

Basic Electronics
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Lecture – 48
Precision rectifiers (continued)

Welcome back to Basic Electronics. In this lecture, we will look at a precision half-wave rectifier in which the op-amp does not enter the saturation region. We will then see how a precision full wave rectifier circuit can be made up using the circuit blocks we have already seen. Finally, we will look at wave shaping using diodes, and how to use it to convert a triangular input voltage to sinusoidal output voltage. Let us get started.

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Improved half-wave precision rectifier

(i) D_1 conducts: $V_- = V_+ = 0V$, $V_{D1} = -V_{D1} = -0.7V$.
 D_2 cannot conduct (show that, if it did, KCL is not satisfied at V_+).
 $\rightarrow i_{D2} = 0$, $V_+ = V_- = 0V$.
 $i_{D1} = i_{D2}$ which can only be positive $\Rightarrow V_i > 0V$.

(ii) D_1 is off; this will happen when $V_i < 0V$.
 In this case, D_2 conducts and closes the feedback loop through R_2 .
 $V_+ = V_- = i_{D2}R_2 = 0 + \left(\frac{0 - V_i}{R_1}\right)R_2 = -\frac{R_2}{R_1}V_i$.

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Let us now look at an improved half-wave precision rectifier. And what is the improvement we are seeking over the super diode circuit, the improvement we are looking for is that the op-amp should not enter saturation, because as we have seen that affects the speed of the circuit. Let us see how this circuit works. There are two diodes now D_1 and D_2 . So, we will take two cases case one in which D_1 conducts; and case two in which D_2 conducts. Case one - D_1 is on this loop is then complete and then the op-amp operates in the linear region, therefore V_{minus} and V_{plus} are equal; V_{minus} is 0 volts. What about V_{o1} in that case, V_{o1} is V_{minus} minus this voltage drop, so that is 0 minus about 0.7, so V_{o1} is therefore minus 0.7 volts.

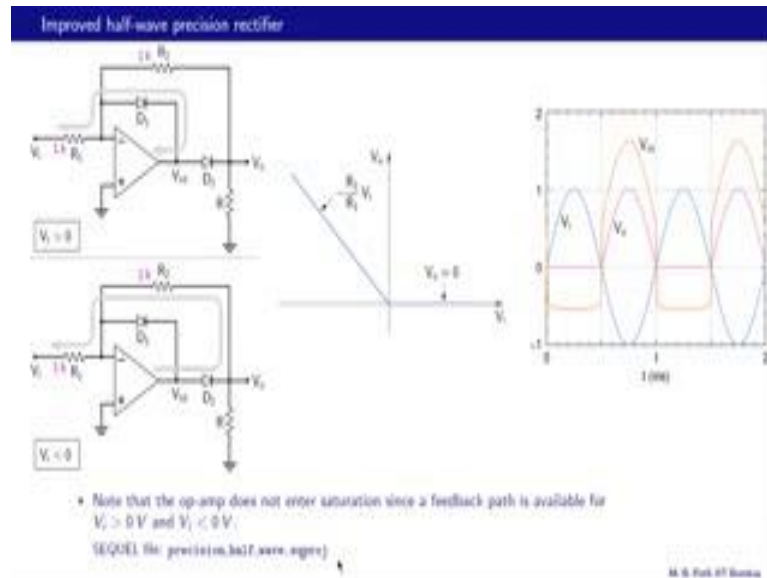
Now, if that happens we can show that D 2 cannot conduct, so that if it did then case 1 is not satisfied at this node. Let us do that suppose D 2 did conduct, what would be this voltage this is 0 volts, $0 - 0.7 - 0.7$, so this V_o would be minus 1.4 volts. This is 0, this is minus 1.4, so this R 2 would conduct like that, and this R would also conduct a current going into that node, because this is 0 and this is minus 1.4 volts. So, this current is going in also this current is also going in. So, the only way KCL can be satisfied is for D 2 to conduct in that direction and that cannot happen because that would be the reverse direction for D 2.

So therefore, we conclude that D 2 cannot conduct in this situation. If D 2 does not conduct then we have an open circuit here and then R 2 and R are in series. This end is at 0 volts and this end is also at 0 volts, so obviously, we cannot have any current in this path. So, this voltage drop as well as this voltage drop is then 0, and V_o is equal to 0. So, our situation now is D 1 conducts D 2 does not conduct i_{R2} is 0, i_R is also 0.

Let us now see what values of V_i this situation corresponds to. So, this is our current path like that. And V_{minus} is 0 volts, and the only way this can happen is if V_i is positive. So, the situation that we have discussed D 1 on, D 2 off can happen only if V_i is positive. Clearly, if V_i is negative then we cannot have D 1 conducting and that brings us to the second situation namely D 1 is off. And let us look at this situation in more detail now.

In this case, the conduction path is like this, diode D 2 conducts and that is how the current flows. The loop around the op-amp does flow and therefore, the op-amp operates in the linear region V_{minus} and V_{plus} are equal, V_{minus} is therefore 0. And because the current is flowing at that direction V_i is negative. So, this is a consistent picture. Let us now figure out, what V_o should be in this case that is easy to do. What is V_o it is equal to V_{minus} plus this voltage drop V_{minus} is 0. And for this voltage drop, we need that current that current is the same as this current, and this current is $0 - V_i$ divided by R 1 like that. And after putting it all together, we get V_o equal to minus R 2 by R 1 times V_i . So, we have two situations D 1 conducting V_o equal to 0; and in that situation D 2 does not conduct; D 2 conducting V_o equal to minus R 2 by R 1 times V_i and in that situation D 1 does not conduct.

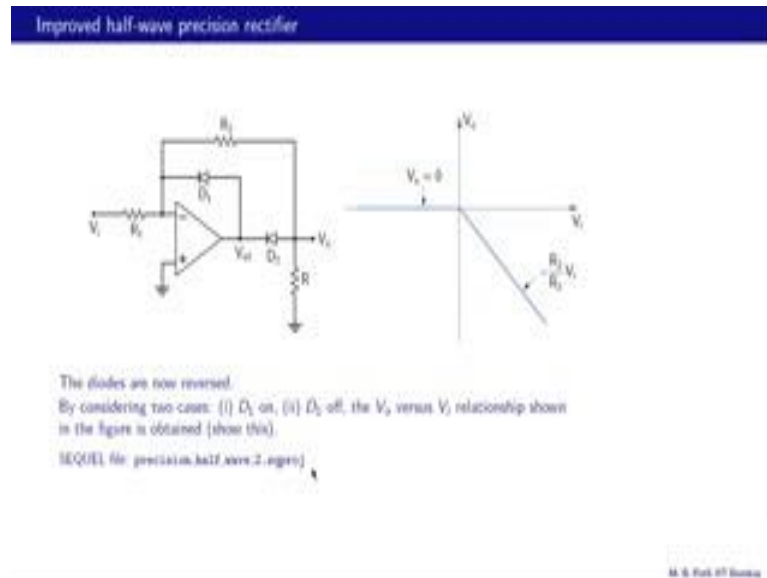
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Here is the summary of the improved half-wave precision rectifier. Positive V_i - D_1 conducts D_2 does not conduct V_o is 0 as shown here. Negative V_i - D_2 conducts D_1 does not conduct and V_o is minus R_2 by R_1 times V_i , so that is a straight line with a negative slope and going through the origin and that is what the waveforms would look like. When V_i is positive, the output voltage is 0; and V_i is negative, the output voltage is positive. And in this example, we have taken R_2 and R_1 to be equal. So, therefore, V_o and V_i are equal in the magnitude.

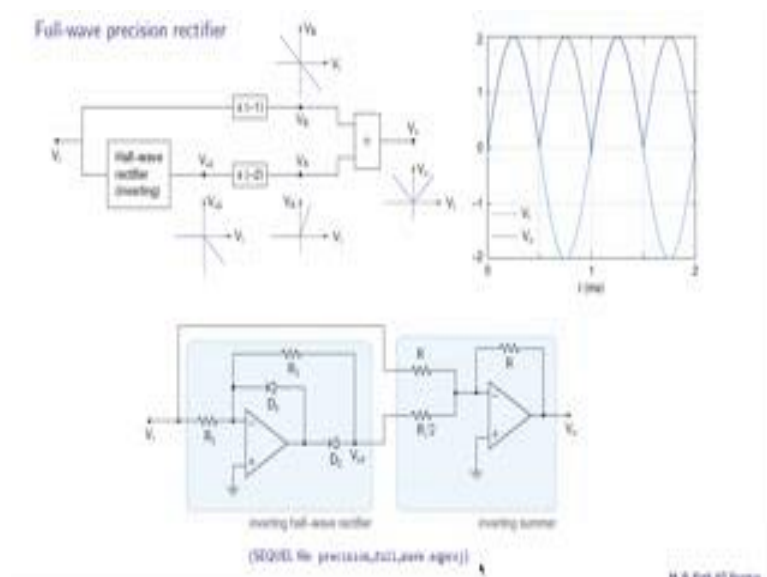
What is the big advantage of this circuit over the super diode circuit, the op-amp always operates in the linear region it does not enter saturation and that is very clear. If we plot this voltage V_o , and that looks like this and clearly it does not go to plus minus V_{sat} . Let us see if we can work out, what V_o should be in each of these regions. When V_i is positive, D_1 conducts this is virtual ground. So, therefore, V_o would be minus V_r , so that is what we observe over here. This is not quite minus 0.7 the exact value would really depend on the current levels. What about V_i negative we have this situation now and then V_o is V_o plus V_1 of D_2 and that is what we observe over here. And in the other case the op-amp does not enter saturation, since the feedback path is always available. Here is a circuit file for this simulation.

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Here is another improved half-wave precision rectifier; looks very similar to the circuit we just discussed except the diodes are now reversed. And as a result, we obtain this V_o versus V_i relationship shown on this figure here. So, take this as homework, figure out the conduction paths when D_1 is on and D_1 is off, and obtain this V_o versus V_i relationship. The circuit file is also available; you can try out the simulation as well.

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We can use the circuits, we have already looked at to make up full-wave precision rectifier. And here is a block diagram V_i is the input voltage, V_o is the output voltage

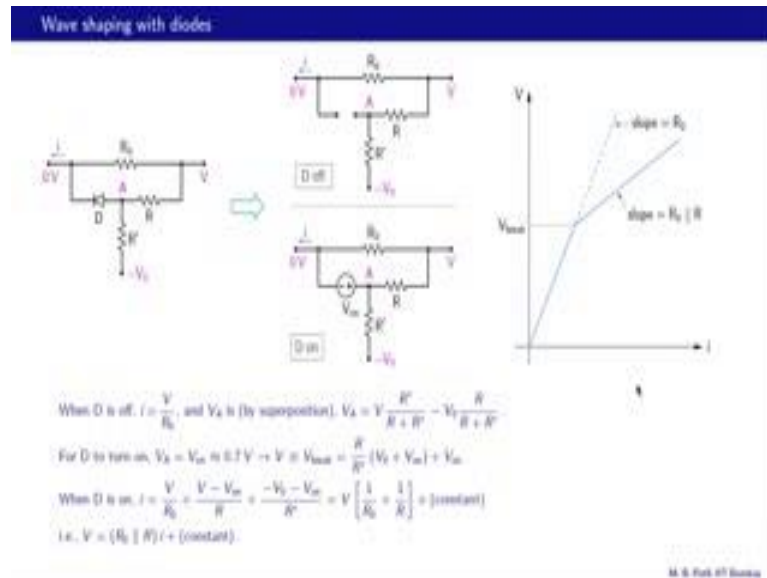
and the relationship between V_o and V_i that we would like is shown here. This is a half-wave rectifier inverting it gets V_i as the input, its output is V_{o1} ; and the relationship between V_{o1} and V_i is shown here. When V_i is negative, V_{o1} is 0; and when V_i is positive, V_{o1} is minus V_i . V_{o1} is multiplied by minus 2 to obtain V_a . Now, in this region when V_i is negative multiplying by minus 2 does not make a difference, so V_a is also 0 here. In this region when V_i is positive V_{o1} is minus V_i and multiplying that by minus 2 will give us plus 2 times V_i and that is what is shown over here.

Now, this plot here multiplies V_i by minus 1 to give V_b . So, if we plot V_b as a function of V_i , we get a straight line passing through the origin with a slope of minus 1. And now what we do is add V_b and V_a and obtain our final output voltage. Now, when V_i is negative, V_a is 0. So, this part goes through as it is right there. When V_i is positive, we have a slope of minus one here and the slope of plus 2 here. So, the net slope is plus 1 and that is how we obtain our desired V_o versus V_i relationship. Let us now see how this can be implemented with circuits.

Here is a circuit implementation of the block diagram. This block is the inverting half-wave rectifier and we have selected these two resistances to be equal, so as to get a slope of minus 1 here. So, this block uses V_{o1} versus V_i given by this graph, so that is V_{o1} . Now, this other three functions this multiplication by minus 2 multiplication by minus 1 and addition, these three functions are performed by this single block the inverting summer that we have already seen earlier.

What does it do let us look at the resistances this is R , this is R , and this is R by 2. So, V_o is equal to minus V_i minus 2 times V_{o1} , and that is exactly what we want. V_o is minus V_i minus 2 times V_{o1} in the block diagram as well. So, this circuit will perform full-wave precision rectification. Here is the simulation result that is our input voltage - the light blue curve and that is the output voltage. And here is the circuit file.

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Let us now talk about wave shaping with diodes. What is the meaning of wave shaping? Let say we have an input triangular wave and we want to convert that into an output sinusoidal wave that is an example of wave shaping. Here is a simple diode circuit and we will see that this can be used for wave shaping. We will take this node voltage as 0 volts, and there is a good reason for doing that as we will see later. This node is sitting at minus V_0 a constant voltage, it could be minus 5 volts or minus 10 volts for example, that is the power supply. And what we want to do is to plot this V as a function of this current I here.

First, let us consider D to be off not conducting, so this is an open circuit. And when D is off, what is the current it is simply V minus V_0 divided by R_0 , so V by R_0 . And what is this node voltage with respect to ground, we have V here, we have minus V_0 here, and this is an open circuit. So, we can obtain V_A by super position and that is given here V_A is V times R' by R' plus R_0 minus V_0 times R by R' plus R_0 , so that is our V_A when a diode is not conducting.

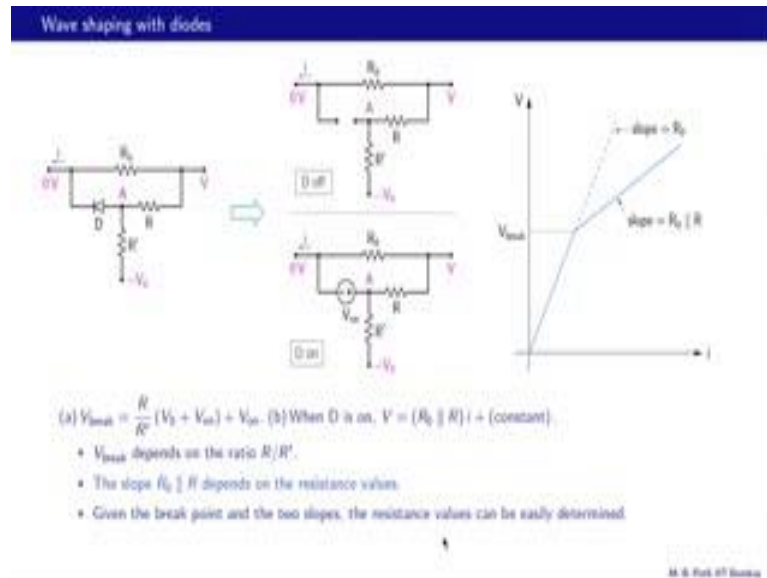
Let us look at this equation. And let us say V is positive. Now, this term is positive if V is positive and this term is negative. As V increases V_A will also increase and at some point it will reach 0.7 volts. Now, V_A becoming 0.7 volts means the diode turns on and that provides a break point in the V versus I relationship. So, for D to turn on V_A should be V_{on} which is about 0.7 volts, and that gives us this break point. So, what do we do

we put V_A equal to V_{on} on here and solve for V_{break} . So, V_{break} then turns out to be $R' \times (V_0 + V_{on})$, this is a positive number remember because minus V_0 is negative that plus V_{on} , so that is our V_{break} . So, when this voltage here is equal to V_{break} , the diode starts conducting, and then we have this equivalent circuit. So, the diode is now replaced with this battery here let say 0.7 volts.

Let us now look at this current when the diode is conducting; it is composed of two parts, this current and that current. Now, this first part is the same as before V_{on} divided by R_0 that is V_{on} / R_0 . And this second current, we can find by adding this current and this current. Now, when the diode is conducting, since this is 0 volts, this V_A is equal to V_{on} . What is this current then it is $V_{on} - V_{on}$ divided by R that is this second term here. And what is this current, it is $-V_0 - V_{on}$ divided by R' , the third term here. Now, we can combine terms containing V that is $V \times (1/R_0 + 1/R)$ plus $V_{on} / R_0 - V_0 / R' - V_{on} / R'$. And all the other terms are essentially constants because V_{on} is a constant V_0 is a constant.

So, we can write our current as $V \times (1/R_0 + 1/R)$ plus some constant. In other words, if you want to write V in terms of I that will look like this, this $R_0 \parallel R$ comes from this term. And now we have all the information we need to plot V as a function of I , and that is a plot. So, let us try to understand this plot. So, when V is small in this range, the diode is off; and the only current is the current through this R_0 , and therefore, the slope of this part is R_0 . At this point, when V is V_{break} the diode turns on; and now the slope of V versus I is $R_0 \parallel R$, which is of course, smaller than R_0 , so that gives us this segment here. So, that is a overall V versus I relationship for this circuit.

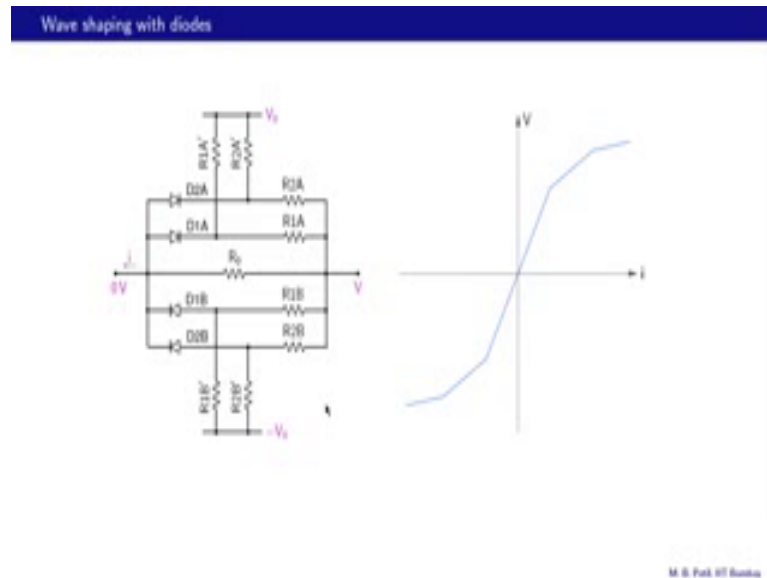
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In summary, we have V_{break} equal to R_0 by R' times V_0 plus V_{on} plus V_{on} that is a break on there. And when the diode is conducting, V is given by R_0 parallel times i plus the constant. So, if you look at this V versus i relationship, we notice that there are three design parameters; one - the slope of this part which is given by R_0 ; second - the slope of this part which is given by R_0 parallel R ; and third - this break part which is given by this expression here. And note that V_{break} depends only on the ratio R by R' and not on the actual values of R and R' .

Whereas, the slope R_0 parallel R does depend on the actual resistance values. And therefore, given the break point and the two slopes, the resistance values can be easily determined and that is why this circuit is very attractive.

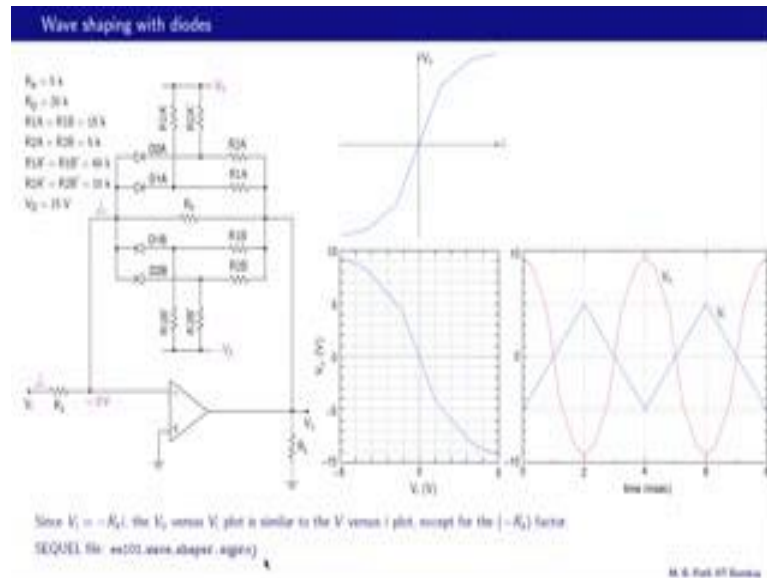
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So, what have we got so far, we have this V versus R relationship and we have seen that this break point is provided by this diode, when the diode starts conducting we have the break point. And this slope here is R_0 parallel with $R_1 B$ here. Now, what we will do is to introduce another branch just like this first one with different resistance values and that is what it looks like. What will this branch do, this will introduce one more break point in the V versus i relationship. And we can design the resistance values such that this break point the second break point occurs after the first break point. And what is this slope this slope is R_0 parallel with $R_1 B$ parallel $R_2 B$.

We can now add a complimentary branch like that. Note that the diode polarity is now different than this one. Also this voltage here is positive, not negative. And with this branch we can add a break point in this part now of the V versus i relationship and that is what it looks like. And you can work out the expression for the break point in this case and also what happens to this slope here and so on. And if you add one more branch like the first one like that then we have one more break point like that. So, this is the net V versus i relationship that we can obtain with this network. And we will see how we can use this entire network for wave shaping.

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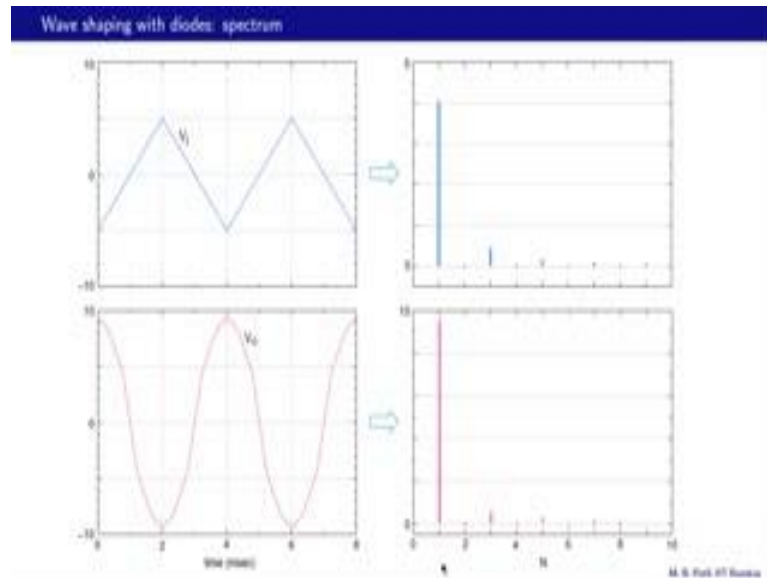


What we have done now is to place this entire diode network, which we saw in the last slide in the feedback path of this circuit. Now, notice that this circuit would otherwise be an inverting amplifier. And what we have done is to replace R 2 of that inverting amplifier by this network here. And now it should be image should be clear, why we took this voltage here as 0 volts, because V minus and V plus are equal, this node is at virtual ground, and therefore it makes sense to treat that as 0 volts. And as we have seen before the relationship between this voltage and the current is given by that curve. And what is this voltage in this circuit; it is a same as V o. So, now, we know the relationship between V o and i.

Our next job is to relate this i to input voltage V i and that is easy to do because this i is the same as this current. And since this is at 0 volts, this V i is simply 0 minus this voltage drops or minus R a times i. In other words, V i is simply a scaled version of i and this scaling factor is given by minus R A. So, using this fact, we can map this V o versus i relationship to the V o versus V i relationship and that is what is shown over here and of course, it has got reflected around the y-axis because of this minus sign.

So, now if we apply an input voltage, which is triangular in shape that is what we get as the output voltage. And as you can see, it is close to a sinusoid. And in the next slide, we will see how good it is how close it is to a sinusoid. Here is the sequel circuit file, you can run this simulation and check out these results.

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We will now look at the spectrum of V_i as well as V_o to figure out whether our output voltage is close to a sinusoid or not. Let us start with the input voltage first; here is the spectrum this is the fundamental frequency, let us say f this is $2f$, $3f$ and so on. And for a pure sinusoid, we would expect this to be nonzero, but all others to be 0 and obviously, this is not a sinusoid and therefore, we have nonzero components at these other frequencies. This even harmonics have got eliminated because of symmetry. So, what is a measure of closeness to a sinusoid, we want these harmonics to be small. So, in other words, this amplitude should be as small as possible as compared to this amplitude.

This is our output voltage, and of course visually we can definitely say that it is closer to a sinusoid than the input triangular waveform, but we want to look at the spectrum now and see that more quantitatively. So, here is a spectrum, and it should be clear when we compare these two figures that the relative magnitude of the third harmonic as compared to the fundamental has done down for sure and that indicates that our output voltage is closer to the sinusoid than the input voltage.

To summarize, we have seen precision half-wave and full-wave rectifier circuits, in which the op-amp works only in the linear region. Since, the op-amp is not allowed to enter the saturation region, these circuits are relatively fast. We have also seen how diodes can be used for wave shaping; and in particular, for converting a triangular input

to a sinusoidal output. In the next class, we will simulate the triangle to sign converter circuit. So, see you next time.