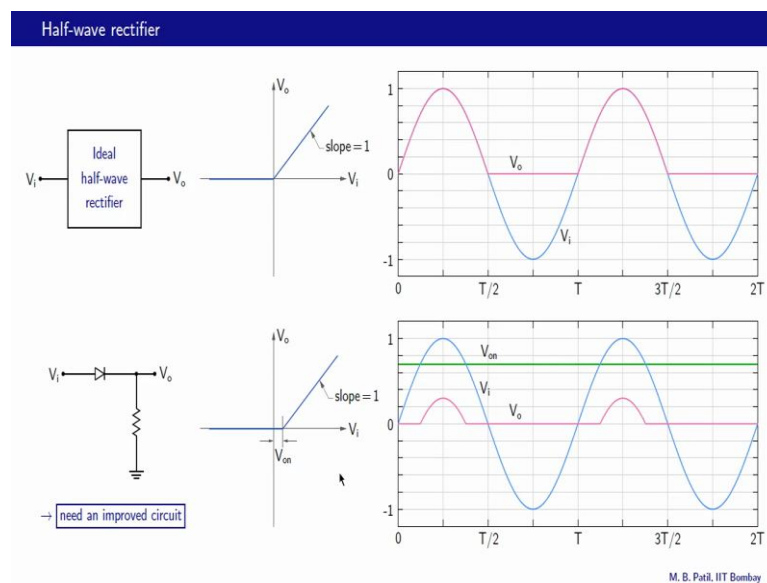


Basic Electronics
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Lecture - 46
Precision rectifiers

Welcome back to Basic Electronics. Earlier in this course we have seen diode circuits of various functions, such as peak detection, clipping, and clamping. We have seen that because of finite turn on voltage of a diode the waveforms for these circuits are not quite ideal. We will now look at a combination of a diode and op-amp for accurate peak detection. We will see how the circuit can be used for AM demodulation. So, let us begin.

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We will now discuss how op-amps can be used for the purpose of rectification along with diodes. Let us start with the half-wave rectifier, here is an ideal of a rectifier black box input V_i output V_o ; V_o on the output voltage to be 0 if V_i is negative and if V_i is positive if we want V_o to be equal to be V_i . It is a straight line going through the origin with a slope of 1. These are the time domain wave forms, that is V_i and V_o would be equal to V_i when v_i is positive and V_o is 0 if V_i is negative.

We have seen this diode circuit which was used for half-wave rectification, but this had this diode voltage drop V_{on} on here and therefore the V_o V_i relationship is not quite what

we want. And this can become an issue if our amplitude of the input voltage is not large enough. For example here; this is our input voltage this is our V on the voltage drop across the diode when it conducts. And now conduction is possible only if V_i exceed V_{on} ; that means up to this point no conduction is possible V_o is 0. And then the diodes starts conducting and then V_o is equal to V_i minus V_{on} .

So, clearly this V_o is not what we would like, and therefore we need an improved circuit.

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Half-wave precision rectifier

Consider two cases:

(i) D is conducting: The feedback loop is closed, and the circuit looks like (except for the diode drop) the buffer we have seen earlier.

Since the input current $i_- \approx 0$, $i_R = i_D$.

$$V_+ - V_- = \frac{V_{o1}}{A_V} = \frac{V_o + 0.7V}{A_V} \approx 0V \rightarrow V_o = V_- \approx V_+ = V_i$$

This situation arises only if $i_D > 0$ (since the diode can only conduct in the forward direction), i.e., $i_R > 0 \rightarrow V_o = i_R R > 0$, and therefore $V_i = V_o > 0V$.

Note: V_{on} does not appear in the graph.

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Here is an op-amp circuit and it works as half-wave precision rectifier. And we will see that the voltage drop V_{on} of the diode does not appear in the V_o versus V_i relationship for this circuit; we will figure out why. So, let us take two cases: one, D is conducting and when the diode is conducting we will replace that with the battery say 0.7 volts for a silicon diode. And in that case this feedback loop is closed, the op-amp operates in the linear region and the circuit looks very much like the op-amp buffer circuit that we have seen except for this voltage drop there.

Now, since the input current i_- is 0 this current i_R is equal to i_D , so the current pass is like that. And what is $V_+ - V_-$ then it is equal to V_{o1} divided by A_V the voltage gain of the op-amp which is a large number something like 100000 for the (Refer Time: 04:01) for 1 op-amp. What is V_{o1} ? Remember the diode is conducting so therefore V_{o1} is V_o plus this diode voltage drop which is say 0.7 volts. Therefore, V_o

plus minus V_{minus} is $V_{\text{o}} + 0.7$ divided by A_v . Now since A_v is such a large number this quantity is nearly 0 volts, and therefore V_{plus} and V_{minus} are nearly equal.

What is V_{o} now? V_{o} is the same as V_{minus} , and therefore V_{o} is nearly equal to V_{plus} which is this same as V_{i} . So, when the diode is conducting we have V_{o} equal to V_{i} . Now let us figure out when this situation happens; that is when does D conduct? This situation arises only if i_{D} is greater than 0, because that is the only way the diode can conduct it cannot conduct in the reverse direction. And therefore, since i_{D} and i_{R} are equal that is our current path i_{R} is also positive and therefore V_{o} which is r times i_{R} is positive.

So, this situation namely diode conducting happens if V_{o} is positive, and since V_{o} and V_{i} are equal that means V_{i} is also positive. So, in short if V_{i} is positive V_{o} is equal to V_{i} that is the straight line passing through the origin with the slope of 1. And the most important point to be noted is that V_{on} the diode drop does not appear in the graph. What happens to V_{on} ? It got divided by this very large voltage gain of the op-amp.

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Half-wave precision rectifier

(ii) D is not conducting $\rightarrow V_{\text{o}} = 0 \text{ V}$.

What about $V_{\text{o}1}$?

Since the op-amp is now in the open-loop configuration, a very small V_{i} is enough to drive it to saturation.

Note that Case (ii) occurs when $V_{\text{i}} < 0 \text{ V}$ (we have already looked at $V_{\text{i}} > 0$).
 Since $V_{\text{+}} - V_{\text{-}} = V_{\text{i}} - 0 = V_{\text{i}}$ is negative, $V_{\text{o}1}$ is driven to $-V_{\text{sat}}$.

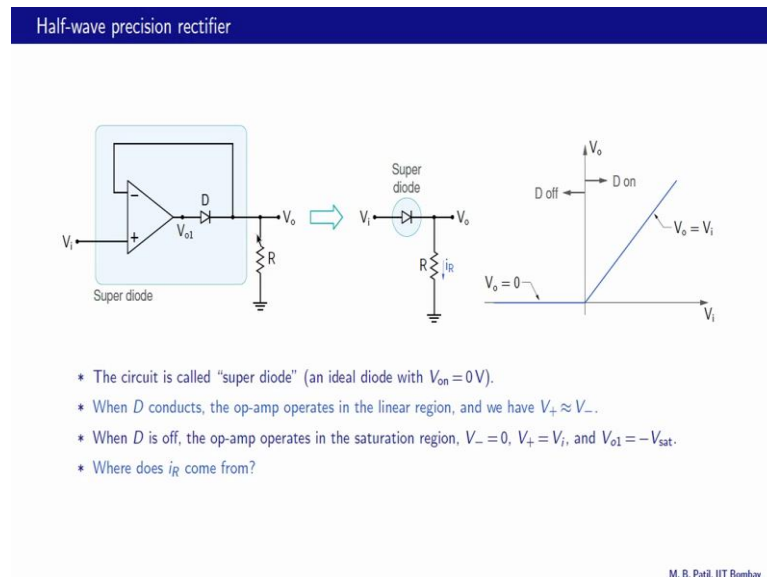
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Let us now consider the second case that is D not conducting. So, we replace D with an open circuit, and now there is no possibility of any current here because there is no current going in or out to the op-amp. So therefore, V_{o} is equal to 0. What about $V_{\text{o}1}$ this op-amp output? Since the op-amp is now in the open loop configuration there is no

feedback path because this loop is broken here. A very small V_i is enough to drive it to saturation.

Note that V_{minus} is the same as V_o which is 0 volts. So therefore, all it requires now to drive the op-amp in to saturation is the small value of V_i . And that V_i has to be negative because we have already consider the other case when V_i was positive, the last slide. That means, V_{plus} is negative V_{minus} is 0. So therefore, the op-amp is going to get driven to minus V_{sat} . And that is what V_o versus V_i would look like in this case: V_o is simply 0 when V_i is negative.

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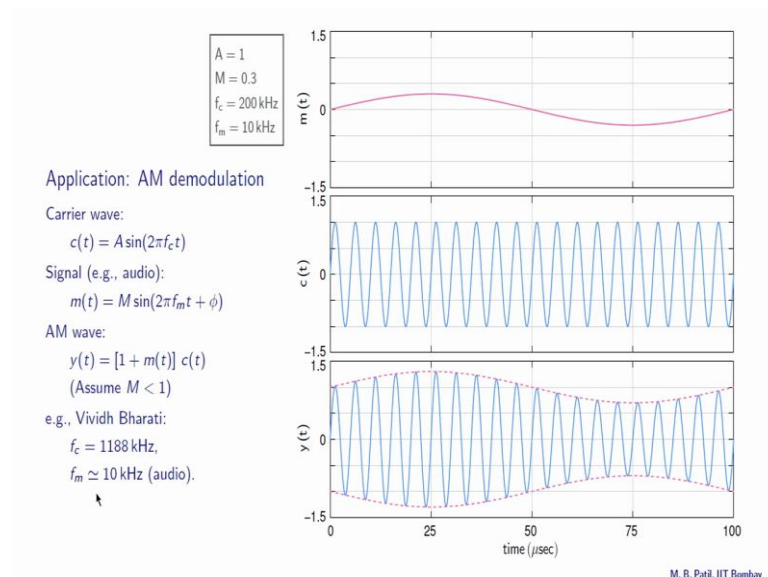


This plot summarizes the operation of the half-wave precision rectifier; when V_i is positive V_o is equal to V_i , the diode conducts, when V_i is negative V_o is 0 and the diode does not conduct. This circuit, this blocks here is called the super diode; why is it called super diode? Because it behaves like an ideal diode with V_{on} equal to 0 volts, and it is represented by this symbols sometimes. When the diode conducts the op-amp operates in the linear region and we have V_{plus} nearly equal to V_{minus} .

Just summarizing the important points that we have already looked at; when the diode is off the op-amp operates in the saturation region V_{minus} is 0 the same as V_o which is 0 when the diode does not conduct V_{plus} is v_i and therefore V_{o1} is equal to minus V_{sat} .

One question that arises is where does iR come from in this figure. Does it come from V_i ? The answer is no, it actually comes from the op-amp so it is supplied by the op-amp power supply; there is something we should remember.

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Let us now look at an application of the super diode or the half-wave precision rectifier. And that is AM demodulation; AM signals are amplitude modulated signals and let us see what those are first. There are three components in amplitude modulation: one is the carrier wave $c(t)$ which is a $\sin 2\pi f_c t$ and f_c is called the Carrier Frequency. Now this is a relatively high frequency and here is an example of $c(t)$. Then there is the signal itself for example, an audio signal and it could be of the form $m(t) = M \sin 2\pi f_m t + \phi$.

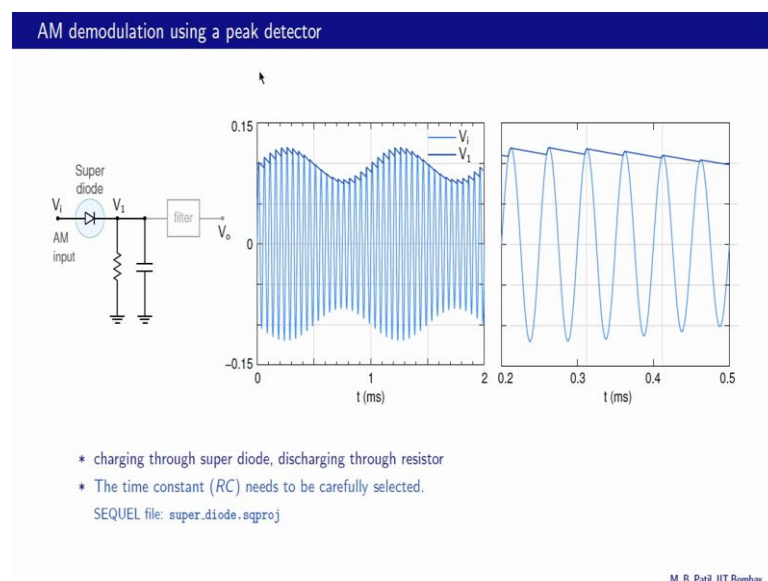
Now, this f_m is a frequency which is much smaller than the carrier frequency and here is an example of $m(t)$. Clearly this frequency is much smaller than this frequency. And in real life of course this modulating signal is not generally just a simple single sinusoid it could be much more complex. But, all the frequency components of the modulating signal are much slower than the carrier frequency. And from the carrier wave and the signal we derive the AM or amplitude modulated wave; $y(t) = [1 + m(t)] c(t)$. And we will assume that this capital M is less than 1.

So, here are the waveforms: we have $A = 1$ the amplitude of the carrier, $M = 0.3$ this number, $f_c = 200 \text{ kHz}$ the frequency of the carrier, $f_m = 10 \text{ kHz}$

the frequency of the signal. And clearly this f_m is much smaller than f_c . This is our y of t , and what do we notice? We notice that the frequency is the same as the carrier signal, but its amplitude goes on changing. And that dash line shows the amplitude of this y of t , and that is of course because we have this $1 + m \cos(\omega_m t)$ here as a pre factor in y of t .

Now, this is called the envelope because if we see carefully this signal waveform is enveloping the carrier in y of t . And the goal of AM demodulation is to detect this envelope which is the same as our signal. Now these numbers are representative in real life if we are talking about audio signals then the numbers can be somewhat different. For example, with the Vividh Bharati channel the carrier frequency is 1188 kilo hertz and f_m is the audio frequencies which can range say from few hertz to like 12 or 15 kilo hertz.

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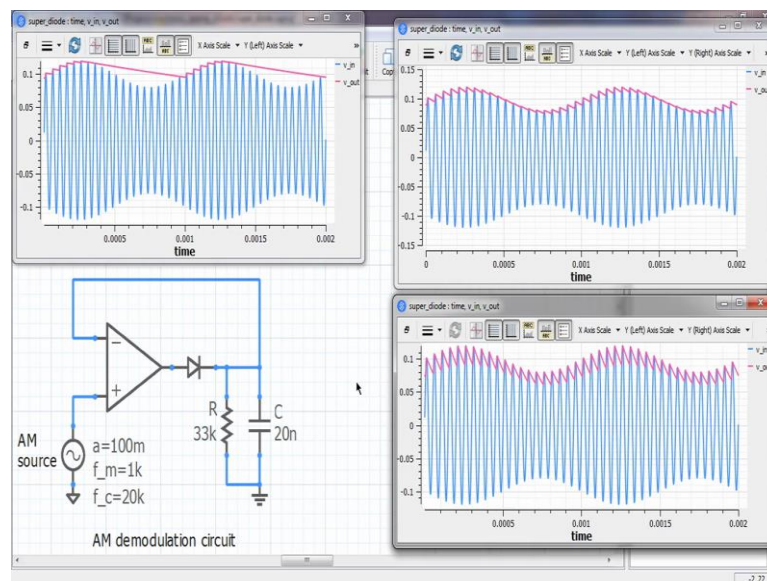


Here is a circuit using the super diode which can be used for demodulation of AM signals. It is essentially a peak detector and we have looked at this circuit earlier when we will talk about diodes. The only difference is that it has a super diode here with V on equal to 0 volts. So therefore, it can go up with small input voltages; for example here the input voltage is only 150 millivolts or less. The input voltage is shown by the light blue waveform that is our amplitude modulated signal, and the purpose of the circuit is to detect this envelope that is our signal.

When V_i is larger than V_1 the capacitor gets charged, otherwise it discharges through this resistor. So, the charging happens through the super diode and discharging through the resistor. And here is an expanded view of these waveforms which shows discharging and discharging process more clearly. So, here we have charging then discharging then charging then discharging and so on. And this V_1 is almost what we want, but not quite because it has got this little ripple riding on it. So, it is not this envelope that we are seeking, but the envelope with some ripple voltage on top of it.

And we of course, want to remove that ripple voltage; and that is done with this filter here which we are not shown in detail. So, the final output is the output of this filter which is indicated here by V_o . Now the time constant RC here, has to be very carefully selected and let us demonstrate that with this circuit file.

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Here are some simulation results with R equal to 33 k and C equal to 20 nanofarads and carrier frequency of 20 kilo hertz and the signal frequency of 1 kilo hertz, we get this result. And here the output is that we would like, this is the envelope which is detected as the output voltage and it has got small ripple riding on it which we can filter out. Now if we increase the capacitance from 20 nano to 100 nano then this is what we get and this definitely has a problem, because we are missing out on some peaks here. And definitely this output voltage is not a faithful reproduction of the signal voltage.

But if we make the capacitance too small; for example, this plot corresponds to c equal to 5 nano ohm and in this case the output does follow the envelope, but then the ripple voltage is a little too large which again is not desirable. So, that indicates that this RC time constant must be carefully selected, and that would depend on all of these parameters.

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Clipping and clamping

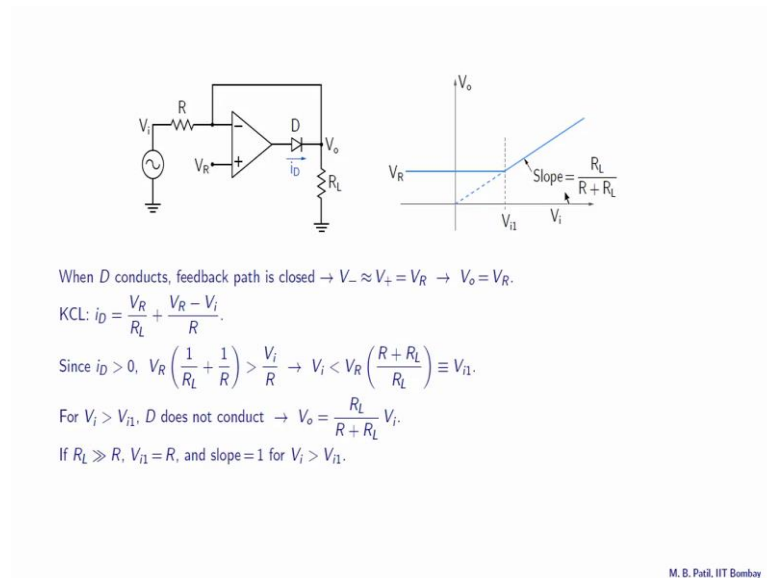
* What is the function provided by each circuit?
 * Verify with simulation (and in the lab).

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Here are some more circuits in which an op-amp is used to eliminate the voltage drop across the diode when it conducts that is V_D . So for these circuits we will also have the following questions in the subsequent slides. Question one: what is the function provided by each of these circuits? We will analyze the circuits and look at the functionality that each circuit provides. Second: we will verify that functionality with simulation. In addition of course, you are encouraged to go to your electronics lab look up these circuits and look at their function as well.

Although there are four circuits here, essentially we need to look at two different circuits. This one and this one and the other circuits operate in a very similar manner. For example, this circuit here is derived from the upper circuit simply by changing the direction of the diode; similarly, this circuit here is derived from this circuit by simply changing the direction of the diode.

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Here is our first circuit. We have an op-amp here with the non-inverting input connected to a reference voltage V_R . This reference voltage could be adjusted using a part which we have not shown in this figure. So, as far as V_R concerned this V_R is simply a constant. This is our input voltage and we will take an example of a sinusoidal voltage applied as V_i and this is the output voltage.

Let us see what this circuit is doing. Let us first consider the case where the diode d is conducting. And when D conducts their feedback path is closed this path here, and we can expect V_{-} to be then equal to V_{+} these two voltages and V_{+} of course is equal to V_R . So therefore, V_{-} is equal to V_R ; V_{-} is in fact the same as V_o , so therefore V_o is equal to V_R . So, that is the situation when the diode D conducts. Now when does that happen? To see that let us write the KCL equation at this node we have three currents here; one is i_D , so that i_D is equal to this current plus this current. This current is simply V_o by R_L and V_o is the same as V_R as we saw. So therefore, this current is v_r divided by R_L . What about this current? This current must be the same as this current here, because the input current for the op-amp is 0 and therefore we have V_R minus V_i divided by R . So, that is our KCL equation.

Now, the diode current i_D then only be positive, because the diode cannot conduct in the reverse direction. So therefore, this quantity must be positive. And what that means is V_R times 1 over R_L plus 1 over r must be greater than V_i by r . In other words V_i must

be less than V_R times R plus R_L divided by R_L . This factor is always greater than 1 and we will define this entire quantity as V_{i1} .

When V_i is less than V_{i1} the diode conducts and we have V_o equal to V_R which is a constant and that happens irrespective of V_i as long as V_i is less than V_{i1} . So, that is one situation that we have. And in the other case that is when V_i is greater than V_{i1} the diode does not conduct. And what do we have then? Then this current is 0 and we have V_i dividing between R and R_L . So, then V_o is given simply by voltage division V_o is then R_L divided by R plus R_L times V_i like that.

And here is the plot of V_o versus V_i ; this axis is V_o , this axis is V_i and this value here is V_{i1} . When V_i is less than V_{i1} ; that means, this region V_o is constant and equal to V_R like that. Otherwise V_o is given by R_L by R plus R_L times V_i which is the straight line passing through the origin this line with the slope equal to R_L divided by R plus R_L . So this circuit is essentially a clipper circuit. Let us now take a special case in which R_L is much larger than R , when that happens this factor becomes equal to 1; and our V_{i1} this boundary here becomes equal to V_R and the slope here becomes equal to 1.

To summarize we have looked at the super diode the combination of a diode and an op-amp which behaves like an ideal diode with a turn on voltage of 0 volts. We then looked at an interesting application of the super diode namely; AM demodulation. After that we have started looking at precision clipping and clamping circuits. We will continue this discussion in the next class, until then goodbye.