## Fundamentals of Power Electronics Prof. L. Umanand Department of Electronics Systems Engineering Indian Institute of Science, Bengaluru

## Lecture - 70 Forward converter design mfile

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Now here I am going to show you an m file wherein I have designed a forward converter. Recall that in the last week resource I had included a forward converter design example, now I am extending that to include inductor design with the core and also the transformer design with the core.

So, for that some extra files are needed I have included cores dot m, ferrite dot m which gives you the data for the ferrite cores like the pot cores ee cores and so on. I have included some for metglas cores, powdered iron cores I have also included the wire table here.

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<pre>9 VMERC ALCULATIONS Prosum(11.1*abs(v0)+Vd).*Io); VTURNS FAITO and GUTY FAITO n=(1.1*abs(v0)+Vd)/Dmax*Vcxin); Dma(Dmax*Vcxin) /VCmax; Dma(Dmax*Vcxin)/VCmax; dmax*Vcxin)/VCmax; dmax*Vcxin)/VCmax*Vcxi</pre>	26 27 core details ≈ [ 28 spore no. 4ρ, mr <sup>4</sup> Ac,m <sup>4</sup> 2 Aw,m <sup>4</sup> 2 29 s 30 1 151.36 16 9.46; 31 2 1140 43 26.6; 32 3 4040 94 53; 33 4 10160 135 74.7;	Total         Total <th< td=""></th<>
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Just to show you, if I go into ferrite dot m you see here POT CORES, EE CORES, UU CORES, RM CORES, TOROID CORES. These are the various varieties that I have included.

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4	36 7 328300 715 5181	
5 Vc=48; \nominal dc-link	VG 27	
6 Vcmin=40; %minimum dc-link 7 Vcmax=60: %maximum dc-link	38 elseif fe_type==2,	
8 Vo=[12]; %isolated multi output	V0 30 6	forward, metglas.m pow.iron.m wires.m
9 dv=[0.05]; hpeak to peak output vo	V940 % EE CORE TYPES	design.m
10 Io=[1]: Noutput currents	42 core name=[ 'E20/10/05';	
11	43 'E25/09/06';	
12 NDESIGNER'S VARIABLES	44 125/11/07:	
13 di=0.3*Io; %inductor current	T45 (E30/15/07)	
14 fs=20e3; %switching freque	16 46 'E36/18/11';	
15 Bm=0.2; \flux density, T		
16 Bml=0.25; %flux density, T 17 eff=0.8; %estimated effici		
18 Dmax+0.45; Smaximum duty cyc		
19 J=3e6; %current density,	<sup>1</sup> 50 'E65/32/13'];	
20 Kw=0.4; %window factor fo	f 53 core datails - I	
21 Kwl#0.6; Nwindow factor fo	53 barona no la maña de maño du maño	
22 Vd=1.0; %diode forward dr	00 s.a. s.	
23 muo=4*pi*le-7; %uo - permeabilit		
24 Rowabs(Vo)./Io; Noutput load res: 25		
26 VPOWER CALCULATIONS	57 3 4780 55 87;	
27 Po=sum((1.1*abs(Vo)+Vd).*Io);	58 4 7100 59.7 119;	
28	59 5 18470 131 141; 60 6 27390 107 256;	"Herrite.m" selected (2.4 kB)
29 NTURNS RATIO and DUTY RATIO	61 7 46590 182 256:	Indiange 117 Bectance 545-22
<pre>38 n=(1.1*abs(Vo)+Vd)/(Dmax*Vcmin);</pre>	62 8 60160 235 2561	inductance.mm 0.67580
31 Dmin=(Dmax*Vcmin)/Vcmax;	63 9 142840 266 5371;	
32	64	
33 %FORWARD TRANSFORMER DESIGN 34 ap=((sqrt(Dmax)*Po*(1+(1/eff)))/(Kw*)*	65 elseif fe_type==3,	valum, uf 375.00000 pg, volts 24.00
35 ap firstmap;	00 \$.	set, ohes 0.13333
36 flag=0;	67 N UU CORE TYPES	ine 265 column #
37 a index=1;	69 core name=[ 'UU015 ';	
38 cnt=1:	To Jimon	8 column 1
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And I have put in the database Ap that is the Area product, Ac the core Cross section Area, window area in into in the form of matrices and I have also included the strings and for all these cores.

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It is simple for you to add as much as you want into this database.

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dv=[0.05]; %peak	4 Warr Honizal dc-Link vg5 Wart Maximu dc-Link vg6 Warr Maximu dc-Link vg7 W Ated milit output vg8 Wh6 to pak output vg8 Wh6 Honizanu dc7, vg1 Minder current 11 5 12 4 4 Minder current 14 Waithing frequent 14 Minder factor fr 21 Minder factor factor fr 21 Minder factor	given as outputs. SMTAX is as follows wire,eth,SMG] = wires(calc, area units are in ar <sup>2</sup> , alc area = calculated area wire = area of harear conduct th = ename! thickness to be af gauge number of anneal is a function in the "power toolbox, , Indian Institute of Scie Ref: Dr (nargchk(1,1,nargin));	en as parameter. The and the SMG gauge type area); of cross section , m" for from databases m? added to hare dia, m led copper er electronic applicati designed at thamand from m"2 to mm"2	on design"	D / moon / effer +	Q E + B
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<pre>s \FORWARD TRANSFORMEF ap=((sqrt(Dmax)*Po*) ap_first=ap; flag=0;</pre>	1+(1/eff)))/(Ku+J+Bn 34 '5 35 '5	WG 41'; WG 40'; WG 39'; WG 38':			value, of 375.00000 mg, volts 24.00 met, ohes 0.13333 ine 265 calume 8	
a index=1;	37 '5	WG 37'; WG 36':			is column 1	
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And then you say, in the wires table I am going to show you that I have included the standard wire gauges details, these are the standard wire gauges starting going down from SWG 45 number toward SWG 7.

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0 Io=[1]: Noutput currents	77 'SWG4/0';			
1	78 'SWG5/0';			
2 NDESIGNER'S VARIABLES	79 'SWG6/0';			
	80 'SWG7/0'];			
4 fs=20e3; hswitching frequer	an MIRE - 1			
5 Bm=0.2; %flux density, T f 6 Bml=0.25; %flux density, T f	83 500000	Bare area of	enamel thickness	
6 Bml=0.25; %flux density, T f 7 eff=0.8; %estimated efficie	84 Spointer	conductor.mm*2	additon to bare dia.mm	
8 Dmax+0.45; Smaximum duty cycl	85 1	0.003973	0.015;	
9 J=3e6; %current density,	¥20 Z	0.005189	0.016;	
0 Kw=0.4; %window factor for	87 3	0.006567	0.018;	
1 Kwl=0.6; Nwindow factor for		0.008107	0.018;	
2 Vd=1.0; %diode forward dro	90 6	0.009810	0.020; 0.020;	
3 muo=4*pi*le-7; %uo - permeability		0.011675 0.013700	0.020;	
4 Rowabs(Vo)./Io; %output load resis	92 8	0.01824	0.023:	
5 6 NPOWER CALCULATIONS	93 9	0.02343	0.025;	
7 Po=sum((1.1*abs(Vo)+Vd).*Io):	94 10	0.02927	0.025;	
8	95 11	0.03575	0.028;	"wires.m" selected (3-
9 NTURNS RATIO and DUTY RATIO	96 12	0.04289	0.033;	ndings 117 Automatic Set 22
0 n=(1.1*abs(Vo)+Vd)/(Dmax*Vcmin);	97 13	0.05067	0.033;	Nictance 546 22 piductance.xm 0.67580
1 Dmin=(Dmax*Vcmin)/Vcmax;	98 14 99 15	0.05910 0.06818	0.035; 0.036;	
2	100 16	0.07791	0.036;	
<pre>3 \FORWARD TRANSFORMER DESIGN 4 ap=((sqrt(Dmax)*Po*(1+(1/eff)))/(Kw*J*E</pre>	101 17	0.09372	0.036;	value, of 375.00000 mg, volts 24.00
<pre>4 ap=((sqrt(Dmax)*Po*(1+(1/ett)))/(kw*J*E 5 ap first=ap;</pre>	102 18	0.111	0.041;	ent, ohas 0.13333
6 flag=0:	103 19	0.1363	0.045;	ine 265 column B
7 a index=1:	104 20	0.1642	0.048;	
8 cnt=1:	105 21	0.2027	0.053;	8 column 1
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With all their bare conductor area and enamel thickness, all these things.

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	118	34 5.48		0.114;				
Vc=48;	<pre>%nominal dc-link vo 119</pre>	35 6.818 36 8.302		0.122; 0.132;			1 10 1	
Vcmin=40;	Wminimum dc-link vol20	30 0.302 37 10.51		0.132;				
Vcmax=60;	Smaximum dc-link vol21	37 10.51 38 12.97		0.142; 0.155;				
Vo=[12]; %is	olated multi output vo 122	39 15.70		0.165;				fas.m pow_iron.m wires
	ak to peak output volt 123 houtput currents 124	40 18.68		0.105;			design.m	
Io=[1];	Noutput currents 124 125	40 18.00		0.175; 0.185;				
		42 27.27		0.195;				
ADESIGNER'S VARIAB		43 32.18		0.205;				
di=0.3*Io;	%inductor current r127	43 38.60		0.220;				
fs=20e3;	hswitching frequence 128	45 45.60		0.240;				
Bm=0.2;	flux density, T fo 129	45 45.00		0.240;				
Bml=0.25;	Sflux density, T fo 130	40 55.19		0.280;				
eff=0.8;	Sestimated efficien 131	48 70.12		0.300;				
Dmax+0.45;	Mmaximum duty cycle 132	49 81.07	- C	0.325:				
J=3e6;	Scurrent density, A 133	50 94.56	1	0.350;				
Kw=0.4;	Navindow factor for 134	51 109.1		0.375;				
Kwl=0.6;	Nwindow factor for 135	52 126.7		0.400];				
Vd=1.0;	Ndiode forward drop 136	32 120.7		0.4001,				
muo=4*pi*le-7;	Nuo - permeability 137 Noutput load resist 138							
Rowabs(Vo)./Io;	Noutput load resist 130	a=WIRE(:,2);						
NPOWER CALCULATION		b=ones(size(a))*w are						
Power CALCOLATION Po=sum((1.1*abs(Vo		cm(bena);	<i>a</i> ,					
Po=sum((1.1.405(VC	142	a=(max(a)+1)-a;						"wires.m" selected ()
ATURNS RATIO and D		C=8.*C:					ofings 117	
n=(1.1*abs(Vo)+Vd)		[x,index]=max(c);					Buctance SMG 22	
	/ (smin remain) ;	awire=WIRE(index,2)*)	0.6				inductance.mm 0	0.67580
Dmin=(Dmax*Vcmin)/	vcnax; 146	eth=WIRE(index,3)*1e-						
VEORWARD TRANSFORM		<pre>swp=gauge(index,:);</pre>	-1					
ap=((sort(Dmax)*Po	*(1+(1/eff)))/(Kw*J*Bm 148	and dealer (manufal)					value, of 375.00000 mg, wolts 24.00	
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So, you have the wire gauge table and also the cores table and in forward design dot m I have included the actual design calculations. So, what is there in forward design? Look at it first the specifications, we saw the specifications we see 48, we see minimum, we see maximum calculation, you can calculate it if you have tolerance otherwise list the minimum and the maximum

Now, the change that I have done, V naught is indicated as a vector twelve volts and dv as another vector the delta v and I naught is also a vector one volte these are single a single secondary, but if you have multi secondary you just have to include comma and put in let us say, you can put in a 15 volts, you can put in a minus 15 volts so on. And accordingly the ripple for the output corresponding that vector will change and the I naught vector also will change, but now I will just bring it back into a single. So, this can be used for multi output forward converter.

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Then the designer variables delta I, I have set it at 30 percent ripple inductor current ripple can change it did that so that to reduce the core size. 20 colour switching frequency, I have given two different flux densities; one for the flux density or transformer where I am setting it as 0.2 tesla, another Bml the flux density for inductors as 0.25 tesla.

The efficiency of the transformer worst case minimum is 80 percent generally, when you design it will be much more than 80 percent. So, this is a safe lower limit to calculate the input power. Dmax are set at 0.45, J is 3 ampere mm 3 ampere mm square or 3 into ten to the power of 6 ampere meter square, Kw 0.44, transformer 0.6 for inductor, Vd and all these other calculations.

# (Refer Slide Time: 04:24)

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59 awp-sum((n.*Io)*sqrt(Dmax)/J); % Area of c/s of pri winding, 60 awd-sum((0.1*(n.*Io)*sqrt(Dmax))/J); % Area of c/s of demagnetising wind 60 awd-sum((0.1*(n.*Io)*sqrt(Dmax))/J); % Area of c/s of demagnetising wind 61 awd-sum((0.1*(n.*Io)*sqrt(Dmax))/J); % Area of c/s of demagnetising wind 62 awd-sum((0.1*(n.*Io)*sqrt(Dmax))/J); % Area of c/s of demagnetising wind 63 awd-sum((0.1*(n.*Io)*sqrt(Dmax))/J); % Area of c/s of demagnetising wind 64 awd-sum((0.1*(n.*Io)*sqrt(Dmax))/J); % Area of c/s of demagnetising wind 65 awd-sum((0.1*(n.*Io)*sqrt(Dmax))/J); % % Area of c/s of demagnetising wind 65 awd-sum((0.1*(n.*Io)*sqrt(Dmax))/J); % Area of c/s of demagnetising wind 6	fing. U=0.5 Vm = 20; Fs = 25000; Lm = 0.02 error: cilles from	
61 aws=(Io*sqrt(Dmax))/J; % Area of c/s of sec windings.	exit forward_design at Line 265 column 1 If Octave 4.2.2, Mon Mar 25103	
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You see first the power calculation P naught is 1.1 times V naught plus Vd into I naught and summing it over all the windings sigma. TURNS RATIO; find out the TURNS RATIO, you have 1.1 times V naught plus Vd of divided by Dmax Vc min or V min Vc max which will give you n of all the all the secondaries with respect to the primary n is a vector because I have I have used MATLABs vectorization strength.

Then the FORWARD TRANSFORMER DESIGN or this is where the new thing comes in, find the ap; ap using the equations and then going to the while loop you call the cores function the cores function which I have indicated here and that will go into the cores function and try to search for cores. So, it will ask which core you want whether you want to have ferrite core, MATLAB metglas different core materials. And once you choose the material it will go into that and then choose the specific core according to the area product calculator.

Then it will give out the core selected core, the selected cores ac selected cores window area and the area product.

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<pre>v Find Ar, Aw for given Ap using cores function v Find Ar, Aw for given Ap using cores function v Find Strip cores, n is a program core selection v Find Strip cores, n is a program core selection v Find Strip cores (selection) v Find Strip cores (selection) v Find Strip cores (selection) v Find Strip Core v Find Strip cores of C/s of pri winding v Find Strip core (selection) v Find Strip core (selection) v Find Strip core v Find Strip cores of C/s of the windings. v Find Strip Core v Find Strip core of C/s of the windings. v Find Strip core (selection) v Find Strip</pre>	Performent (Frontes) manufer () 2 Oriente (1.1.3) The O O Perent Seconder or Manufer (1.1.3) Seconder of Manufer (1.1.3) Secon
8         [aud,eth_SMG] = wires(aud);           9         SGGs <sup>-1</sup> , vires(aud);           9         SGGs <sup>-1</sup> , vires(aud);           10         faul,eth(i),sup);           2         SGGs <sup>-1</sup> , vires(aud);           3         end           4	Noticities         Matter of scattage         137           Films

And using that Np, Nd, Ns are calculated and then you are calculating the wire gauges here and for that I am using the wires using the wires table and the wires table will give you the aw wire cross section actual for the wires and the and the SWG, Standard Wire Gauge.

(Refer Slide Time: 06:10)

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30 57 % Calculation of Area of c/s of the windings. 58 58	File Browser 8 * Command Window 8 manuted	×
39 augusum((n.*Io)*sqrt(Dmax)/J); % Area of c/s of pri winding. 80 aud=sum((0.1*(n.*Io)*sqrt(Dmax))/J); % Area of c/s of demognetising windis 61 aut=(Io*sqrt(Dmax))/J; % Area of c/s of sec windings. 6	Ing - None	К
<ol> <li>Find SWG of the wire to be used using the wires function</li> <li>Note: Wires.m is a program for wire gauge selection</li> <li>For details contact Dr. L.Umanand, CEDT, IISc, Bangalore-560 012.</li> </ol>	The ground stream former former bettern transfer metalum powjanum witeum designin and Discontern	
67         [awp,ethy,566] = viresiaw];           68         [awp,ethy,566] = viresiaw];           69         SMGsw <sup>+</sup> ;'iintitalize to null string           70         for i= 1:lengthiaw];           71         [smGil,ethi[],smg] = wires(sm(i));           72         SMGswirvat(SMGs,smg);           73         edd           74         74	I and A Development I and Mose Browney Browne	
<pre>&gt;&gt;</pre>	Ware <ul> <li>Other Leasting</li> <li>Bin</li> <li>Choice</li> <li>Diman</li> <li>Diman</li> <li>Rit</li> <li>Diman</li> <li>Rit</li> <li>Diman</li> </ul>	
64         else           5         flap1;           66         end           7         a.jdoce1.1;           88         critecnt1;           99         thDuctoRestStM           91         thDuctoRestStM           92         L=[0.*(r/l.lowin)/(di*fs);           93         Intalcot(d/2);           94         thEvent.theyen	winding         Matter of Vacinity         10           Connect/Minty         #         winding         Matter of Vacinity         10           Connect/Minty         #         Winding         Matter of Vacinity         10         #           Mint         Image         *         Generation         #	
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Then you do the window area check if it is not fitting it will go into the next loop it will ask you which again to choose a core and so on.

(Refer Slide Time: 06:17)

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84 else 85 flag=1; 86 end 87 a.index=1.1;		* 1 ×
<pre>8 a_lock=l1; cnt+crti; 80 end Vor WHILE 91 butTR DeSIGN 92 t=(Ls.Wer(1-bein).//diffs); 92 t=(Ls.Wer(1-bein).//diffs); 93 t=(a)(crt(a)); 94 t=(a)(crt(a)); 95 t=(a)(crt(a)); 95 t=(a)(crt(a)); 96 coret=";ikinitalise with null string 97 for i=1:length(L), Vor as many secondary windings 108 a) first=a)(crt(a)); 108 a] first=a)(crt(a)); 109 a) first=a)(crt(a)); 109 a) first=a)(crt(a)); 109 a) first=a)(crt(a)); 109 a) first=a)(crt(a)); 100 a) first=a)(crt(a)); 100 a) first=a)(crt(a)); 100 a) first=a)(crt(a)); 101 a) first=a); 102 a) first=a)(crt(a)); 103 a) first=a); 103 a) first=a); 104 a) first=a); 105 b) first=a); 105 b) first=a); 106 b) first=a); 107 b) first=a); 108 a) first=a); 108 a) first=a); 109 b) first=a); 109 b) first=a); 109 b) first=a); 109 b) first=a); 109 b) first=a); 100 c) first</pre>	Image         Others         Others </th <th>WITA</th>	WITA
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And then the INDUCTOR DESIGN comes in finding out the value of L for every secondary you have an inductor. So, L here will be a vector and find out the energy of the inductor and finally, you do a area product design just like we discussed.

(Refer Slide Time: 06:45)

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112       [alc(i),alw(i),alp(i),cort]=cores(alp(i),1,a_index);         113       corestruct(core);         114       corestruct(core);         115       V         116       V         117       N(i)=read(i)=int(i)=int(i)=int(i);         118       V         119       V         110       V         111       V         112       V         113       V         114       V         115       V         115       V         116       V         117       N(i)=read(i)=read(i)=read(i)=read(i)         118       V         119       V         111       V         111       V         112       V         114       V         115       Alf(i)=read(i)=read(i)=read(i)=read(i):         116       V         116       V         116       V         116       V         116       V         111       V         111       V         111       V         111       V         11	Plac Brever     0 *     Constant Unitation     0       Names     C     O famore     1.000 </th
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And do the core you I am using cores here again, to select the cores and then wires here to select the wire gauge for the inductor and only here you also calculate the air gap and goes into an iteration.

(Refer Slide Time: 06:59)

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10.         Idaw/IdawToma;           10.         Vdbrm-Wcmax;           10.         Vdbrm-Wcmax;           10.         Secondary side freewheeling diades           10.         Idaw/IdawTomax;           10.         IdawYouth;           10.         IdawYouth;           10.         IdawYouth;	Dr         initiality         Master of Violation         137           Community         0         initiality         Keep of Initiations         862 2           Term
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If it is not fitting and then the OUTPUT CAPACITOR FILTER DESIGN; the OUTPUT FILTER CAPACITOR DESIGN, the DIODE DESIGNS. The various diodes demagnetising diode, the secondary blocking diode in the secondary freewheeling diode POWER SWITCH all those things.

(Refer Slide Time: 07:12)

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* forward, design.m (home/hums/hums, der/MOOC/PE/wk010/resources/mfiles/horward, design.m) - Bisefish 22.30	X Otree X
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ID         ID <tdid< td="">         ID         ID         ID<!--</td--><td>Reference         # *         Consult Window         # *           Reference         # *         Seconder to M. A.H.#         #         #           Reference         # *         Seconder to M. A.H.#         #         #         #           Reference         # *         Seconder to M. A.H.#         #</td></tdid<>	Reference         # *         Consult Window         # *           Reference         # *         Seconder to M. A.H.#         #         #           Reference         # *         Seconder to M. A.H.#         #         #         #           Reference         # *         Seconder to M. A.H.#         #
<pre>194for i-litength[lo], 386 fprint[ld], vok1 %s/t &amp; &amp; . 396 fprint[ld], vok1 %s/t &amp; . 397 for i-litength[di], 398 fprint[ld], vok1 %s/t %s/t %s.2fvn', 'Inductor current ripple, amps',['ripple',num2) 308 fprint[ld], vok1 %s/t %s/t %s/t %s/t %s/t %s/t %s/t %s/t</pre>	Image: Constraining and the set of solutions of the set of the s
203fprintf(id,'%s\t %5.2f\n','Switching frequency, KHz',fs/1000); 204fprintf(id,'%s\t %5.2f\n','Bm for transformer, Tesla',Bm);	Vin + 20, Fs = 25000, Lm = 0.02 eval eval forward_design at Line 265 column 1
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(Refer Slide Time: 07:15)

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<pre>3) fprintf(id, 'Not V. S.21', 'Suitching frequency, DU: fs/1000); bip:inf(id, 'Not V. S.21', 'Suitching frequency, DU: fs/1000); bip:inf(id, 'Not V. S.21', 'Suitching for transformer, Ver(#f100); D'frintfid, 'Not V. S.21', 'Transformer, Teola, 'Deal', 'Deal</pre>	Part Preser     # *     Constant (Thister       Amoret C > Original Constants (Milling)     M.2.8       Amoret C > Original Constants (Milling)     Market (Milling)       Amoret C > Original Const
<pre>iS fprintf(id, '\t\s\t %5.2f\n', 'PIV, volts', Vddrm);</pre>	exit vinding1 Capacitance value, of 375.40000 B Catage 4.2.2. Fo Mar 2215 22: vinding1 Voltage rating, volts 24.00
<pre>#for i = litemybi(%) for i = litemybi(%)</pre>	With 2017 - 20200 (1m + 0.00)         custoring         OR registrement, status         8, 33333           Diright 2017 - 20200 (1m + 0.00)         entracting in the status         Line 2016 (1m + 0.00)         entracting in the status           Diright 2017 - 20200 (1m + 0.00)         entracting in the status         Image: Status         entracting in the status           Diright 2017 - 20200 (1m + 0.00)         entracting in the status         Image: Status         entracting in the status           Image: Diright 2017 - 20200 (1m + 0.00)         entracting in the status         Image: Diright 2016 (1m + 0.00)         entracting in the status           Image: Diright 2017 - 20200 (1m + 0.00)         entracting in the status         Image: Diright 2016 (1m + 0.00)         entracting in the status           Image: Diright 2017 - 20200 (1m + 0.00)         entracting in the status         entracting in the status
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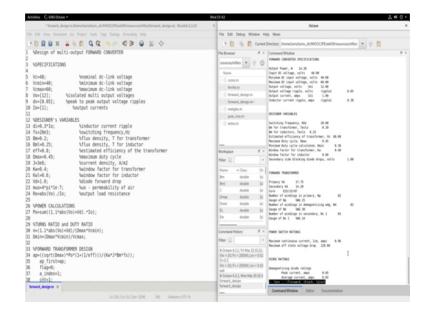
Then comes the display section where you display all the area details. So, let me just run this for you for this specification.

(Refer Slide Time: 07:23)

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cnt=1:	# Octave 4.2.2, Man Mar 25.003 forward, design		
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So, I will go into octave I am already in that folder you see that you see forward design and the other m files

### (Refer Slide Time: 08:15)



So, let me type in forward convert FORWARD DESIGN and then you execute that it will ask you to choose a core material, I will choose Ferrite which is 1. I will choose ferrite and then within ferrite it will ask you to choose POT CORES, EE CORES this is the data which I have entered. A minimal set of data you can always increase it you can add your own set of new cores and cores shapes.

Let me choose EE CORE now, second and then see that it may then it is asking for the INDUCTORS and I will again choose this one again EE CORE. And that is it the design is done and it will get printed you see the specifications and the DESIGN VARIABLES, FORWARD TRANSFORMER see, choice of E25 13 0 7, the primary windings, the Gauges, Demagnetizing Winding Gauge so on, the POWER RATING of the switch.

(Refer Slide Time: 08:35)

* forward, design,r	(home/lums/lums_dir/MOOC/PE/wk09i/resources/in/files/forward_design.m) - Bluefish 2.2.50			Octave	
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<pre>\Design of multi-</pre>	output FORWARD CONVERTER	File Browser	<i>d</i> >	Command Window 6	
3 \SPECIFICATIONS 5 VC=48: \nominal dc-link voltage	rsources,Imfiles	• 9.0	Secondary IA 14.20 Gore E23/33/07 Sumber of Vindings in primary, Np 82		
	Name		Gauge of Np SWG 15 Number of windings in demogratising wdg, Nd N2		
Vcmin=40:	Wininum dc-link voltage	- Cores.m		Gauge of Nel SH5 38	
Vcmax=60;	Smaximum dc-link voltage	ferite.m		Number of windings in secondary, No 1 45 Gauge of No 1 546 24	
	solated multi output voltages	- E forward_de	esign.m	andle of an 1 Date for	
	ešk to peak output voltage ripples	forward_de	esign.m-	PIMER SWITCH RATINGS	
0 Io=[1];	houtput currents	- D metglas.m			
1	pow, iron.r		Maximum continuous current, Ice, amps 0.06 Maximum off state voltage drop 120.00		
<pre>12 hDESIGNER's VARIA 13 di=0.3*Io:</pre>	hinductor current ripple	- D wires.m		and an entry of the second second	
13 d1=0.3-10; 14 fs=20e3;	Switching frequency,Hz			SIDDE BATING	
5 Bm=0.2:	Sflux density, T for transformer				
6 Bml=0.25;	Sflux density, T for inductor			Demographic diode ratings Peak current, angs 0.45	
7 eff=0.8;	Sestimated efficiency of the transformer	Workspace	8 ×	Average current, anps 0.42	
8 Dmax+0.45;	Mmaximum duty cycle	Filter (1)		PTV, volts 120.00 Blocking diode ratings for winding 1	
9 J=3e6;	\current density, A/m2			winding2 Peak current, amps 1.25	
0 Kw=0.4; 1 Kwl=0.6;	Window factor for transformer	Name + Ci		winding] FIV, volts 47.33	
2 Vd=1.0:	Winder forward drop		suble 1x	Freewheeling diade ratings for winding 1 winding] Pask current, amon 1.15	
3 muo=4*pi*le-7;	Nuo - permeability of air		ubie 10	winding] Average current, amps 0.00	
4 Romabs(Vo)./Io:	Noutput load resistance		whie 14	winding1 PTV, wolts 47.33	
5					
6 NPOWER CALCULATIO				INDUCTOR DESIGN	
7 Po=sum((1.1*abs(V	<pre>b)+Vd).*Io);</pre>			winding1 Inductance value, ext 1.40000	
8	NUT BITTO	L9 00	suble 14	vinding1 Core E25/13/07 vinding1 Number of vindings 117	
<pre>9 \TURNS RATIO and DUTY RATIO 8 n=(1.1*abs(Vo)+Vd)/(Dmax*Vcmin);</pre>				winding1 Gauge of inductance 546 22	
1 Dmin=(Dmax*Vcmin)		Command History		winding1 Airgap for inductance.mm 0.67580	
2	Former's	Filter 🗌		CAPACITOR FILTUR AATINGS	
<b>3 AFORWARD TRANSFOR</b>	MER DESIGN	II Octave 4.2.2, Fi	< Mar 22 15 22 C	winding] Capacitance value, of 375.00000	
	p*(1+(1/eff)))/(Kw*J*Bm*fs));	Vn = 20; Fs = 25	000; Lm = 0.02	winding1 Wultage rating, volts 24.00 winding1 EDE requirement, shes 0.13333	
5 ap_first=ap;		Die a be fan Make im a diel			
5 flag=0;		ever filese: invalid stream number = }		error: fclose: invalid stream number = 1 error: called from	
7 a_index=1; 8 cnt=1:			# Octave 4.2.2, Mon Mar 25 50:3 forward_design at Line 265 column 3		
e cntrat		forward_design	forward_design as		
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And the DIODE RATINGS, Demagnetizing, Blocking, Freewheeling, INDUCTOR DESIGN all these things are calculated and you see the output. I will allow you to explore this and leave it to you fine tune it and try to understand this forward design m file.