

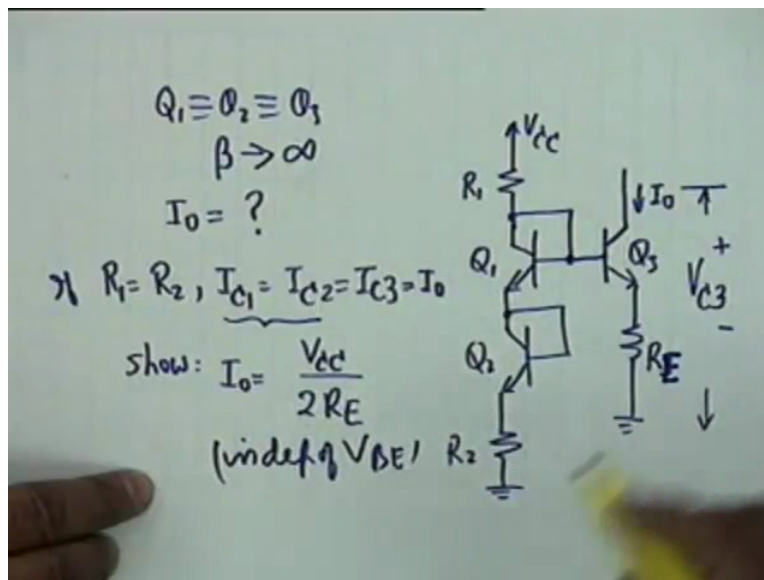
Analog Electronic Circuits
Professor S. C. Dutta Roy
Department of Electrical Engineering
Indian Institute of Technology Delhi

Lecture no 12
Module no 01

Problem Session 3 on Mid-Frequency Analysis of CE Amplifier

This is the 12th lecture and this our problem session 3, we will work out problems on mid-frequency analysis of common emitter amplifiers, the theory that we developed yesterday. We will see its applications in calculating figures for practical problems, but before that we want to take up a couple of problems couple of interesting problems about BJT biasing and current mirrors which we had not done earlier and the 1st problem is this.

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We had a fairly elaborate circuit, try to draw with me, this is Q_1 and its base is connected to the collector, we have a 2nd transistor like this Q_2 whose base is also connected to the collector and then we have a resistance R_2 which goes to ground and this transistor Q_1 drives another transistor Q_3 , the current here is I_0 and the resistance here is R_E connected to the emitter it is R_E and the voltage measured from here to ground is V_{C3} okay, it is not V_{CE} because from collector to ground V_{C3} this is the circuit, it is not the ordinary circuit it is not the ordinary current mirrors circuit, it is not the (∞) (2:53) either, there is an extra transistor and let us see what the question says.

The question says in this circuit assume all transistors to be identical, Q 1, Q 2, Q 3, there are 3 transistors made on the same chip and therefore they are identical. And the Betas are so large that they can be assumed to go to infinity, which means that the base current is negligible compared to the collector current and the collector current and emitter current are the same okay alright, beta tends to infinity, the question is to find an expression for I_0 , this current the current that is drawn by the load transistor, it is this current which is required to be stabilized okay, so find I_0 this is the 1st part of the question and then it says that if $R_1 = R_2$, if these 2 resistors are equal if $R_1 = R_2$ and all collector currents are equal that is $I_{C1} = I_{C2} = I_{C3}$, now obviously this does not require a stipulation, I_{C1} must be the same as I_{C2} because they flow like this.

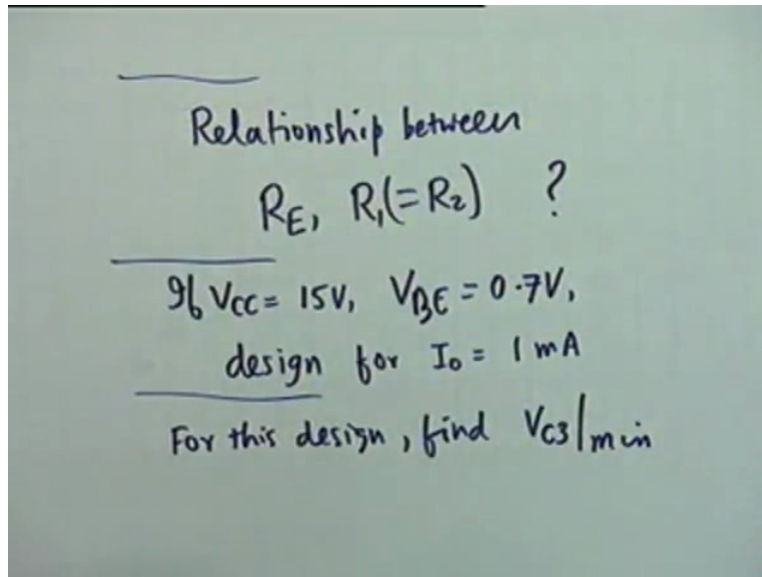
The base current, the only diversion is this base current, this is negligible and therefore $I_{C1} = I_{C2}$ is given by this circuit, what you want to do is I_{C3} which = I_0 , $I_{C3} = I_0$, you want this current to be a mirror of this current alright, you want I_0 to be a mirror of I_{C1} , I_{C1} is the same as current through R_1 because the base currents are negligible.

Student: But there is base current in Q 2 also.

Professor: That is correct, all base currents are negligible.

Beta tends to infinity and therefore what you want is this current which is the reference current should flow in the load transistor also so it says if this is so then show that $I_0 = V_{CC}$ divided by twice R_E , the idea is you remember in the ordinary current mirror, the reference current is $V_{CC} - V_{BE}$ divided by the reference resistance R_1 , here you see this is independent of V_{BE} and this is the purpose of this circuit, this is also a current mirror, you wanted to make I_0 even if V_{BE} is small compared to V_{CC} , V_{BE} decreases with temperature, it is a temperature sensitive element and therefore what you want to do is this current you want to make independent of V_{BE} and this is the purpose of this circuit okay.

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Under this condition the next question is, what is the relationship between, this is also wanted, relationship between R_E, R_1 and R_2, R_1 and R_2 are equal given so what is the relationship that is wanted that means what is the value of R_E required to satisfy this condition that all collector currents are equal then a numerical part, if $V_{CC} = 15$ volts and V_{BE} can be taken as 0.7 volts, design the circuit to have... Design means you find out these resistors R_E, R_1 and R_2 okay, design the circuit to have $I_0 = 1$ milliamperes alright, this is third-party. And the 4th part is, under this condition that is for this design for this design, what is the lowest voltage that can be applied to the collector of Q_3 that is find $V_{C3|min}$, what is the lowest voltage required for the current mirror to operate?

Is there a lowest voltage? Why cannot we apply any voltage that we like? Why is this question, find the lowest V_{C3} ? Pardon me... Saturation that is right, we do not want Q_3 to be in saturation, we want Q_3 to be in the active region that is V_{CB} must be... A quantity like voltage being reversed bias does not make sense, V_{CB} should be either positive or negative, what do you require V_{CB} to be?

“Professor–student conversation starts”

Student: Negative.

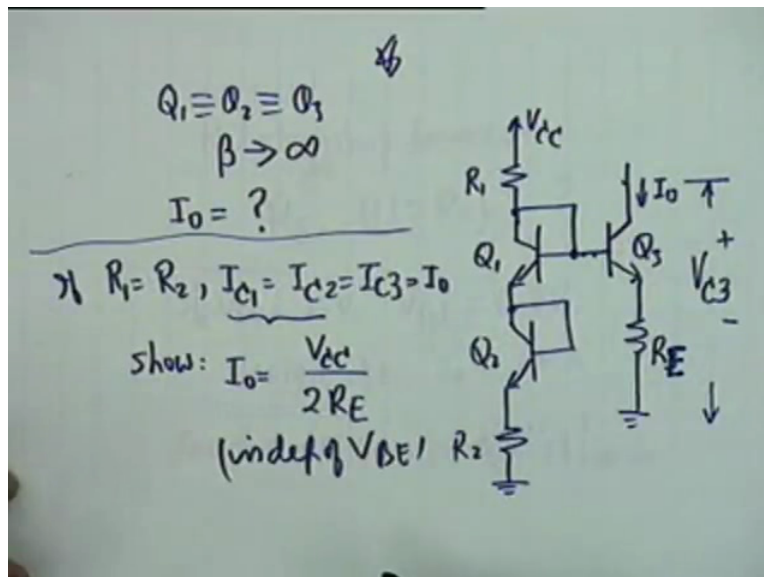
Professor: No.

Student: Positive.

Professor: Positive because it is to be reverse bias, it is an NPN transistor okay, so you want V CB to be positive. Now what is V CB? Just a minute, $V_{CB} = V_{CE} + V_{EB}$ no, let us put it the other way round. $V_{CE} = V_{CB} + V_{BE}$ right, so lowest V CE that is required is V CB at the most can be 0, it should be positive so V CB is greater than = 0 and therefore V CE must be greater than = V BE that means the collector emitter voltage must be no less than V BE no less than 0.7 okay that is the meaning of the 4th question, is the question clear? Yes.

Student: Sir (())(9:26)

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Professor: Oh we have to find a lots of things okay, let me go bag. 1st thing is we have to find I 0 general expression okay, 2nd is R 1 and R 2 and all collector currents are made equal then show that I 0 is this okay. Now if this is to be true then what is the relationship between R E and R 1, if all collector currents have to be equal what is the relationship, then a numerical part design the circuit for a given load current of 1 milliampere.

Student: $I_0 = V_{CC} / 2 R E$ is also a condition for (())(10:12)

Professor: That is correct that is correct, that is if all collector currents have to be equal, what is the relationship between R E and R 1, it is only under that condition that $I_0 = V_{CC} / 2 R E$

alright. Then this is the numerical part and then finally for this design what is the minimum V_{C3} and that I have already explained, why a minimum is needed. Now if you look at this circuit carefully, you can see that this voltage the voltage from here to ground can be calculated by 2 roots, one is via Q 3 and the other is via Q 1 Q 2 R 2 alright.

“Professor–student conversation ends”

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$$V_{BE3} + I_0 R_E = V_{BE1} + V_{BE2} + I_0 R_2$$

$$I_C = I_S e^{qV_{BE}/kT}$$

$$I_0 = \frac{R_2 V_{CC} - V_{BE1} - V_{BE2} - V_{BE3}(1 + R_2/R_1)}{2R_E(1 + R_2/R_1)}$$

$$I_{C1} = I_{C2} = I_{C3} = I_0, R_1 = R_2$$

If I do that then you notice that $V_{BE3} + I_0 R_E$ that is the voltage drop across R_E this should be $= V_{BE1} + V_{BE2} +$ the current through R_2 multiplied by R_2 , now what is the current through R_2 ? If you look at this well, we do not... I want 1st an expression for I_0 so I cannot assume that $I_0 =$ this, I_{C2} okay now I do not want I_{C2} because this is another variable. Even I_{C1} is not guaranteed in general I_{C1} is not guaranteed to be I_0 so what I do is, look at this I find out current in this, what is this current? This is V_{CC} - this drop which contains I_0 , these are tricks of the trade, I do not want extra variables I want I_0 so I do not want to write in terms of any... so V_{CC} - this drop divided by R_1 is the current...

Student: We should get it directly Sir, $V_{CC} - V_{BE}$ was $- V_{BE2}$ divided by $R_1 + R_2$.

Professor: Yeah that also I can do yes that also I can do, I prefer to do it this way because I_0 is involved here okay, let us try this. So this current is, let me use a different colour, this currently is $V_{CC} - V_{BE3} - I_0 R_E$ divided by R_1 and this is the current that flows through R_2 and

therefore the drop in R_2 would be $= V_{CC} - V_{BE3} - I_0 R_E$ divided by R_1 multiplied by R_2 , why did not I do it the other way that this gentleman suggested because V_{BE1} and V_{BE2} are already there and this would be an identity okay. I want I_0 , I want to find an expression for I_0 in terms of known quantities V_{BE} , I_0 that is the load current and V_{CC} .

If I... obviously now I get a general expression for R_E , if you clear the algebra then I get I will skip this algebra, what I get is $I_0 = R_2$ by R_1 multiplied by V_{CC} which you can see R_2 by R_1 multiplied by $V_{CC} + V_{BE1} + V_{BE2}$ - this V_{BE3} comes on the other side, it comes on the other side, $V_{BE3} + \dots + 1$ comes from here and R_2 to by R_1 is here so $1 + R_2$ by R_1 whole divided by R_E , $I_0 R_E$ and here $I_0 R_E R_2$ by R_1 so R_E , $1 + R_2$ by R_1 , this is the general expression alright. Now if I_{C1} the collector current of the 1st transistor, I_{C1} and I_{C2} are obviously equal, if I_{C1} and I_{C2} are equal, obviously their V_{BE} must be identical, collector current is I_s exponential e to the power V_{BE} by $k T$, so V_{BE1} and V_{BE2} can be written as twice V_{BE1} agreed we have eliminated one of the unknown quantities.

And then if it says that $I_{C1} = I_{C2}$ this is given and if it is required if it is forced to be $= I_{C3}$ that is I_0 , this implies that V_{BE3} is also $= V_{BE1}$ alright, and in addition...

“Professor–student conversation starts”

Student: Under what conditions it = that?

Professor: Under what conditions... If the collector currents of 2nd and 3rd transistors are same, if collector currents of the 2 transistors are same their V_{BE} must be identical.

Student: Only then?

Professor: Yes because they are identical transistors, their saturation current I_s are equal. You remember $I_{sub C}$ is approximately $= I_{sub E}$ is given by $I_s e$ to the power $q C V_{BE}$ by $k T$.

Student: Sir in this case there is no quantity as I_{C3} , why are we including other variables unnecessarily?

Professor: I_{C3} is same as I_0 , just to indicate that it is the collector current of 3rd transistor that is all Okay, any other questions? No.

“Professor–student conversation ends”

So what I get is under the special condition that all collector currents are equal and also $R_1 = R_2$ then you see twice V_{BE1} shall cancel with this quantity, is not that right? This is $1, 1 + 1 = 2, 2 V_{BE3}, V_{BE3}$ is same as V_{BE1} , so these 2 quantities shall cancel with each other under the special condition and this will become a 2 alright, so and R_2 and R_1 are equal for this also becomes unity.

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The image shows a whiteboard with handwritten mathematical equations. At the top, it says $I_0 = \frac{V_{CC}}{2R_E}$. Below that, a circled equation states $I_0 = \frac{V_{CC}}{2R_E} = I_{C1} = \frac{V_{CC} - 2V_{BE1}}{2R_1}$. At the bottom, the final derived relationship is $R_1 = R_E \left(1 - 2 \frac{V_{BE1}}{V_{CC}}\right)$ with a checkmark to its right. A hand holding a yellow marker is visible at the bottom center of the whiteboard.

In other words I get $I_0 = \frac{V_{CC}}{2R_E}$ which was the 2nd part of the question okay, $\frac{V_{CC}}{2R_E}$ and obviously you see this is independent of V_{BE} , this was the purpose of the current mirror, this is the current mirror this is the purpose of the current mirror. Then the relationship between R_E and R_1 , you see $I_0 = \frac{V_{CC}}{2R_E}$ divided by twice R_E , this is also $= I_{C1}$, which is I_{C1} if $V_{CC} -$ now the resistors are equal and Q_1 and Q_2 identical so twice V_{BE1} divided by $2R_1$, now we use this formula because I want the relationship between R_E and R_1 , obviously if you take these 2 quantities off you get a relationship between R_1 and R_E and this relation after clearing the algebra will become $R_1 = R_E \left(1 - 2 \frac{V_{BE1}}{V_{CC}}\right)$, this is the required relationship okay.

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$$\begin{aligned}I_0 &= 1\text{mA} \\R_E &= \frac{V_{CC}}{2I_0} = \frac{15}{2\text{mA}} = 7.5\text{K} \\R_1 = R_2 &= 7.5\text{K} \left(1 - \frac{2 \times 0.7}{15}\right) \\&= 6.8\text{K} \\V_{C3|min} &= 0.7 + 7.5 = \underline{\underline{8.2\text{V}}}\end{aligned}$$

Now as far as design is concerned is very simple, design is I_0 is required to be 1 milliampere, therefore R_E shall be = V_{CC} divided by twice I_0 this is the relationship that we have obtained, I_0 was V_{CC} by $2R_E$ so this is 15 volts. Did I give you V_{CC} ? V_{CC} is 15 volts divided by 1 milliampere is required the current so this is 2 milliampere and that becomes 7.5 K and from the relationship between R_1 and R_E , I get $R_1 = R_2 = R_E$, which is 7.5 K multiplied by $1 - 2 \times 0.7$ divided by 15 and this calculates out to 6.5 K. Finally the $V_{C3|min}$ what would this be... Not 0.2... $0.7 + I_0 R_E$ which is which is 7.5 volts, R_E is 7.5 K and 1 milliampere so this = 8.2 volts, this is the minimum voltage that is required to be maintained between the collector and ground, if it falls below this, Q_3 shall go into the saturation region agreed? That completes the question.

“Professor–student conversation starts”

Professor: Any questions on this relation? No.

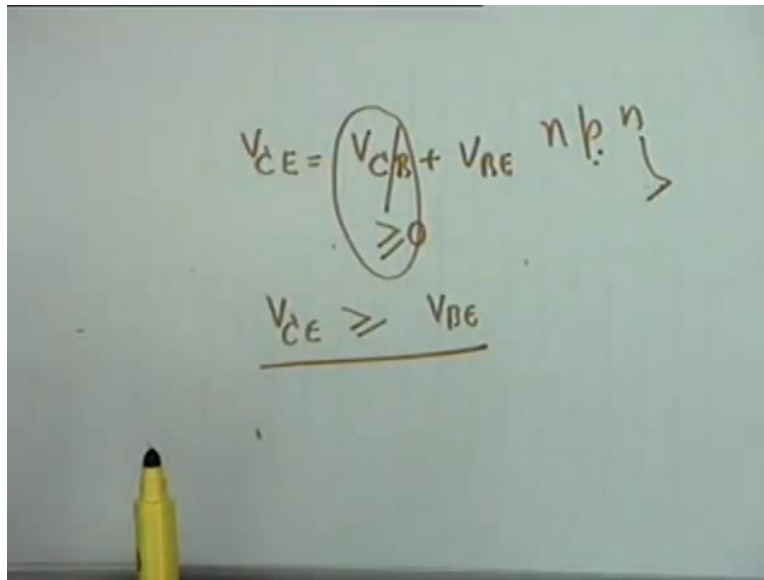
Student: Sir.

Professor: Yes please.

Student: Like V_{BE} for the saturation and active phase you have taken it to be 0 or positive?

Professor: V_{BE} we have taken as 0.7 for the active region yes... No, I have not taken it 0, I must explain that.

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You see what I said was V_{CE} alright, let us go back is $V_{CB} + V_{BE}$ alright, and V_{CB} has to be greater than = 0 therefore V_{CE} has to be greater than = V_{BE} that is what I said.

Student: Why did you take V_{CB} greater than = 0.

Professor: Because the collector base junction must be reversed bias and since it is an NPN transistor...

Student: Sir but it would be reversed bias for (())(21:16).

Professor: No, collector has to be positive with respect to the base, V_{CB} cannot be negative that is what we are saying.

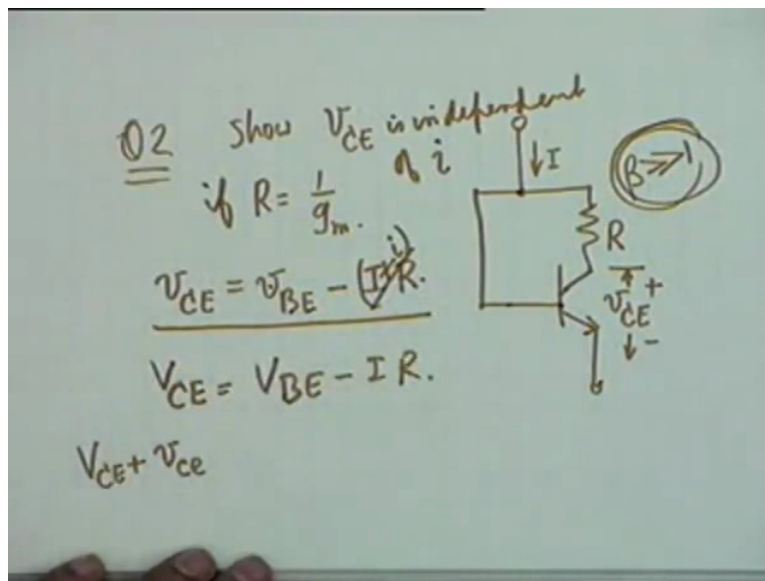
Student: There is specific voltage for active cut in also.

Professor: No, that is not what we are considering, we are only saying that V_{CB} must be reverse biased, V_{CB} cannot be negative V_{CB} must be positive, collector must be positive with respect to the base so V_{CB} is greater than 0 greater than = 0 so V_{CE} must be greater than = V_{BE} , mind

you we are finding the lowest voltage okay. It is only when V_{CE} is greater than $= V_{BE}$ that it will go into the active region otherwise it will not, this is the lowest, you cannot go below this.

“Professor–student conversation ends”

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Question 2 is a mixture of AC and DC and it is a tricky question, a simple question but a tricky question. It says a very simple circuit, a current I flows here and a single transistor with a resistance R this voltage is $V_{CE} + -$ and the supply is connected directly to the base, this is the circuit very simple circuit. It says that the question is the following, listen to the question carefully. The question is, with change in I if I changes, show that V_{CE} is a constant show that V_{CE} is independent of I provided $R = 1/g_m$ okay, show that V_{CE} is independent of small changes in I provided this resistance is carefully chosen okay. Now to look at this $v_{CE} =$ pardon me...

Question is complete Question is complete, you have to show that small v_{CE} is independent of... Variation in capital I we will write as small i okay. If capital I changes, show that v_{CE} does not change provided $R = 1/g_m$ this is the question, how do we solve it?

“Professor–student conversation starts”

Student: Sir is the emitter connected to ground?

Professor: It does not matter, it could be connected to ground, it could be connected to a negative supply, it could be connected to a resistance and ground it does not matter, wherever it is connected.

Student: (0)(24:46)

Professor: Pardon me.

Student: If it does not matter where it is connected, we can use it as (0)(24:52) any circuit.

Professor: Yeah, you can use it as part of any circuit provided there is a flow of, there is a path for flow of current, it cannot be hanging okay, it must be connected to ground through a supply through a resistance whatever it is alright. Now how do we solve the circuit? You if you look at V_{CE} , this point is same as this point so it is v_{BE} - the drop in R , is not that right? Okay, so it is v_{BE} - what is the drop in R ? Capital $I R$ is the total...

Student: Sir there will be base current also.

Professor: There is a base current, we assume that Beta is much greater than 1, this condition is required alright.

“Professor–student conversation ends”

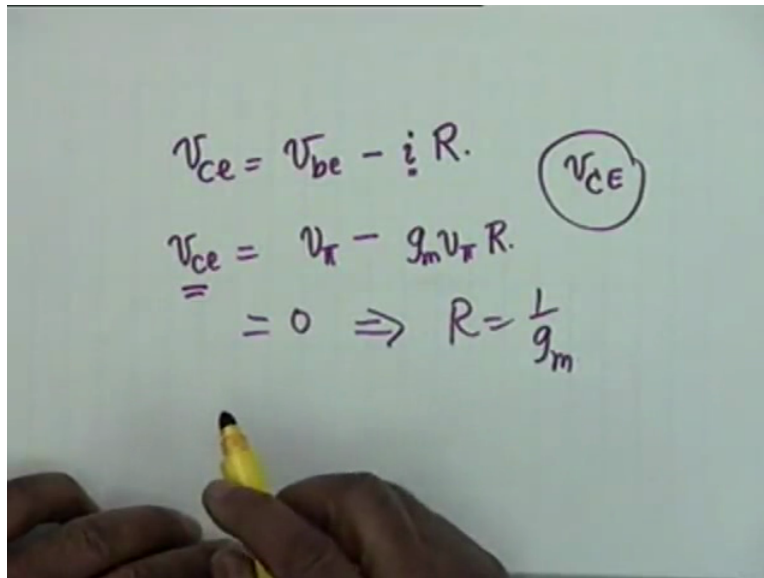
Now small v_{CE} is the total collector emitter voltage, small v_{BE} is the total base emitter voltage so I must include in I if I is taken of the DC part small variations that is $I + i$, is the point clear? If we write the V_{CE} , V_{CE} is fine V_{CE} is this $V_{BE} - I R$, if I write the total what is the total? This is $V_{CE} + \text{small } v_{CE}$ okay the total voltage, similarly V_{BE} the total voltage is capital $V_{BE} + \text{small } v_{be}$, similarly I must include the total current here that is small changes in I therefore I changes to $I + i$.

Student: (0)(26:56)

Professor: Yes if Beta is much greater than... Not 1 not just greater, much greater therefore we ignore this current okay, we ignore this current. Now let us let us take the incremental part of this equation this totally equation, I can write v_{CE} is $V_{CE} + v_{ce}$ similarly, v_{BE} is some of the DC

part + AC part, then obviously because the circuit is linear, the DC part will balance and AC parts will balance alright.

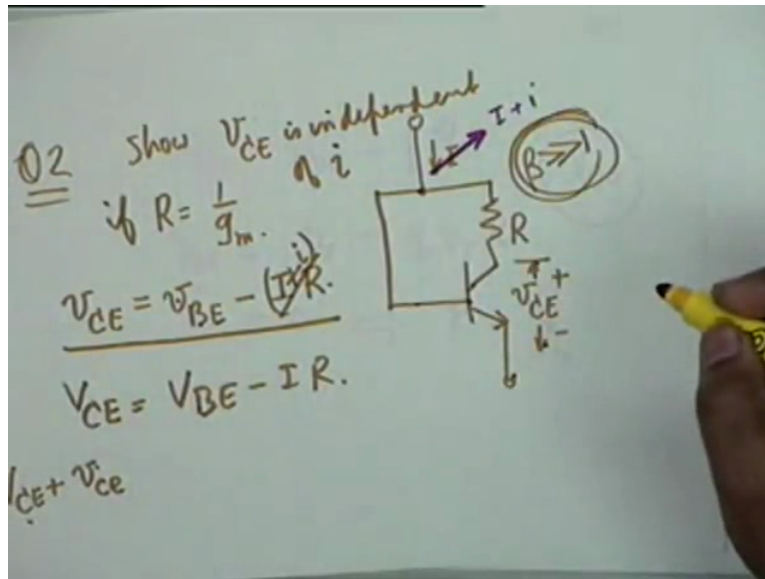
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The image shows a whiteboard with handwritten equations in purple ink. The first equation is $v_{ce} = v_{be} - i R$. To the right of this equation is a circled label v_{CE} . The second equation is $v_{ce} = v_{\pi} - g_m v_{\pi} R$. Below this, the equation is set to zero: $= 0 \Rightarrow R = \frac{1}{g_m}$. A hand holding a yellow marker is visible at the bottom of the whiteboard.

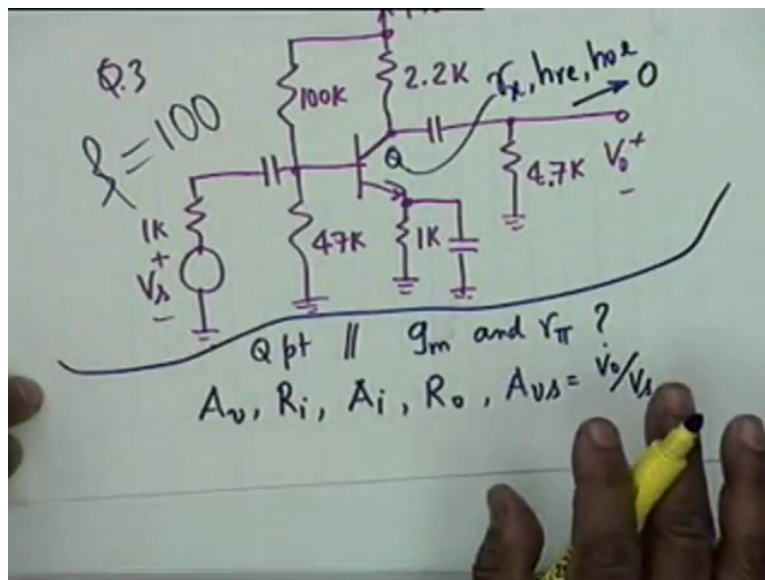
So if I write the AC part of this equation, what I get is, I get $v_{ce} = v_{be} - i R$ okay, now what is the relationship between v_{be} and v_{π} ? They are equal approximately ignoring r_x okay. And what is the relationship between this incremental collector current and v_{π} ? $g_m v_{\pi}$ okay $g_m v_{\pi} R$, so I get $v_{ce} =$ this agreed. What I want is that that v_{CE} should be independent of small i the total collector emitter voltage should not depend on small i , so what I want is even if there is an i the v_{ce} should be $= 0$ so this is 0 which leads to $R = 1$ by g_m .

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My question was that even if this I changes, this should be independent of this change. In other words if $R I$ changes to $I + i$, v_{CE} should remain as V_{CE} , it should not contain any AC part, which means that the AC part of this should be $= 0$ which is what I have done here. So I proved that if $R = 1/g_m$, the collector emitter voltage remains steady, it is independent of variations of the collector current, question 3 is a question on common emitter amplifier.

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Question 3, draw the amplifier with me, there is a + 10 volts supply, 2.2K the transistor with an emitter resistance of 1K, there is a capacitor goes to 4.7K, there is a capacitor here also which I forgot to draw, there is a capacitor here also and the base biasing is through 100K and 47K , there is a capacitor here coupling and the source resistance is 1K, you have a V_s here and this is V_0 , this is a simple common emitter amplifier okay. The questions are the following, have you been able to draw?

Firstly we have to find the Q point of the transistor Q that means you have to find out I_{CQ} and V_{CEQ} okay Q point. And from that you have to estimate g_m and r_{π} , it is given Beta for the transistor is given as 100 and 25 degree C and it is also given that for the transistor r_x now note the way it is specified, r_x , here now we are mixing hybrid π parameters with hybrid parameters because these are what are specified by the manufacturers. It says r_x , h_{re} and h_{oe} these 3 quantities are specified to be negligible they go to 0, this is the total specification of the amplifier of the transistor, beta is 100, r_x , h_{re} and h_{oe} can be neglected okay, we will see what this means.

Now you are required to find out Q point then g_m and r_{π} and also these quantities A_v voltage gain, input resistance R_i , current gain A_i , output resistance R_0 and A_{vs} , which is as I said V_0 by V_s okay, this is the complete question now let us see let us proceed step-by-step. The 1st thing we have noticed is we have to calculate the base current, to determine the Q point you require collector current and collector emitter voltage, how do you calculate the collector current, you 1st require the base current. Now as far as the base current is concerned, you have to find out V_{BB} which is 10 multiplied by 47 divided by 147 okay that is V_{BB} . You have to find out R_B , 100 K parallel 47, I will give you the numerical values I have calculated them 100K parallel 47K. Then I_B would be $V_{BB} - V_{BE}$, which you shall take as 0.7 divided by R_B which is the parallel combination of these $2 + \text{Beta} + 1$, 101 times 1K okay very good, so the biasing has gone in I am very happy at this.

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$$\begin{aligned}V_{BB} &= V_{CC} \frac{R_2}{R_1 + R_2} = 10 \times \frac{47}{147} \text{ V} \\ &= 3.2 \text{ V} \\ R_B &= 100 \text{ K} \parallel 47 \text{ K} = 32 \text{ K} \\ I_B &= \frac{3.2 - 0.7}{32 \text{ K} + (101) \times 1 \text{ K}} \\ &= 18.8 \text{ } \mu\text{A}\end{aligned}$$

V_{BB} is $V_{CC} R_2$ by $R_1 + R_2$ and as I said this is 10 times 47 divided by 147 volts and this comes out as 3.2 volts. R_B which is 100k parallel 47K, this calculates out to 32K in my calculations I often make approximations which I do not advise that you do okay. Therefore, $I_{sub B} = 3.2 V_{BB} - 0.7 V_{BE}$ divided by R_b which is 32K + 101 multiplied by R_E which is 1K and this comes out as 18.8 microampere.

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$$\begin{aligned}I_C &= 1.88 \text{ mA} \\ V_{CE} &= 10 - (1.88 \text{ mA}) \times 3.2 \text{ K} \\ &= 3.96 \text{ V} \\ g_m &= \frac{I_C}{26 \text{ mV}} = \frac{1.88}{26} \text{ } \Omega^{-1} \\ &= 72 \text{ m}\Omega \\ r_{\pi} &= \frac{\beta}{g_m} = \frac{100}{72 \text{ m}\Omega} = 1.389 \text{ K}\end{aligned}$$

Therefore the collector current $I_{sub C}$ would be simply Beta times this which means 1.88 milliamperes. And if this is so then V_{CE} , the collector emitter voltage the DC part shall be $V_{CC} - I_{sub C} (R_C + R_E)$ this you must not forget, 3.2K and this comes out as 3.96 volts. Now this is the Q point the question is to find g_m and r_{Pi} , now g_m is $I_{sub C}$ by 26 millivolt and $I_{sub C}$ is 1.88 divided by 26, this is so many mhos and this comes out as 72 millimho, we do not want to write 72 multiplied by 10 to the - 3 or 0.072, right it in this form it is your choice. Therefore, r_{Pi} which is Beta by g_m can be very easily found out, 100 by 72 millimhos and therefore this will come out in K, 1.389K so we have found out the answer to the 2nd part of the question.

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$$\begin{aligned}
 A_v &= -g_m (R_C \parallel R_L) \\
 &= -72 \text{ mS} (2.2 \text{ K} \parallel 4.7 \text{ K}) \\
 &= -110 \\
 R_i &= R_B \parallel r_{\pi} = 100 \text{ K} \\
 &= 32 \text{ K} \parallel 1.389 \text{ K} \\
 &= 1.33 \text{ K}
 \end{aligned}$$

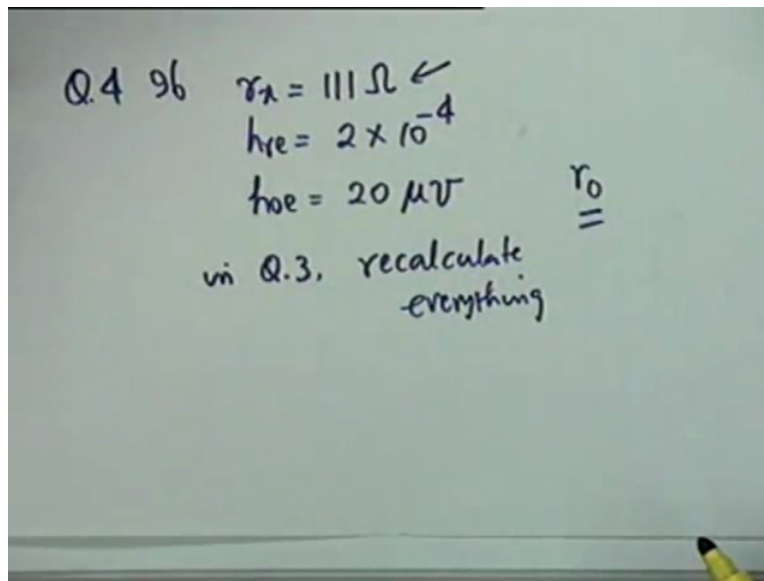
The 3rd part is to calculate all those gains, 1st A_v Beta is given as 100, Beta was given as 100 okay. The voltage gain is $-g_m$ approximately RC parallel RL so it is RC parallel RL, g_m is 72 millimhos, 2.2K, 4.7K that is the load okay so this is - 72 millimho multiplied by 2.2 K parallel 4.7 K and this my calculation gives this is - 110 a good figure, a voltage you know 1 millivolt becomes how much, 0.1. The R_i input resistance will be R_B parallel, r_x is ignored so it is R_B parallel r_{Pi} , which = 100 K, we had already found out R_B 32 K parallel 1.389 K which will be approximately 1.389, this is 1.33 K that is not too different.

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$$\begin{aligned} A_i &= A_v \frac{R_i}{R_L} \\ &= -110 \frac{1.33}{4.7} \\ &= -31.1. \quad r_o \rightarrow \infty \\ R_o &= R_c = 2.2 \text{ K.} \\ A_{vs} &= A_v \frac{R_i}{R_i + R_s} = -110 \frac{1.33}{2.33} \\ &= -62.8 \end{aligned}$$

The current gain A_i as you remember the current if the voltage gain is known then the current gain is known, A_i is A_v voltage gain multiplied by R_i divided by R_L therefore this = - 110, this is 1.33 divided by R_L is 4.7 okay this becomes - 31.1, R_o your hoe was given as 0 and therefore r_o tends to infinity r_o tends to infinity therefore output resistance will be simply = R_C which = 2.2 okay. And finally $A_{vs} = A_v$ multiplied by V_i divided by V_s which is R_i divided by $R_i + R_s$, therefore this is - 110 1.33 divided by 2.33, R_s is given as 1K and this comes out as - 62.8 that completes the question, now let us complicates matters.

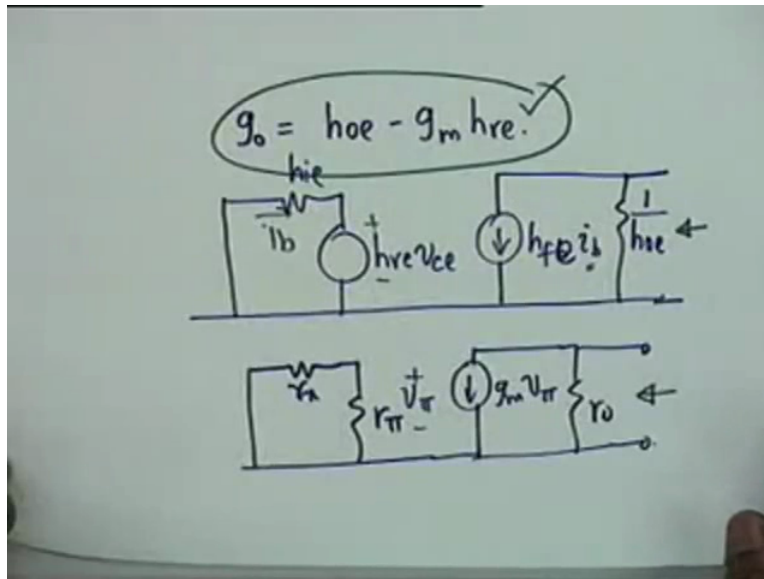
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This was simple this was simple, in this problem in the same problem question 4 says in problem 3 if r_x , h_{oe} and h_{re} are not neglected how do the things change, this is the basic theme of question number 4, r_x is given in question 3, we had assumed $r_x = 0$, $h_{re} = 0$ and $h_{oe} = 0$. Now r_x is given as 111 Ohms, h_{re} from the manufacturers data is given as 2 times 10 to the - 4 and h_{oe} is given as 20 Micromhos, if that is so in question 3 recalculate everything. Now you do not ignore, let us see how this transform into the hybrid Pi model, r_x can be taken directly, r_x obviously measured from h_{ie} okay and finding out g_m and r_{π} then r_x is $h_{ie} - r_{\pi}$ that is correct so I know r_x , how to take care of h_{re} and h_{oe} okay.

What is it that we are missing in the hybrid Pi model, the value of small r_o that is all that we are missing, r_{μ} anyway we do not want to go anywhere near r_{μ} , why? Because that complicates the analysis, it makes a 3 by 3 matrix inversion we do not want that. So hopefully deserve Pious thought that r_{μ} would be very large okay, so let us see how r_o can be calculated from these 2 alright.

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If you remember we derived this, we did not derive we simply say the relationship between g_0 and h parameters is $h_{oe} - g_m h_{re}$, this is what will give you r_0 okay. Now we did not derive it, I ask you to derive it yourself let me give you a hint as to how to derive this okay. What we want is from the h parameter model h_{ie} , $h_{re} v_{ce}$, $h_{fe} i_b$ is the h parameter model and h_{oe} , the corresponding hybrid Pi parameter is r_x , these 2 should be identical you see r_x .

Student: Should not it be $1/h_{oe}$.

$1/h_{oe}$ wonderful, r_x , r_{π} and this is v_{π} and then you have $g_m v_{\pi}$, r_0 , we do not want r_{μ} okay, if r_{μ} come then things become a little more complicated. But if these 2 if these 2 are to be identical then obviously if we measure a resistance here with the input shorted it should be the same as the resistance here with the input shorted out you. Now what do you get here if you measure the resistance here? These 2 this is the hybrid parameter model and this is the hybrid Pi, we want to find out the hybrid Pi parameters in terms of hybrid parameters. Since these are identical, if the inputs are shorted in both the output resistance would be the same, if you calculate these 2 output resistances you shall see that this is precisely what you get.

You have to figure out what you should do, either open circuit or short-circuit somewhere and since the 2 circuits are identical wherever you measure voltage or current they should be identical, terminal voltages and currents should be identical alright, so this is the trick for

proving his relationship Pardon me... Oh I wanted to establish this relationship okay, how do I do that, g_0 obviously g_0 is $1/r_0$ and if we measure the resistance here r_0 figures here. Now I can measure it under open circuit, short-circuit, whatever condition I will do it under short-circuit condition because if I keep it open circuit then v_{ce} does not come into the picture at all is not that right so I make it a short-circuit I make it a short-circuit then v_{pi} is 0 so here it is simply $1/r_0$, here h_{re} and h_{fe} , h_{oe} all the 3 quantity shall be involved and you shall see that they conspire to give a simple relation like this, it is a very simple exercise.

Student: Why all 3 will come?

Professor: Why all 3 will come... You do it and then you shall know... Because I_b is here and I_b is this current do not you see the coupling, I_b is this current, this is not 0 so this drives the current in the other direction, you think about it I cannot do everything.

(Refer Slide Time: 46:01)

The image shows a whiteboard with handwritten mathematical derivations. The first part calculates g_0 as follows:

$$g_0 = 20 \mu\text{V} - \underbrace{72 \text{ mV} \times 2 \times 10^{-4}}_{14.4 \mu\text{V}}$$

$$= 5.6 \mu\text{V} \Rightarrow r_0 = 179 \text{ K}$$

The second part calculates the voltage gain A_v as follows:

$$A_v = -g_m (r_0 \parallel R_c \parallel R_L)$$

$$= -72 \text{ mV} (179 \text{ K} \parallel 2.2 \text{ K} \parallel 4.7 \text{ K})$$

$$= -99.2$$

Okay now if I use this relationship then g_0 is 20 Micromho, h_{oe} is given, $-g_m$ is found out oh incidentally since r_0 , r_x , h_{oe} and h_{re} are not ignored, do they change the DC conditions at Q point? No, so g_m remains the same alright so I use the same g_m multiplied by h_{re} is given as 2 times 10 to the -4 and this comes out as 14.4 micromho no, this calculates to 14.4 this part, is not it? 144 milli is 10 to the -3 so 10 to the -7 and therefore g_0 becomes $= 5.6$ micromho, which leads to $r_0 = 1/g_0$ and that becomes 179K, pretty large let us see how this affects.

A_v the voltage gain is now $-g_m$, instead of R_L flying we must also include r_o so $-g_m r_o$ parallel R_C parallel R_L . And if you substitute the values, 72 millimhos multiplied by 179K 2.2K and the 3rd one was 4.7K alright and this calculates to -99.2 , what was it earlier? 110 so it has reduced. Why has it reduced? Because of r_o because of shunting effect of r_o okay.

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The image shows handwritten calculations on a whiteboard. The first part calculates the transconductance g_m as $20 \mu V - 72 mV \times 2 \times 10^{-4}$, which simplifies to $14.4 \mu V$. This is then used to find $r_o = 179K$ from $5.6 \mu V \Rightarrow r_o = 179K$. The second part calculates the voltage gain $A_v = -g_m (r_o \parallel R_C \parallel R_L)$, substituting the values to get $-72 mV (179K \parallel 2.2K \parallel 4.7K) = -99.2$.

What about R_i how does it change? It would be R_B parallel since r_x is not ignored, r_x shall come $r_x + r_{\pi}$ and this is 32K parallel 1.389 that is $r_{\pi} + 0.111K$, this is 1.5 as you can see so 32K and 1.5K they become 1.43K it is I am now why, because the shunting effect is reduced due to the introduction of r_x , previously it was 1.33 K it is slightly larger. The current gain $A_{sub i}$ is A_v divided by R_L so this is -99.2 , R_i has increased to 1.43K this has decreased but R_i is increased, but we still see the gain goes down, divided by 4.7K and that is -30.2 , not too much, the earlier value was 31.1 so that is not too much, our output resistance also changes yes...

Student: Previous concept... Should not A_i be positive?

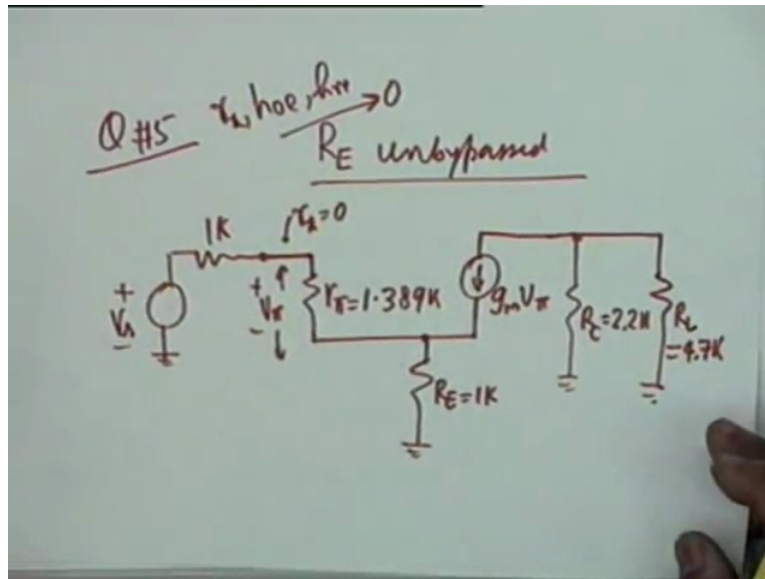
Professor: No... What is A_i ? A is the collector current... A_i is not the collector current, A_i is the load current and load current was taken as flowing into the load that is why this sign is negative.

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$$\begin{aligned}R_o &= r_o \parallel R_c \\ &= 179\text{K} \parallel 2.2\text{K} = 2.17\text{K} \\ A_{v_s} &= A_v \frac{R_i}{R_i + R_s} \\ &= -99.2 \frac{1.43\text{K}}{1.43\text{K} + 1\text{K}} \\ &= -58.4\end{aligned}$$

Okay the output resistance R_o , which is r_o parallel R_c now becomes 179K parallel 2.2 K and this becomes 2.17K not too much difference. The gain from the source that is A_{v_s} is given by A_v multiplied by R_i divided by $R_i + R_s$, when you do such problem the equivalent circuit should be flashing in your mental Picture okay, Source R_s then what does it see is R_i so the division between V_i and V_s is R_i divided by $R_i + R_s$, you must make this imprinted in your mind – 99.2 1.43K by 1.43K + 1K and this is - 58.4 this gain is also reduced, previously it was 62.8 alright that completes this question.

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The last one question no 5 says, repeat the same problem with R_E unbypassed okay R_E unbypassed, now if R_E is unbypassed and you remember the equivalent circuit, we have V_S 1 k then we have let us ignore r_x alright, we put $r_x = 0$, we can include it for a change let us ignore this, this is 1.389K then you have an R_E which = 1 K it is unbypassed then this is g_m ...

Student: (())(51:56)

Professor: No but v_{π} is across r_{π} , we will enter into unnecessary complications let us work this out under the conditions of problem 3 where r_x , h_{re} and h_{oe} are 0, r_x , h_{re} and h_{oe} all of them tend to 0, r_0 tends to 0 so this is simply $g_m v_{\pi}$, this is v_{π} , r_0 tends to infinity and so what we have here is R_C which is 2.2 K and R_L and we shall do things almost by inspection as you will see R_L is 4.7K. This is the equivalent circuit so all that changes is that this R_E as far as input side is concerned it reflects the resistance of $\beta + 1 R_E$, if you take care of this everything else fits into place, as you will see we will do it almost by inspection.

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$$\begin{aligned}V_o &= -g_m R_L' V_{\pi} \\V_{\pi} &= \frac{V_i r_{\pi}}{r_{\pi} + (\beta + 1) R_E} \\A_v = \frac{V_o}{V_i} &= -g_m R_L' \frac{r_{\pi}}{r_{\pi} + (\beta + 1) R_E} \\&= -1.51\end{aligned}$$

The output voltage is $-g_m R_L'$ times V_{π} okay $g_m V_{\pi}$ times R_L' and $V_{\pi} = V_i$ this is V_i , V_{π} is V_i potential division between r_{π} and $\beta + 1 R_E$ and therefore V_{π} is $V_i R_{\pi}$ divide by $r_{\pi} + \beta + 1 R_E$. Therefore, A_v which is V_o by V_i would be $= -g_m R_L'$ multiplied by r_{π} divided by $r_{\pi} + \beta + 1 R_E$. And if you put the numerical values, (()) (54:18) gain becomes -1.51 . All that you had the gain in $-g_m R_L'$ has been killed by this factor okay because there is a large quantity here $\beta + 1 R_E$, 1.51 only as compared to 110 earlier okay -110 .

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$$\begin{aligned} R_i &= R_{B11} [r_{\pi} + (\beta + 1)R_E] \\ &= 24.4 \text{ K} \\ A_i &= A_v \frac{R_i}{R_L} = (-1.51) \frac{24.4}{4.7} \\ &= -7.8 \\ A_{vs} &= A_v \frac{R_i}{R_i + R_s} = -1.45 \end{aligned}$$

But what it does is the input resistance $R_{sub i}$ it becomes parallel now no longer r_{π} it becomes $r_{\pi} + \beta + 1 R_E$ and if you calculate the values this comes as 24.4 K which is about 20 times the previous value okay. The input resistance has increased, the current gain usual thing $A_v R_i$ divided by R_L , R_i is now increased and this will become - 1.51 24.4 divided by 4.7 and this becomes - 7.8, current gain is also reduced. And A_{vs} you did not make any further analysis, just that factor that R_E reflects is reflects is $\beta + 1 R_E$ solves everything okay, and A_{vs} is A_v times again that Picture in mind R_i divided by $R_i + R_s$ and if you put down numerical values this is - 1.45, the gain is slightly greater than 1 and that brings us to the close of this session.