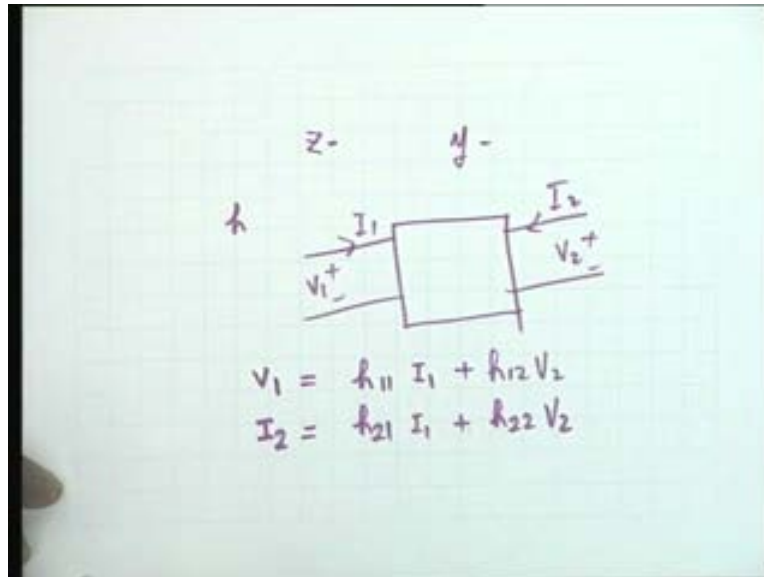


Circuit Theory
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Lecture - 24
The Hybrid and Transmission Parameters of 2-Ports (Continued)

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This is twenty-fourth lecture and we are going to discuss the hybrid and transmission parameters of 2-ports. We have already discussed the open circuit z parameters and the short circuit y parameters. The hybrid parameters or h parameters are defined like this; our convention for the 2 ports is the same $V_1 I_1$, $V_2 I_2$ conventions are the same and the quantities that we take as dependent variables are 1 voltage and 1 current, V_1 and I_2 and this should tell you why the parameters are called hybrid. They are not both voltages, they are not both currents, 1 voltage and 1 current. Not only that, the voltage and current are not at the same port.

There are different ports so there is a hybridization of all kinds and the quantities are written as $h_{11} I_1$, the independent parameters are I_1 and V_2 , so $h_{12} V_2$, $h_{21} I_1$ plus $h_{22} V_2$, these are the 4 parameters and if you look at the definition, which I shall repeat and the next slide.

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$$V_1 = h_{11} I_1 + h_{12} V_2$$

$$I_2 = h_{21} I_1 + h_{22} V_2$$

$$h_{11} = \left. \frac{V_1}{I_1} \right|_{V_2=0}$$

$$= \frac{1}{y_{11}} \leftarrow \text{s.c. d.p. imp.}$$

$$h_{12} = \left. \frac{V_1}{V_2} \right|_{I_1=0}; \quad h_{21} = \left. \frac{I_2}{I_1} \right|_{V_2=0}$$

s.c. current TF

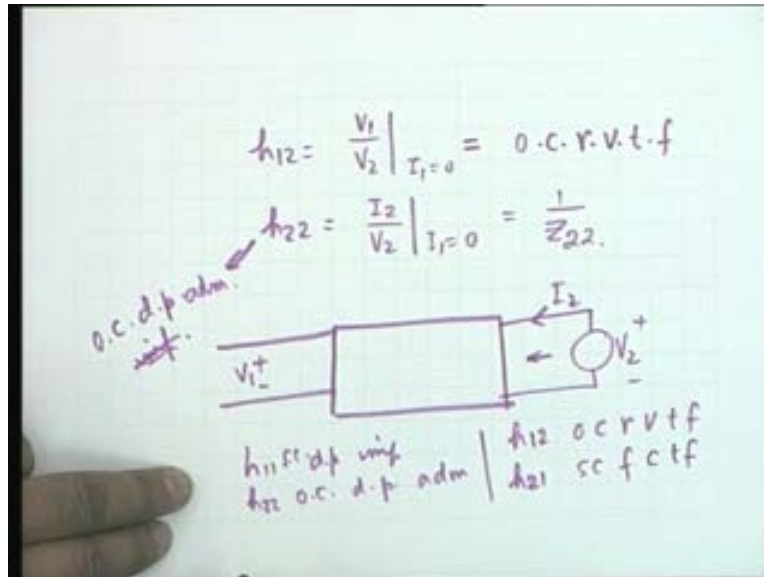
V_1 equal to $h_{11} I_1$ plus $h_{12} V_2$ I_2 equal to $h_{21} I_1$ plus $h_{22} V_2$, the thing to remember is, it is the input voltage or voltage at port 1 and current at port 2. Now if you look at the definition, h_{11} , obviously is V_1 by I_1 , with V_2 equal to 0, the output short circuited. Let us look at, we will go very slowly, let us look at the condition V_2 equal to 0, means, if this is short circuited, this is the current I_2 which is not of interest. What is of interest is V_1 by I_1 and therefore, it is the input, V_1 by I_1 is the input impedance under short circuited output.

So what is the admittance? By definition, this admittance is y_{11} and therefore, h_{11} is simply related to divide parameter y_{11} . It is input impedance under the output short circuited, output short circuited gives the input admittance as y_{11} and therefore, h_{11} is y_{11} and this is a short circuit driving point impedance, short circuit driving point impedance. Let us look at h_{12} . By definition, h_{12} is V_1 by V_2 , under the condition, I_1 equal to 0. But before you take this, let us take the other one. h_{21} is equal to I_2 by I_1 , under the condition V_2 equal to 0.

So h_{21} can be calculated from this diagram. Under the condition V_2 equal to 0 find the ratio of I_2 to I_1 and that shall be h_{21} and as you see, h_{21} is a current transfer function, agreed? It is a dimensionless quantity current transfer function that is the output current divided by input

current with the output short circuited. So this is a short circuit, s c short circuit current transfer function.

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Now let us look at the other 2 parameters, namely h_{12} is equal to V_1 by V_2 I_1 equal to 0 and h_{22} . If you see, it is I_2 by V_2 with I_1 equal to 0, and I_1 equal to 0 means open circuit at port number 1. So let us draw the circuit, let us draw the block. Port number 1 is open circuit and therefore, no current. The only thing you can measure is the voltage, and port 2 there is a voltage excitation v_2 . Obviously, the excitation cannot be at port 1, why not?

Student: Open.

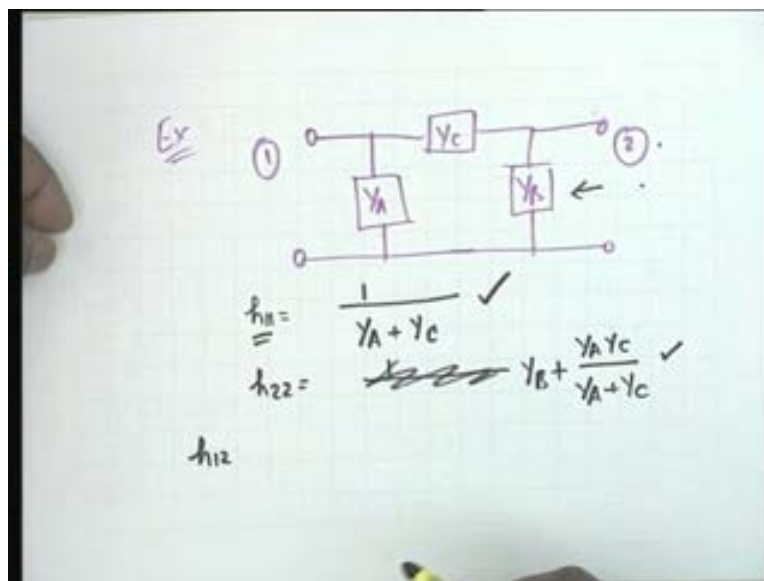
Sir: It is open and therefore, any source that you connect will drive a current and therefore, the source must be V_2 , I_1 equal to 0 and all that you calculate now is V_1 by V_2 . V_1 by V_2 is the actual transfer function. So this is the reciprocal, no, I beg your pardon; this is an open circuit, not V_2 by V_1 . You see, V_2 is the excitation and V_1 is the response. So it is correctly V_1 by V_2 , this is therefore, the reverse voltage transfer function, but also open circuit reverse voltage transfer function. Reverse because it goes from port 2 to port 1. Our convention is that power or energy travels from port 1 to port 2.

This is another way of obtaining a transfer function. This is an open circuit reverse voltage transfer function and if you look at h_{22} , h_{22} is I_2 by V_2 with I_1 equal to 0 and therefore, I_2 by V_2 , h_{22} therefore, is an open circuit driving point. I_2 by V_2 is admittance and therefore, this would be simply equal to 1 over z_{22} , agreed? So h_{22} is driving point open circuit, driving point impedance function, no, admittance function. Now let us look at the dimensions, h_{11} was impedance and it is driving point and it is short circuit. h_{11} is short circuit driving point impedance h_{22} is open circuit driving point admittance, h_{12} , h_{12} is open circuit reverse voltage transfer function and h_{21} is short circuit is it a forward or reverse? Forward.

Student: Forward

Sir: Forward current transfer function. Now you see the hybridization, it is a mixture of all kinds of things. Impedances, admittance, current transfer function, voltage transfer function, under open circuit or short circuit reverse or forward and that is why these parameters are called hybrid parameters and they have very important application in dealing with transistor circuits. As you know the hybrid pi equivalence circuit is the most universal and the most desirable kind of equivalence circuit for a transistor and they originate from the h parameters h parameter model of a general 2 port.

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Let us take an example suppose I have you take the familiar pi network; Y_A Y_C Y_B . This is port 1 and port 2. The first thing we do is, h_{11} , as you know, h_{11} is $1/y_{11}$. h_{11} is the impedance.

Student:

Sir: Okay, $1/y_{11}$ impedance looking here with this short circuited. So it is simply the parallel combination of Y_A and Y_C . So $1/y_{11}$ is $1/(Y_A + Y_C)$, it is an impedance. It is the input impedance so the output short circuited. In a similar manner, h_{22} would be the impedance measure from here with port 1 opened and therefore, it would be $1/y_{22}$, is that right?

Student: (..)

Sir: $1/z_{22}$, agreed? $1/z_{22}$. Now, obviously h_{22} is an admittance, is not that right? So the admittance measured here would be Y_B plus the admittance of the series combination of this 2 , which is exactly equal to $Y_A Y_C$ divided by $Y_A + Y_C$.

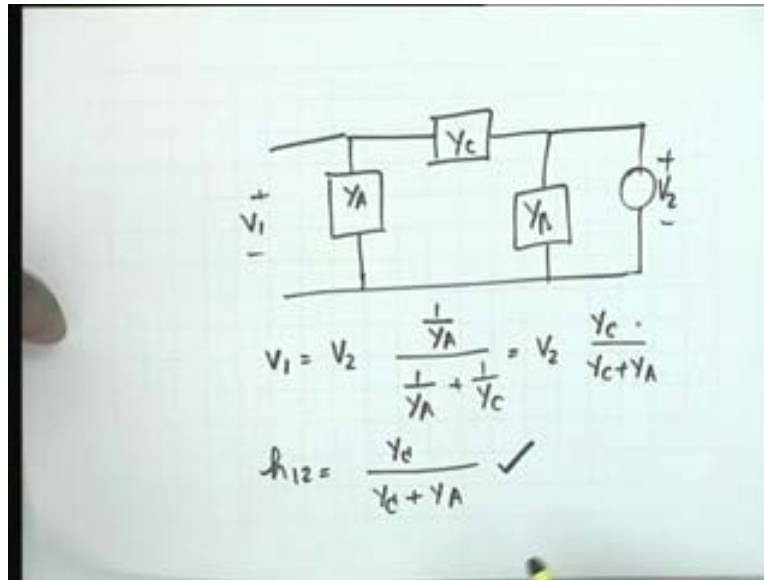
Student: Should not h_{11} be $1/y_{11}$ plus $1/y_{11}$?

Sir: No, h_{11} is an impedance.

Student: Yes sir.

Sir: Consisting of consisting of Y_A and Y_C in parallel. So the total admittance is $Y_A + Y_C$ and therefore, the impedance is $1/(Y_A + Y_C)$, is this result correct? Let us find out the other 2 parameters, that is, h_{12} and h_{21} . h_{12} , for example, for finding h_{12} , what we have to do is Y_A , let me draw the network first, Y_C and Y_B . h_{12} by definition is V_1/V_2 with I_1 equal to 0 . It is open circuit reverse voltage transfer function.

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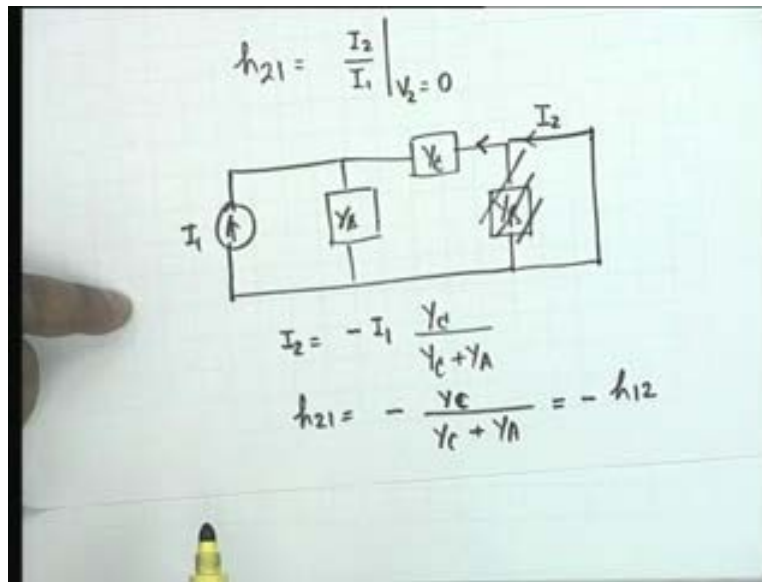
Now this comes in parallel with V 2, so it has no effect, so V 2, therefore divides, there is a potential division between YC and YA therefore, V 1 would be equal to V 2 1 by YA divided by 1 by YA plus 1 by YC, is that clear? This impedance, that is, z A divided by z A plus z C, not YA divided by YA plus YC. This is, in fact, this is V 2 YC divided by YC plus YA and therefore, h 1 2 is V 1 by V 2 therefore it is simply Y sub C divided by Y sub C plus Y sub A, is that clear? This is h 1 2. Now to find out h 2 1, h 2 1 is by definition I 2 by I 1 with?

Student: Short circuit current.

Sir: V 2 equal to 0 is that correct V 2 equal to 0 so let us see we have YA we have YC and we have YB, obviously, the excitation is I 1. There is a current source I 1, this is 0 and you are required to find out this current I 2, which is, obviously the current in Y sub C also, because this goes out of picture being short circuited and therefore, I 2 would be equal to I 1 minus I 1, then?

Student: (..)

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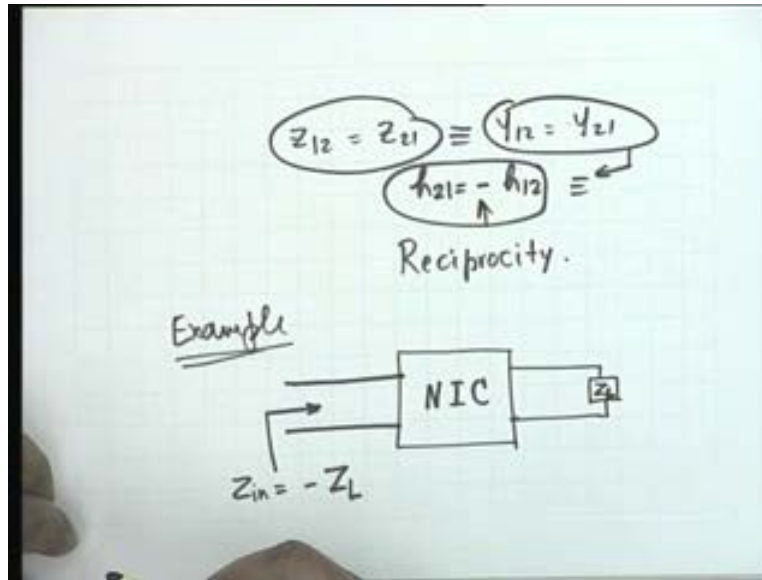


Sir: Y_C divided by Y_C plus Y_A , is that okay? And therefore, h_{21} would be equal to minus Y_C divided by Y_C plus Y_A , and if you recall what is h_{12} , you see that this is exactly minus h_{12} and what does this indicate? This indicates the condition for reciprocity. We assume that Y_A , Y_B , Y_C are bi-lateral elements that they pass current equally value in both directions, and therefore, what was z_{12} equal to z_{21} or $Y_{12} = Y_{21}$, in terms of z and Y parameters, now transfers into $h_{21} = -h_{12}$, this negative sign should be noticed, this is the, these 3 are identical conditions, that is, this condition equivalent to this condition and the whole thing is equivalent to the third condition. These are all conditions for reciprocity condition, reciprocity. Let us take another example.

Student: Sir the Negative sign comes in because one is a forward parameter, transfer function?

Sir: No, it is not because of that it is because of the directions of I_1 and I_2 , both go in. so if there is a current I_1 , if there is a current I_1 fitting here, the current through I_2 must flow in this direction, whereas our convention is that I_2 goes in. That is why its sign is negative.

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Student: Sir, this negative sign does not imply anything, for this current direction?

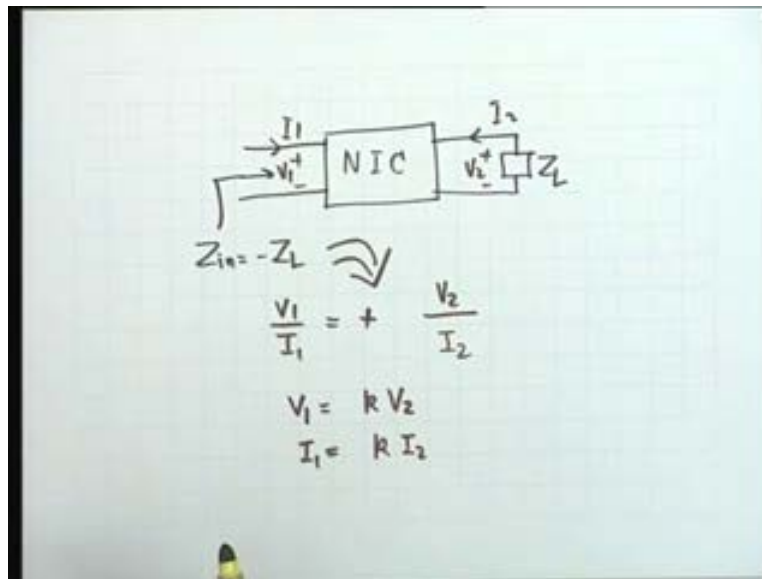
Sir: With this convention, with this convention h_{21} must be equal to minus h_{12} , okay?

Student: Sir, if h_{21} equal to minus h_{12} , then we can say it is reciprocal?

Sir: It is reciprocal is a necessary as well as sufficient condition, yes, that is correct. In fact, this is a test for reciprocity. Let us take another example and this example is that of a 2 port having the particular property, that whatever you connect at port number 2, a load z_L reflects at the input as the negative of z_L , that is, z_{in} equal to minus z_L , which means that you have a, if you connect it, if you connect a positive resistance here, it will reflect as a negative resistance and this is the way to make the negative elements.

We have all ways talked a positive R L and C, there is a way of making negative elements and this is a 2 port which is not a dream 2 port, it can be realize in practice and such a 2 port goes by the name of negative impedance converter, NIC. Obviously, it converts a positive impedance into negative impedance and this is why it is called a negative impedance converter or NIC.

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The NIC has the property that the impedance at the input is the negative of the impedance of the terminating impedance. Let us write it again, z_{in} is equal to minus z_L . Now if I indicate the voltage is in currents, this is $V_1 I_1$ and $V_2 I_2$, you notice that z_{in} is V_1 by I_1 minus z_L is V_2 by I_2 , no. The relation between V_2 and I_2 is V_2 is equal to minus $I_2 z_L$, is not that right? because the directions not agree and therefore the sign of the plus, is that okay?

z_{in} is equal to minus z_L indicates that V_1 by I_1 is equal to V_2 by I_2 . Obviously, this relation can be satisfied in many ways and the way that is usually, it is tried to be satisfied in an NIC is that V_1 is proportional to V_2 and so I_1 proportional to I_2 . If V_1 is k times V_2 and k is a constant, then I_1 must be equal to $k I_2$.

If I write these relationships, in the form of h parameters, that is, my NIC is characterized by V_1 equal to $k V_2$ I_1 equal to $k I_2$ and my h parameters relationship is between V_1 and I_2 as depended variables and I_1 and V_2 as independent. So $h_{11} I_1$ plus $h_{12} V_2$, I_2 is $h_{21} I_1$ plus $h_{22} V_2$. If I compared this relation with this relation, then obviously what I get is, h_{11} is 0, V_1 equal to simply $k V_2$ and h_{12} is equal to k , agreed? Is it okay? All right and I compared this relation with this but before that let me convert this as I_2 is equal to 1 over $k I_1$.

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NIC

$$V_1 = k V_2$$
$$I_1 = k I_2 \Rightarrow I_2 = \frac{1}{k} I_1$$
$$V_1 = h_{11} I_1 + h_{12} V_2$$
$$I_2 = h_{21} I_1 + h_{22} V_2$$
$$h_{11} = 0 \quad h_{12} = k$$
$$h_{21} = \frac{1}{k} \quad h_{22} = 0$$

I can write it that way? Now I compare this with this. Then I get h_{21} as 1 over k and h_{22} is equal to 0 , therefore,

Student: The assumption that V_1 is equal to $k V_2$ and I_1 is equal to $k I_2$, sir, have we taken it?

Sir: Pardon me.

Student: We assumed it, something?

Sir: No, I made a statement that this is the usual way 1 raised to satisfy the NIC condition. The practical circuits are built on this assumption. You can have other kinds of assumption also that V_1 equal to $k I_1$ and V_2 equal to $k I_2$, yes, you can do that. There are many other ways and

Student: Sir, we are not trying to synthesize the circuit? The NIC?

Sir: No, I am trying to show you an example of a 2 port, which is neither reciprocal nor passive and it is a circuit which can be made with transistors are (..) I am not synthesizing what is inside NIC. Inside NIC, we look at in a different course. What I am showing is that the NIC is an

example of a 2 port, which is neither reciprocal nor passive. It is not reciprocal is obvious because h_{12} is not equal to h_{21} , is it passive?

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$$\begin{aligned}
 & V_1 I_1 + V_2 I_2 = \quad \begin{array}{l} V_1 = kV_2 \\ I_1 = kI_2 \end{array} \\
 & = \underline{V_2 I_2 (1+k^2)} \\
 & = \underline{-I_2^2 Z_L (1+k^2)} < 0 \\
 & \quad \begin{array}{l} V_2 = -I_2 Z_L \\ Z_L = R_L \end{array} \\
 & \text{Circled note: } V_1 I_1 + V_2 I_2 \geq 0 \\
 & \text{Active Nonreciprocal}
 \end{aligned}$$

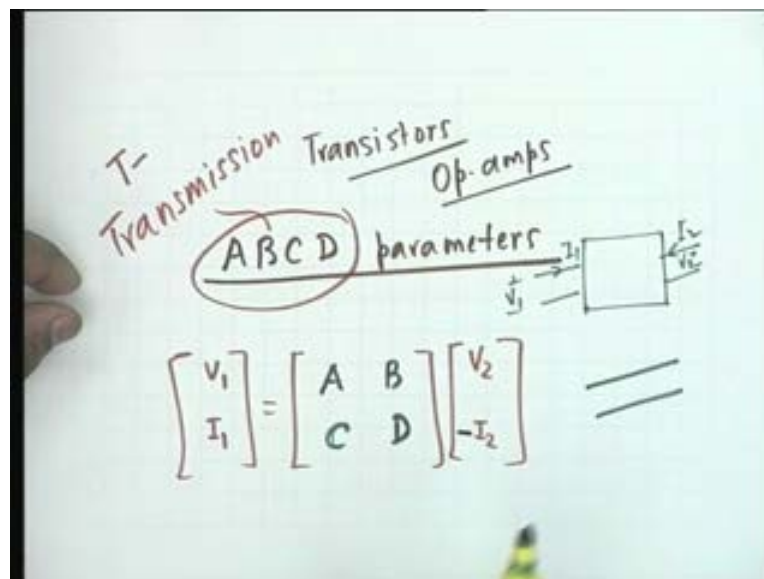
Well, for that, you see $V_1 I_1$ the total power that goes into the network. $V_1 I_1$ plus $V_2 I_2$, this is the total power that goes into the network and this is equal to, you see V_1 equal to $k V_2$ and I_1 equal to $k I_2$ and therefore, I can write this as $V_2 I_2 (1+k^2)$ plus k^2 , agreed? $V_2 I_2 (1+k^2)$ plus k^2 , also V_2 no $V_1 I_1$ is $k V_2$ multiplied by $k I_2$, so case

Student: (..)

Sir: I do not understand why it should be $1 - k^2$. I am substituting for V_1 . I am substituting for I_1 . $k V_2$ multiplied by $k I_2$ is $k^2 V_2 I_2$. I am writing this product in terms of $V_2 I_2$. I have a purpose, you see V_2 is equal to $-I_2 Z_L$ and therefore, this is equal to $-I_2^2 Z_L (1+k^2)$. Therefore, the power that goes in can be negative, the sign negative. I_2^2 , if it is a resistive network, let us say, if Z_L equal to a positive resistance R_L , then I_2^2 is a positive quantity and therefore, the power that goes in can be negative, which means that the 2 port generates power. It does not observe power, it generates power.

A condition for passivity is that $V_1 I_1$ plus $V_2 I_2$ must be greater than or equal to 0. It must either absorb power or may not observe power, but it should not generate. If it is greater than 0 then the network we say is lossy, that is, a dissipate power then absorbs power. If it is equal to 0 then you say the network is loss less. On the other hand, what do you have here is negative and therefore, the network generates power, which means that the network is active and non reciprocal non reciprocal and obviously, if it is non reciprocal, it cannot be made out R L C elements positive R positive L positive C. We must have non reciprocal elements, non uni lateral elements like diodes or transistors are a combination of transistors to make an op amp.

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In fact, an NIC can be made with transistors and or op amps and simple circuits can be build to demonstrate the action of NIC. If you are interested, we shall look at some circuits at a later stage. Our next concern is the ABCD parameters, and you shall have very interesting examples of ABCD parameters also. ABCD parameters, as you know, are also known as transmission parameters and why they are so denoted? Why they are called transmission parameters, shall be obvious. They are also sometimes called T parameters, capital T we do not use a small t because small t we deserve for time.

Capital T, yes, you can use but in the literature right from the days of Lord Kelvin. Lord Kelvin was the originator of the transmission line concept, transmission line theory and he used ABCD parameters and therefore, we have respects for the older generation and we still call them ABCD. Although it is a bit messy, 4 things to be mentioned. But capital T, you see, has many other connotation is also used for time

Student: Temperature.

Sir: Temperature and what not. So we refrain from using all this. We will call them ABCD parameters and the relationship now is based on the input parameters being looked at as depended parameters V_1 I_1 and V_2 I_2 as the independent parameters, that is, in terms matrix notation, I will come to the actual notations later actual equations later and therefore, matrix notation, there is a 2 by 2 matrix which relates to V_2 and I_2 and one thing that must remember is Lord Kelvin used a negative sign V_2 minus I_2 .

Student: (..)

Sir: No, they are dependent.

Sir: They are dependent. Did I say they are the independent? Well, then I made a mistake. One of the end mistakes that (..) does in the class, where and may be a large quantity but it is your responsibility to correct them. What I want you to notice is this negative sign. Well, if I look at the 2 port V_1 I_1 V_2 and I_2 , what it means is that I_2 , the output current is taken as going out of the network instead of coming in. If it is coming in, you should used a plus I_2 and Lord Kelvin argued that whatever you feed in, if I feed in a current in this direction, I will take it. Lord Kelvin's convention was that I will take it going out, the current going out. So this is why, to keep track with modern practices, in which a 2 port parameters is defined with all currents going in, I must use a negative sign and these parameters are A B C and D. These are the transmission parameters.

The negative sign must get imprinted in your mind this is the only set of parameters of before z y h and ABCD that we use a negative sign in front of a, negative sign appended to a current or a voltage. It is the current all right, this is only set of parameters.

Student: Sir, the current direction is taken to be outwards?

Sir: That is right, Lord Kelvin said I will take it out of the (..)

Student: Excuse me sir, at one time we cannot use both the current generator and voltage generator.

Student: Sir, 1 time we cannot use both the voltage generator and the current generator at the point.

Sir: Pardon me.

Student: Sir, at one time we cannot use both the current generator and voltage generator.

Sir: No, you do not.

Student: Sir, if you are taking v_1 and I

Sir: It just the variables it is not way of measuring. As you will see, measurement requires only one generator. It does not required 2. It is only a way of looking at. You see, I said out of 4 parameters, V_1 V_2 I_1 I_2 I can take any 2 as dependent, the other 2 as independent. I will not able to connect voltage generator and current generator in parallel, no.

Student: Sir but independent parameters are the forcing parameter

Sir: Right

Sir: Forcing parameters.

Sir: Right.

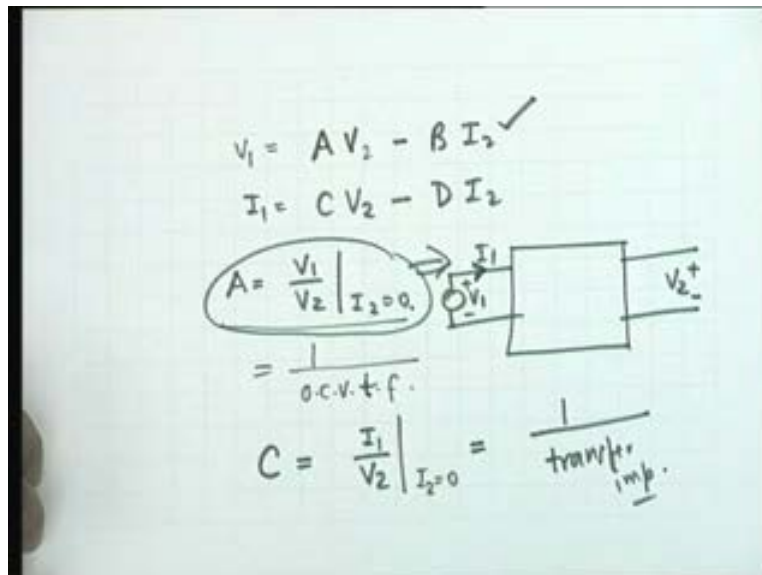
Student: So we want to force some voltage or some current

Sir: Okay.

Student: If we say that v_1 and i_2 are independent variables

Sir: As I say, this is only a semantics, this independent and dependent. Since I write V_1 in terms of V_2 and minus I_2 , I say V_2 and minus I_2 are my independent parameters. It does not mean that measurements will also be made with 1 current generator and 1 voltage generator. You see, even in z parameters, y parameters, h parameters, there is only 1 generator at a time. If you notice, all the measurements are made with only 1 generator, not 2. So this independence, in the context of ABCD in particular, means that 2 parameters V_1 I_1 are expressed in terms of V_2 and minus I_2 , that is all. No other significance.

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We will see how to measure them. If you write in full, then V_1 is equal to $A V_2$ minus $B I_2$, note the negative sign, and I_1 is equal to $C V_2$ minus $D I_2$ and therefore, we will see why they are called transmission parameters. Therefore, you see, A is equal to V_1 by V_2 with I_2 equal to 0. Now what does this mean? Let us draw the 2 port. I_2 equal to 0 means port 2 is open and therefore, the measurement is of V_2 with a V_1 here, which means that here, V_1 is the independent supply. Generator is V_1 not V_2 .

So in terms of measurements, measurements have nothing to do with what we called independent parameters, independent currents or voltages. But you see, that A is obviously the reciprocal, you see here the transfer function open circuit voltage transfer function is V_2 by V_1 , and A is the reciprocal of 1 by an open circuit voltage transfer function reciprocal of a voltage transfer function.

Student: We should have taken V_1 as the voltage generator and generator at the other end?

Sir: That is what I have done. V_1 is the voltage generator and V_2 is the, that is, I have unconstrained by this.

Student: Sorry sir, V_2 as the voltage generator.

Sir: I cannot, because I_2 is 0. If I connect a voltage generator here, it will definitely send a current, is not that right? And therefore, I am constrained by the definition to use a figure like this. You must remember these essential, important points and you cannot make a mistake because if you go back to the roots, if you go back to the definition, you cannot make a mistake. I_2 equal to 0 constrains means not to put a generator here. So generator must be here and this is why it is the reciprocal of an open circuit voltage transfer function. The reciprocal of an open circuit voltage transfer function may not be itself another voltage transfer function, it is the reciprocal.

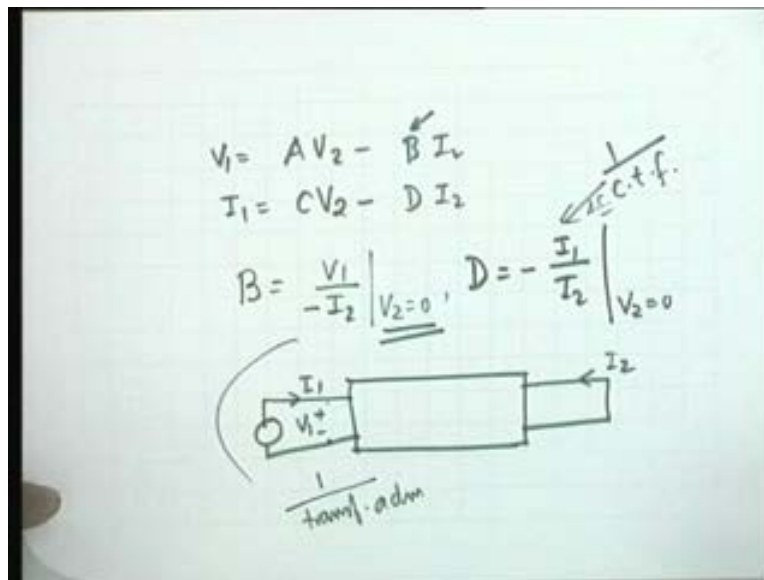
Similarly, I can, another parameter that I can find out is C , from this network. C is I_1 by V_2 with I_2 equal to 0 and therefore, once again, my response shall be V_2 , agreed, because I_2 equal

to 0, response will be V_2 , but this time the excitation is I_1 the current. So what we will do is, we will connect a current generator here or does not matter, we can also connect a voltage generator, that is not a problem. What we have to find out is I_1 . I have to find out I_1 and V_2 this ratio and you see, this is the reciprocal of?

Student: (..)

Sir: No, reciprocal of a transfer impedance. You see, V_2 is the response, I_1 is the excitation, so I_1 by a transfer impedance transfer impedance. C equal to 1 by a transfer impedance.

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Next let us look at the interpretation of B and D. V_1 is equal to AV_2 minus BI_2 . I_1 equal to CV_2 minus DI_2 and therefore, B is equal to V_1 by I_2 minus I_2 . B is equal to V_1 by minus I_2 , under the condition V_2 equal to 0 and D is equal to?

Student: Minus I_1 by I_2 .

Sir: I_1 by, minus I_1 by I_2 , under the condition? V_2 equal to 0. So let us make V_2 equal to 0. Obviously, I cannot connect a generator here, the generator has to be connected here. It is either

a voltage generator or a current generator. Whatever be it, the voltage here is V_1 and the current here is I_1 and what is measured, V_2 is 0 and therefore, all that can be measured is I_2 . The current, now if you take the ratio of this voltage to the negative of this current, which means, you will get B, so what is B? B is the reciprocal of reciprocal of?

Student: Transfer admittance.

Sir: Transfer admittance, well, negative or positive we will see. It is minus i_2 , we will see if it comes negative will take this negative. But dimensionally, it is 1 by a transfer admittance and capital D, as you see, is the reciprocal of

Student: Transfer current function.

Sir: Current transfer function, 1 by current transfer function.

Student: Short circuit.

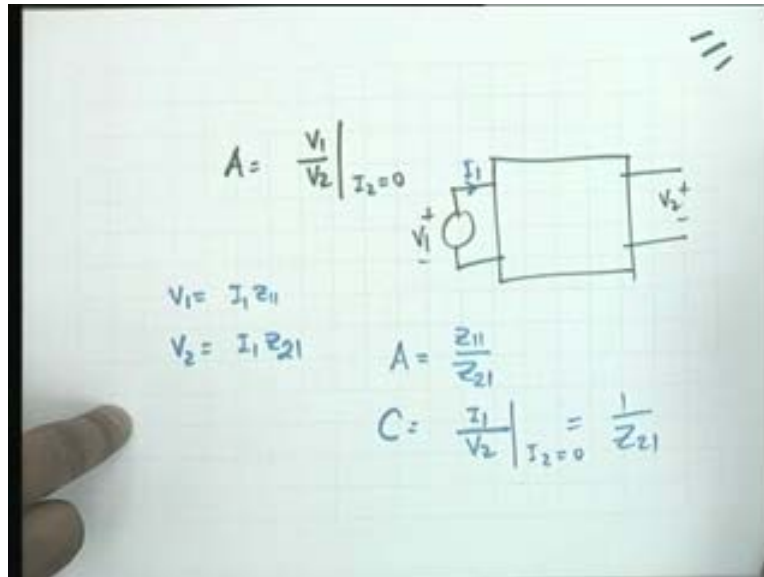
Sir: Short circuit, all right? But there something common between all these parameters, ABCD, there are all transfer parameters. None of them are driving point parameters. 1 is a voltage transfer function, reciprocal of a voltage transfer function, reciprocal of a current transfer function, reciprocal of a transfer impedance, reciprocal of a transfer admittance. The word transfer is common to all of them. In other words, the excitation and the response are a different ports and since every parameter has a transfer associated with it, they should be called either transfer parameters or, a better language, transmission parameters. This is the reason, yes?

Student: Sir, while calculating B, B is a short circuit at the second port and apply voltage source at first port, can we apply a current source at second port?

Sir: No, the constraint is that I have to make V_2 equal to 0. If I apply a current source here, I cannot guarantee that V_2 equal to 0, agreed? Any other question? Now without much of a

discussion now, let us see if you can relate these parameters to the familiar ones, the z and y parameters for example.

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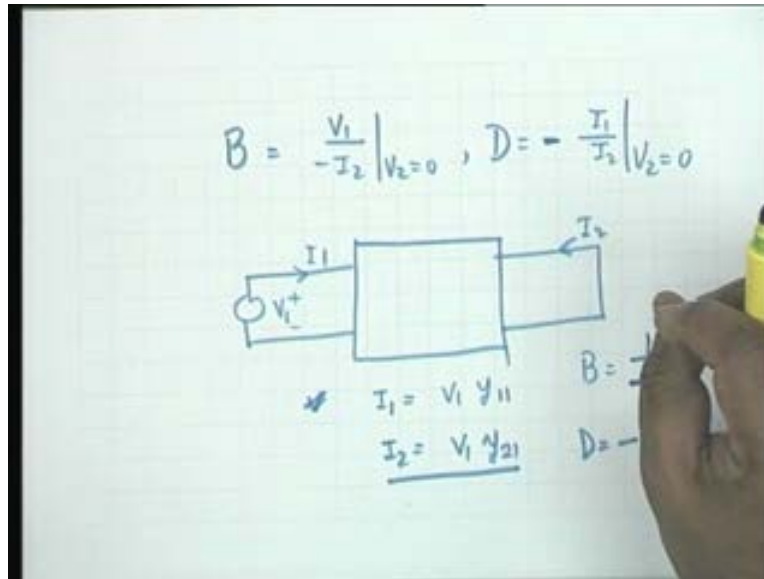
Suppose I consider A, the A parameter by definition is, if I remember, V_1 by V_2 under the condition I_2 equal to 0. Let us take the network, I have I_2 equal to 0, so the response must be here and this is V_1 . Now, to find out the ratio of V_2 by V_1 and take the reciprocal, now if you recall, please do follow me, if you recall our z parameters definition is V_1 equal to $I_1 z_{11}$ plus $I_2 z_{12}$, I_2 is 0, so let me not write that, the other is V_2 equal to $I_1 z_{21}$, agreed? Therefore, my capital A shall be simply equal to z_{11} by z_{21} , is that clear?

If you know the z parameters, I know the capital A parameters, the transmission parameters. Transmission parameter is simply the ratio of z_{11} by z_{21} . The other parameter that we can find out from here is the C parameter. C is I_1 by V_2 , if I am not mistaken, with I_2 equal to 0. So I_1 is this current and V_2 , can you tell me what is, pardon me

Student: 1 by z_{21}

Sir: 1 by z 2 1, that is correct, 1 by z 2 1. Now I could relate this, I could relate A and C to z 1 1 z 2 1 because, very easily because, I kept this open and you see, open circuit, the z parameters are measured under open circuit conditions. On the other hand, the other 2 parameters are most easily related to the short circuit parameters, namely y parameters.

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For example, the parameter B as I have said is V_1 divided by minus I_2 , under the condition V_2 equal to 0, and the parameter D is minus I_1 by I_2 , under the condition V_2 equal to 0. So let us take this network, V_2 equal to 0 is this. Only thing you can measure is I_2 and here, you connect either a voltage source or a current source but the net result is that the voltage is in current cell V_1 and I_1 and now what I have to do is, find V_1 by I_2 V_1 by minus I_2 or I_1 by minus I_2 . Now, if I write the short circuit parameters, V_1 , I am sorry, short circuit parameters I_1 is $V_1 y_{11}$, V_2 is 0, and I_2 is equal to $V_1 y_{21}$ because I_2 is 0, I am sorry, V_2 is 0, the second time I need not write. Is not it obvious that V_1 by minus I_2 , that means, B V_1 by minus I_2 would be?

Student: Minus 1 by y_{21} .

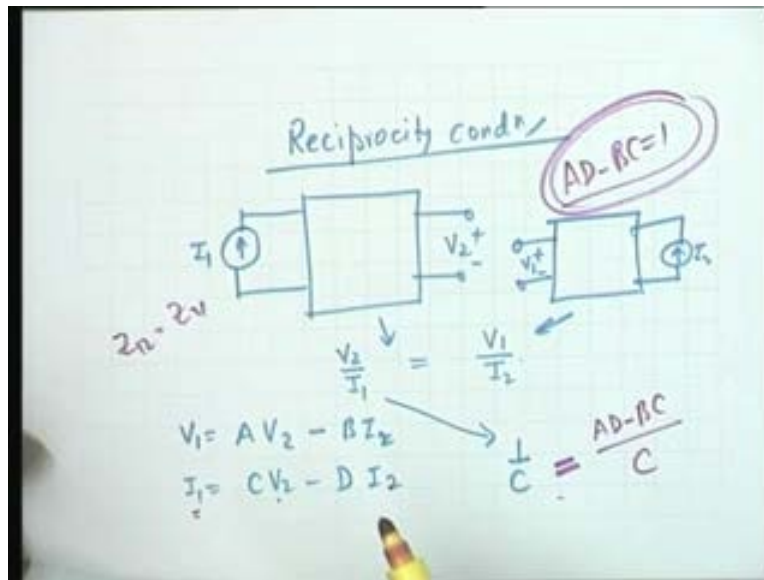
Sir: Minus 1 by y_{21} , minus.

Student: No sir, current?

Sir: You see, this is the relation for this situation. I_2 equal to V_1 y 2 1 so V_1 y by minus I_2 would be minus y 2 1 . Do not forgot this negative sign, it is extremely important. We will make a mess if this is not included and as for as D is concerned, for D you simply have to take the ratio of the 2 with a negative sign. So D would be minus y 1 1 divided by not quite, I am sorry, this is perfectly all right because the negative sign is there. Minus y 1 1 by y 2 1 , is that clear?

This is an example to show that all these parameters, whether h parameters, h parameters also related to the z parameters, did not we? We did not relate h_{21} and h_{22} and h_{12} . We will do that in a short while but any set of parameters can be converted to any other set of parameters, what is the reason? why can we do it? What is that facilitates this conversion? Because it is a set of linear equations, 2 linear equations, can be manipulated any manner you like, all right, without any problem.

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Let us take now another important derivation, that is, what is the reciprocity condition in terms of ABCD parameters? Reciprocity condition, in terms of ABCD parameters and for these we appeal

to the network itself, that is, what you do is, we excite the network by a current and measure the voltage open circuit voltage V_2 , agreed?

Now reciprocity demands that if the current source is taken to the right hand side and the voltage is measured under open circuit condition on the left hand side, the ratio should be equal. In other words, if I change my excitation and responses, I_2 and V_1 , under these 2 conditions, the relation between V_2 and I_1 should be equal to V_1 by I_2 , all right? V_2 by I_1 is measured from here and V_1 by I_2 from here. This is the reciprocity condition, this is the reciprocity theorem. Now if I appeal to my equations, you see, V_1 equal to $A V_2$ minus $B I_2$ and I_1 is $C V_2$ minus $D I_2$, then you see, under the condition that I_2 is 0, for this, I_2 is 0, what is V_2 by I_1 ? It is simply, yes? 1 by C .

And for the other condition, that is, I_1 equal to 0, you have to put this equal to 0. Let me indicate to you how it is done, I will skip the algebra. What we will do is, for finding out this V_1 by I_2 , we have to put I_1 equal to 0. So if I put I_1 equal to 0, I get a relation between V_2 and I_2 , all right? Then in the first equation, we have to find out V_1 , so the place V_2 in terms of its value I_2 , in terms of I_2 . Then you can find out V_1 by I_2 .

Student: (..)

Sir: Pardon me, say it again.

Student: AD minus BC by C ?

Sir: AD minus BC by C , so these 2 should be equal, which means that AD minus BC should be equal to 1, if the network is to be reciprocal. We have proved it, how did you prove it? We applied the theorem itself, we went to the roots, but if you look at carefully, these roots mean nothing but equating $z_1 z_2$, $z_2 z_1$ what is this parameter? V_2 by I_1 with I_2 equal to 0? Obviously, it is z , no, not $1/z$.

Student: $z_2 z_1$

Sir: Z_{12} and this is Z_{21} , V_1 by I_2 , under the condition I_1 equal to 0 is Z_{12} . So what have to done is, we have taken the condition Z_{12} equal to Z_{21} and then applied the definition of ABCD parameters, this is the condition for reciprocity.

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$$\begin{aligned}
 Z_{12} &= Z_{21} \\
 Y_{12} &= Y_{21} \\
 h_{12} &= -h_{21} \\
 AD - BC &= 1
 \end{aligned}$$

$\begin{bmatrix} A & B \\ C & D \end{bmatrix}$
 ↑
Transmission matrix

To summarize, our condition for reciprocity is Z_{12} equal to Z_{21} Y_{12} equal to Y_{21} , this is fine, h_{12} is minus h_{21} , there a negative sign, and in terms of transmission parameters it is AD minus BC equal to 1. You see that this is the only set of parameters in which all the 4 parameters are involved, that is, left hand side is nothing but the determinant of this matrix, the determinant of this matrix, where as the other 3 relate to the off diagonal parameters. Diagonal parameters are Z_{11} , Z_{22} , off diagonals are Z_{12} , Z_{21} . This is also off diagonal parameter, this is also off diagonal parameter. Only 2 of the 4 parameters are involved in reciprocity, if you describe the network in terms of z , y or h .

But if you take transmission parameters, then all the 4 are involved and it is the determinant of the transmission matrix, this is called transmission matrix. This is what will start from, in the next lecture.