# **Power Electronics**

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#### **Lecture - 26**

In my last class we discussed the operation of boost converter. We found that for a given value of D and the input voltage  $V_{DC}$ , output voltage is higher if the current is discontinuous. If the inductor current is discontinuous for a given value of D, output voltage is higher than if the current were to be discontinuous. If it is continuous, output voltage is  $V_{DC}$  divided by 1 minus D. Now, if it is discontinuous, now is going to be function of beta. We found that this value is the new value. The output voltage when the current is discontinuous is higher than the current rate to be continuous and second point that we discussed was the use of buck as well as a boost converter, the speed control of DC machine.

We found that both speed control, 0 to rated or the operation in the first quadrant and the regenerative braking - feeding energy back to the source is possible by using these 2 converters; buck as well as boost converter. So, 2 quadrant operation of the DC machine is possible just by using a buck and boost converter.

Recall, in the line commutated converter,  $\frac{2 \text{ quadrant}}{2}$ , using a using 2 quadrant converter we had to interchange the armature terminal. We interchanged the armature terminals for  $i_A$  to reverse, whereas, using a DC to DC converter, buck as well as boost, I do not need to interchange the armature terminals. Having studied buck and boost, there has to be buck and boost converter, buck - boost converter, what is known as a buck - boost converter which is a cascade connection of a buck converter and a boost converter.

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So, here is a buck, buck - boost converter; switch S, inductor, diode and this is the output stage. Similar to buck converter, close S. I am storing the energy in the inductor. See, this sort of, this feature is similar to a buck converter and this is some sort of a boost converter … and stored energy, you pass it through the load, using through D. Hence the name, buck - boost converter. How does it operate? I close S for DT duration where D is a duty cycle, voltage across the inductor is the supply voltage itself, diode cannot conduct.



So therefore, at the output stage, capacitor supplies power. See now, we are all most, this is a boost converter topology, capacitor supplying power. We never had this sort of situation in buck converter, buck converter, whereas, I have a switch in the main path of the flow similar to buck converter. I will open S after some time. So, stored energy in the inductor is transferred to the load and diode starts conducting, this is the circuit.

So, KVL gives for this loop, taking the resisting into account, this is the equation that I will get; R into  $i_L$  plus L di divided dT into  $V_{DC}$  and KCL at this node is  $i_C$ , the capacitor current is equal to the load current. So, capacitor is discharging here and similarly here,  $i_L$  is equal to  $i_C$  plus  $i_0$ .  $i_L$  is equal to C dV<sub>0</sub> by dt plus V<sub>0</sub> by R and the circuit equation is L divided by dt plus R into  $i_L$ plus  $V_0$  is equal 0, plus  $V_0$  is equal to 0. Voltage across the inductor is minus  $V_0$  now, whereas here, voltage across inductor is  $V_{DC}$ .

By the way, what is the polarity of  $V_0$ ? What is the polarity of  $V_0$ ? If you see in this circuit, I have shown the direction in this way because when I open the switch current starts flowing in this direction. So, this terminal is positive, this is negative, this is negative. But then for the sources, this line is a reference point. So, I cannot have 2 reference points in 1 circuit, remember, you cannot have 2 reference points in 1 circuit. If I am taking the reference as a negative DC bus, it is a reference point for to measure the voltages at other point.

So, voltage applied to the load is negative, negative. It is minus  $V_0$  that is appearing across the load. If I see this waveform in the oscilloscope with this as the ground, this is plus  $V_{DC}$ , whereas, if I touch this, it is minus  $V_0$ , minus  $V_0$ , is minus  $V_0$ .

So, let us find out transfer function by solving this equation. So, this is the voltage equation; r into iL plus L di by dt plus  $V_{DC}$  and when I open the switch, this is the KVL. So, if I find out average values of this equation, here I need to integrate from 0 to dt and this equation, I need to integrate from dt to T and if I add, see, r i<sub>L</sub> is there, L di by dt is there,  $V_{DC}$  is present from 0 to DT, whereas,  $V_0$  is present from DT to T.

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$$
A_{V_{1}} \text{ values of } v_{n} \& \ i_{i} \text{ are } V_{n} \& \ i_{i}
$$
\n
$$
A_{V_{2}} \text{ values of } v_{n} \& \ i_{i} \text{ are } V_{n} \& \ i_{i}
$$
\n
$$
r i_{i} + i \left(\frac{di_{i}}{dt}\right)_{av} + \frac{1}{T} \int_{0}^{T} V_{n} dt = DV_{oc}
$$
\n
$$
C\left(\frac{dV_{n}}{dt}\right)_{av} + \frac{V_{n}}{R} = \frac{1}{T} \int_{0}^{T} i_{i} dt
$$
\n
$$
At \text{ steady state} \left(\frac{di_{i}}{dt}\right)_{av} \& \left(\frac{dv_{n}}{dt}\right)_{av} = 0
$$
\n
$$
r i_{i} + (1 - D)V_{n} = DV_{oc}
$$
\n
$$
\frac{V_{n}}{R} = i_{i} (1 - D)
$$

So, I will get an equation something like this; r into  $i<sub>L</sub>$  L di by dt average,  $V_0$  is there only from dt to T and  $V_{DC}$  is there from 0 to dt. So, this is the average, this is the equation giving the average values. Similarly, if I find out the average values here,  $dV_0 C dV_0$  is there in both the equations,  $V_0$  by R is there in both the equations and  $i_L$ . So, average of this plus average of this should be equal to or the average value of  $i<sub>L</sub>$  from DT to T. So, here is it, dt to T. At steady state, the di by dt average should be 0. Current should start current at  $T$  is equal to 0 should be equal to current at T is equal to T and that is only then I am saying, circuit has attained a steady state.

Similar is true for the output voltage  $V_0$ , voltage ripple should remain constant over a cycle. So, this term is 0, this term is 0, so therefore, r into  $i_L$  plus 1 minus D into  $V_0$  is equal to  $DV_{DC}$  and this is the equation giving the load current in terms of the inductor current,  $V_0$  by R is the average load current.

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$$
r \frac{V_n}{R(1-D)} + (1-D)V_n = DV_{\infty}
$$
  
\n∴  $V_n = \frac{V_{\infty}D(1-D)}{\frac{r}{R} + (1-D)^2}$   
\n∴  $V_n = \frac{V_{\infty}D(1-D)}{\frac{r}{R} + (1-D)^2}$   
\n $I_t = \frac{V_{\infty}D}{r + R(1-D)^2}$   
\nif  $r \to 0$   $V_n = V_{\infty} \frac{D}{(1-D)}$   
\n $I_t = V_{\infty} \frac{D}{R(1-D)^2}$ 

So, if solving this and then substitute it for  $i_L$ , substituting for  $i_L$  in this equation using this values, I get this equation. So,  $V_0$  in terms of  $V_{DC}$  and the internal resistance of the inductor is given by this and  $i<sub>L</sub>$  is this equation. So, if R tends to 0, if I consider inductor to be ideal, I will get a voltage equation which is given by  $V_0$  is equal to  $V_{DC}$  divided by 1 minus D, 1 minus D and  $i_L$  is equal to  $V_{DC}$  divided by R into 1 minus D squared into D.

This equation can also be solved by equating the average voltage across the inductor, what we did for buck or the boost converter. So, if I know voltage across the inductor from 0 to DT from DT to T, I will equate it and I will get transfer function. It is very simple. I do not need to write, I do not need to take the value of R into account.

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So, here is the equation -  $V_{DC}$  into T, voltage across the inductor during DT is  $V_{DC}$  and voltage across the inductor when when the switch is open, it is minus  $V_0$ . That is for this duration, I will equate it,  $\overline{I}$  will equate it and I will get this transfer function.  $V_{DC}$  is the voltage across inductor when the switch is on and when the switch is off, voltage across the inductor is at the output voltage. So, this is for the ideal buck - boost converter. What does it say?

The magnitude of output voltage  $V_0$  is less than the input voltage  $V_{DC}$  for D varying from 0 to 0.5. So, we have a step down action here or the buck the operation. For 0 to 0.5, magnitude of output voltage is less than the input voltage. This is nothing but buck operation and from  $0.5$  to D, 0.5 to 1, the magnitude of output voltage is higher than the input voltage. So, this is nothing but the boost operation. But then what happens at D is equal to 1? Similar to boost converter, even in ideal buck - boost converter, magnitude of output voltage tends to infinity as D tends to1.

I will repeat; similar to boost converter, the magnitude of output voltage tends to infinity as D tends to 1. See, the in the equivalent circuit if you see here, we had assumed that output voltage remains constant,  $V_0$  is constant and ripple free and we said that  $V_0$  is the voltage that is appearing the across **across** the inductor when the switch is opened and we equated it. Equated the voltage across the inductor when switch is on and when the switch is off, we equated and we found that the transfer function is D divided by 1 minus D.

But then what happens at D tends to 1 or as the value of D increases? Most of the time, at input inductor is charging and at the output, capacitor is supplying power. So therefore, capacitor voltage has to fall and it will fall. So, the very basic assumption that I made saying that output

voltage will remain constant is not valid. Similarly, at the input, most of time we are applying a DC voltage to the inductor. Current increases linearly and it will so happen that inductor may saturate.

So, whatever that happened in the boost converter for high values of D, happens in buck - boost also. So, as D tends to 1 or if you see in this circuit here, D tends to 1, output voltage will become 0. Output voltage will becomes 0 because capacitor is permanently connected across the load and it is discharging and at the input, inductor is permanently connected across the DC supply and it will saturate. So, this we should get from an equation which we have derived taking the resistance into account, inductive resistance into account.

See here, this is the equation we derived taking the non idealities of the interactive r by R. So, if I substitute here, D is equal to 1, output voltage becomes 0. D is equal to 1, output voltage becomes 0, this is 0 and the inductor current is when D is equal to 1 is  $V_{DC}$  divided by R, at steady state. So, a very high current and which may damage the source or inductor or the switch. This is what it is.

So, last observation that I have need to make is the output voltage is negative with respect to the reference point of the source voltage. I have taken negative DC negative bus as the reference point. So, output voltage is negative with respective to this line, DC line.



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Now, we will  $\ldots$  a non ideal converter, this is the variation; when D is equal to 0, output voltage is 0, whereas, in boost converter, output voltage, the ratio of  $V_0$   $V_{DC}$  is equal to 1. Buck converter when D is equal to 0, output voltage is also 0, D into  $V_{DC}$ . It starts increasing, tends to infinity for ideal buck – boost. At D is equal to 0.5, the ratio is 1.

Similar to boost, the magnitude of  $V_0$  reaches a peak and it comes down and D is equal to 1 which is equal to 0. So what is a value of D for which the magnitude reaches, magnitude of output reaches a peak? We need to differentiate the voltage equation with respect to D. So,  $D_{\text{max}}$ is found to be this which is relatively bit complicated compared to compared to the boost converter. This is a  $D_{\text{max}}$  and  $V_0$  (max) is this value,  $V_0$  (max) is this value.

Now, let us draw the various wave forms. I have drawn both continuous and discontinuous cases for buck as well as boost. For buck – boost, I will draw only for continuous current. I encourage you people to go back and draw it for a discontinuous case.

So, what happens when I close S? Voltage across the inductor is  $V_{DC}$ , current increases linearly, so when I close S, if you see here, the circuit, whatever the current that was flowing through the diode starts flowing through S.

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So, this is the inductor current  $i<sub>L</sub>$ , this path or during this period, diode is on. So, this is the current that is flowing through the diode. At this instant, we have turned on the switch. So, whatever the current that is flowing through the diode starts flowing through the switch S. This is also equal to the source current waveform this is also the source current waveform.

When switch is on, source supplies power. When switch is off, there is no current from the source, similar to buck similar to buck. So, this is a buck converter source current waveform. So, current instantaneously changes. There are abrupt changes in the source current when I turn on as well as when I turn off, whereas, this is not the case in the boost converter. The source current waveform will look like this in the boost converter. Source is always there in the circuit. So, I have a source current waveform which is similar to the buck converter.

So, when I open S, whatever that the current that was flowing through the inductor starts flowing through the load and the diode. The so diode, this is a diode current. At this point, there is an abrupt change because we have turned on the switch. How does an output voltage vary or how does the capacitor current waveform look like?

I told you, this is similar to a boost operation **boost operation**, only capacitor supplies power. This set of thing does did not takes place or does not takes place in buck converter, buck converter. Inductor is always there with the with the output capacitor and the load, even when the switch is open as well as when the switch is closed. So, when the switch is closed, diode is reversed biased or diode cannot conduct. Capacitor supplies power. We have assumed that  $V_0$ remains constant. Even if  $V_0$  changes over a very narrow band,  $V_0$  by R remains approximately constant.

So, I am assuming that load current is constant. So, the capacitor discharges. So, this is the capacitor current, constant. KCL gives, here that  $I_0$  is equal to minus i<sub>C</sub>. So, this is the capacitor current, discharges at a constant rate. Therefore, capacitor voltage, output voltage varies or decreases linearly here. I have opened the switch, the inductor current starts flowing through capacitor and load. KCL at this point gives  $i_L$  is equal to  $i_C$  plus  $i_0$  and I am assuming, whatever the assumption that I made while drawing the waveform, in the case of boost converter. I said that in the entire on period of the switch, capacitor is discharging. So I will assume that when the switch is opened or during the off period of the switch, capacitor is charging.

In other words, in other words, just prior to closing S, inductor current is higher than  $i_0$ . I will repeat; just prior to closing S, inductor current is higher than  $i_0$ . If inductor current is higher than  $i<sub>0</sub>$ , the remaining current has to go through has to go through the capacitor, capacitor continuously charging.

So, if you see here, capacitor current is positive at this point because inductor current  $i<sub>L</sub>$  is higher than i<sub>0</sub>. I am just assuming, it need not be true. If I only thing I have to I need to I have to apply only KCL at this point. If I know the magnitudes of  $i<sub>L</sub>$ ,  $i<sub>C</sub>$ ,  $i<sub>0</sub>$  I assumed to be constant, I can

determine or I can plot  $i<sub>C</sub>$  waveform. So, at this point I am assuming that  $i<sub>L</sub>$ , the inductor current is higher than i<sub>0</sub>. So, the remaining current has to flow into the capacitor which is positive. At this point, I am turning on S, D turns off and capacitor supplying the entire  $i<sub>0</sub>$ . Mind you, capacitor current can change instantaneously. Only capacitor voltage cannot change instantaneously.

So, if I plot  $V_0$ , so it is minimum at just prior to opening the switch and this voltage is maximum just prior to closing the switch. I am assuming that just prior to closing the switch, capacitor current is positive. Only this under this condition it is true, mind it. So, at this point  $i<sub>L</sub>$  is higher than  $i_0$ . So,  $i_c$  is positive, capacitor is charging. But immediately when I close this switch,  $i_c$ becomes negative, it starts discharging. But definitely, the peak of the capacitor voltage or output voltage occurs just prior to closing the switch.

Now, what is the voltage rating and voltage rating of the switch and the diode? See the circuit, when I close the switch, what is the cathode potential of the diode? When I close S, this positive point gets connected to the cathode. These 2 are at the same potential. So, in other words, cathode potential with respect to the negative DC bus is  $V_{DC}$ . Anode potential is minus  $V_0$  minus  $V_0$  with the respect to the negative DC bus.

Anode potential is minus  $V_0$ , cathode potential is plus  $V_{DC}$  with respect. So voltage across diode is sum of these 2 voltages. Plus minus is the voltage at this point and here is  $V_{DC}$ . So, it is a sum of these 2 voltages that the voltage that the diode should block. Diode should block the sum of these 2 voltages and this same voltage appears across this switch when diode starts conducting. See, when diode starts conducting, this point is at minus  $V_0$  with respect to the negative DC bus, whereas, this point is at  $V_{DC}$  with respect to negative DC bus.

So, the voltage across S is  $V_{DC}$  plus  $V_0$ . So, the switch has to block the sum of the output voltage and the and the and the source voltage. The voltage rating of S and D is the same and the minimum voltage rating is the sum of the input voltage,  $V_{DC}$  plus  $V_0$ . That is about the buck boost converter. In all 3; buck, boost and buck – boost, when I am saying continuous conduction it implies that *implies that* inductor current is continuous. If it is discontinuous, it implies that inductor current is discontinuous not the output current, remember.

Now, I will compare the buck, buck - boost and the boost, all 3. Just see the source current waveform in all 3 as well as a load current waveform in all 3. What sort of a current source current waveform we had in buck and buck – boost? They are same. The source current, there is the instantaneously, it has to supply the current that is flowing through the diode. Abrupt change if the current is continuous and it comes abruptly to 0 when I open the switch in both cases; buck as well as buck – boost, there are abrupt changes when I close the switch as well as open the switch in the switch current.

What happens in boost? The source current is approximately a smooth one. There is a large inductor connected in series with the battery. So, I told you yesterday that input stage for a boost converter can be thought of as if it is a current source. The voltage source and an inductor, we can combine it and we can represent it as a current source. So, we have a current source at the input for a boost, whereas, the source current abruptly changes when I open the switch as well as close the switch. So therefore, we require input filters for buck as well as buck boost.

What sort of an output stage I have for a buck converter? The output stage of a buck converter, there is always an inductor comes in series with the capacitor and  $\ldots$  inductor is always there. So, I can represent the output stage of a buck converter as a current source; can represent it as a current source. So, load current or the capacitor current, it is not constantly discharging or capacitor does not discharge at a constant rate when the switch is opened or closed as in the case of boost converter.

In the case of boost converter what happened or in the case of buck boost converter? Both cases; boost as well as buck - boost capacitor was discharging at a constant rate when the switch was closed. Where, that sort of a thing did not happen in the buck converter. Inductor is always present only even when I open the switch or close the switch. So, there is a step change or capacitor current instantaneously changes there.

It is see in this figure, this is source current waveform for a buck converter, same as the buck  $$ boost, whereas, the source current waveform for a boost converter is slowly increasing when the switch is closed and slowly decreasing when the switch is opened. But the output current waveform or the capacitor current waveform in capacitor is discharging at a constant rate. Same thing is true here, capacitor is discharging at a constant rate, discharging.

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So definitely, if compared to the buck converter, ripple in the output voltage in boost as well as buck - boost is higher. I am saying this because capacitor in both the cases is discharging at a constant rate. I will repeat; the ripple in the output voltage will be higher for a buck - boost and a boost converter because output capacitor is discharging when the switch is closed at a constant rate. The entire load current is being supplied by the output capacitor. Definitely, capacitor has to change, voltage has to change, whereas, this sort of a thing does not happened in a buck converter, inductor is always present there. Some sort of a  $\ldots$  some sort of a current source is there in the output stage of a buck converter.

So, it is always desirable to have a current source at the input as well as at the output. See, the since the source current abruptly changing in buck as well as buck – boost, I said we require the input filters and that sort of filter is not required for a buck converter and I told you that output voltage ripple definitely is higher in buck, boost and buck – boost.

I will repeat; output voltage ripple is higher in boost and buck boost because capacitor is discharging at a constant rate, whereas, that sort of a thing does not happen in buck converter. So can I combine the advantages of boost and advantages of buck? whereas wherein, wherein, I have a current source at the input in the boost converter and I have a current source at the output in buck converter.

So, both; current source at the input as well as the output, can I have a converter, wherein, have these 2 features. So, in chuk converter both input as well as output has a current source. So, input stage and an output stage of a chuk converter is a current source. How does it look?



Here is a circuit; source, an inductor and a switch. An inductor and an output stage, **inductor and** an output stage and the diode and am connecting a capacitor between these 2 points. Looks complicated but is very simple and it became very popular, very popular and named after the inventor.

How does it work? Close S, what happens when I close  $S$ ?  $L_1$ ,  $V_{DC}$ ,  $S_1$  sorry S, this is the stage. The moment I close S,  $diode$ , this point gets connected to this point. In other words,  $V_{C1}$  appears across D. See, the negative plate is connected to the anode; the positive plate gets connected to the cathode of D because I am shorting this.

In other words,  $V_{C1}$  is appearing across the diode in the reverse now. Therefore, diode is reverse biased. So, this point gets connected here and the remaining circuit -  $L_2$   $C_2$  and R. I am just closing S. There is the short circuit here,  $V_{C1}$  appears across the diode, cannot conduct and this  $V_{C1}$ , this voltage is a forcing function for this part. I will open S, what happens? The stored energy in the inductor starts flowing through capacitor  $C_1$ , diode D and back to source.

So, open S. Whatever there was the current that was flowing through  $L_1$  starts flowing through the capacitor and the diode, back to source. So, here is the output, when I open the switch, here is an equivalent circuit. What happens to the load side? Current was flowing in this fashion that is is, the source current. So, diode is on  $d$ iode is on and this load current i<sub>2</sub> also starts flowing through  $D_2$ .

So, at the load stage or the at the output stage, I have a circuit something like this;  $L_2 C_2 R$  and D. Current through D is sum of  $i_2$  as well as  $i_S$ , the source current. Sorry, I should have shown here a switch or I need to I should have shown here D. So,  $L_1$ ,  $C_1$ , D, back to source: similarly, L2, this combination, D, back to source.

Now, before deriving the transfer function, can I see these equivalent circuits and can I use whatever that I have studied so far; those 3 converters; buck, buck - boost and boost and can I derive or can I write down the relationship between  $V_{DC}$ , capacitor voltage  $V_{C1}$  and output voltage  $V_0$ ? We can by just by inspecting, I can write the equations. What are they? What happens at the input stage? At closed switch S, current started increasing in the inductor. Open the switch S, whatever the stored energy in the inductor is transferred to the capacitor  $C_1$ . Nothing but a **buck** boost converter operation.

Let me repeat; it is a boost converter operation. I closed S, opened S, whatever that the current that has flowing through  $L_1$  starts flowing through the capacitor  $C_1$ . At the input stage I have a voltage source and an inductor. So, I can represent  $\frac{1}{1}$  the input stage as a current source, similar to boost. Voltage source and inductor, I said we can represent it, the input stage by a current source. Similarly here,  $V_{DC}$  and  $L_1$  the inductor can be a thought of as a current source. That current source was flowing through, the value of the current was flowing through S when I closed that and when I opened it, it starts flowing through the capacitor  $C_1$ . Same thing what that has happened in the boost converter.

So therefore, the relationship between  $V_{C1}$  and  $V_{DC}$  should be equal to or the same transfer function that we derived for the boost converter should be valid here between  $V_{C1}$  and  $V_D$ . The relationship between  $V_{C1}$  and  $V_D$  is 1 divided by 1 minus D, same as the boost converter. So therefore,  $V_{C1}$  is  $V_{DC}$  divided by 1 minus D. See the circuit here, circuit here, source S, we closed them and opened S,  $V_{C1}$ , same thing. So, relationship between  $V_{C1}$  and  $V_{DC}$  is same as, this is nothing but **buck a** boost converter circuit. This is nothing but boost converter circuit. So,  $V_{C1}$  is equal to  $V_{DC}$  divided by 1 minus  $V_{C}$ .

What happens in the secondary side or in the load side? What happens on the load side? Do not you think this is nothing but a buck converter? Buck converter with the input as  $V_{C1}$ ? When I close S, input voltage is applied to the inductor as well as the output stage, same equivalent circuit that we got when switch is on in the buck converter. When I opened S, diode starts conducting and this is the equivalent circuit. This is nothing but the buck converter.

So, we have a relationship between  $V_{C1}$  and  $V_0$ ? What is that?  $V_0$  is equal to D into  $V_{C1}$ , whereas, here we have  $V_{C1}$  is equal to  $V_{DC}$  divided by 1 minus D. Boost converter, a buck converter,  $V_0$  is equal to D into  $V_{C1}$ . So therefore, what is the relationship between  $V_{DC}$  and  $V_0$ ?  $V_0$  is equal to D into  $V_{C1}$  and  $V_{C1}$  is equal to  $V_{DC}$  divided by 1 minus D. Therefore,  $V_0$  is equal to D divided by 1 minus D into  $V_{DC}$ , nothing but a buck - boost operation, buck boost operation.

So, transfer function of a chuk or a chuk converter is the same as that of a buck - boost converter. Again, the output voltage, the polarity is the same as same as the buck – boost.

Now, we will analyze this circuit taking the resistances of  $L_1$  and  $L_2$  into account. Now, the process may be bit tedious but then very simple equations. After all, R into I plus L di 1 by dt is equal to  $V_{DC}$ , there is the max is the term that come into the appearing the equations. The, you may or they may appear to be bit tedious, please do not lose patience; solve this equations. Now, we will start writing the circuit equations in terms of resistances.

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S is closed, input is  $V_{DC}$  is equal to  $L_1$  dis by dt plus  $r_1$  into is, is is the source current, not the switch current and at the at the load side,  $V_{C1}$  is equal to  $L_2$  di 2 by dt plus  $r_2$  into i<sub>2</sub> plus  $V_0$  and at the output, KCL gives i<sub>2</sub>, the inductor current i<sub>2</sub> is equal to capacitor current C  $dV_0$  dt plus  $V_0$ R C and and the entire  $i_2$  is being supplied by the capacitor 1, C<sub>1</sub> V<sub>C1</sub>. So, C<sub>1</sub> dV<sub>C1</sub> by dt is equal to minus i<sub>2</sub>. The entire, the inductor current i<sub>2</sub> which is the sum of output current and the capacitor 2 current,  $C_2$  current, is flowing through  $L_2$  that is  $i_2$  is equal to the rate of change of the capacitor voltage  $C_1$ ,  $V_{C_1}$  by dt.

So, if I represent a load side by a current source of  $i_2$  because there is an inductor coming in series with the output stage, I can assume that or I can say that  $C_1$  is discharging at a constant rate of  $i_2$ . See, same thing whatever that happened  $\frac{in}{a}$  in a buck converter. Buck converter, the load side we represented or I said we can represent it by a current source. So, here also if I represent the load side by a current source of  $i_2$  that current is being supplied by the capacitor  $C_1$ .

So, we can say that  $C_2$  is discharging at a constant rate. Current that is flowing is  $i_2$  for 0 to dt when the switch is closed.

What happens when I open the switch? Switch is open, whatever the current that was flowing through  $L_1$  starts flowing through  $C_1$ . I said, the input stage of a cuk converter, the  $V_{DC}$  in series with  $L_1$  can be represented by a current source of is, similar to the boost converter. Now, that entire current source current of a current or the value of the current source is flowing through the capacitor  $C_1$ . In other words, capacitor is charging at a constant rate. Current that is flowing is constant and it is at is. I am neglecting the ripple, please. So,  $V_{C1}$  increases when the switch is off.

In other words, capacitor  $C_1$  is charging when the switch is off. When I open the switch, capacitor  $C_1$  starts charging. It was supplying  $i_2$ , constant current when the switch was closed when the switch was closed. So therefore, from 0 to DT,  $V_{C1}$  is decreasing linearly because I assume that current that is flowing out of out of  $C_1$  is  $i_2$  and from DT to T, capacitor voltage  $V_{C_1}$ is increasing at a increasing linearly because I assumed that current that is flowing through it is  $i_1$ or  $i<sub>S</sub>$  is the current source.

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So, here is the equation; C dV<sub>C1</sub> by dt is equal to i<sub>s</sub>. Capacitor V<sub>C1</sub> is increasing or C<sub>1</sub> is charging. At the load side,  $r_2i_2$  plus L<sub>2</sub> di 2 by dt plus V<sub>0</sub> is equal to 0 and  $i_2$  is equal to same, C  $dV_0$  by dt plus  $V_0$  by R,  $V_0$  by R.

Now, how would I find out the average values? Same, integrate it over the cycle, integrate it over the cycle only when the switch is on as well as switch is off and I will get these 2 equations. See, here are the equations. Please I have just written integration, actually, we have to find the average values.  $\frac{1}{1}$  over t is there, 1 over t is there. I have to find out the average values. So definitely, 1 over t time period has to be there.

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$$
\int_{0}^{1} V_{\infty} = \int_{0}^{1} t_{1} t_{2} + \int_{0}^{1} L_{\frac{\pi}{100}}^{1} = 0 \leq t \leq 0
$$
\n
$$
\int_{0}^{1} V_{\infty} = \int_{0}^{1} t_{1} t_{2} + \int_{0}^{1} L_{\frac{\pi}{100}}^{1} + \int_{\frac{\pi}{100}}^{1} V_{\infty} = 0
$$
\n
$$
\therefore V_{\infty} = t_{1} I_{2} + L_{1} \left( \frac{dI_{3}}{dt} \right)_{\infty} + \frac{1}{t_{2}} \int_{0}^{1} V_{\infty} = 0
$$
\nsimilarity,  $t_{2} I_{2} + L_{2} \left( \frac{dI_{3}}{dt} \right)_{\infty} + V_{1} = \frac{1}{t_{1}} \int_{0}^{1} V_{\infty} = 0$ 

\n
$$
I_{2} = C \left( \frac{dV_{2}}{dt} \right)_{\infty} + \frac{V_{2}}{R}
$$
\n
$$
C \left( \frac{dV_{\infty}}{dt} \right)_{\infty} = \frac{1}{t_{1}} \int_{0}^{1} (L_{1}) dt + \frac{1}{t_{2}} \int_{0}^{1} I_{\infty} dt
$$

This is the equation for 0 to DT and this is the equation, the voltage equation, mind you, from DT to t T from DT to T. So, if I add up both,  $V_{DC}$ ,  $i_1$  to rs is there, L di by dt is there average, 1 over T DT to T, this capacitor term appearing only when the switch is opened. This term, average is  $0\,0$ .

Similarly, in this load side we have this sort of equation.  $r_2$  i<sub>2</sub> plus L<sub>2</sub> di 2 by dt average plus V<sub>0</sub> is equal to 1 over T, 0 to DT  $V_{C1}$  dt and  $i_2$  current is this constant. I can represent it by a current source is C  $dV_0$  by dt average plus  $V_0$  by R is at load side and at the input side, this is the current. How would I get them? Finding out these 2 values, this this is current waveform or this is the equation for the current when the switch is opened and here at the load side, equation for the current when the switch is opened. Similarly, we have here. These are 2 equations, combine them and you get this.

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So, at steady state, the ripple at the input because we have a  $V_{DC}$  and an inductor, we have at the output also, i<sub>2</sub> a current source. At steady state, ripple in both, ripple in these 2 inductors should be the same. Peak to peak ripple should be the same. Similarly in the output voltage,  $V_{C1}$  and output voltage  $V_0$ , that is nothing but the voltage across the capacitor  $C_2$ , it should be the same. So, we will get neglecting ripple and all this we will get these 4 equations.  $V_{DC}$  is equal to  $i_1$  into rs and 1 minus D V<sub>C1</sub>. So, if I neglect  $r_1$  see we have V<sub>C1</sub> is equal to V<sub>DC</sub> divided by 1 minus D. Nothing but the boost converter transfer function, **boost converter transfer function.** 

This is at the secondary side or sorry the load side, the load side. Secondary side, I mean the load side.  $r_2$  i<sub>2</sub> plus V<sub>0</sub> is equal to D V<sub>C1</sub>. If  $r_2$  is 0, V<sub>0</sub> is equal to D into V<sub>DC</sub>. I told you that output stage is nothing but a buck converter with the forcing function of  $V_{C1}$  forcing function of  $V_{C1}$ . i<sub>2</sub> is the average load load current,  $I_2$  is a average current that is flowing through the inductor that is given by  $V_0$  by R because average value of the current that is flowing through the capacitor  $C_2$ should 0, mind you. Same, whatever that  $I$  that we said for a buck converter, there is the inductor, capacitor and R is always present. Even in cuk converter,  $L_2$   $C_2$  and R is always present. So, average value of the inductor current should be equal to the average current of the load in in in buck as well as cuk converter of the load side because average current flowing through the capacitor should be 0 at steady state.

So,  $i_2$  is the average value of the inductor current  $L_2$  should be equal to the average value of the load current and this is the another equation. So, again by solving these equations, these are the 4 equations that we get.

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V = \frac{D}{(1-D)} I_2 \rightarrow Av, \text{ load } 1 \quad \forall \text{ or } 1 \text{ through } C = 0
$$
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$$
I_2 \frac{V_1}{R} + V_2 = DV_{\text{cl}}
$$
\n
$$
\therefore V_{\text{cl}} = \frac{V_2}{DR} (I_2 + R)
$$
\n
$$
= I_1 I_2 + (1-D) I_3 \frac{(1-D)}{DR} (I_3 + R)
$$
\n
$$
= I_3 I_3 + (1-D) I_3 \frac{(1-D)}{D^2} (I_2 + R)
$$
\n
$$
\therefore I_4 = \frac{V_{\text{loc}}}{I_4 + (\frac{1-D}{D})^2} (I_2 + R)
$$
\n
$$
= \frac{1}{I_3} \times \frac{1}{I_4} \times \frac{1}{I_5} \times \frac{1}{I_5} \times \frac{1}{I_6}
$$
\n
$$
= \frac{1}{I_5} \times \frac{1}{I_6} \times \frac{1}{I_7} \times \frac{1}{I_7} \times \frac{1}{I_8}
$$
\n
$$
= \frac{1}{I_7} \times \frac{1}{I_7} \times \frac{1}{I_8} \times \frac{1}{I_9}
$$
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$$
= \frac{1}{I_9} \times \frac{1}{I_9} \times \frac{1}{I_9} \times \frac{1}{I_9}
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= \frac{1}{I_9} \times \frac{1}{I_9} \times \frac{
$$

Substitute for  $V_{C1}$  in the equation representing  $V_{DC}$ . See, these are the equations that we are getting. is in terms of  $V_{DC}$  and D. How did I get them? Just by substituting 1 variable in other, in the previous equation, add  $V_{DC}$  and substitute here and I will get this. For I<sub>S</sub> in terms of  $V_{DC}$  is given by this equation;  $V_{DC}$  divided by  $r_1$  plus whole square into  $r_2$  plus R. Average source current is the source current in terms of the input voltage and the duty cycle, and the duty cycle.

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$$
V_n = I_n R = \left(\frac{1-D}{D}\right) R I_n = \left(\frac{1-D}{D}\right) R - \frac{V_{nc}}{I_n + \left(\frac{1-D}{D}\right)^T (I_n + R)}
$$
\n
$$
\therefore V_n = \frac{V_{nc}}{R (1-D)} + \left(\frac{1-D}{D}\right) \left(\frac{R + I_n}{R}\right) \Rightarrow \text{ov. } V_n \text{ in terms of } V_{nc} \triangle D
$$
\n
$$
V_{c1} = \frac{V_{c}}{DR} (I_n + R) = \frac{V_{nc}}{(1-D) + \frac{I_n}{(I_n + R)} + \frac{D^2}{(1-D)}}
$$

Similarly, output voltage  $V_0$  in terms of  $V_{DC}$  and the duty cycle D,  $V_0$  in terms of  $V_{DC}$  into D. Same,  $V_0$  is equal to  $I_2$  into R. I will substitute now, I know the relationship between  $I_2$  and  $I_S$ , I will substitute here. This what I will get? This is what I will get. These are the equations and here is the equation, capacitor  $V_{C1}$  in terms of  $V_{DC}$  and this is ...

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)(1-D)T  $-$  DV $_{\rm ct}$  (is buck converter with V $_{\rm ct}$  as the input voltage) 16

So, if I make  $I_1$  and  $r_1$ , if I neglect the resistances, neglect the resistances, I will get this equation. Substitute for  $r_1$  and  $r_2$  and make them, make  $r_1$  and  $r_2$  is equal to 0. Substitute, simplify, we will get this equation. See here,  $V_{C1}$  is equal to  $V_{DC}$  divided by 1 minus D, boost converter and we have a buck, this is V<sub>0</sub> and V<sub>DC</sub>, a buck - boost converter, <mark>buck - boost converter, buck - boost</mark> converter. That is about the cuk converter. We will draw the various wave forms tomorrow.

Please, compared to buck, buck - boost and boost, they may look bit, the cuk converter may look bit complicated. But it is very simple and and it is very interesting circuit, very interesting circuit. You can derive the transfer of function just by drawing the equivalent circuit when S is equal to on and S is equal to off, buck and the boost operation. This is more about it, we will see tomorrow.

Thank you.