

Computational Electromagnetics and Applications
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Lecture No 14
Boundary Conditions

Welcome back we started with the Maxwell equation inside an anisotropic model we came to the point of deriving first step of the PML equations.

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$$\bar{\mu} \partial_t H_x = -\partial_y E_z$$

$$\begin{pmatrix} \mu_0 \\ \mu_0 \\ \epsilon_0 \end{pmatrix} \begin{pmatrix} 1/a & 0 & 0 \\ 0 & a & 0 \\ 0 & 0 & a \end{pmatrix} \partial_t \begin{pmatrix} H_x \\ H_y \\ E_z \end{pmatrix} = \begin{pmatrix} -\partial_y E_z \\ \partial_z E_x \\ \partial_x H_y - \partial_y H_x \end{pmatrix}$$

$$\mu_0 \cdot \frac{1}{a} \partial_t H_x = -\partial_y E_z$$

$$\mu_0 \cdot a \partial_t H_y = \partial_x E_z$$

$$\epsilon_0 a \partial_t E_z = \partial_x H_y - \partial_y H_x$$

Where we are now in the step so we have got basic certifications we are in the process of deriving step by step the 3 field equations from to curl equations so we have started with the permittivity model which is going to be an isotropic in X direction we have casted it on the Standard Maxwell equation terms so we are at the point of getting the simplified equations for all the three feel terms so let's not start with the first equation of H x.

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The image shows a whiteboard with handwritten mathematical equations. At the top, the equation is $\mu_0 \cdot \frac{1}{a} \partial_t H_x = -\partial_y E_z$. Below it, the same equation is written with a circled term: $\mu_0 \cdot \frac{1}{1 + \frac{\sigma_x}{j\omega\epsilon}} \partial_t H_x = -\partial_y E_z$, where the fraction $\frac{1}{1 + \frac{\sigma_x}{j\omega\epsilon}}$ is circled and labeled as $= K_x$. The next line is $\partial_t K_x = -\partial_y E_z$. Finally, the expression for K_x is given as $K_x = \frac{\mu_0}{1 + \frac{\sigma_x}{j\omega\epsilon}} H_x$. An NPTEL logo is visible in the bottom left corner.

So what we have got now is the term $\mu_0 \times \frac{1}{1 + \frac{\sigma_x}{j\omega\epsilon}}$ by a $\partial_t H_x$ that is equal to $-\partial_y E_z$. So I am going to plug in the value for which I have given in the earlier module which is going to be $1 + \frac{\sigma_x}{j\omega\epsilon}$ so let us put that in. It is going to be μ_0 multiplied by $\frac{1}{1 + \frac{\sigma_x}{j\omega\epsilon}}$ multiplied by $\partial_t H_x$ is equal to $-\partial_y E_z$.

So what I am going to do is I am going to substitute the value $\mu_0 H_x$ this one to be equal to the value called k_x . I'm using the term k_x because it is an arbitrary variable so I am going to use k_x because it corresponds to H_x . So I'm going to have $\partial_t k_x$ is equal to $-\partial_y E_z$. If I plug this value as k_x I'm going to get the equation like this word of course k_x itself is going to be equal to μ_0 divided by $1 + \frac{\sigma_x}{j\omega\epsilon}$ $\partial_t H_x$.

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The image shows a whiteboard with handwritten mathematical equations. The first equation is $k_x \left(1 + \frac{\sigma_x}{j\omega\epsilon}\right) = \mu_0 H_x$. The second equation is $k_x \left(\frac{j\omega\epsilon + \sigma_x}{j\omega\epsilon}\right) = \mu_0 H_x$, with an arrow pointing from the second equation to the first. The third equation is $j\omega\epsilon k_x + \sigma_x k_x = \mu_0 \epsilon j\omega H_x$. An NPTEL logo is visible in the bottom left corner.

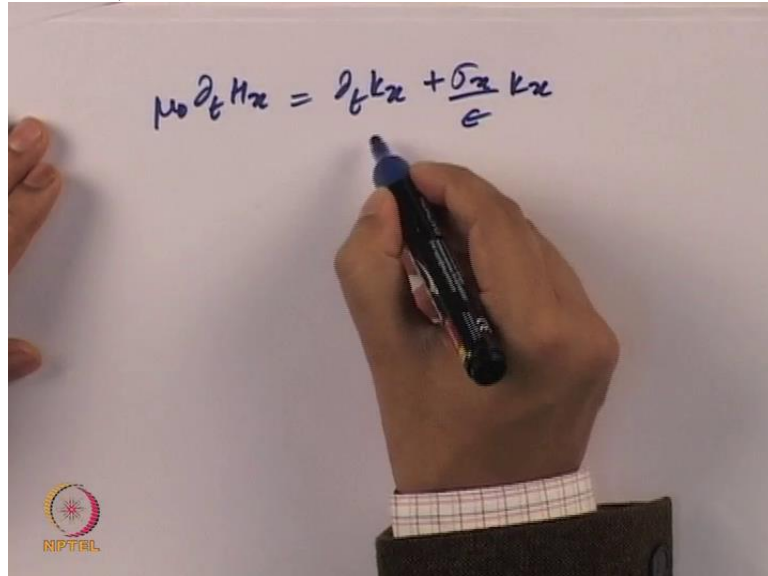
So let's go forward in simplifying this equation so what you will get is a value for H_X and k_x in a much simplified form so what we will get is k_x multiplied by $1 + \sigma_x$ multiplied by $j\omega \epsilon$ is equal to $\mu_0 H_x$. And now we can multiply this even further it is going to be equal to $K_x (j\omega \epsilon + \sigma_x)$ divided by $j\omega \epsilon$ equal to $\mu_0 H_x$. I am going to take the value $j\omega \epsilon$ on the other side so what I will get is $j\omega \epsilon K_x + \sigma_x k_x$ is equal to $\mu_0 \epsilon j\omega H_x$.

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The image shows a handwritten derivation on a chalkboard. It starts with the equation $k_x \left(1 + \frac{\sigma_x}{j\omega \epsilon}\right) = \mu_0 H_x$. This is then rearranged to $k_x \left(\frac{j\omega \epsilon + \sigma_x}{j\omega \epsilon}\right) = \mu_0 H_x$. A box on the right contains the substitution $j\omega = \frac{\partial}{\partial t}$. The next step is $j\omega \epsilon k_x + \sigma_x k_x = \mu_0 \epsilon j\omega H_x$. This is then written as $\epsilon \frac{\partial}{\partial t} k_x + \sigma_x k_x = \mu_0 \epsilon \frac{\partial}{\partial t} H_x$. Finally, the equation is divided by ϵ to get $\frac{\mu_0 \epsilon \frac{\partial}{\partial t} H_x}{\epsilon} = \frac{\epsilon \frac{\partial}{\partial t} k_x}{\epsilon} + \frac{\sigma_x k_x}{\epsilon}$.

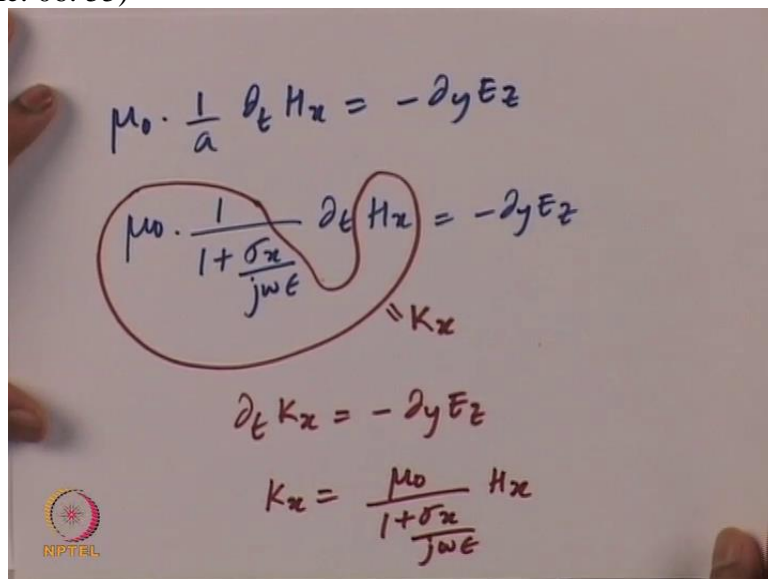
And now we can substitute the value $j\omega$ equal to $\frac{\partial}{\partial t}$ by partial derivative with respect to time this is in the frequency space and then we are going back to the time space this is the frequency domain we are going to the time domain so if I do that what I will get here is $\epsilon \frac{\partial}{\partial t} k_x + \sigma_x k_x$ is equal to $\mu_0 \epsilon \frac{\partial}{\partial t} H_x$. I am going to divide the entire equation by ϵ and I will get rid of the ϵ and I will get the denominator ϵ for this term and I am going to rearrange the term so that I get $\frac{\partial}{\partial t} H_x$ on the left hand side. So $\frac{\partial}{\partial t} H_x \mu_0$ divided by ϵ is equal to $\frac{\partial}{\partial t} k_x + \frac{\sigma_x k_x}{\epsilon}$. So here there is a ϵ , here there is a ϵ , so I am dividing it by an ϵ and I have k_x here. So get rid of this excellent get rid of the ϵ and this ϵ space.

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$$\mu_0 \partial_t H_x = \partial_t k_x + \frac{\sigma_x}{\epsilon} k_x$$

So what we will get is a simplified equation for $\partial_t H_x$ which is given by $\partial_t H_x \mu_0$ equal to $\partial_t k_x$ plus σ_x by ϵ k_x .

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$$\mu_0 \cdot \frac{1}{a} \partial_t H_x = -\partial_y E_z$$
$$\mu_0 \cdot \frac{1}{1 + \frac{\sigma_x}{j\omega\epsilon}} \partial_t H_x = -\partial_y E_z$$

$= k_x$

$$\partial_t k_x = -\partial_y E_z$$
$$k_x = \frac{\mu_0}{1 + \frac{\sigma_x}{j\omega\epsilon}} H_x$$

And of course we know that what is the value for $\partial_t k_x$ because we got that from our earlier equation. Which is nothing but minus $\partial_y E_z$.

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$$\mu_0 \partial_t H_x = \partial_t k_x + \frac{\sigma_x k_x}{\epsilon}$$
$$\mu_0 \partial_t H_x = -\partial_y E_z + \frac{\sigma_x k_x}{\epsilon}$$

So I am going to substitute that value here size equal to minus $\partial_y E_z$ plus $\sigma_x k_x$ by ϵ . And this $\mu_0 \partial_t H_x$. This is going to be one of the equation ;

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$$\mu_0 \cdot \frac{1}{a} \partial_t H_x = -\partial_y E_z$$
$$\mu_0 \cdot \frac{1}{1 + \frac{\sigma_x}{j\omega\epsilon}} \partial_t H_x = -\partial_y E_z = k_x$$
$$\partial_t k_x = -\partial_y E_z$$
$$k_x = \frac{\mu_0}{a} H_x$$

This is going to be one of the equation.

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$$\mu_0 \cdot \frac{1}{a} \frac{\partial_t H_x}{\partial_t} = -\partial_y E_z$$

$$\mu_0 \cdot a \frac{\partial_t H_y}{\partial_t} = \partial_x E_z$$

$$\epsilon_0 a \frac{\partial_t E_z}{\partial_t} = \partial_x H_y - \partial_y H_x$$

So let's write down the second equation which is here;

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$$\mu_0 \cdot a \cdot \frac{\partial_t H_y}{\partial_t} = \partial_x E_z$$

$$\mu_0 \left(1 + \frac{\sigma_x}{j \omega \epsilon} \right) \frac{\partial_t H_y}{\partial_t} = \partial_x E_z$$

$$\mu_0 \frac{\partial_t H_y}{\partial_t} + \frac{\sigma_x}{j \omega \epsilon} \frac{\partial_t H_y}{\partial_t} = \partial_x E_z$$

$j \omega = \frac{\partial_t}{\partial_t}$

$$\mu_0 \frac{\partial_t H_y}{\partial_t} + \frac{\sigma_x}{j \omega \epsilon} j \omega H_y = \partial_x E_z$$

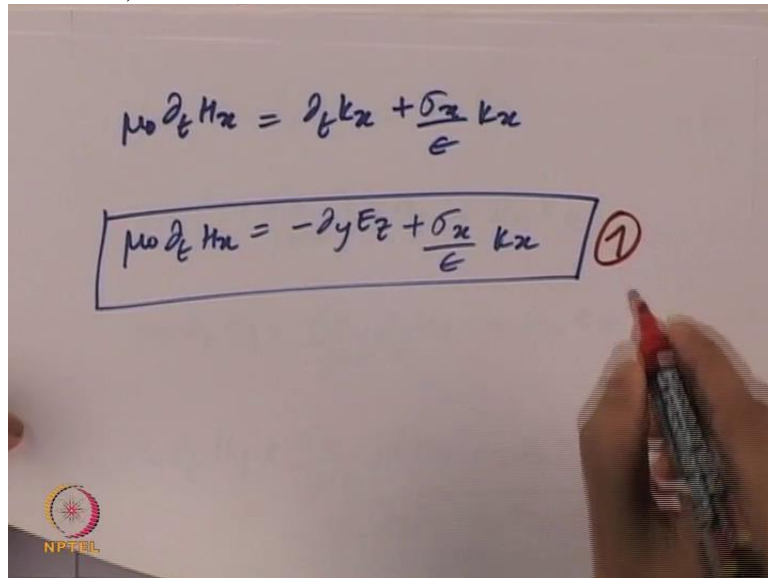
$$\boxed{\mu_0 \frac{\partial_t H_y}{\partial_t} = \partial_x E_z - \frac{\sigma_x}{\epsilon} H_y}$$

So let's write it down μ_0 multiplied by a $\frac{\partial_t H_y}{\partial_t}$ equal to $\partial_x E_z$. Again the value is going to be μ_0 multiplied by $\left(1 + \frac{\sigma_x}{j \omega \epsilon} \right) \frac{\partial_t H_y}{\partial_t}$ equal to $\partial_x E_z$. So now we are going to expand this term what we will get is $\mu_0 \frac{\partial_t H_y}{\partial_t} + \frac{\sigma_x}{j \omega \epsilon} \frac{\partial_t H_y}{\partial_t}$ is equal to $\partial_x E_z$. So I am going to substitute the value $j \omega$ equal to $\frac{\partial_t}{\partial_t}$ and I am going to do it in a different way. Instead of substituting $j \omega$ equal to $\frac{\partial_t}{\partial_t}$ I am going to substitute $\frac{\partial_t}{\partial_t}$ equal to $j \omega$. So this is what I am going to do here. So I will get $\mu_0 \frac{\partial_t H_y}{\partial_t} + \frac{\sigma_x}{j \omega \epsilon} j \omega H_y$ equal to $\partial_x E_z$. I can cancel $j \omega$ on both sides on the numerator and denominator. What I will get is the term update equation for the H_y term which is given by $\mu_0 \frac{\partial_t H_y}{\partial_t} = \partial_x E_z - \frac{\sigma_x}{\epsilon} H_y$ this will go on the right hand side and become minus

sigma x divided by Epsilon H y. So I am going to put them in the bracket. So this is going to be my third equation.

So the first equation is going to be the one for H x which we have just derived.

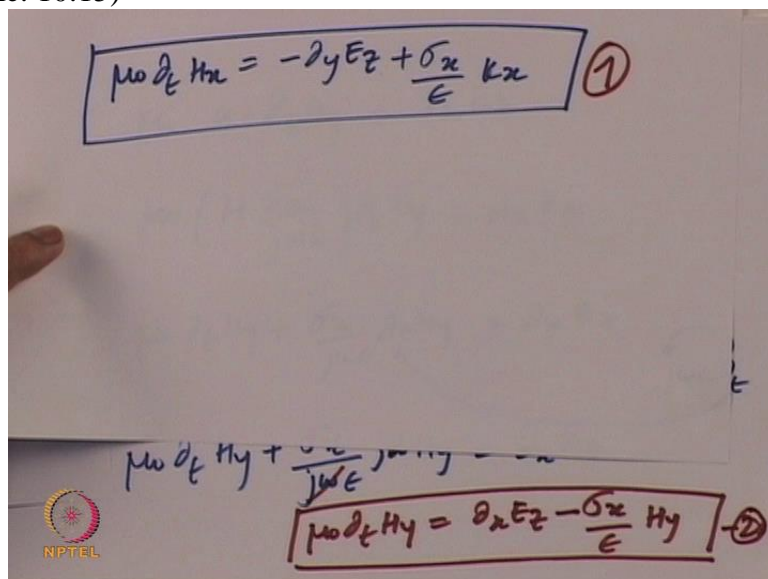
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A hand-drawn equation on a whiteboard. The equation is $\mu_0 \partial_t H_x = \partial_y k_x + \frac{\sigma_x}{\epsilon} k_x$. Below it, the same equation is boxed and labeled with a circled 1: $\mu_0 \partial_t H_x = -\partial_y E_z + \frac{\sigma_x}{\epsilon} k_x$ (1). A hand holding a red marker is visible on the right side of the board.

So this is going to be our first equation.

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A hand-drawn equation on a whiteboard. The equation is $\mu_0 \partial_t H_y = \partial_x E_z - \frac{\sigma_x}{\epsilon} H_y$. The equation is boxed and labeled with a circled 2: (2). A hand is visible on the left side of the board.

So this is going to be our second equation. And we are now going to look for the third field equation which is the E z.

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$$\vec{\mu} \partial_t \vec{H} = -2y E_z$$

$$\begin{pmatrix} \mu_0 \\ \mu_0 \\ \mu_0 \end{pmatrix} \begin{pmatrix} 1/a & 0 & 0 \\ 0 & a & 0 \\ 0 & 0 & a \end{pmatrix} \partial_t \begin{pmatrix} H_x \\ H_y \\ E_z \end{pmatrix} = \begin{pmatrix} -2y E_z \\ 2x E_z \\ 2x H_y - 2y H_x \end{pmatrix}$$

$$\mu_0 \cdot \frac{1}{a} \partial_t H_x = -2y E_z$$

$$\mu_0 \cdot a \partial_t H_y = 2x E_z$$

$$\mu_0 \cdot a \partial_t E_z = 2x H_y - 2y H_x$$

So we are now starting with the third equation here. So we will derive the equation for E z as well.

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$$\epsilon_0 a \partial_t E_z = 2x H_y - 2y H_x$$

$$\epsilon_0 \left(1 + \frac{\sigma_x}{j\omega\epsilon} \right) \partial_t E_z = \dots$$

$$\epsilon_0 \partial_t E_z + \frac{\sigma_x}{j\omega\epsilon} E_z = \dots$$

$$\boxed{\epsilon_0 \partial_t E_z = 2x H_y - 2y H_x - \frac{\sigma_x}{\epsilon} E_z} \quad (3)$$

So what we have got is Epsilon 0 a Doe t E z is equal to Doe x H y minus Doe y H x. I am going to substitute the value for a Epsilon 0 (i plus sigma x divided by j omega Epsilon) multiplied by Doe t E z equal to the right hand side. I am expanding it so you get Epsilon 0 Doe t E z plus sigma x j omega Epsilon. And I am going to do the same thing what I did for the H y term. I am going to write dt as J omega E z. That is going to be equal to my right hand side. And I wanted to make sure that you know what I have done here. So I have substituted the value for dt as j omega.

And now I can get rid of these two things and write that in a simplified form by taking it on the right hand side. And hence we will have the third equation that we are looking for Epsilon

dt E z is equal to Doe x Hy minus Doe y H x. And in the right hand side this term will come to the right hand side. We will have minus sigma x divided by Epsilon E z. This is going to be our third equation.

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$$\mu_0 \cdot \frac{1}{a} \partial_t H_x = -\partial_y E_z$$

$$\mu_0 \cdot \frac{1}{1 + \frac{\sigma_x}{j\omega\epsilon}} \partial_t H_x = -\partial_y E_z = K_x$$

$$\partial_t K_x = -\partial_y E_z \quad (4)$$

$$K_x = \frac{\mu_0}{1 + \frac{\sigma_x}{j\omega\epsilon}} H_x$$

Of course there is a fourth equation that we will have which is going to be given by this equation for K x. So I am going to write down all the four equations one by one so that you can have a quick view of all of them in one sheet.

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$$\mu_0 \partial_t H_x = -\partial_y E_z + \frac{\sigma_x}{\epsilon} K_x$$

$$\mu_0 \partial_t H_y = \partial_x E_z - \frac{\sigma_x}{\epsilon} H_y$$

$$\epsilon_0 \partial_t E_z = \partial_x H_y - \partial_y H_x - \frac{\sigma_x}{\epsilon} E_z$$

$$\partial_t K_x = -\partial_y E_z$$

So the first equation is going to be for H x, so it is going to be Mu 0 Doe t H x equal to minus dy E z plus sigma x Epsilon K x. So the second equation is for H y so it is going to be Mu 0 Doe t H y is equal to Doe x Ez minus sigma x Epsilon H y. And the third equation is going to be epsilon 0 Doe t E z is equal to Doe x H y minus Doe y H x minus Sigma x by Epsilon E z.

And the fourth equation which is the equation that we are going to use for k_x is going to be given by the term so the fourth equation is going to be $\partial_t k_x$ is equal to minus $\partial_y E_z$. So as you can see there is going to be few remarks one has to give about this equation.

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$$\begin{aligned} \mu_0 \partial_t H_x &= -\partial_y E_z + \frac{\sigma_x}{\epsilon} k_x \\ \mu_0 \partial_t H_y &= \partial_x E_z - \frac{\sigma_x}{\epsilon} H_y \\ \epsilon_0 \partial_t E_z &= \partial_x H_y - \partial_y H_x - \frac{\sigma_x}{\epsilon} E_z \\ \partial_t k_x &= -\partial_y E_z \end{aligned}$$

The equations that are marked within the green line is nothing but a standard Maxwell equation for 2D transverse magnetic mode.

The terms that are within the blue colour or the loss terms that we are going to consider inside the PML and of course the loss terms are going to come because of the σ_x value. So there is a fourth term an auxiliary equation that we have to consider because we are going to have the loss terms. And these loss terms are to be updated as well. So there is going to be a fourth equation and its $k_x \neq 0$ because we are considering an x oriented PML.

So with that being said what will be the analogy or what will be the counter part of the x PML when we consider the Y PML so when we consider the Y PML you will have a very similar equation and I am going to write it down so we don't need to go step by step deriving it one more time but the logic is very similar you can drive it by yourself but I am going to explain the set of equations.

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$$\mu_0 \partial_t H_x = -\partial_y E_z - \frac{\sigma_y}{\epsilon} H_x$$

$$\mu_0 \partial_t H_y = \partial_x E_z + \frac{\sigma_y}{\epsilon} K_y$$

$$\epsilon_0 \partial_t E_z = \partial_x H_y - \partial_y H_x - \frac{\sigma_y}{\epsilon} E_z$$

$$\partial_t K_y = \partial_x E_z$$

So what we will have is $\mu_0 \partial_t H_x$ equal to $\partial_y E_z$ minus σ_y divided by ϵ H_x . And the second equation is going to be $\mu_0 \partial_t H_y$ is equal to $\partial_x E_z$ and we are going to have a plus σ_y divided by ϵ K_y . And the third equation is going to be $\epsilon_0 \partial_t E_z$ is equal to $\partial_x H_y$ minus $\partial_y H_x$ minus σ_y divided by ϵ E_z . And the fourth equation is going to be because of the K_y so it is going to be $\partial_t K_y$ is equal to $\partial_x E_z$. So if you compare these two equations side by side there is a lot of similarities that you can see

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$$\mu_0 \partial_t H_x = -\partial_y E_z + \frac{\sigma_x}{\epsilon} K_x$$

$$\mu_0 \partial_t H_y = \partial_x E_z - \frac{\sigma_x}{\epsilon} H_y$$

$$\epsilon_0 \partial_t E_z = \partial_x H_y - \partial_y H_x - \frac{\sigma_x}{\epsilon} E_z$$

$$\mu_0 \partial_t H_x = -\partial_y E_z - \frac{\sigma_y}{\epsilon} H_x$$

$$\mu_0 \partial_t H_y = \partial_x E_z + \frac{\sigma_y}{\epsilon} K_y$$

$$\epsilon_0 \partial_t E_z = \partial_x H_y - \partial_y H_x - \frac{\sigma_y}{\epsilon} E_z$$

Let us look at them one by one. So what I have go in the first three equations here you see that the plus sign is going to be there for loss term. Whenever the PML is oriented in that particular direction when we are considering a x oriented PML the plus sign is going to be on

the H_x term. When we are considering the y oriented PML there will be a plus sign for the loss term for y oriented PML on H_y .

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$$\epsilon_0 \partial_t E_z = \partial_x H_y - \partial_y H_x - \frac{\sigma_x}{\epsilon} E_z$$

$$\partial_t K_x = -\partial_y E_z$$

$$\mu_0 \partial_t H_x = -\partial_y E_z - \frac{\sigma_x}{\epsilon} K_x$$

$$\mu_0 \partial_t H_y = \partial_x E_z + \frac{\sigma_y}{\epsilon} K_y$$

$$\epsilon_0 \partial_t E_z = \partial_x H_y - \partial_y H_x - \frac{\sigma_y}{\epsilon} E_z$$

$$\partial_t K_y = \partial_x E_z$$

Similarly the K_x term will be there for x oriented PML whereas K_y term is going to be there for a y oriented PML. And the Loss terms are going to be very symmetric since there are not going to be any variations in the z direction E_z direction will be very symmetric. Of course in the case of y oriented PML we will have σ_y and in the x oriented PML we will have σ_x .

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$$\mu_0 \partial_t H_x = -\partial_y E_z + \frac{\sigma_x}{\epsilon} K_x$$

$$\mu_0 \partial_t H_y = \partial_x E_z - \frac{\sigma_x}{\epsilon} H_y$$

$$\epsilon_0 \partial_t E_z = \partial_x H_y - \partial_y H_x - \frac{\sigma_x}{\epsilon} E_z$$

$$\partial_t K_x = -\partial_y E_z$$

So this is going to be the structure and also you will have a dt k_y expression which is going to be the exactly same flux that we are computing the same field the curl term that we are computing that is going to be sitting here. Similarly the dt k_x what you see is the field term

that we are computing is going to be the same as the field term that we will compute for a standard Maxwell equation without PML for H x. So these two terms are the same
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$$\mu_0 \partial_t H_x = -\partial_y E_z - \frac{\sigma_y}{\epsilon} H_x$$

$$\mu_0 \partial_t H_y = \partial_x E_z + \frac{\sigma_y}{\epsilon} K_y$$

$$\epsilon_0 \partial_t E_z = \partial_x H_y - \partial_y H_x - \frac{\sigma_y}{\epsilon} E_z$$

$$\partial_t K_y = \partial_x E_z$$

Similarly these two terms are the same both are the analogies that we have to put in place. And now we can see how we can combine this to be ml in a single set of equation that will have regardless of which orientation we are considering and that can be done in a very simple manner so what we are going to do is we are going to write the standard Maxwell equation as we have returned and we are going to add the Sigma x divided by Epsilon, Sigma x divided by Epsilon, Sigma x divided by Epsilon in such a manner that will be for the x oriented PML. And we will also have Sigma y divided by Epsilon and Sigma y divided by Epsilon and Sigma y divided by Epsilon for those terms that that are going to come so we are going to combine them in a very simple manner and I am going to write the equation directly then you can check it for yourself at a later stage.

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$$\begin{aligned} \mu_0 \partial_t H_x &= -\partial_y E_z + \frac{\sigma_x}{\epsilon} K_x \\ \mu_0 \partial_t H_y &= \partial_x E_z + \frac{\sigma_y}{\epsilon} K_y \\ \epsilon_0 \partial_t E_z &= \partial_x H_y - \partial_y H_x - \frac{\sigma_x}{\epsilon} E_z - \frac{\sigma_y}{\epsilon} E_z \\ \partial_t K_x &= -\partial_y E_z \\ \partial_t K_y &= \partial_x E_z \end{aligned}$$

So what he will have here is $\mu_0 \partial_t H_x$, $\mu_0 \partial_t H_y$, $\epsilon_0 \partial_t E_z$ and we will have $\partial_t K_x$, $\partial_t K_y$. $\partial_t K_y$ and $\partial_t K_x$ are very straightforward they are the fields that come from the Maxwell equation itself so we can write them down directly it is going to be minus $\partial_y E_z$, $\partial_x E_z$. And the standard fluxes are minus $\partial_y E_z$, $\partial_x E_z$, $\partial_x H_y$ minus $\partial_y H_x$. So these are the loss terms and now I am going to add flux terms as I said.

So it's going to be plus $\sigma_x K_x$ divided by ϵ for the x oriented PML. And similarly it's going to be plus σ_y divided by ϵ K_y for the y oriented PML and we are going to have both the loss terms for σ_x and σ_y so its going to be σ_x divided by ϵ E_z minus σ_y divided by ϵ E_z . And we are going to have the counterpart terms which are the H_x and H_y terms.

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$$\begin{aligned} \mu_0 \partial_t H_x &= -\partial_y E_z + \frac{\sigma_x}{\epsilon} K_x \\ \mu_0 \partial_t H_y &= \partial_x E_z - \frac{\sigma_x}{\epsilon} H_y \\ \epsilon_0 \partial_t E_z &= \partial_x H_y - \partial_y H_x - \frac{\sigma_x}{\epsilon} E_z \\ \partial_t K_x &= -\partial_y E_z \end{aligned}$$

Like we have got here this is an x oriented PML we will have σ_x divided by ϵ H_y

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Handwritten equations on a whiteboard:

$$\nabla \cdot \mathbf{H} = -\sigma_y E_z + \frac{\sigma_x}{\epsilon} K_x$$

$$\nabla \cdot \mathbf{E} = \sigma_x E_z + \frac{\sigma_y}{\epsilon} K_y - \frac{\sigma_x}{\epsilon} H_y$$

$$\epsilon_0 \partial_t E_z = \partial_y H_x - \frac{\sigma_x}{\epsilon} E_z - \frac{\sigma_y}{\epsilon} E_z$$

$$\partial_t K_x$$

$$\partial_t K_y$$

The NPTEL logo is visible in the bottom left corner.

So I am going to write it down here, so its going to minus sigma x divided by epsilon H y.

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Handwritten equations on a whiteboard:

$$\mu_0 \partial_t H_x = -\sigma_y E_z - \frac{\sigma_y}{\epsilon} H_x$$

$$\mu_0 \partial_t H_y = \sigma_x E_z + \frac{\sigma_y}{\epsilon} K_y$$

$$\epsilon_0 \partial_t E_z = \partial_x H_y - \partial_y H_x - \frac{\sigma_y}{\epsilon} E_z$$

$$\partial_t K_y = \partial_x E_z$$

The NPTEL logo is visible in the bottom left corner.

Similarly for the y oriented PML we will have minus sigma y divided by epsilon h x that is going to be minus sigma y divided by epsilon H.

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$$\begin{aligned} \mu_0 d_t H_x &= -d_y E_z + \frac{\sigma_x}{\epsilon} K_x - \frac{\sigma_y}{\epsilon} H_x \\ \mu_0 d_t H_y &= d_x E_z + \frac{\sigma_y}{\epsilon} K_y - \frac{\sigma_x}{\epsilon} H_y \\ \epsilon_0 d_t E_z &= d_x H_y - d_y H_x - \frac{\sigma_x}{\epsilon} E_z - \frac{\sigma_y}{\epsilon} E_z \\ d_t K_x &= -d_y E_z \\ d_t K_y &= d_x E_z \end{aligned}$$

Update
Time-derivatives

Uniaxial
x & y pml
UPML

So that's it and we have got now generalized equation for both the X and Y oriented uniaxial anisotropic PML. I have written specifically the equation terms in different colours so the blue colour terms are the update terms with time derivatives, the red terms are the standard Maxwell equation except for these two terms, they are coming because of the PML X and Y oriented PML, and the green ones are the Loss terms that are coming because of the uniaxial PML. So X and Y PML, else normally we also called them as uniaxial PML but one has to be careful we are having too many abbreviations here. UPML means uniaxial PML perfectly match there.

So this is going to be our starting point for us to model the PML using finite difference method and we are going to do that in Matlab environment and we are going to take the test case where we will have a rectangular domain we are going to truncate this domain using UPML and obviously there are certain things which I have not mentioned about the PML itself that we will see when we looked at numerical simulation and we are going to simulate a point source which is sinusoidal in nature and we are going to see how this point source is going to come and impinge on a scatterer which is a model as a perfect electric conductor and we'll see how the scattering gets reflected in all directions and how these X and Y oriented PML is going to absorb those incoming radiation so this is going to be a modelling exercise we will do in the next module.