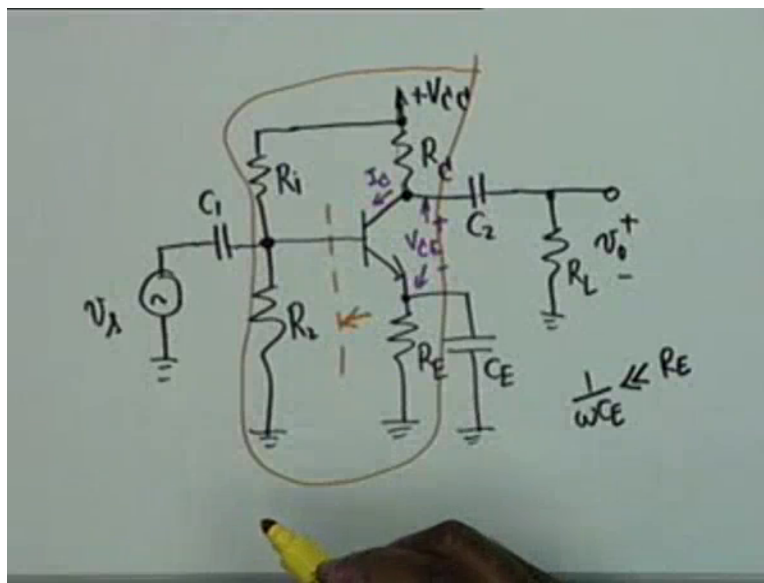


Analog Electronic Circuits
Prof. S. C. Dutta Roy
Department of Electrical Engineering.
Indian Institute of Technology Delhi
Lecture No 05
BJT Biasing and Bias Stability

This is a 5th lecture we start BJT biasing and bias stability. That biasing is a very important phenomenon. For using a device as an amplifier can hardly be over emphasized.

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And the discussion we shall make with regards to a common emitter amplifiers. But the principles shall be applicable everywhere a common emitter. A common emitter BJT amplifier typical circuit is this you have an R_E and R_E is usually bypassed to ground by a capacity C_E the collector is connected to a resistance R_C collector resistance that to power supply plus V_{CC} . And the base biasing the base current is provided from the same supply with 2 resistances with a potential divider. We call traditionally we call this resistance as R_1 and this resistance as R_2 . Obviously this is an npn transistor. And the signal is applied the signal to be amplified is applied through a capacity C_1 to the base circuit, this is the signal to be amplified V_s and the out is take from the collector through a decoupling capacity C_2 to whatever the load is R_L . So this is V_o and this is the AC for the signal output.

You know the purpose of these 2 capacitors C_1 and C_2 are to decouple DC to AC. What we want is that the DC from here should not pass through the signal source. You see what is the internal resistance of this source? If you say voltage generator then the internal resistance is 0. Say it loud why are you so afraid, if you're wrong I will correct you. Okay so if this capacity is not there, then obviously R_2 will be short circuited isn't it right? If this capacitor is not there, the internal resistance of the source is 0 therefore R_2 will be short circuited. And therefore the base will be connected to ground. And the transistor would be off, it cannot be in the active region.

So the capacity C_1 decouples DC being short circuited. Sorry if the capacitor C_2 is not there then the current through R_C will partly flow through to the collector and partly through R_L we don't want that. For example this R_L could be a loudspeaker. The load could be a loudspeaker. If it is an amplifier audio amplifier it could be a loud speaker. If it is a loudspeaker and a DC passes through a loudspeaker the magnet may get into saturation and therefore it may not respond to this signal okay. We don't want DC to pass through the load also if the load varies then the collector current shall also vary. If R_L varies then the proportion by which I_C and I_L change that will change and therefore the biasing point shall also change. So this is a decoupling capacitor. This is another decoupling capacitor. These are facts of life you have to use them.

Student: Sir could you please () (4:45)

Professor: Functions of C_1 and C_2 .

C_1 prevents DC flowing through the signal source and C_2 prevents DC flowing through the actual load that's it. They decouple DC from AC. And the purpose of C_E the third capacitor across the emitter resistance is to act as a short circuit to AC. As far as DC is concerned R_E is effective. There is a drop in R_E but as far as AC is concerned we don't want any drop in R_E so we bypass R_E by a large capacitor. If $1/\omega C_E$ the reactance of the capacity is much less than R_E . Then whatever AC tries, whatever AC comes from the emitter will flow through C_E not through R_E so C_E is effectively an emitter short circuit. It is a short circuit to R_E it is also it is also called a bypass capacity that is AC doesn't not flow through R_E it flows through the bypass. It's called a bypass capacitor.

Student: What is the use of R_L in this, we can directly take the input from the () (6:04).

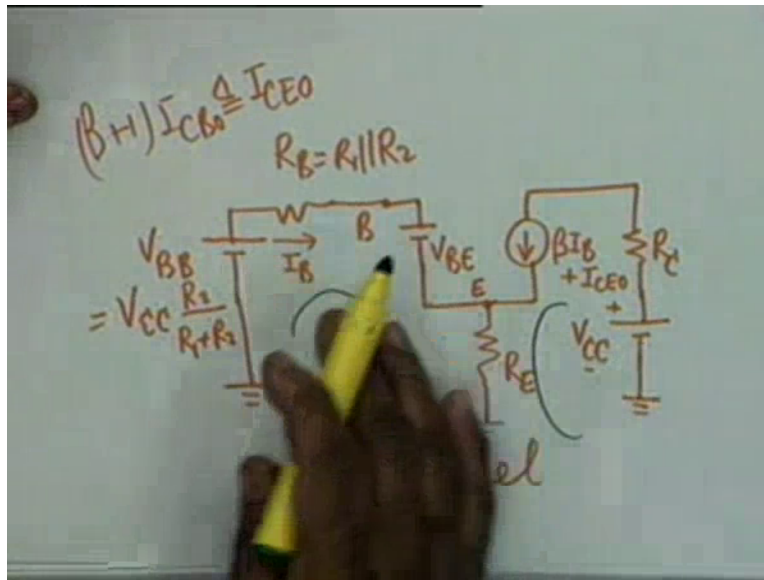
Professor: Then DC as well as AC will come.

Student: No No No if we connect a capacity and we don't connected R L then we take..

Professor: R L is not a matter of choice it's fixed for example let say audio amplifier R L is the loudspeaker, we have to pass the AC through the loudspeaker in order to reproduce the sound. It's not a choice it's not your choice okay. It could be that the output is (∞) that is the load is infinite. For example if you apply this to an oscilloscope, while the effective input impedance is infinity. And therefore it could be open circuit, R L is not your choice R L is dictated okay.

Now the point is in order that this may act as a good amplifier you must choose these 2 quantities carefully that is one is V_{CE} and the other is the collector current I_C . V_{CE} and I_C this define the operating point of the transistor and this operating point must be chosen carefully. Let's look at the DC model of this amplifier and then see where should the operating point be. If notice carefully as far as DC is concern, we can forget about C_1 and V_S , V_{CE} is not affected by this. We can forget about C_E we can forget about C_2 and R L. Therefore as far as DC is concerned all that we have to consider is this resistance, let me use some other color. All that we have to consider is this part of the circuit okay. The rest of the circuit can be ignored as far as DC is concerned. Also you notice that V_{CC} the voltage source is applied across R_1 and R_2 . It is a potential divider, so if I apply thevenin theorem to the left of this line I can replace V_{CC} , R_1 and R_2 by an equivalent voltage source which is $V_{CC} \frac{R_2}{R_1 + R_2}$ open circuit voltage source. And the effected resistance looking back which is R_1 parallel R_2 alright.

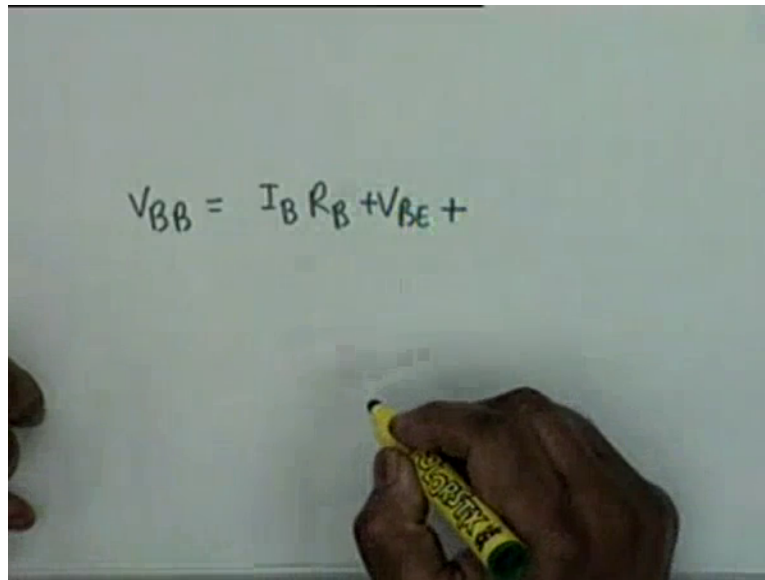
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So if I do that if I do that then my equivalent circuit shall be V_{BB} which is equal to V_{CC} times R_2 divided by R_1 plus R_2 okay this is the thevenin's source then a resistance R_B which is R_1 parallel R_2 okay then we come to the base terminal. From the base to the emitter in the active region you know there is a drop of 0.7 volt. So let's call this as V_{BE} 0.7 the numerical value we will come to later. This comes to the emitter. We are considering the active region so we're not using the diode. Ideal diode is the short circuit anyway okay. The transistor is in the active region and therefore all that happens is there is a drop V_{BE} this is the emitter terminal.

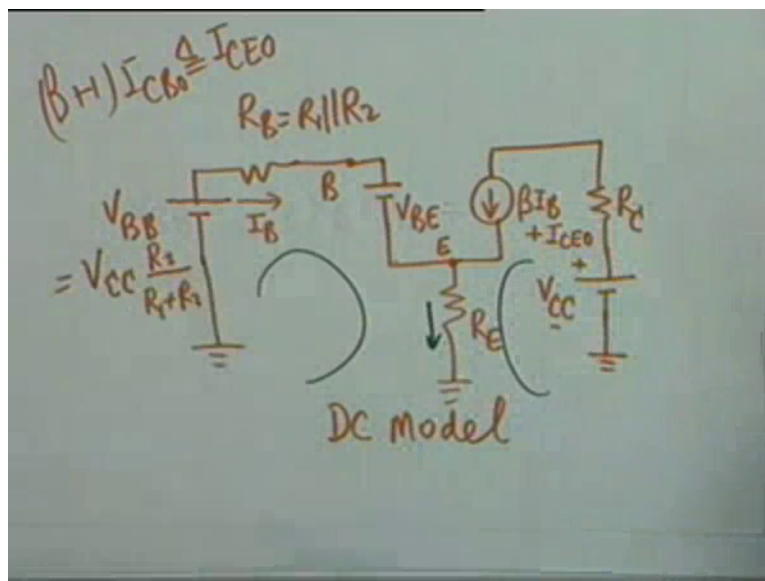
The emitter goes to ground through the resistance R_E this is effective in DC and as far as the collector circuit is concerned what we have is I_C which is equal to βI_B if this current is I_B then βI_B plus β plus one I_{CBO} . I_{CBO} sometimes we call I_{CBO} alright I_{CBO} . So β plus one I_{CBO} and you also know that β plus one I_{CBO} we denote by I_{CEO} . So let's denote it by I_{CEO} . This is the current generator. This is the effective collector current. And we of course have the resistance R_C which goes to not ground it's the DC model, I wanted you to make this mistake yes, it was intentional V_{CC} so this is V_{CC} plus minus that goes to ground the negative terminal okay. So this is my DC model of the common emitter PNP transistor amplifier. And now there are two loops in this circuit. I can write one loop equation here and the other loop equation here okay. Let's look at this loop equation. The first loop the loop to the left.

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You notice that I can write V_{BB} as equal to I_C times R_B this is the drop in the resistance R_B which is the parallel combination of R_1 and R_2 plus V_{BE} plus the current through R_E . let's look at this current.

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This current is the sum of I_B and this current βI_B plus I_{CE0} alright.

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$$V_{BB} = I_B R_B + V_{BE} + [(\beta+1)I_B + I_{CEO}] R_E$$
$$I_B = \frac{V_{BB} - V_{BE} - I_{CEO} R_E}{R_B + (\beta+1) R_E} \checkmark$$
$$I_C = \beta I_B + (\beta+1) I_{CEO} + I_{CBO}$$

So the current is beta plus 1 I B okay. Beta I B and I B from I B from the left and the beta I B from the right, plus I C E O multiplied by R E. This is the base current. This is the left loop equation which gives you a base current as equal to, if you solve for base current it would be simply V B B minus V B E this term goes to the left. And what else minus I C E O R E divided by R B plus beta plus 1 R E. This is the base current alright. Here you will see uhh later on in order to find out I C. Can we find I C from here? I C is beta I B plus I C E O okay and therefore if I substitute beta I B from here, I can get an expression for I C. I will write this expression later because I shall need that. Alright and usually what I will do is when I write the expression for I C I will go back to I C B O that is instead of I C E O I would write beta plus 1 I C B O okay this is a side line we don't need this equation now but we will require this later on, we shall have to utilize this expression for I B.

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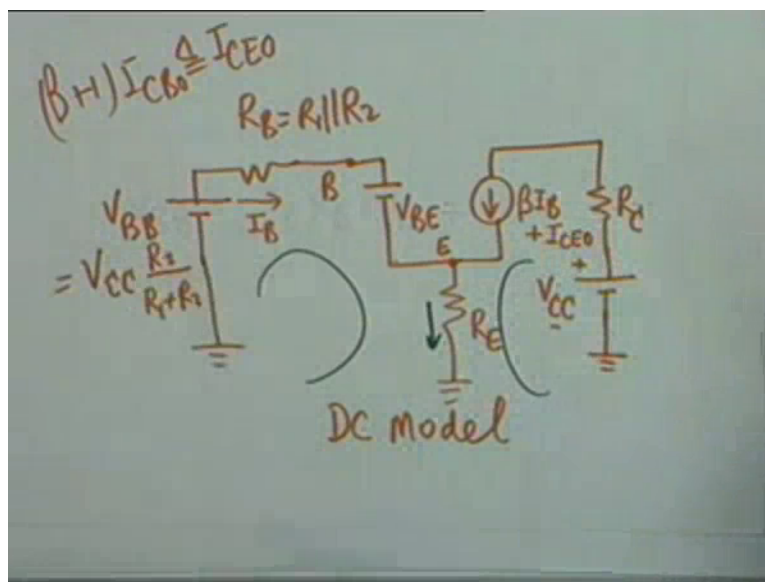
$$V_{CE} = V_{CC} - I_C R_C - (I_C + I_B) R_E$$

$$I_C = \beta I_B + (\beta + 1) I_{CBO}$$

$$I_B = \frac{I_C - (\beta + 1) I_{CBO}}{\beta}$$

$$V_{CE} = V_{CC} - I_C \left[R_C + R_E \left(1 + \frac{1}{\beta} \right) \right] + I_{CBO} \frac{(\beta + 1) R_E}{\beta}$$

$$V_{CE} \approx V_{CC} - I_C (R_C + R_E) \quad \text{DC LOAD LINE}$$



On the right loop if you notice I have V_{CE} okay this voltage from here to here V_{CE} . V_{CE} would be V_{CC} minus this drop drop in R_C which is $I_C R_C$ and then the drop across R_E which is also we have found out. Therefore my V_{CE} should be equal to V_{CC} minus $I_C R_C$ minus I_C plus I_B I want to write this expression in terms of I_C alright. So I don't write βI_B plus I_{CEO} . Instead I write I_C plus I_B times R_E and in this I substitute I want to write this expression in terms of I_C only. I don't want I_B , so what I do is I write I_C equal to βI_B plus $\beta + 1$ I_{CBO} which means that I_B I substitute in this as I_C minus $\beta + 1$ I_{CBO} divided by β agreed and this expression I substitute here. This expression for I

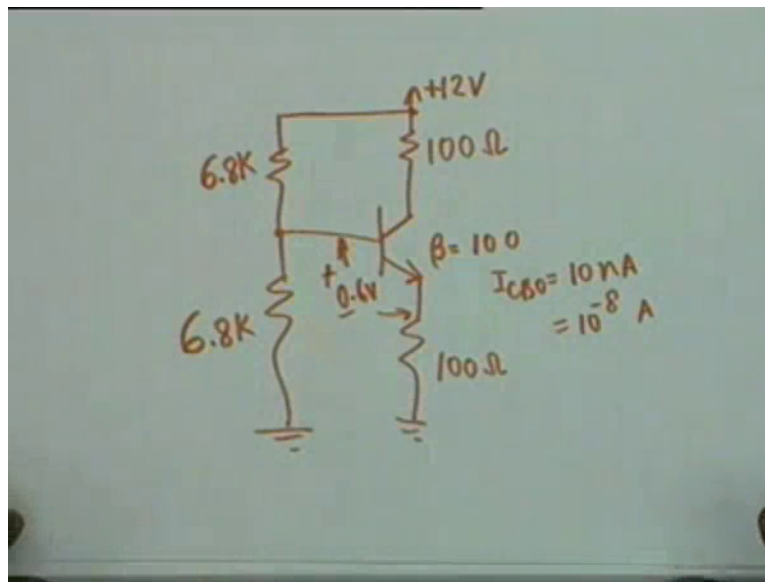
B you see I_B now contains of I_C and some parameters of the transistor. If I do that then I can simplify V_{CE} . I leave the algebra to you as $V_{CC} - I_C R_C + R_E (1 + \beta) I_C$ plus $I_C R_E$ times $\beta + 1$ divided by $\beta + 1$ multiplied yes that is correct. So this is my equation. Is the whole equation visible on the monitor, whole equation including this part?

Student: Yes

Professor: Okay fine.

Now a couple of comments before I go to the next point for consideration. Couple of comments, you know that β is normally much greater than 1. β is the order of 100 and therefore $1 + \beta$ by β approximately you can ignore this part. You can ignore this term $1 + \beta$. It will be 0.01 1 percent of this term. Similarly. $\beta + 1 + \beta$ you can take approximately as 1. Not just that $I_C R_E$ you know is of the order of nano ampere 10s of nano amperes. And R_E is of the order of a K and therefore this whole term is very very small and therefore you can approximate this by $V_{CC} - I_C R_C + R_E$ agreed and this equation describes what is known as the DC load line, DC load line. At DC the load of the transistor is equivalent load is $R_C + R_E$. They don't exactly add to each other. They add with the factor $1 + \beta$. Because β is very large one can take the total load to be $R_C + R_E$ and this equation describes the collector emitter voltage V_{CE} and the operating current I_C in terms of constants in the circuit namely V_{CC} and the total load resistance. So this is called as DC load line. We shall see what import of the DC load line is, but before that let's take a small example.

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And this example we shall we shall continue to take the same example again and again to illustrate the points. It's a typical common emitter pnp transistor amplifier. The plus V C C is 12 volt beta is equal to 100 V B E is given as 0.6 volt for a change 0.6 volt I C B O is given as 10 nano-amperes which is equal to 10 to the power of minus 8 amperes this is given. R 1 and R 2 both are 6.8K. And R E and R C both are 100 ohms. Suppose this is the circuit alright. We r required to find out the operating point of the transistor.

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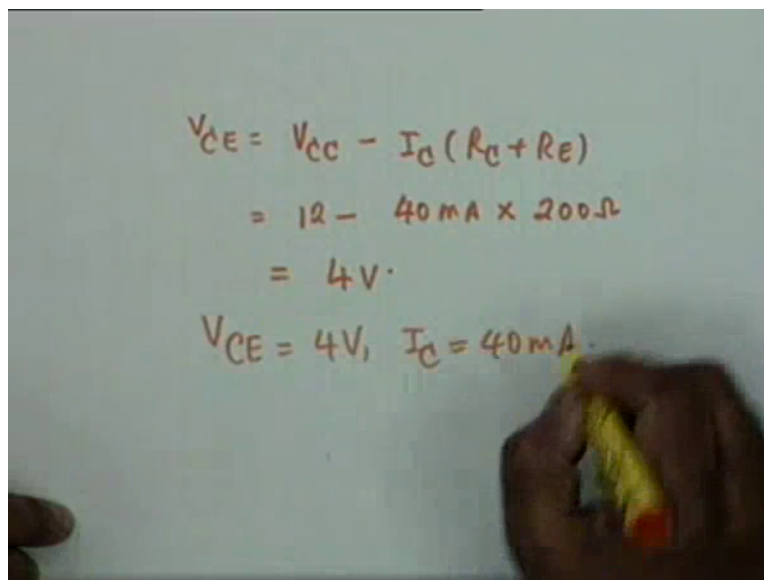
$$\begin{aligned} I_B &= \frac{V_{BB} - V_{BE} - I_{CBO}(\beta + 1)R_E}{R_B + (\beta + 1)R_E} \\ &= \frac{6 - 0.6 - 10^{-8} \times 101 \times 100}{3400 + 100 \times 101} \\ &= 0.4 \text{ mA} \\ I_C &= 40 \text{ mA} \end{aligned}$$

The first thing one does is one uses the relation for I_B and you remember that I_B is equal to $V_{BB} - V_{BE}$ what else minus I_{CBO} times beta plus 1 times R_E divided by R_B plus Beta plus 1 R_E . If you substitute this, $6 V_{BB}$ would be 6 volts now $V_{CC} R_1 R_2$ divided by R_1 plus R_2 minus 0.6 minus 10 to the minus 8. Beta plus 1 is 101 R_E is 100. Even if this, this is of the order of 10 to the minus 4, isn't it right?

Student: Yes sir.

Therefore it can be ignored okay, divided by R_B is 3400 ohms. R_B is the parallel combination of 6.8K and 6.8K so it is 3.4K, 3400 ohms plus 100 multiplied by 101, agreed okay. So this comes out as 0.4 milli-ampere. Which means that I_C if this is 0.4 milli-ampere then I_C is beta times this that is 40 milli-amperes plus beta plus 1 I_{CBO} which is negligible okay and therefore it is 40 milli-ampere. You see in this relationship I_B equal to 0.4 milli-amps and I_C equal to 40 milli-amps the effect of I_{CBO} is negligible because I_{CBO} itself is very very small okay, it's a good transistor. 10 nano-ampere I_{CBO} is a good transistor.

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Handwritten equations on a whiteboard:

$$V_{CE} = V_{CC} - I_C (R_C + R_E)$$

$$= 12 - 40 \text{ mA} \times 200 \Omega$$

$$= 4 \text{ V}$$

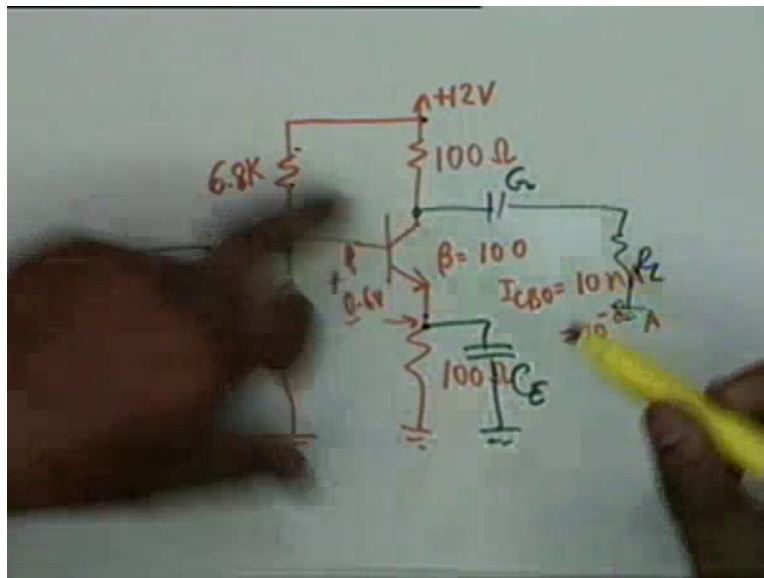
$$V_{CE} = 4 \text{ V}, I_C = 40 \text{ mA}$$

Now if you know I_C naturally you can find out V_{CE} . V_{CE} is yes V_{CC} minus I_C times R_C plus R_E . We have ignored that beta 1 by beta term. And also beta plus 1 plus beta and then the whole I_{CBO} term. It must be understood because in a lousy transistor where I_{CBO} is not that small you have to consider the effect of that alright also if the temperature rises you know I_{CBO} I told you that the reverse saturation current of a diode approximately doubles for every 10

degree centigrade rise in temperature. And therefore if there is rise in temperature you might have to consider I C B O.

For example if rise in temperature is let say by 100 degree C, room temperature is 25 suppose the temperature is raise to 125 then I C B O will multiply by 2 to the power 10, is that clear. We will consider such an example later, now in this particular this is 12 I C is 40 milli-amperes multiplied by 200 ohms. So this is equal to 4 volts okay. So this is my operating point, operating point is V C E equal to 4 volt and I C equal to 40 milli-amps. Now let's look at this operating point uhh I am tempted to alright this is the operating point now, I have slight temptation which I which I want to discuss, a little bit of detour.

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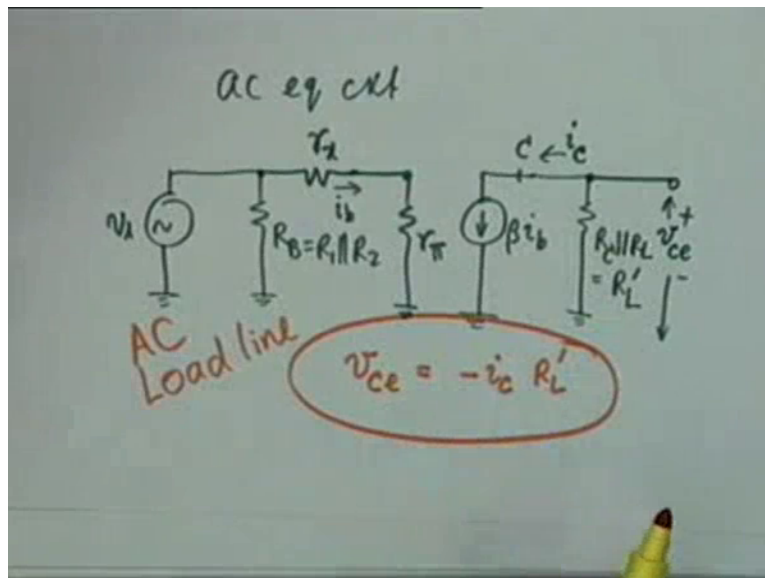
You see all that I need to make this into and amplifier all we shall need to make it into and amplifier is to connect a voltage source here and connect a load here okay. That's all I need, now if I want to draw the AC equivalent circuit alright. What we shall have is the source V S the capacity C 1 and C 2 I also need to connect a bypass here C E. The capacity C 1 and C 2 are so large that at the signal frequency they will act as short circuits. Similarly C E will also act as short circuit. So in the AC equivalent circuit the emitter shall be virtually grounded yes.

Student: Why don't you want any drop in the R E in case of.

Professor: If there is a drop in R_E then it causes loss of gain, it acts as a negative feedback as you shall see later we don't want this. We want as much gain as possible unless it is intentional. Sometimes it is intentional, sometimes negative feedback is used intentionally to stabilize the amplifier, but normally we don't it we want to bypass.

Okay so R_E will be short circuited in other words the emitter itself shall go to ground between the base and emitter I shall have the parallel combination of $6.8K$ and $6.8K$ is that right, between this point and the emitter or ground. At AC this point will be virtually grounded virtually grounded. So between this point and ground we shall have $6.8K$ and $6.8K$ in parallel because the battery is virtually grounded AC grounded so that would be equivalent to $3.4K$. Then from here to here I shall have R_X plus R_{Pie} and the current that flows with the small I_B okay when I come to the collector side. In the collector side only the current generator beta times I_B shall remain alright and in parallel with in parallel with R_C and R_L . R_C and R_L shall be parallel.

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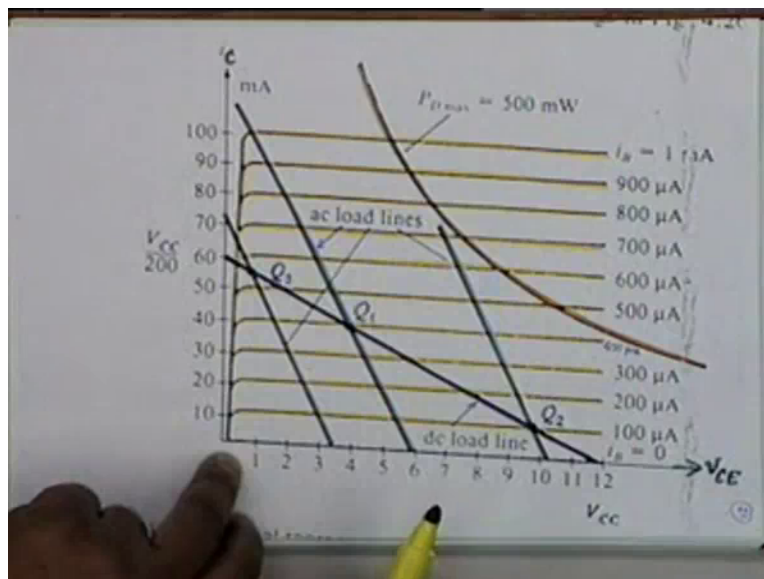
So this this small discussion should convince you that my AC equivalent circuit would be like his V_S then I shall have R_B which is a parallel combination of R_1 and R_2 let me indicate this R_1 parallel R_2 then I shall have R_X which is the base spread IN resistance and R_{pie} . This current is I_B this current is I_B and then on the other side I shall have the current generator from the collector. This is the collector. From the collector I shall have Beta times I_B okay beta times I_B then in parallel with R_C parallel R_L . Let's call this resistance as R_L prime and this value this

voltage therefore is the output voltage and as you see this is the voltage between small v voltage between the collector and the emitter. And since this is AC we write this as V_{CE} plus minus agreed?

Student: Sir please repeat.

This point is the collector and the emitter has been grounded so the output voltage is the incremental part of collector emitter voltage. And since this is AC voltage we used a symbol small v small c small e agreed. And this is the collector current AC collector current which is i_c okay. What is the relationship between this voltage, this current and this voltage. Isn't this simply V_{CE} as equal to minus i_c times $R_{L'}$ agreed. We will require this relationship a little later. We will require this relationship, there is a negative sign because there is a phase change alright, there is a negative sign minus $i_c R_{L'}$ is parallel combination of R_C and R_L . This in fact we brought this in because this equation describes the AC load line. The DC loadline had R_C plus R_E as the load DC load. The AC load is R_C parallel R_L so it is $R_{L'}$. And this is the relationship. V_{CE} equal to minus I_C times $R_{L'}$. We will require this in few moments.

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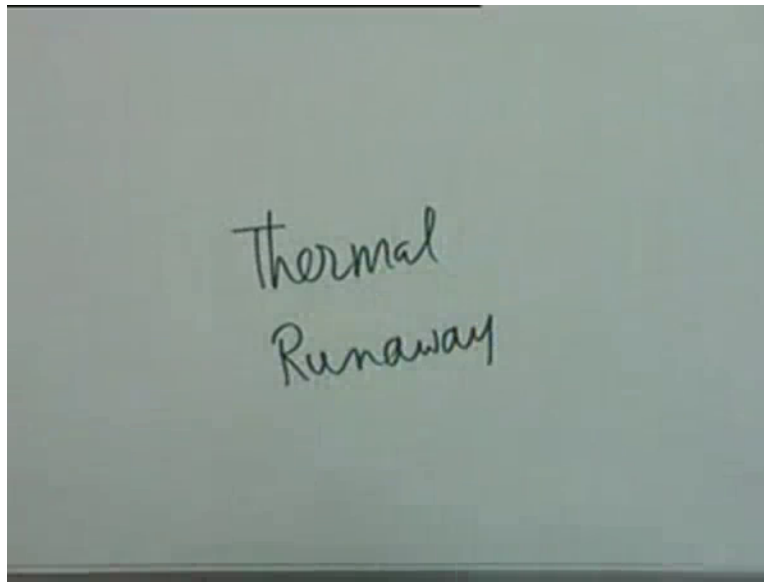


Now let's look at this figure the limits on operation of the common emitter transistor amplifier. I want a different color, green one shall do okay. These are the transistor characteristics this yellow, light yellow shaded curves, these are the transistor characteristics. Typical BJT characteristics as you can see they are approximately parallel to each other and they are

approximately equi-distant. That is from 500 to 600 the increase is about 10 milli-amperes. From 500 to 400 500 is the base current. From 500-400 the difference is approximately again 10 milli-amperes okay. I_C is a plot of I_C versus V_{CE} . It is a plot I_C versus V_{CE} . This line is the saturation line. So our amplifier operation should never go below this line alright. Now there is another line which restricts the operation of a transistor, and this is what I want to introduce at this moment. You see V_{CE} and I_C they denote the Q the operating point of the transistor.

Now if you maintain a voltage V_{CE} in a device across 2 terminal through which a current I_C flows obviously the product V_{CE} times I_C this much power is absorbed by the device alright. And this power is dissipated in the device. How is dissipated, the transistor gets heated. It gets dissipated in the form of heat. Now if the heat is excessive if the heat is excessive then the junction temperature rise and if the temperatures rise 3 things happen. Beta changes, beta changes approximately 50 percent for a 100 degree centigrade rise in temperature. Beta changes if beta changes, it changes it increase, if temperature rise beta increases. Now if beta increases then naturally the collector current again increases isn't that right? If I_B remains the same then the collector current is beta times I_B so it changes it increases. If it increases it causes more dissipation and therefore the transistor temperature goes higher up and this is a regenerated process that means it's a vicious circle ultimately, unless you put off the power supply the transistor may burn.

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This phenomenon is called thermal runaway, Thermal Runaway. The transistor ultimately gets destroyed.

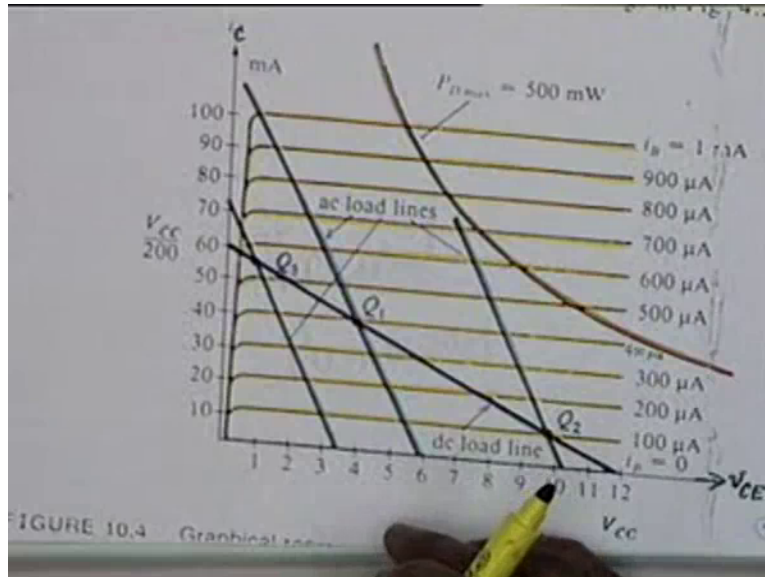
Student: Sir explain this heating effect once more.

Professor: This heating effect okay.

If the transistor is heated, if the transistor is heated because of an excessive current going through the transistor. Then the junction temperature rises and if the junction temperature rises 3 things happen beta changes beta increases V_{BE} decreases I_C no I am sorry I_{CBO} what happens to I_{CBO} ? Increases okay beta this rates our beta approximately changes 50 percent for every 100 degree centigrade rise in temperature. That is if beta was 100 and the temperature is raised by 100 C then beta will become 150. If beta increases, well the other 2 are V_{BE} decreases at the rate of, I told you. V_{DD} V_{DDP} in the first lecture itself 2.5 millivolt per degree C. V_{BE} decreases by 2.5 volt per degree C. This is the rule of thumb okay. And I_{CBO} doubles for every 10 degree centigrade rise of temperature. But the most harmful effect is that of increase in beta if beta increase I_C which is beta times I_B increases causes further dissipation further heat generation and therefore, and this is a regenerative process. The transistor cannot come out of it, ultimately more heat more I_C more heat and ultimately the transistor gets burnt off. And this phenomenon is called Thermal Runaway.

Therefore there must be all manufactures say your V_C and I_C must be such that the maximum power dissipation allowed is not exceeded.

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And for this transistor which is a 2N 222 transistor the PD max is 500 millivolt. This is specified by the manufacturer. Therefore you draw a curve on $I_C V_{C E}$ such that the product. $I_C V_{C E}$ is 500 milli-volts obviously this would be a hyperbola.

Student: Sir how do they calculate the power dissipation of transistor is it simpl $V_{C E}$ into I_C .

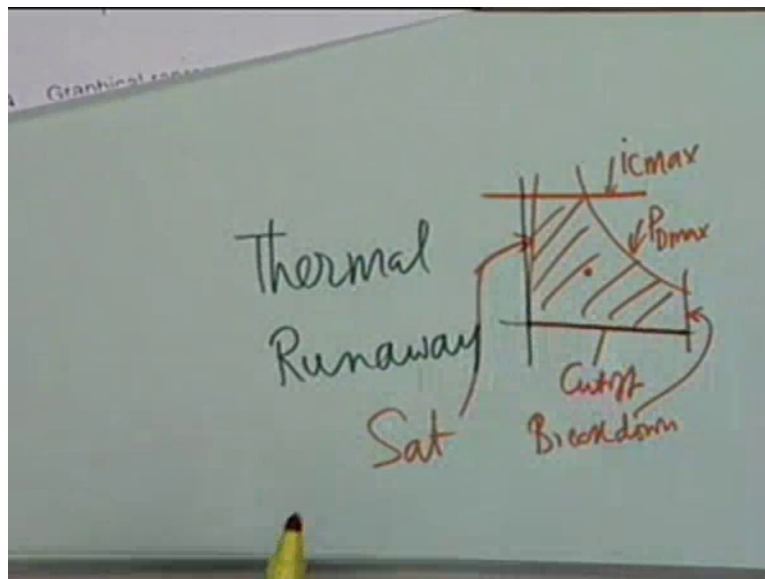
Professor: It is $V_{C E}$ into I_C plus $V_{B E}$ times I_B but normally I_B is 100 times beta times less. And therefore that dissipation is negligible compared to the collector junction dissipation. We normally take $V_{C E}$ times I_C now on this characteristics if you plot $V_{C E}$ time I_C equal to PD max, there is a max allowed power dissipation. You will get a hyperbola. So your operating point must be on the left side of this hyperbola. Is the point clear. This light brown shaded hyperbola. This is the Pd max curve. And do you understand how this is plotted? It is simply $V_{C E}$ times I_C is equal to P D max alright. So you're operation must be to the left of this line. Left of this hyperbola. You're operation must be to the right of this saturation line. So it gradually constraint.

In addition there are other constraints, for example you cannot increase $V_{C E}$ beyond a certain limit what happens? There occurs a breakdown and this breakdown for this particular transistor occurs at about 30 volts. So 12 volt is a safe limit okay, you can't apply a $V_{C C}$ of let say 100

volts, then in all probably the transistor will breakdown. So there is a vertical here, there is a vertical line which restricts not only PD max curve but there is a vertical line occurring at $V_{CE\ max}$. This will also be specified by the manufacturers. Sometimes it is specified as breakdown collector voltage, there are various terms, but you should understand.

Similarly the current that can be drawn from a transistor there is an absolute limit. There is a limit you cannot drop more than that, so there would be a vertical line somewhere here for this transistor this is 800 milli-amps and our operation normally will be restricted to about $1/10^{\text{th}}$ or $1/8^{\text{th}}$ of this. About 100 milli-amps we will not draw more than that.

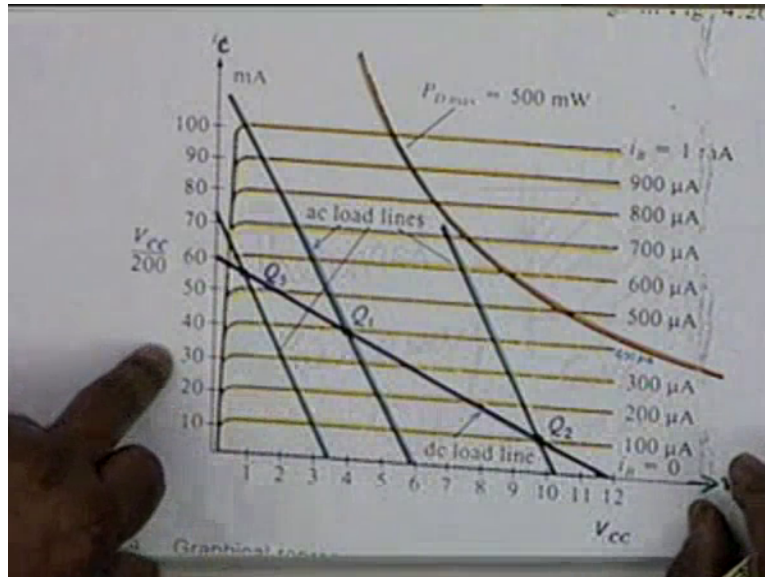
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So you see the operation the Q point of a transistor must lie between several is bounded by several limits one is Pd then you have the saturation line, you have the vertical line collector breakdown limited by collector breakdown. You have a horizontal line limited by the maximum allowable collector current. This is the $I_{C\ max}$, this is Pd max, this line is saturation, this line is decided by breakdown. And whatever the other dimension, cut-off, cut-off is obviously this line right so cut-off. Your key point must lie in this shaded region. Your Q point cannot should not should not lie outside this. Also to be able to operate this as a good amplifier with a reasonably good dynamic range that is if you want a large signal operation then your Q point must be somewhere, somewhere well inside the region isn't it? It should not be too close to the cut-off. It should not be too close to saturation, it should not be too close to Pd max curve, it should not be

too close to breakdown or the I_C max. It must be well inside this, is the point clear? The general principle, that Q point must be well inside this region. What is the best, what is the best? That depends on the situation.

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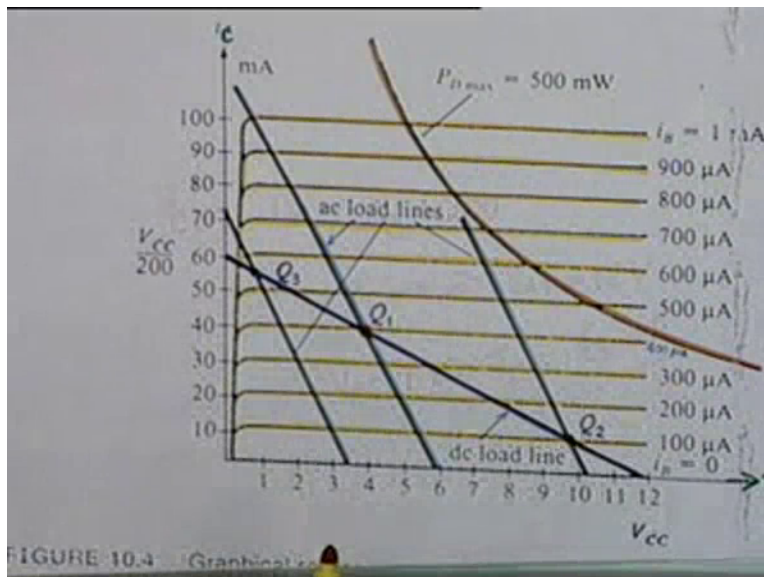
Let's look at the present example. In the present example this light violet colored line joining Q1 Q2 Q3 is the DC load line. You see DC load line as I have told you the equation to the DC load line what is the equation.

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$$V_{CE} = 12 - I_C \times 200$$
$$I_C = 0 \Rightarrow V_{CE} = 12V$$
$$V_{CE} = 0 \Rightarrow I_C = \underline{60mA}$$

V C E is equal to 12 minus I C multiplied by which is 200 ohms. So if I C is 0 V C E is 12 volt alright. And if V C E is 0 then I C is 60 milli-amperes agreed. So to draw 1 straight line 2 point are enough.

(Refer Time Slide: 40:15)



These are the 2 points. You see 12 volt and 0 current 60 milli-amperes and 0 volt. So join these two, then this is the DC load line okay. We have also found out the Q point or the operating

point. The operating point was 4 volt and 40 milli-amps. So Q1 is the operating point, is the point clear? The operating point clear, point about the operating point?

Student: No Sir.

Professor: Is the load line clear?

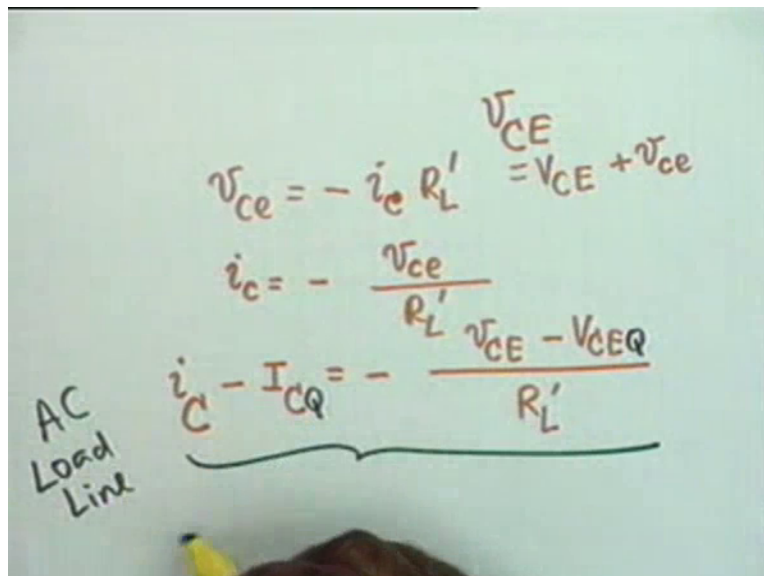
Student: Yes

Okay we had already found out that I C with the kind of biasing that we had found out for the example the collector current was 40 milli-amp and the collector emitter voltage was 4 volts. So draw a vertical line at 4 volt and draw a horizontal line at 40 milli-amps where they meet is the operating point. So Q1 is our operating point alright. Now if Q1 is the operating point and this is the DC load line okay and we're working as, no is Q1 reasonably good operating point?

Student: Yes sir.

It's well inside it's well inside but let's see how it behaves in the in the phase of AC. In the phase of a signal okay. If there is a signal then you know the DC load line is not enough.

(Refer Time Slide: 41:53)



Handwritten equations on a whiteboard:

$$v_{ce} = -i_c R'_L \quad v_{CE} = V_{CE} + v_{ce}$$
$$i_c = -\frac{v_{ce}}{R'_L}$$
$$i_c - I_{CQ} = -\frac{v_{CE} - V_{CEQ}}{R'_L}$$

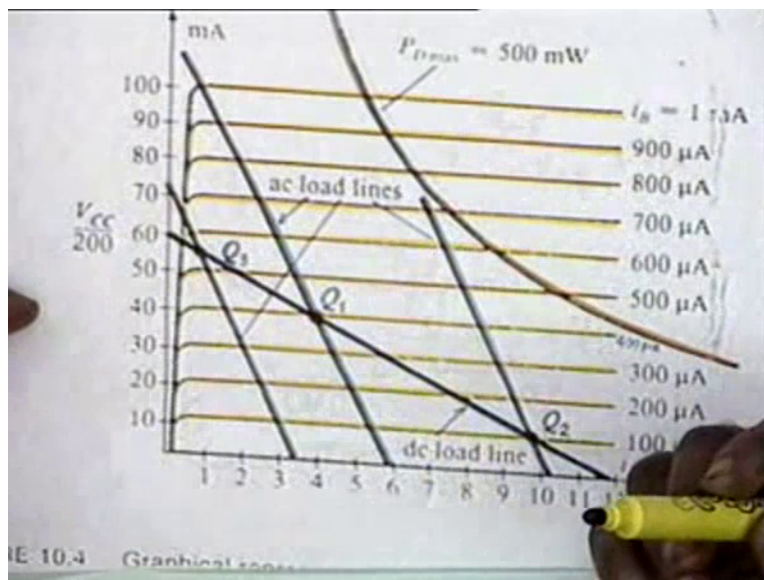
AC Load Line

We have to draw an AC load line and AC load line from the AC equivalent circuit we have already seen, that the AC load line is V_{CE} is equation minus I_C small c small c R_L prime. I can write this as I_C as minus V_{CE} divided by R_L prime.

Student: Sir you said V_{CE} is the increment, can you please repeat that?

Professor: V_{CE} is the AC signal that means it is the power transition well as I have said the total collector emitter voltage is equal to V_{CE} the DC voltage plus small v small c small e. So this is an increment on the DC collector voltage, okay. In order to, well in order to bring this into the picture I write this as i_C total collector current minus I_C alright, this is the value of I_C that is equal to minus 1 over R_L prime. V_{CE} can be written as total collector emitter voltage minus V_{CE} . And in order to emphasize that this is an increment over the Q point or the operating point. Operating point is also called the Q point. I will introduce the additional symbol Q here. That is I_C minus $I_C Q$ equal to V_{CE} minus $V_{CE Q}$ divided by R_L prime. One thing is obvious that this is the AC load line. AC Load line. Significance of Q.

(Refer Time Slide: 43:48)



Operating point is sometimes called the Q point and therefore our amplifier operates around this point that is a signal excursion on the either side of this point. If the signal goes up the collector current goes up, if the signal goes down the collector current goes down okay.

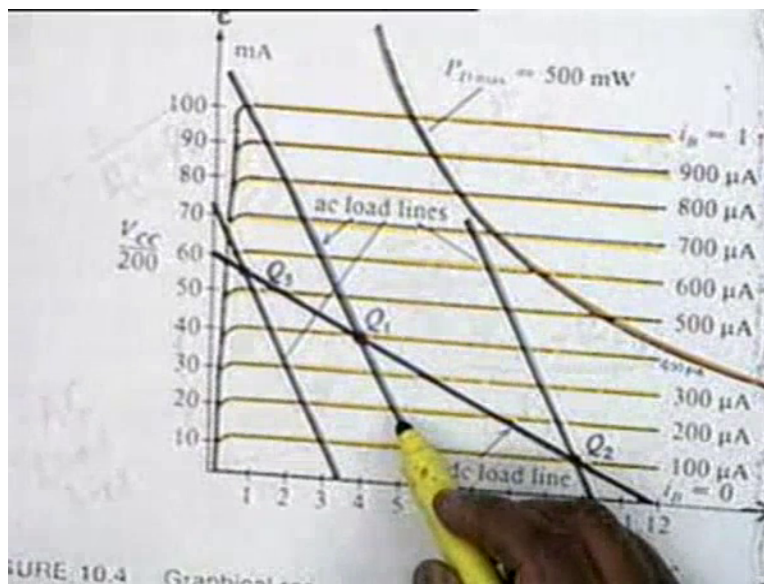
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$$-\frac{1}{R_C + R_E} \quad v_{ce} = -i_c R'_L \quad v_{CE} = V_{CE} + v_{ce}$$

$$i_c = -\frac{v_{ce}}{R'_L} \quad v_{CE} - V_{CEQ}$$

$$i_c - I_{CQ} = -\frac{v_{CE} - V_{CEQ}}{R'_L}$$

AC Load Line



So I have used the additional symbol Q here to emphasize that amplifier operation is around that particular operating point. This is the equation to the AC load line. And one of the things that is obviously is that it is a straight line, isn't it right? Y equal to MX plus C Y is your total collector current. And the slope is minus 1 by R L prime. This slope obviously is greater than the slope of the DC load line. What is the slope of the DC load line? Minus 1 by R C plus R E and R L prime is less than R C. Therefore the slope of AC load line is greater than the slope of the DC load line. Is that point clear?

And the second thing is that the AC load line must pass through the Q point, why? Because when V_{CE} is equal to V_{CEQ} I_C must be equal to I_{CQ} , isn't it right? So the AC load line must be passed through the Q point. And this blue line is the AC load line. As you can see its slope is minus 1 by, what is the value here? 100 ohms and, did I mention what the load is? Load I didn't mention. Take the load as 100 ohms. R_C was 100 ohms, take this also equal to R_L . Then the slope of this line, the slope of this line is minus 1 by the DC load line minus 1 by 200. The slope of this line is minus 1 by 50. So if you know the slope and one point on the line you can draw the line?