

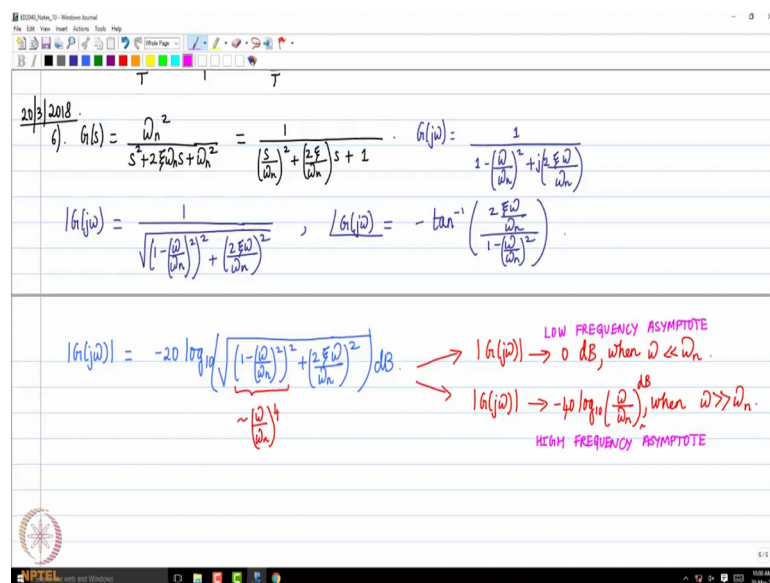
Control Systems
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Lecture - 53
Bode Plot 3
Part - 1

So, we will get started. So, we are looking at bode diagrams, right and we looked at the bode plots of a few individual factors. The last factors that we are going to look at, our last set of factors that we are going to look at are essentially second order factors, right. So, we know that by and large we can write a second order transfer function in this manner, right.

So, I am just considering the structure which we are already familiar with, ok. So, that is what I am doing.

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So, omega n squared divided by S squared plus 2 zeta omega S plus omega n squared, right. So, that is a typical transfer function of a second order system that we have been considering in this course. So, now the question is that like how do I plot the bode diagram of this particular factor, ok. So, let us start doing that today.

So, this can be rewritten as 1 divided by I just divided by ωn square in both numerator and denominator. So, essentially I will get it as S by ωn whole square plus 2ζ by ωn S plus 1, right. So, that is what will happen, correct. So, if I divide both numerator and denominator by ωn squared, so immediately what is going to happen is that like if I calculate G of $j\omega$, so what would I get? I would get 1 divided by $1 - \omega$ by ωn whole square plus 2ζ ω by ωn j , right. So, that is what I will have, ok.

So, 2ζ ω by ωn , right. So, that is what we will have as the sinusoidal transfer function. So, once I have this, what can I how can I write the magnitude of this particular factor? So, I can say this is going to be 1 divided by square root of the real part square. So, the real part square is going to be $1 - \omega$ by ωn whole square and this I have 2 square. That is a real part. Then, I take the square of the real part plus the imaginary part squared so 2ζ ω by ωn whole square, right.

So, that is what I do, ok. So, then what will be the phase of the sinusoidal transfer function? That is going to be minus tan inverse of 2ζ ω by ωn divided by $1 - \omega$ by ωn whole square, right. So, that is what we get as the phase, right of this particular factor, right. It is pretty straightforward algebra, ok.

So, now let us look at the magnitude will once again we will follow the same process as we did in the previous class with the first order factor. So, let us look at the magnitude of this factor and then, let us try to figure out what are the asymptotes for this particular factor, right. So, we can immediately see that the magnitude of this particular factor in decibels is going to be minus $20 \log$ to the base 10 square root of $1 - \omega$ by ωn whole square square plus 2ζ ω by ωn square, ok.

So, that is what will happen, ok. So, this is going to be in decibels, right. So, what will happen as ω is very small. What do you think will happen to this magnitude when ω is very small when compared to ωn let us say. So, the magnitude of G of $j\omega$ you can immediately see that will tend to 0 decibels as ω is much smaller than ωn . Why am I taking ωn ? It is because we have ω divided by ωn , right as a term, right.

So, I have to compare the frequency in relation to ω_n , right. So, when the frequency of interest becomes much less than ω_n which is the natural frequency of the system, we can see that ω/ω_n becomes very small. So, obviously, ω/ω_n whole squared also will be pretty small, right. So, in the square root term, I will effectively end up with 1. So, I am essentially going to take log of 1, so that I will get zero decibels, right. So, that is what is going to happen when I have ω much lower than ω_n and what is going to happen when ω is much greater than ω_n , ok. So, let me erase this and say when ω is much less than, ok. What do you think happens when ω is much greater than ω_n ?

Obviously, ω/ω_n is now going to be much greater than 1, ok. So, now within this first term if you look at it, you have $1 - \omega/\omega_n$ squared. So, that will effectively become minus ω/ω_n squared, but you are squaring it. So, the first term is going to be like ω/ω_n to the power 4, right.

The second term is $2\zeta\omega/\omega_n$ whole square. Now, which term is going to dominate? First term, right that is ω/ω_n to the power 4. So, now when you take the square root of ω/ω_n to the power 4, what do we get? We get ω/ω_n whole square, right. So, then if I take the logarithm of that, what will I get?

Student: $40 \log$.

I am going to get minus $40 \log$ to the base 10 ω divided by ω_n . Is it clear? How? Of course, this is in decibels, right. So, is it clear how we got minus $40 \log \omega$ by ω_n because I am sorry what is it?

So, you can see that the first term tends to ω/ω_n to the power 4, the second term is like ω/ω_n whole square. Just think that ω/ω_n is 10^3 . So, the first term is going to be like 10^{12} , right. The second term is going to be like 10^6 . So, the first term is obviously dominate, right. You take the square root, you are going to get ω/ω_n squared.

So, \log of ω/ω_n squared is $2 \log \omega/\omega_n$. So, there is already a minus 20, you multiply it by 2, you get minus 40, right. So, that is why the magnitude

tends to minus 40 log to the base 10 omega by omega n decibels when omega is much greater than omega n. So, obviously we already know that this one is going to be the low frequency asymptote, right and this one is going to be the high frequency asymptote just like what we did yesterday, right.

So, this is going to be the high frequency asymptote, ok.

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$|G(j\omega)| = -20 \log_{10} \sqrt{\left(1 - \left(\frac{\omega}{\omega_n}\right)^2\right)^2 + \left(\frac{2\zeta\omega}{\omega_n}\right)^2} \text{ dB}$

$\sim \left(\frac{\omega}{\omega_n}\right)^4$

LOW FREQUENCY ASYMPTOTE
 $|G(j\omega)| \rightarrow 0 \text{ dB, when } \omega \ll \omega_n$

$|G(j\omega)| \rightarrow -40 \log_{10} \left(\frac{\omega}{\omega_n}\right) \text{ dB, when } \omega \gg \omega_n$
 HIGH FREQUENCY ASYMPTOTE

Q: Where do the 2 asymptotes intersect? At $\omega = \omega_n \rightarrow$ CORNER FREQUENCY.

Q: What is the slope of the high frequency asymptote?
 $-40 \log_{10} \left(\frac{\omega}{\omega_n}\right) \text{ dB} = -40 \text{ dB} - 40 \log_{10} \left(\frac{\omega}{\omega_n}\right) \text{ dB}$
 Slope of the high frequency asymptote = $-40 \frac{\text{dB}}{\text{decade}}$

Q: When is $|G(j\omega)|$ a maximum?

So, that is what we will have here. Now, once again a set of questions there like the first one is, where do the two asymptotes intersect? Where do you think the two asymptotes intersect each other? Omega equals omega n. We can immediately figure out the answer as omega equals omega n. Why? It is because you see that when you substitute omega equals omega n in the high frequency asymptote, you get zero decibels, right.

So, essentially zero decibel line is the low frequency asymptote. So, essentially the two asymptotes intersect at omega equals omega n, right. So, consequently omega equals omega n is the corner frequency, right for this particular factor, right the second order term, ok. The natural frequency is the corner frequency, ok. Is it clear because that is the frequency at which the two asymptotes intersect?

So, the second question that we need to ask ourselves is that what is the slope of the high frequency asymptote? What do you think is a slope? So, the high frequency asymptote is minus 40 log to the base 10 omega by omega n, right. So, how do we figure out the

slope? Let us say you go one decade further right from omega. So, instead of omega, you substitute ten times omega. What do we get? So, immediately we see that minus 40 log to the base 10, 10 times omega by omega n that is going to be equal to what? Of course, in decibels that is going to be equal to minus 40 decibels, all right minus 40 log of log to the base 10 of omega by omega n in decibels, right. So, what is the slope?

So, slope of the high frequency asymptote is going to be minus 40 decibels per decade, right. So, is equal to minus 40 decibels per decade, ok. That is what matters. So, please note that here the slope is going to be slope of the high frequency asymptote is minus 40 decibels per decade. So, as frequency increases, the magnitude decreases like minus 40 decibels per decade, ok. That is important, ok.

Now, another question which we are going to ask ourselves is that when is the magnitude of G of j omega a maximum or at what frequency ok? So, in other words, you know like at what frequency is the magnitude of G of j omega a maximum, right? So, that is a question we are going to ask ourselves. So, let us try to answer that.

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$|G(j\omega)| = \frac{1}{\sqrt{\left(1 - \frac{\omega^2}{\omega_n^2}\right)^2 + \left(\frac{2\zeta\omega}{\omega_n}\right)^2}}$

Let $f(\omega) = \left(1 - \frac{\omega^2}{\omega_n^2}\right)^2 + \left(\frac{2\zeta\omega}{\omega_n}\right)^2$

$\frac{df(\omega)}{d\omega} = -2\left(1 - \frac{\omega^2}{\omega_n^2}\right)\frac{2\omega}{\omega_n^2} + 2\left(\frac{2\zeta\omega}{\omega_n}\right)\frac{2\zeta}{\omega_n} = 0$

$\left[-1 - \frac{\omega^2}{\omega_n^2} + 2\zeta^2\right]\omega = 0$

$\omega = 0, \zeta > \frac{1}{\sqrt{2}}$

$2\zeta^2 = 1 - \frac{\omega^2}{\omega_n^2} \Rightarrow \omega = \omega_n \sqrt{1 - 2\zeta^2}$

RESONANT FREQUENCY
 $\omega_r = \omega_n \sqrt{1 - 2\zeta^2}$
 exists only when $1 - 2\zeta^2 > 0$
 $\Rightarrow \zeta < \frac{1}{\sqrt{2}}$

Undamped 2nd order system:
 $P(s) = -\omega_n^2$

$u(t)$
 $|y(t)|$

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So, what is the magnitude of G of j omega. It is going to be 1 divided by square root of 1 minus omega squared by omega n square whole square plus 2 zeta omega by omega n whole squared, right. So, this is the magnitude, right.

So, now when is this going to be a maximum? Of course, how can I find out at what frequency this is going to be a maximum I differentiate equated to zero and then, like take the second derivative figure out where it is, the second derivative is negative for a maximum right, but here I can use a simpler method because this in the numerator is 1, right. So, I will have a maximum where the denominator is going to be a minimum. I can even what you say remove the square root, right.

So, at whatever frequency the term within the square root in the denominator is a minimum, that is the frequency at which the magnitude of G of $j\omega$ is going to be maximum, right. So, let us say we call f of ω some f of ω as $1 - \omega^2$ squared by ωn square whole square plus $2\zeta\omega$ by ωn whole square.

Now, if we take the derivative, the first derivative of f of ω with respect to ω , what do we get? We get two times $1 - \omega^2$ squared by ωn squared times 2ω divided by ωn square, right. So, first I just then I have a minus sign, right. So, when I take the derivative of the term within the square, right I will get a minus sign, right. So, let me put this minus sign here, and then, what will I have here? I will have essentially $2 \times 2\zeta$ by ωn , correct. Then, what will I have? I will have 2ζ by ωn , correct. So, this should be equal to 0, ok.

So, now if I process this, what will I get for ω ? Can you calculate and tell me? So, you can see that I immediately have this ωn squared cancelling off with this ωn . Let us say this 2, this 2 cancelling off these 2, right. So, what will I have? I will have minus 1 by ω^2 squared divided by ωn squared. Obviously, ω is non-zero, right. So, of course I can have two solutions, ok. We will come to that shortly you know like. So, plus 2ζ times ω is equal to 0, right.

So, this has two solutions, right. I just simplified this and wrote it. So, obviously you know like ω is 0 is one particular solution, right. It can be 0, right or the term within the square bracket is 0. That will imply that 2ζ is going to be equal to $1 - \omega^2$ squared by ωn square, ok. Sorry this should be $2\zeta^2$ squared, right correct. I think I missed a ζ here, right. So, $2\zeta^2$ square. So, this will tell me that ω can also be ωn times square root of $1 - 2\zeta^2$ squared, ok. Correct? I am just rearranging the terms and doing some simple algebra.

Now, when will this solution be a real number because we are dealing with frequencies, right. See I want a positive real number, right. When will this solution exist? This exists only when 1 minus 2 zeta squared is greater than 0 or in other words, zeta should be less than 1 over root 2, right 0.70 so on, right. 1 over root 2 is 0.70 approximately, right.

Student: (Refer time: 17:46).

Sorry.

Student: (Refer time: 17:47).

But, anyway zeta is a positive number, ok. Of course, when we started off, I have to say that zeta and omega n are a positive parameter. You are right in general, but since we are essentially dealing with systems where zeta and omega are not positive, this is what I have, right.

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$$\left[-\left(1 - \frac{\omega^2}{\omega_n^2}\right) + 2\zeta \right] \omega = 0 \Rightarrow \omega = 0, \zeta > \frac{1}{\sqrt{2}}$$

$$2\zeta = 1 - \frac{\omega^2}{\omega_n^2} \Rightarrow \omega = \omega_n \sqrt{1 - 2\zeta^2}$$

$\omega_r = \omega_n \sqrt{1 - 2\zeta^2}$

RESONANT FREQUENCY
 $0 < \zeta < \frac{1}{\sqrt{2}}$
 exists only when $1 - 2\zeta^2 > 0 \Rightarrow \zeta < \frac{1}{\sqrt{2}}$

- 1) Natural frequency, ω_n .
- 2) Damped Natural Frequency, $\omega_d := \omega_n \sqrt{1 - \zeta^2}$.
- 3) Resonant frequency, $\omega_r := \omega_n \sqrt{1 - 2\zeta^2}$.

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Undamped 2nd order system:
 $P(s) = \frac{\omega_n^2}{s^2 + \omega_n^2}$
 $u(t) = \sin(\omega_n t) \Rightarrow Y(s) = \frac{\omega_n^2 \omega_n}{(s^2 + \omega_n^2)^2}$
 $|y(t)| \rightarrow \infty$ as $t \rightarrow \infty$

So, this frequency omega r is called as the. Have you encountered this frequency before? This is what is called as a resonant frequency, and of course, it exists only when zeta is greater than 0 and less than 1 over root 2, otherwise it does, for zeta greater than 1 over root 2 omega tending to 0 will give you the maximum value that is the 0 decibel value, but for zeta between 0 and 1 over root 2, you know like you have the resonant frequency

basically giving you the maximum value of the amplitude or magnitude of the sinusoidal transfer function for the second order factor, ok.

So, what is this resonant frequency? See we had we already defined a couple of frequencies, right. So, what was natural frequency? See you take a second order system let us say you remove the damping, right then you give a perturbation, the frequency at which the undamped system oscillates is what is called as the natural frequency, right and also, if you look at it, let me write it as an aside if you look at an undamped second order system.

So, undamped second order system, the plant transfer function is going to be like ω_n squared divided by s squared plus ω_n squared. Do you agree? So, that is how we got, we have the visualization right of natural frequency, you give a perturbation, or essentially then the frequency at which the output will oscillate is essentially the natural frequency, but if you also give an input which is essentially let us say \sin or \cos of ω_n , let us say you give $\sin \omega_n t$. What is going to happen to the output? We are going to get ω_n square times ω_n divided by s squared plus ω_n square whole square, right. So, once I have this, what will happen? I think we already discussed these things, right. What would happen once I have s squared plus ω_n squared whole square? I am going to have $t \sin t$ or $t \cos t$, right term.

So, consequently what will happen to the magnitude of Y of t ? It will go to infinity, right as t tends to infinity, right. So, this is another visualization of a natural frequency that is if you have an undamped second order system and you give an input which essentially which has a frequency equal to the natural frequency, the output will just explode to infinity, ok. That is natural frequency, ok. That was the first data what was undamped natural frequency. Sorry? Sorry, this is the, sorry this is the natural frequency. What is damped natural frequency?

Damped natural frequency was the frequency at which the damped second order system oscillator, right when the damping ratio was between 0 and 1 in response to an step input, right. So, we looked at ω_d if you remember, right. So, there are three natural frequencies of interest. So, the first one is natural frequency which by definition corresponds to the undamped system, right.

The second one was the damped natural frequency which essentially corresponds to an under damped second order system, and the damped natural frequency is ω_n times square root of $1 - \zeta^2$, right. So, physically what is say notion of this damped natural frequency? We have a stable second order system. You give a step input, the frequency at which the corresponding output would oscillate is what is called as the damp natural frequency and even if you give a sinusoidal input equal to the damped natural frequency, the system output would be bounded because you have an under damped stable second order system, ok. No doubt about it.

Now, the third frequency is the resonant frequency ω_r . So, what is this ω_r , which is essentially ω_n times square root of $1 - 2\zeta^2$. This essentially means that I have a stable under damped second order system with damping ratio between 0 and $1/\sqrt{2}$. If I have such a system, this is the frequency at which the amplitude of the corresponding sinusoidal transfer function will be maximum, ok. So, that is the implication, ok.

So, in other words, if you give a sinusoidal input equal to whose frequency is equal to ω_r , you would get the maximum amplification of the input because p the amplitude of the transfer function is maximum with this frequency. That is what we have seen right. Isn't it? So, that is the physical meaning of the resonant frequency. Resonant frequency resonance and resonant frequency still correspond to a stable second order system, but then it is bad in practice because of the amplification of the oscillations because what is this physically? What is this magnitude of $G(j\omega)$?

If you recall our derivation, the output steady state output was u magnitude of the input times magnitude of $G(j\omega)$. So, the output is also going to be a sinusoid, but the input amplitude is going to be multiplied by the magnitude of the sinusoidal transfer function. So, imagine frequency at which the magnitude of the sinusoidal transfer functions of the maximum.

So, the output amplitude which is a sin wave that will also be a maximum there; it is still bounded mathematically ok, but physically it may create issues, ok. The system is still stable no doubt about it right, but then resonance can lead to oscillations of reasonably high magnitude which can cause structural damage, ok. So, one famous example you

know like which is typically given to illustrate this is what is called as Tacoma Narrows Bridge Collapse, right.

So, you please search online and watch the video Tacoma Aquas Narrows Bridge, ok. So, you will see that the wind essentially excited the resonant frequency and the entire bridge swayed, ok. Yes, mathematically it is bounded, the amplitude is bounded, but what happened the structure field, because of the excessive oscillations, right. So, that is what happened. So, just watch the video, right.

So, that is the resonant frequency, right. So, that is why I just wanted to do this analysis to convey the difference between natural frequency, damped natural frequency and resonant frequency. I hope the physical meaning is clear for each frequency because this understanding is extremely critical and we want to analyze second order systems, right.

So, please know that resonant frequency once again is applicable only for those second order systems where the damping ratio is between 0 and 1 over root 2, ok. I hope this point is clear, right but we are not done with the derivation yet. As homework, what I want you to do is that you have to take the second derivative and then, ensure that $f''(\omega)$ is going to be positive at this frequency, right. That I leave it for your homework because whenever you do maximization or minimization, you need to do both steps. I cannot leave it hanging like this, but I am going to leave it to your homework, ok.

So, as homework evaluate the second derivative, and comment ok. So, that is essentially your homework. Obviously, you will see that at this resonant frequency, the second derivative is positive. So, as a result the magnitude of $G(j\omega)$ will be a maximum, because magnitude of $G(j\omega)$ is $1/\sqrt{1 - \zeta^2}$, right. So, that is why when ζ is minimum, magnitude of $G(j\omega)$ will be a maximum, ok. So, that is what we will have, ok.

So, please do that and we can easily show that, this is also I am going to leave it as homework.

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2) Damped Natural Frequency, $\omega_d := \omega_n \sqrt{1 - \zeta^2}$.

3) Resonant Frequency, $\omega_r := \omega_n \sqrt{1 - 2\zeta^2}$.

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$|G(j\omega)|_{\max} = |G(j\omega_r)| = \frac{1}{2\zeta\sqrt{1-\zeta^2}}$

$\angle G(j\omega) = -\tan^{-1}\left(\frac{\sqrt{1-2\zeta^2}}{\zeta}\right)$.

$Y(s) = \frac{\omega_n^2 \omega_n}{s^2 + \omega_n^2}$

$y(t) = \frac{\omega_n^2 \omega_n}{(\zeta^2 + \omega_n^2)^2} \sin(\omega_n t) \Rightarrow |y(t)| \rightarrow \infty \text{ as } t \rightarrow \infty$.

So, the magnitude of G of $j\omega$, the maximum value which is the magnitude of G of $j\omega$ at $\omega = \omega_r$ is going to be $\frac{1}{2\zeta\sqrt{1-\zeta^2}}$, ok. So, this you just need to plug in the value of ω in that expression, ok. You will easily get it and the phase of G of $j\omega$ at $\omega = \omega_r$, you will if you substitute in that equation for the phase, you will get it as $-\tan^{-1}\left(\frac{\sqrt{1-2\zeta^2}}{\zeta}\right)$. Immediately you see that the maximum magnitude and the phase at the corresponding resonant frequency depend on the damping ratio, the ζ , ok.

So, that is what we have, ok. You can just substitute and then, very straightforward you just substitute and then figure out.