes? It is possible. For TE modes, E_z must be equal to zero, and what will happen to E_x in this case? E_x will be minus one by h^2 , right. E_z component is zero, so $j \omega \mu \text{del } H_z$ by $\text{del } y$, so you get minus $j \omega \mu$ by $h^2 \text{del } H_z$ by $\text{del } x$. Similarly, you can write down what is E_y , okay and write down what is H_x and H_y , okay.

You will actually see that E_x and H_y pair can be found, okay. E_y and H_x pair can be found just as you would form in a plane wave scenario, okay. Can I have TM modes? Certainly possible. So, for TM modes, all that we need to ensure is H_z is equal to zero and then E_x , E_y , H_z , E_x , E_y , H_x and H_y will simply be functions of E_z itself, okay. So, this is also possible. So, since we are not writing down the expressions let me write down this over here.

TM modes implies that H_z is equal to zero and these are also valid mode patterns for us, okay. Now, we need to solve the equations, okay because all we have done so far is to establish that we can write down E_x , E_y , H_x and H_y in terms of E_z and H_z and then we can characterize the modes that is possible set of solutions of this Maxwell's equation in this waveguide problem to have two times of modes, TE modes and TM modes, okay.

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So, for these modes we need to actually obtain what is E_z and H_z , okay, but before we do that one, we need to first of all obtain an expression for E_z itself, okay. How do I do that? Well, that is actually quite simple, right. I know from Helmholtz equation, right, I know from Helmholtz equation that $\nabla^2 E_z + k^2 E_z = 0$ for any component of the electric field or magnetic field I can write this Helmholtz equation.

So, $\nabla^2 E_z + k^2 E_z$ must be equal to zero. What is ∇^2 here? ∇^2 is nothing but the Laplacian operator operating on the component E_z . What does a Laplacian operator consist of ∇^2 by ∇_x^2 ∇^2 by ∇_y^2 and ∇^2 by ∇_z^2 . So, this particular operator has components for x , y and z or rather has differential operators with x , y and z , okay. x and y are transverse; z is the longitudinal one.

In fact, I can split this ∇^2 itself into $\nabla^2_{\text{transverse}}$ and $\nabla^2_{\text{longitudinal}}$, okay. There is no inherent advantage of doing this, but this is something that you would find in my grove literature quite often. So, transverse component of the Laplacian is given by $\nabla^2_{\text{transverse}} = \nabla^2_x + \nabla^2_y$. The longitudinal component is actually ∇^2_z which is nothing.

But ∇^2_z multiplied by itself because remember each ∇_z constitutes a γ , so multiplying this one what you get is γ^2 , okay. So, this equation can actually be rewritten in terms of transverse components, $\nabla^2_{\text{transverse}} E_z + \gamma^2 E_z = 0$, okay. So, this is what you wanted to write down.

But, I already know what is k^2 , right because I have this waveguide, right, which is filled with μ and ϵ material.