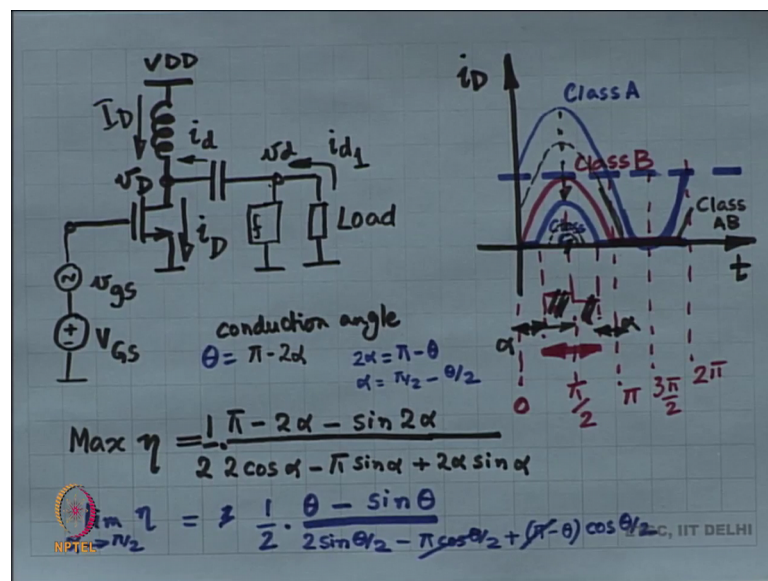


Analog Electronic Circuits
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Lecture – 38
Class D amplifiers, push-pull amplifiers

Welcome to Analogue Electronics. This is a lecture 38 and today we will continue from the power amplifiers that we had discussed in the last class. So, in the last class we were discussing class A, class B, class A B, class C power amplifiers, we had just about started our discussion on class D power amplifiers. So, today our agenda is to cover class D amplifiers and then push pull amplifiers which is another variation of power amplifiers of class B power amplifiers ok. So, in the last class what we were doing so, our power amplifier circuit is the same standard one.

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There is a big inductor for bias purposes, f is a filter ok. And my input has a bias voltage V_{GS} plus a signal voltage which is the actual input. And most of the gain is in this bias voltage. So, you change the bias voltage, you get to select which class of amplifier you are going to be; whether it is class A class B or class C or class A B, where you are in the picture depends on this bias voltage. So, this is what we have studied so far. So, I apply a bias voltage, I apply a signal if the bias voltage is let us say enough to continuously

conduct the MOSFET then, you are in a as a your working as a class A amplifier class A power amplifier.

And we saw that the theoretical upper bound of the efficiency of a class A power amplifier is 50 percent ok. So, the capacitor and the inductor are such that, you can split the DC bias, the DC quantity of the voltage and the current from the signal quantity of the voltage on the current ok. And this filter does a further splitting, the signal small i_d is filtered by this filter such that, only the fundamental component goes into the load, all the other components go through the filter, so this is the arrangement. Now, what we do is, if I start lowering the bias voltage then what happens is that the MOSFET is no longer continuously conducting.

So, let us draw the picture. So, this is small i_d as a function of time. And so one possibility in class A the best case scenario is going up and down in this fashion this is the best case scenario in class A right. In class B you cut off the negative half cycle all together. Alright, so the conduction angle is just 180 degrees. In class C, so let me write this down. So, in between class A and class B if you are somewhere in between then what is that going to be called, it is going to be called class A B ok. So, that is the conduction angle more than 180 degrees, but less than 360 degrees that is class A B.

Then you have got class B, where the conduction angle is 180 degrees. Then, I decrease the conduction angle further and I get class C ok. So, here the conduction angle is less than 180 degrees. Alright, and what we did in the last class was we came up with a closed form expression actually, we said that lets say that the conduction angle is 2 times alpha. So, we said let us say this angle is alpha ok. So, let us say that the MOSFET is conducting from $\pi/2 - \alpha$ to $\pi/2 + \alpha$ in this region. Alright and we came up with a closed form expression for the maximum efficiency of the power amplifier. And we found that this was the maximum efficiency for example, if alpha is 0 so, I am sorry if alpha is yeah am I making a mistake.

Student: Sir that is the, not alpha (Refer Time: 08:16) 0 2.

So, this is what we have done in the last class ok. So, here the conduction angle is actually $\pi - 2\alpha$ is the total conduction angle. So for example, if alpha is equal to 0 then you are actually boiling down to a class B situation so, you get $\pi - 0$. So, π in the numerator and 2 times cos of alpha that is $2 - \cos 0$, so, there was a

half also. Please check the notes there was a half also factor in this. So, we had got a π by 4 as the efficiency when the conduction angle is π ; that is it is a class B circuit ok.

So, this was the situation. And for example, if we now decrease the conduction angle further; let us say I make this α a little more let us say I make α equal to π by 4 then, we had worked out π minus π by 2 minus \sin of π by 2 that is 1 divided by whatever you have and overall you will find that the efficiency has increased. Now, what you are also going to notice is that the efficiency has increased, but the actual values of the numerator and the denominator are both decreasing the actual values ok.

For example, when α has become π by 4 ok, π minus 2 α 2 α is π by 2 minus \sin 2 α , \sin of π by 2 is 1. So, π minus π by 2, so that is π by 2 minus 1. So, you find that the numerator has become of the order of 0.5 little more than 0.5 ok. And the denominator, if you look at the denominator now the denominator has become 2 times \cos α \cos π by 4 ok. So, that is $\sqrt{2}$ minus π \sin α π times $\sqrt{2}$ sorry π by $\sqrt{2}$ plus 2 α \sin α so, 2 times π by 4. So, that is π by 2 times 1 by $\sqrt{2}$ ok. So, if you work this out this boils down to something a little more than 0.5 ok. Overall, you will find that the quantity in the numerator has decreased, the quantity in the denominator has decreased, but overall somehow this ratio has increased as you increase the value of α .

And the reason why this is happening is because remember the quantity in the numerator is related to the power delivered to the load. And the quantity in the denominator is related to the power absorbed from the voltage source VDD. So, the net power delivered to the load, as well as the net power drawn from the supply are decreasing. Ok, you will find the just one factor has cancelled out, there is nothing much in it ok. Both of those quantities are decreasing, that is being reflected by the fact that the height of this current waveform has decreased, when you are decreasing the conduction angle you are making this current waveform smaller and smaller and smaller in size, right the rest of it is all 0 ok.

Now if that is your small i sub capital D that is being delivered by VDD, the average of that is being delivered by VDD. So, the average current is also going down. So, it is not like you are going to give more than you take, the entire thing is going down in size. Alright, in the limit suppose you plug in α equal to π by 2. So, in the limit α is


equal to pi by 2, so you say I am not going to conduct at all or I am just going to conduct at this point, at this one point ok. What you going to find let us try it out if, alpha is equal to pi by 2, how are you going to do it. You are going to plug in alpha equal to pi by 2, so pi minus 2 times pi by 2 is 0 minus sin of pi is 0.

So, your numerator has become a big 0. Your denominator is 2 times cos of pi by 2, cos of pi by 2 is a 0 minus pi times sin pi by 2, so that is minus pi plus 2 times pi by 2, which is pi times sin pi by 2 so, that is also 1. So, minus pi plus pi which is 0, so your numerator is 0 denominator is 0 ok. So, you have got a 0 by 0 situation and therefore, we have to take the limit alpha tends to pi by 2. Alright, instead of alpha tending to pi by 2 let us replace, let us call pi minus 2 alpha as some theta ok. Just so that the maths is easy and I will do limit theta tends to 0.

So, pi minus 2 alpha is theta minus sin 2 alpha. So, 2 alpha is pi minus theta right. So, sin 2 alpha is sin of pi minus theta sin pi minus theta is equal to sin of theta. 2 times cos of alpha 2 alpha is pi minus theta. So, cos so alpha is pi minus theta by 2 or the other pi by 2 minus theta by 2. So, cos of pi by 2 minus theta by 2 is just sin of theta by 2 minus pi times again sin alpha which is going to be cos theta by 2, 2 alpha is pi minus theta and in the denominator you see there is pi minus pi cos theta by 2 plus pi cos theta by 2, so they cancel out alright.

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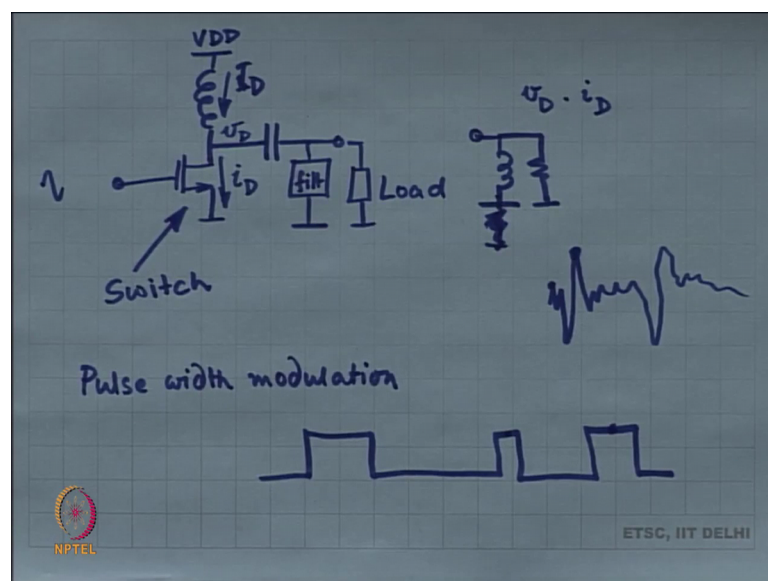
$$\begin{aligned}
 \lim_{\theta \rightarrow 0} \eta &= \frac{1}{2} \cdot \frac{\theta - \sin \theta}{2 \sin \theta/2 - \theta \cos \theta/2} \\
 &= \frac{1}{2} \cdot \frac{1 - \cos \theta}{\cancel{\cos \theta/2} - \cancel{\cos \theta/2} + \theta/2 \sin \theta/2} \\
 &= \lim_{\theta \rightarrow 0} \frac{1 - \cos \theta}{\theta \sin \theta/2} = \frac{2 \sin^2 \theta/2}{\theta \sin \theta/2} \stackrel{\text{L'Hôpital}}{=} \lim_{\theta \rightarrow 0} \frac{\sin \theta/2}{\theta/2} = 1.
 \end{aligned}$$


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And then you get, you can double check, if you plug in theta equal to 0 this is 0 0 0 0 so, you still have 0 by 0 and then we will do a limit. How do you do a limit when there is a 0 by 0, you take the derivative right of both numerator and denominator your L'Hospital's rule. So, you take the derivative of the numerator, you get 1 minus cos theta divided by 2 times sin theta by 2 derivative is half cos theta by 2. And theta cos theta by 2 you have to break it up and these cos theta by 2 is cancel out, this by 2 also cancels out. And you again plug in theta equal to 0 and you see that you have still got a 0 by 0, which is still not good enough, so you do the derivative again perfect. So, one possibility is instead of doing a derivative again, you suggest that 1 minus cos theta is equal to 2 times sin square theta by 2. There is a half which is disappeared mysteriously ok.

So, this sin theta by 2 cancels out yeah it is fine, no there was a theta here, yeah that is right it is correct, we are still doing limit theta tends to 0 and then it is sin theta by 2 by theta by 2, which is equal to 1. So, what do you see over here, you see that as you are dropping the conduction angle all the way to 0, it is as if the efficiency is building up higher and higher and higher all the way to 1. Although in reality as your dropping the conduction angle to 0, you are not doing anything, you are barely supplying any current and barely pushing that current into the load, but whatever you are doing it is very good it is 100 percent efficient ok. So, this limiting case of the amplifier is called a class D amplifier ok where you are conduction angle drops all the way to 0.

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Now, what does that mean; that means that the MOSFET barely ever switches on and when it done switch on ok, so this is our circuit ok. Now, considered the following situation, consider this MOSFET to be a very good MOSFET, very large in size and it is going to operate as a perfect switch. What does a switch do, a switch is either on or off ok. When the switch is on these two voltages are equal. Therefore, the power consumed by the MOSFET, when the switch is on is equal to 0 because, these two voltages are equal ok. Power consumed by the MOSFET is the voltage times the current, right power consumed by the MOSFET is V_D times i_D , when the switch is on V_D is equal to 0, the MOSFET does not get to consume any power.

When the switch is off, i_D is 0 because, the switch is off in which case again the MOSFET does not get to consume any power. So, if I can operate the MOSFET as a switch then the MOSFET does not consume any power at all. Which means, whatever comes from the power supply makes its way to the load, the power that the power supply produces can only be delivered to the load because, nothing else consumes any power ok. So, this is the understanding, this is the class D amplifier. In the class D amplifier what you are going to do is you are going to operate this MOSFET as a switch.

You think nothing is going to happen over here ok, you think you are not going to do anything, the MOSFET is not doing anything, but no you are wrong wait a second ok. What you are going to do is this voltage, what you going to do is you are going to make sure that the signal is enough to switch the device either on or off and the MOSFET is not going to behave like an amplifier at all. This device is so large, so great and the input amplitude is so large, so strong that the MOSFET is going to work like a switch. When it is on immediately V_D is going to become equal to 0 ok. So, all the current will get delivered to the load. When it is off i_D is equal to 0, which means all the power will get delivered to the load ok.

So, this is a classic class D amplifier; class D amplifiers are very hard to make right, the theoretical efficiency of the class D amplifier is 100 percent. However, in a lot of audio systems, a lot of audio systems we find that the class D amplifier is quite popular because of its efficiency. So, what you do is at the input over here instead of applying the actual audio signal right, the audio signal look like this, something instead of applying this audio signal, you encode this audio signal as a pulse width modulated waveform ok. A very fast this audio signal has a bandwidth of 20 kilo hertz maximum bandwidth

including music right, high quality music the human audio signal has a range of 20 kilo hertz, some 20 hertz to 20 kilo hertz ok.

Now, what we do is instead of just a 20 kilo hertz bandwidth, you say that lets take a 1 mega hertz bandwidth alright. And in this 1 mega hertz bandwidth, you convert this 20 kilo hertz signal into a pulse width modulated waveform. What is pulse, what is pulse width modulation, what is it? Here the it is a square wave, where the width of the pulse is proportional to the signal amplitude ok. Suppose, the signal amplitude is this much then I produce this, suppose the signal amplitude is this much, I produce this ok, this pulse. And these pulses are coming fast right much faster than the bandwidth of the signal ok.

So, the bandwidth of this particular signal is much much larger than the bandwidth of the original signal, the original signal is just 20 kilo hertz, this one is very high bandwidth and it is a switching waveform. Now we apply the switching waveform over here right. The current the MOSFET is switching on and off this is a digital signal. Alright this is a pure digital signal the MOSFET is just switching on off on off, when it is on V_D is 0. MOSFET does not consume any power. Power is delivered to the load. When it is off, current is 0, once again power is delivered to the load; no matter what you do, power is delivered only to the load and nowhere else alright.

Applications such as the hearing aid dumb they do not even put the filter over here, lot of hearing aid applications. They do not even bother putting a filter over here why because, they say that the human ear is a good enough filter right. Anyway, the human ear has a range of 20 kilo hertz right, all the harmonics outside of 20 kilo hertz is going to filter it out anyway right. Of course, this leads to a lot of distortion because, if the signal was not 20 kilo hertz, if the signal was 1 kilo hertz then, all its harmonics are there right 3 kilo hertz, 5 kilo hertz, 2 kilo hertz all the harmonics are there, if the signal is 1 kilo hertz, but the hearing aid engineer said that that guy the patient was not able to hear anything, let him hear at least distorted signal it is ok.

Right at this price this is what I am going to give him, he eliminates the filter all together. Ok then, a lot of other applications what they do is they say that the load is inductive in an audio speaker, the loudspeaker right, the speaker itself is an inductor. So, you form an LC filter over here right away. And you engineer the LC values such that, you get the right filtering ok, this is also something that a lot of engineers do. So, they eliminate this

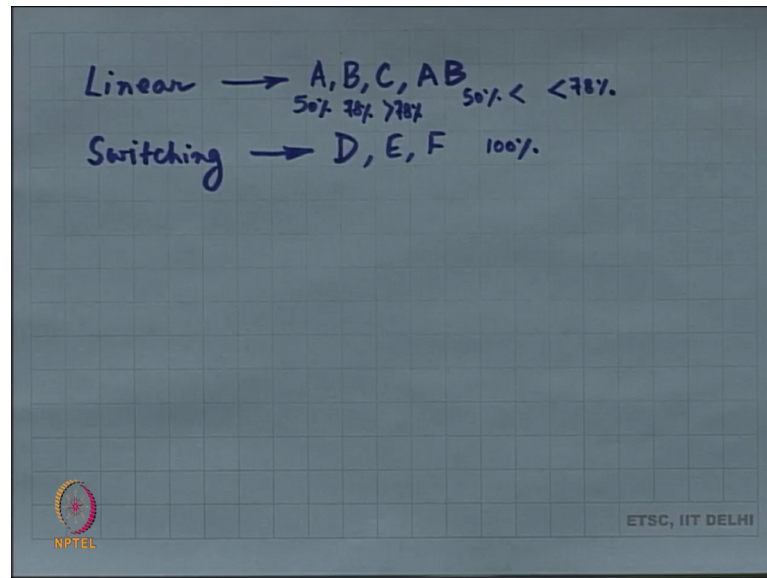
filter altogether alright. So, thus audio speaker is can be modeled as an inductor in series with the resistor, right it is not a pure resistor in which case you have got L c r in series.

Now, you play with the c value and you make sure that it is a nice filter and cuts out all the signals that you do not want ok. You could also remodel this as L in shunt with r right, so lot of possibilities are there. In fact, that would be a more natural model right, L in shunt with r will be a more physical model then L in series with r anyway. So, you play around with these values and you can actually it is possible to eliminate the filter altogether. Hi fi applications will actually put a filter over here right, let us say you have got a hi fi high fidelity audio application, let us say you pay a lot of money and buy nice stereo player right, they are going to actually implement a real filter over there and make sure that the output sound is clean.

However, a lot of these systems come like this ok. There are a few exceptions, the exceptions being car audio amplifiers ok. Car audio amplifiers, audio amplifiers that you used in the car, your radio car, radio speaker right, there you do not use this. And the reason is that this generates a lot of harmonics right, things are very different in the car. There is a lot of electromagnetic emission inside the car and that is going to create a lot of problems right. You do not want for example, this audio amplifier to start it interfering with the engine control ok.

So, lot of critical things are there and as a result in applications like a car, you are going to stick to cleaner amplifiers which are class A and class B are best not class D. Because class D is called is known as a switching amplifier alright. So, these power amplifiers can be classified into two broad classes.

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One class is the linear power amplifier, the other class is the switching power amplifier ok, where the device is being used as a switch. So the switching power amplifier is class D, the linear power amplifier ok. This linear take it with a pinch of salt alright, the circuit is not a linear circuit as such, however the amplitude of the signal varies with the amplitude, the amplitude of the output power, the output power changes with the input amplitude ok.

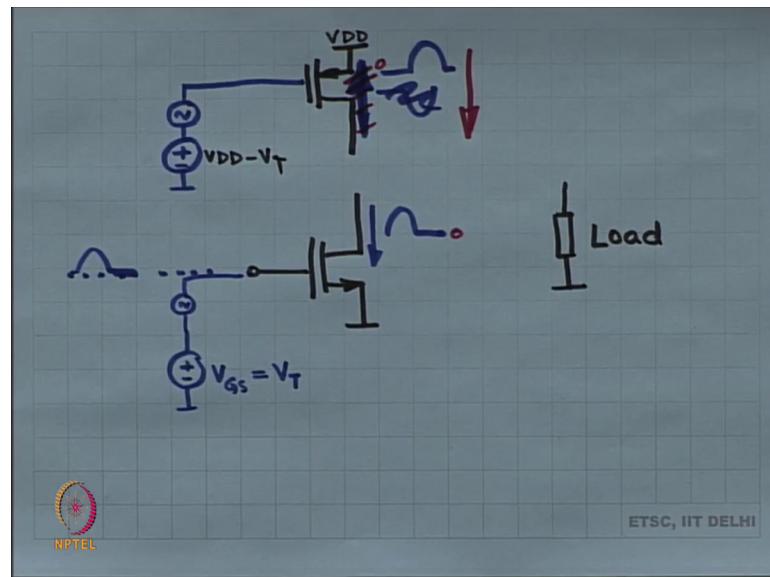
So, these are called linear power amplifiers. A switching power amplifier is class D and then there are a few more they are called class E and class F ok. So, they all are variants of class D power amplifiers, we are not going to study them. Fine efficiency in class A is 50 percent, class B is 78 percent theoretical maximum, class C is greater than 78 percent, class A B is between 50 and less than 78, these the theoretical maximums and class D E F they are all switching their theoretical maximum is a cool 100 percent ok. But then again these are all theoretical maximums, you never really going to hit these values.

For example, if you start designing a class A amplifier, then you are never going to achieve 50 percent, your supervisor, your boss will be happy if you hit 25 ok. You start designing a class C amplifier, you are never going to hit 78 percent you know anything greater than 78 percent, it will be nice if you can manage 70 percent. You start designing a class D D class D E F's are very very hard to design, but you start designing them. Let us say you start designing a class C amplifier right, your target is 10 percent, but you will

never reach anywhere close by, you will probably be somewhere around 70 75 percent you should be happy ok.

So, these are the different power amplifiers right and they are all what is the circuit, the circuit is the same this one right, there is nothing different. It is the same circuit, you are just playing with the VGS value and in case of the switching amplifiers you know, you change the input signal as well, you make it a pulse width modulator nice huge digital signal right, you make the MOSFET big in case of a class D E F amplifier right, but otherwise the basic circuit is the same. The idea is how to split up the current waveform the voltage waveform how to take out the fundamental that is where everything is ok.

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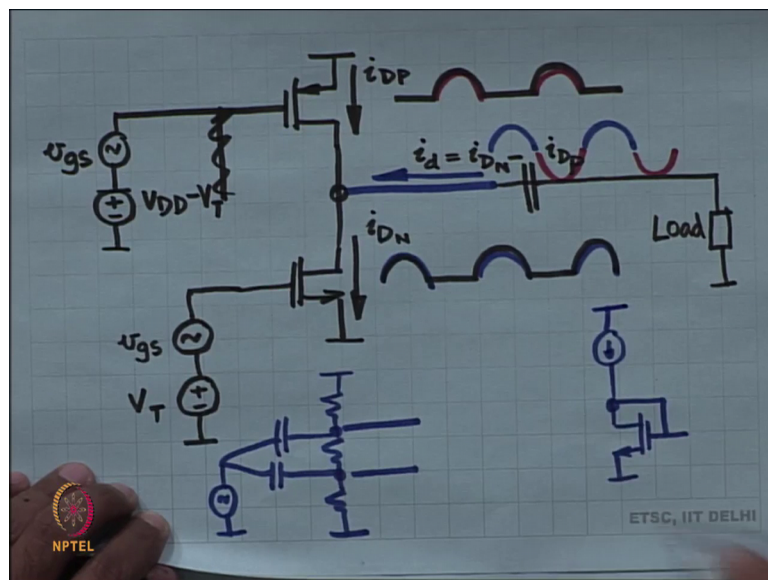
Now, we are going to do one more, one last power amplifier and so let us think about this. So, let us say we are doing a class B power amplifier, we are trying to attempt a class B power amplifier, where the conduction angle is perfect 180 degrees. So, what does that mean; that means, that when my input, so my V G S is probably exactly equal to V T right, something like V T such that, when the input goes below V G S, when the input goes below V G S, this MOSFET does not conduct at all. When it goes above VGS, the MOSFET starts conducting ok.

So, the shape of this current is this fine. What if I make one more amplifier ok, so what if I make one more amplifier, where the shape of the current is this, is that possible? I can implement it easily with another class B P MOS amplifier ok. In case of the P MOS

amplifier, what do I have to do, I have to make sure that this voltage the bias voltage is exactly $V_{DD} - V_T$ such that, when V_{GS} the input signal goes up, this one blocks out everything, but when it goes down it pushes current or rather it draws current the other way right when it goes down yeah ok.

So, this current waveform. If this is equal to 0 the current is 0. If the signal is 0, there is no current. If the signal goes down, there is no current sorry, if the signal goes up there is no current, but when the signal goes down, I am sorry these arrows are wrong. When the signal goes down, the current that is being pushed goes up fine, all of these references are 0. That is the current that is being pushed. Alright is this so far so, the same signal is being applied to both of these transistors both of these MOSFETs. So, let us redraw.

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So, here I am applying something like this and this current has a conduction angle of 180 degrees, the other current also has a conduction angle of 180 degrees fine. And then I hook them up ok, if I hook them up and make sure that the current drawn from V_{DD} is a constant. Suppose the DC current ok, if you look them up what is this other current, this I minus, this minus the other current ok. And this particular current is therefore, going to be in this phase it tracks the first one fine.

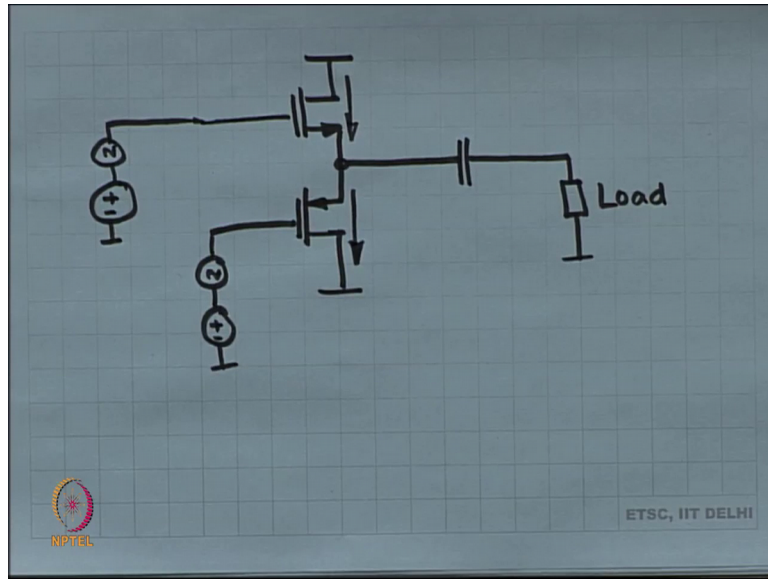
So, what I am doing is I am calling this i_{DN} , i_{DP} and i_d is equal to $i_{DN} - i_{DP}$ alright. And what I do is, I am going to put this across my load alright. When I do that, I get both of these MOSFETs are operating with a conduction angle of 180 degrees pi, pi

is the conduction angle, both of them are class B ok, both of the MOSFETs are operating in class B, is that ok. The resulting current is coming through the load. So, one P MOS is pushing current into the load the other N MOS is pulling current out of the load.

So, this kind of strategy is called a push pull class B power amplifier. The efficiency of this power amplifier is exactly the same as that of the original class B. All that you have done is you have replaced the inductor with the PMOS right and for the PMOS you have replaced the inductor with a NMOS ok. And then you have to organize these bias voltages. These bias voltages are critical ok. You have to organize this to be perfect such that the P MOS is class B, you have to organize this as perfect such that the NMOS is in class B. Once you have organized the biased voltages, everything is going to fall into place. Now, how you are going to do, this is actually your own business alright, it actually is your own business right, one possibility would be that you somehow generate this ok, somehow and then couple the input signal in ok.

You can do this through a resistive network, you can do it through other, but you have to be perfect. It has this has to be something like V_T right, maybe you can do it through another MOSFET right, which emulates a V_T voltage right this should emulate a PMOS V_T voltage right, you can do a number of things to do that. For example, you could have a current source, which is drawing current from VDD right and it gives you a V_T drop over. So, this part is your business, as long as you do this part right this is going to push, this is going to pull. You can even make this as common drain, as a post to commons source. Actually the common drain is also very popular.

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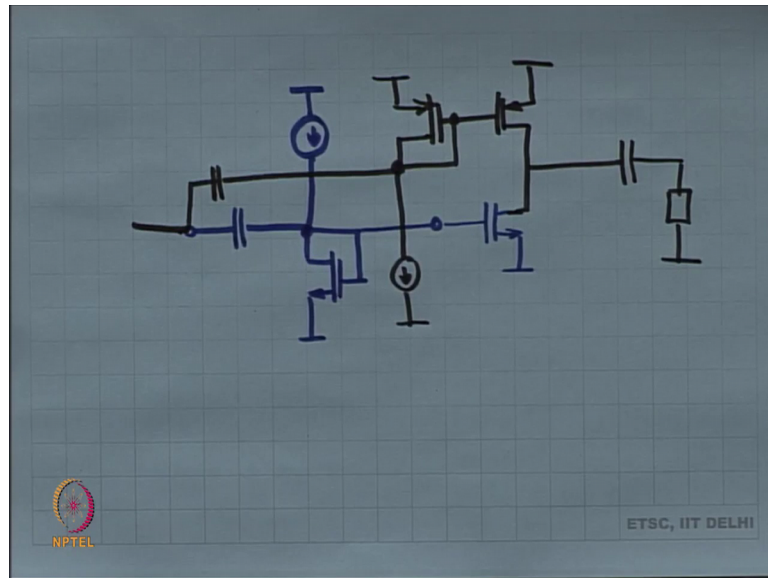
It is a very popular push pull class B power amplifier, where you put the N MOS on top and the P MOS at the bottom. I forgot to put the capacitor over here ok. So, here what you have to do, the N MOS has to be biased just right so that, when the voltage goes up the N MOS works, when the voltage goes down the N MOS does not should not produce any current ok. And likewise, the P MOS is just the same right. This voltage should be such that, it should be perfect such that, when the voltage goes up the P MOS does not conduct, but when the voltage goes down the P MOS draws current.

So, in this case the N MOS is pushing current, the P MOS is pulling current. So, this is also a push pull class B power amplifier ok. The classical ones, the classical push pull power amplifier are made with BJD's bipolar junction devices and you will find them in the books, I encourage you to check them out. However, since we are not going to talk about by BJD's Bipolar Junction Devices in this course at all, I am not going to talk about those classical push pull class B power amplifiers with BJD's ok. With MOSFETs you just have to organize these bias voltages right, BJD is also the problem is the same organizing those bias voltages. They do a lot of tricks to do that with BJD's they use diodes and so on.

In case of the MOSFETs, you can use similar tricks, you can use you can imagine a resistive network like this right, where this drop just has to be V_T of the PMOS, this drop has to be perfectly V_T of the NMOS ok. V_T of the NMOS can be obtained by, you

can obtain a V_T of the N MOS by pushing a small current through a large N channel MOSFET. If I push a small current through a large N channel MOSFET right, V_{GS} required for this MOSFET is going to be very low, which means that this is just going to be enough, it is just going to be V_T right.

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So, for example, this bias network could be built in this fashion. You push a weak current through a large MOSFET; you get your V_T ok. And then of course, you have to couple in the signal into this, your input signal and this goes to your input transistor, input NMOS. And likewise, a weak current if you pull it through a large PMOS, you get a V_T drop over here right and you can couple in your signal and that goes to your input PMOS. And then you organize them as push pull, decouple the load and there you are ok. So, these things can be done alright. So, this more or less concludes our what is the efficiency of this, what is going to be the efficiency of this? 78 percent not 50, 50 is class A right. Here the N MOS is off for half of the time, while the N MOS is off it is not consuming any power ok.

So, during the second half cycle, only the P MOS is pushing power, the N MOS is off. During the first half cycle only the N MOS is pushing power, the P MOS is off alright. Overall it is class B in the first half cycle, class B in the second half cycle overall you get a class B performance of something close to 78 percent π by 4 ok. So, this more or less concludes our discussion on power amplifiers. We have looked at them in quite some

detail right, we have not done enough to actually make real R F power amplifiers for cell phones, but we have done quite a bit right. We have covered the basics of power amplifiers both in terms of audio power amplifier as well in terms of cell phone power amplifiers, which are going to drive an antenna. So, both of those we have covered.

And next we are going to look at voltage regulators in the next class.

Thank you.