

# Fundamentals of Wavelets, Filter Banks and Time Frequency Analysis.

Professor Vikram M. Gadre.

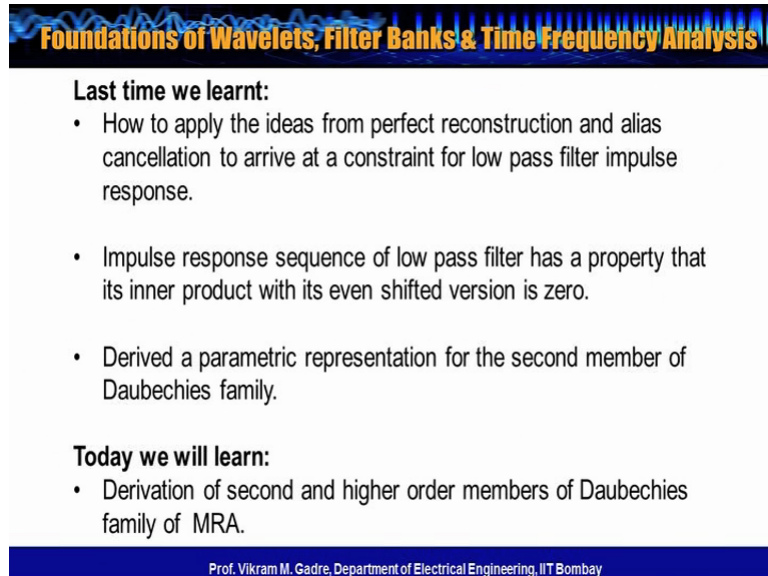
Department Of Electrical Engineering.  
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Week-5.

Lecture-14.1.

Effect of minimum phase requirement on filter coefficient.

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**Foundations of Wavelets, Filter Banks & Time Frequency Analysis**

**Last time we learnt:**

- How to apply the ideas from perfect reconstruction and alias cancellation to arrive at a constraint for low pass filter impulse response.
- Impulse response sequence of low pass filter has a property that its inner product with its even shifted version is zero.
- Derived a parametric representation for the second member of Daubechies family.

**Today we will learn:**

- Derivation of second and higher order members of Daubechies family of MRA.


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A warm welcome to the lecture on the subject of wavelets and multirate digital signal processing. We continue in this lecture to discuss the Dobash or Deubeshies filter bank which we had very briefly introduced in the previous lecture. I would like to put before you the salient points of that filter bank once again and then complete the design that I had begun in the previous lecture. So recall that we had based the construction of the series of Dobash filter banks on the idea of annulling polynomials of higher and higher degree.

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WAVELETS AND MULTIRATE DIGITAL SIGNAL PROCESSING C-DEEP IIT BOMBAY

Second member of Daubechies' family:  
Highpass filter:  
factor of  $(1 - \bar{z}^{-1})^2$   
 $= \bar{z}^{-D} H_0(-\bar{z}^{-1})$




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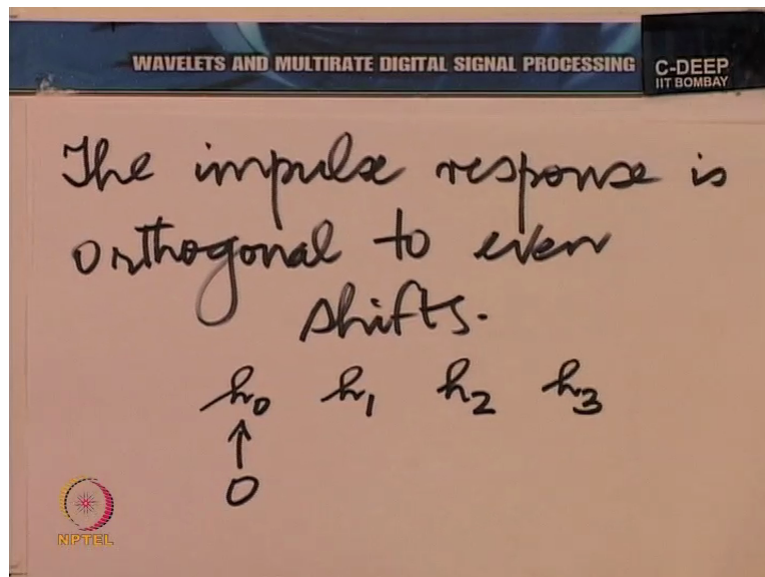
where  $H_0(z) =$   
Corresponding (analysis)  
lowpass filter  
 $\Rightarrow H_0(z)$  would have  
factor  $(1 + \bar{z}^{-1})^2$



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$H_0(z)$  has 3 roots.  
2 already specified  
( $\bar{z} = -1$ ).  
3<sup>rd</sup> to be determined.





So we said that we wanted more and more factors of the form  $1 - Z^{-1}$  appearing in the high pass filter. So for example, let me put down the structure of the next member in the family after the Haar case where instead of one, we would have 2 factors. What we said was the 2<sup>nd</sup> member of the Daubechies family would look like this. The high pass filter would have a factor of  $1 - Z^{-1}$  the whole squared. Now therefore, if you look at the lowpass filter, remember the high pass filter was essentially of the form  $Z^{-1} H_0 - Z^{-1}$ .

Where  $H_0 Z$  is the corresponding lowpass filter. Of course I am talking about the analysis side. So essentially the analysis lowpass filter would now have a form like this,  $H_0 Z$  would have the factor  $1 + Z^{-1}$  squared. And then we recall that we had even length for the filter and therefore we have a situation  $H_0 Z$  has 3 zeros, 2 already specified, obviously they belong to  $-1$  and therefore the 3<sup>rd</sup> to be determined. And why do we determine this 3<sup>rd</sup> root from? Well, we go back to the requirement of orthogonality to even shifts.

So recall that we have said that the impulse response is orthogonal to even shifts. That means if I assume that this filter has the impulse response  $h_0, h_1, h_2, h_3$  at 0, then this is orthogonal to its shifts by 2, 4 and so on.

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Nontrivial equation  
(Shift by 2) :

$$\dots h_0 \quad h_1 \quad h_2 \quad h_3 \quad \dots$$

$$\dots \quad h_0 \quad h_1 \quad \dots$$

$h_0 h_2 + h_1 h_3 = 0$

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$$h_0 + h_1 z^{-1} + h_2 z^{-2} + h_3 z^{-3}$$

$$= C_0 (1 + z^{-1})^2 (1 + B_0 z^{-1})$$

Compare coeff on both sides

NIPTEIL

So the nontrivial case, the only nontrivial equation that we get is the following. It comes from a shift by 2  $h_0, h_1, h_2, h_3$  and when it is shifted by 2, you have  $h_0, h_1$  and then you know there are all zeros after this, there are zeros before and there are zeros before. So all that you have is  $h_0 h_2 + h_1 h_3$  is equal to 0, this is the only nontrivial equation that we get. Now from the location of the zeros and the free parameters, we need to express  $h_0$  through  $h_3$  in terms of the free parameters. So what do we have, we have  $h_0 + h_1 Z$  raised to the power - 1 +  $h_2 Z$  raised to - 2 +  $h_3 Z$  raised to - 3 is of the form some constant, let us say  $C$  or  $C_0$  if you please, times  $1 + Z$  inverse the whole squared times  $1 + B_0 Z$  inverse.

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$$(1 + z^{-1})^2 (1 + B_0 z^{-1})$$
$$(1 + 2z^{-1} + z^{-2}) (1 + B_0 z^{-1})$$
$$1 + 2z^{-1} + z^{-2} + B_0 z^{-1} + 2B_0 z^{-2} + B_0 z^{-3}$$

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Except to within constant  $C_0$ ,

$h_0$	$h_1$	$h_2$	$h_3$
1	$2 + B_0$	$1 + 2B_0$	$B_0$

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$$h_0 h_2 + h_1 h_3 = 0$$
$$\Rightarrow 1 + 2B_0 + (2 + B_0) B_0 = 0$$
$$\Rightarrow 1 + 4B_0 + B_0^2 = 0$$

NPTEL



And we need to compare coefficients on both sides. Now the constant  $C_0$  does not affect orthogonality. So we shall just focus on the rest of the equation because we 1<sup>st</sup> need to satisfy the requirement of orthogonality, orthogonality to even shifts I mean. And from there we need to write mean the constant  $C_0$ . We will see later what helps us determine  $C_0$ . So in fact if you look at it, what we are asking for is the following expanded term  $1 + Z^{-1}$  inverse the whole square times  $1 + B_0 Z^{-1}$  where  $B_0$  needs to be determined. And this as we said could be expanded as  $1 + 2 Z^{-1} + Z^{-2}$  times  $1 + B_0 Z^{-1}$  and if we collect terms that gives us  $1 + 2 Z^{-1} + Z^{-2} + B_0 Z^{-1} + 2 B_0 Z^{-2} + B_0 Z^{-3}$ .

So we aggregate terms together here, we will take the coefficients. So essentially, you know, except for the constants,  $h_0$  is essentially therefore 1,  $h_1$  is of the form  $2 + B_0$ ,  $h_2$  is of the form  $1 + 2 B_0$  and  $h_3$  is of the form  $B_0$ . And now we can write down the orthogonality equation that we seek. It says  $h_0 h_2 + h_1 h_3$  must be 0 implying that  $1 + 2 B_0 + 2 + B_0$  into  $B_0$  is 0, where we are effectively saying  $1 + 4 B_0 + B_0^2$  is 0. So there we have an expression for  $B_0$ , it is easy to determine, so  $B_0$  has got constraint as you see, not surprising.

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Solving the equation

$$B_0 = \frac{-4 \pm \sqrt{16 - 4}}{2}$$

$$= \frac{-4 \pm 2\sqrt{3}}{2} = \underline{\underline{-2 \pm \sqrt{3}}}$$

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$$h_0 h_2 + h_1 h_3 = 0$$

$$\Rightarrow 1 + 2B_0 + (2 + B_0) B_0 = 0$$

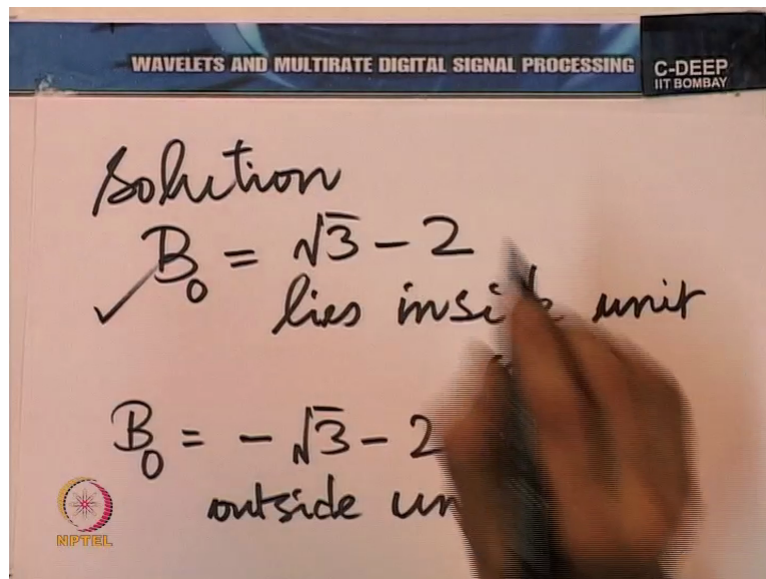
$$\Rightarrow 1 + 4B_0 + B_0^2 = 0$$

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There was one free parameter and one nontrivial constraint. Solving the equation we have  $B_0$  is  $-B \pm \sqrt{B^2 - 4AC}$  by  $2A$ , that gives us  $-4 \pm 2\sqrt{3}$  divided by 2. And that gives us 2 solutions,  $-2 \pm \sqrt{3}$ . Now we have 2 solutions here, which of them should we choose? Well, what distinguishes these 2 solutions? It is very clear from the quadratic equation and let me go back to it. You see if we look at this term, this tells us the product of the roots, the term one.

And the product of the roots clearly has a magnitude of 1. So if one of them lies inside the unit circle, the other must be outside. In fact they cannot lie on the unit circle because none of them has a magnitude of 1. And therefore one must lie inside the unit circle and the other outside. Let us take note of that, in fact it is very easy to see which lies inside and which lies outside. If you look at the  $-2 - \sqrt{3}$  solution, it clearly has a magnitude greater than normal one and the other one has a magnitude less than 1.

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So among the solutions  $B_0$  is square root 3 - 2 lies inside the unit circle and  $B_0$  is - square root 3 - 2 lies outside the unit circle. Now we have a choice, we could either choose this or this, we shall choose this and there is a reason for it. You see, very often we like to choose what is called the minimum phase solution, there is this idea of minimum phase. I shall not dwell too much on it at this moment. Suffice it to say that minimum phase essentially means choosing all zeros inside the unit circle wherever possible.

In fact the idea of minimum phase comes from what is called minimum phase delay. So when we you know after all one interesting thing is that whether we choose the roots inside the unit circle or outside, the magnitude of the frequency response would be the same, the magnitude would not be different, what would be different is the phase. And if we put the root outside the unit circle, there is going to be an increased phase delay. And very often that would also point to an increased group delay, increased phase delay, increased group delay in the filter.



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We take the "minimum phase" solution  
( $B_0$  inside unit circle)

$$B_0 = \sqrt{3} - 2$$
$$|B_0| < 1$$

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Except to within constant  $C_0$ ,

$h_0$	$h_1$	$h_2$	$h_3$
1	$2+B_0$	$1+2B_0$	$B_0$

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Impulse response of Daubechies lowpass filter:

$1$	$2+B_0$	$1+2B_0$	$B_0$
$\uparrow$	$= \sqrt{3}$	$= 1-4+2\sqrt{3}$	$\sqrt{3}-2$
$\circ$		$= -3+2\sqrt{3}$	

to within constant  $C_0$ !

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And when we take the solution inside the unit circle, we are reducing the phase of the group delay as much as we can in the filter. So it is essentially a question of choosing the better solution in terms of phase. So let us summarise that. We take the minimum phase solution, that is  $B_0$  inside the unit circle and we have  $B_0$  is square root  $3 - 2$ , obviously  $\text{mod } B_0$  is less than 1 here. And one can also evaluate this approximately. If you recall square root of 3 is about 1.73, so this would be  $1.73 - 2$  and one can come up with an approximate value, that is not really an issue.

Anyway, we can now put down the impulse response of the Daubeshies lowpass filter therefore. It is essentially, well let me read off the impulse response from here. Let me flash the impulse response before you once again and then we will substitute. So this was the impulse response, now we substitute for  $B_0$ . So  $1, 2 + B_0$  which is essentially square root 3 and then you have  $1 + \text{twice } B_0$  which is  $1 - 4 + 2 \text{ root } 3$  or  $-3 + 2 \text{ square root } 3$  and finally  $B_0$  which is just square root  $3 - 2$ . So this is  $h_0$  of course, well, please remember this is to within a constant. So there is still that constant  $C_0$  that needs to be determined.

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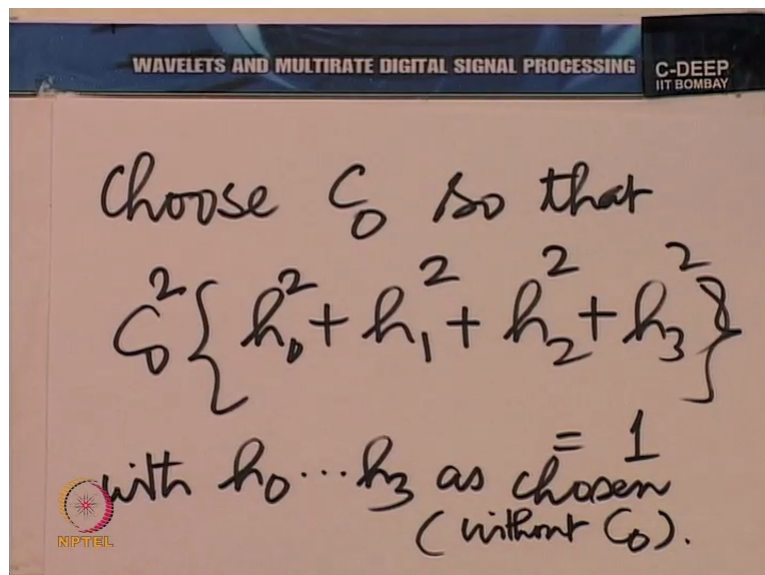
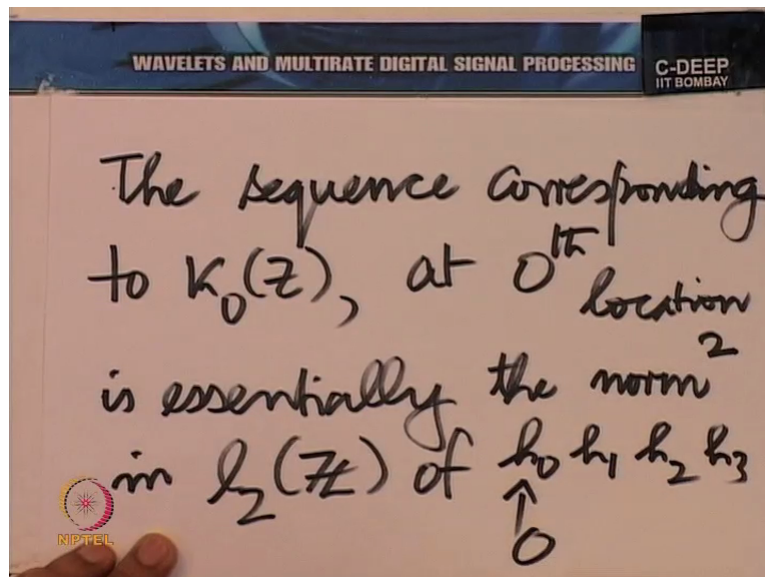
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$$K_0(z) = H_0(z)H_0(\bar{z}^{-1})$$

$$K_0(z) + K_0(-z) = \text{Constant}$$

Choice of  $C_0$  means choosing this constant.

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How do we determine the constant  $C_0$ ? Well, we go back to the original equation of  $K_0(z)$  that we had. So we wanted  $K_0(z)$  defined by  $H_0(z)$  times  $H_0(z)$  inverse to obey the following  $K_0(z) + K_0(-z)$  is a constant. And in fact what it really means is we now need to choose this constant, choice of  $C_0$  means choosing this constant. The easy thing to do is to ensure that the impulse response has a unit norm in the sense of  $L_2$ . Because if you look at it, the dot product of the impulse response with itself, you know what we are saying essentially is  $K_0(z)$ , you know the sequence corresponding to  $K_0(z)$  at the  $0^{\text{th}}$  location is essentially the norm of in  $L_2(\mathbb{Z})$ , the norm square actually in  $L_2(\mathbb{Z})$  of the impulse response.

It is a dot product of the impulse response with itself. And we could as well make that 1 for convenience. So now we shall choose  $C_0$  in order that this becomes one. And in fact I do not need to carry out the computations, essentially what I am saying is choose  $C_0$  so that  $C_0$

squared times  $h_0$  squared +  $h_1$  squared +  $h_2$  squared +  $h_3$  squared is equal to 1 with  $h_0$  through  $h_3$  as chosen before, without  $C_0$ . So I leave that little calculation for you to do and I would strongly recommend that students look at various texts that list the Daubeshies filter responses and verify that the Daubeshies filter response for a filter length of 4 exactly coincides with what we calculate from here.

So much so for the Daubeshies filter bank. Now the next step is to build  $\Phi_t$  and  $\psi_t$ , how would you do that?