

Mechanics of Material
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Stresses and deflection in beams not loaded about principal axis
Lecture – 74
Bending equation about arbitrary axis

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$M_v = - \int (u-u_0) \sigma_{xx} dx$ similar to $M_y = - \int (y-y_0) \sigma_{xx} dx$ $z \rightarrow v$
 $y \rightarrow u$
 $M_v = E \int \left[(u-u_0)^2 \frac{d^2 Du}{dx^2} + (v-v_0)(u-u_0) \frac{d^2 Du}{dx^2} \right] dx$
 $M_v = E I_{vv} \frac{d^2 Du}{dx^2} + E I_{uv} \frac{d^2 Du}{dx^2}$ $\left\{ \begin{array}{l} u_0 = v_0 = 0 \text{ because origin is at } (u_0, v_0) \\ \text{the beam is homogeneous.} \end{array} \right.$
 $M_u = \int (v-v_0) \sigma_{xx} dx$ similar to $M_y = \int (z-z_0) \sigma_{xx} dx$
 $M_u = E \int \left[(u-u_0)(v-v_0) \frac{d^2 Du}{dx^2} + (v-v_0)^2 \frac{d^2 Du}{dx^2} \right] dx = -E I_{uv} \frac{d^2 Du}{dx^2}$
 $E \frac{d^2 Du}{dx^2} = \frac{M_v}{I_{vv}} \quad \& \quad E \frac{d^2 Du}{dx^2} = -\frac{M_u}{I_{uv}} \quad \left| \quad \sigma_{xx} = \frac{-M_v(u-u_0)}{I_{vv}} + \frac{M_u(v-v_0)}{I_{uv}} \right.$

Next what do you want to do is, see what happens when Iuv is not 0 when Iuv is not 0 that is i am dealing with the given axis y and z what happens.

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If $I_{yz} \neq 0$ then
 $u = - \left[(y-y_0) \frac{dDy}{dx} + (z-z_0) \frac{dDz}{dx} \right] \epsilon_x + D_y(x) \epsilon_y + D_z(x) \epsilon_z$
 $\sigma_{xx} = -E \left[(y-y_0) \frac{d^2 Dy}{dx^2} + (z-z_0) \frac{d^2 Dz}{dx^2} \right]$; $\int \sigma_{xx} dx = 0 \Rightarrow \begin{cases} y_0 = \frac{\int E y dx}{\int E dx} \\ z_0 = \frac{\int E z dx}{\int E dx} \end{cases}$
 $M_z = - \int (y-y_0) \sigma_{xx} dx$ $\& \quad M_y = \int (z-z_0) \sigma_{xx} dx$
 $M_z = E I_{zz} \frac{d^2 Dy}{dx^2} + E I_{yz} \frac{d^2 Dz}{dx^2}$ $\& \quad M_y = -E I_{yz} \frac{d^2 Dy}{dx^2} + E I_{yy} \frac{d^2 Dz}{dx^2}$ $\leftarrow \text{Beam is homogen -ous}$
 $\begin{Bmatrix} M_z \\ M_y \end{Bmatrix} = E \begin{bmatrix} I_{zz} & I_{yz} \\ I_{yz} & I_{yy} \end{bmatrix} \begin{Bmatrix} \frac{d^2 Dy}{dx^2} \\ \frac{d^2 Dz}{dx^2} \end{Bmatrix} \Rightarrow E \begin{Bmatrix} \frac{d^2 Dy}{dx^2} \\ \frac{d^2 Dz}{dx^2} \end{Bmatrix} = \frac{1}{I_{zz} - I_{zz} I_{yy}} \begin{bmatrix} I_{yy} & I_{yz} \\ I_{yz} & I_{zz} \end{bmatrix} \begin{Bmatrix} M_z \\ M_y \end{Bmatrix}$

If I_{yz} is not equal to 0, then what we did till here holds this equation still holds and still i will get y naught as this z naught as this. And then whatever we did till their holds. So, when I_{yz} is not 0 i have u in general given by $-\frac{y}{d} \frac{\delta y}{dx} + \frac{z}{d} \frac{\delta z}{dx} + \epsilon + \delta y$ function of x Ey plus δz function of x Ez , expression field similar to u and v i replace u and v with y and z here remains are same.

Then M_y σ_{xx} would be $-\epsilon \frac{y}{d} \frac{\delta y}{dx} + \frac{z}{d} \frac{\delta z}{dx}$ square plus z minus z naught times $\frac{\delta z}{dx}$ square. This will be M_y stress and then the condition that $\int \sigma_{xx} dx$ has to be 0 would imply that y naught is given by $\int E y dx$ here are not assumed the beam is homogeneous $E dx$ and $M_y z$ naught would be $\int E z dx$ by $\int E dx$. This will get from this equation and then you have moment equation M_z to be given by $-\int y \sigma_{xx} dx$ from our definition the very first class when we began the beam bending problem, this will be the definition of M_z and you are definition of M_y as $\int z \sigma_{xx} dx$ right ax .

Now, this will tell us that M_z is given by $E I_{zz} \frac{\delta z}{dx} + E I_{yz} \frac{\delta y}{dx}$ and M_y would be given by $E I_{yz} \frac{\delta y}{dx} + E I_{yy} \frac{\delta z}{dx}$. This assumes beam is homogeneous. That is made of the same material there is no difference in tension and compression or there is no difference of materials in tension and compression.

Now, what I have to do is i have to solve these 2 equations to get $\frac{\delta y}{dx}$ and $\frac{\delta z}{dx}$ in terms of M_y and M_z . So, there will be a negative sign in here. So now, to solve this equation i class it in this following form $M_z M_y$ is equal to E times $I_{zz} I_{yz}$ minus $I_{yz} I_{yy}$ into $\frac{\delta y}{dx} \frac{\delta z}{dx}$ square.

Now, I invert this 2 by 2 matrix from here i get $\frac{\delta y}{dx} \frac{\delta z}{dx}$ into E is $\frac{1}{I_{zz} I_{yy} - I_{yz}^2}$ times $M_z I_{yy} - M_y I_{yz}$ into I_{zz} into $M_z M_y$.

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$$E \frac{d^2 \Delta y}{dx^2} = \frac{I_{yy} M_z + I_{yz} M_y}{I_{zz} I_{yy} - I_{yz}^2} \quad \alpha \quad E \frac{d^2 \Delta z}{dx^2} = - \frac{I_{yz} M_z + I_{zz} M_y}{I_{yy} I_{zz} - I_{yz}^2}$$

$$\Delta_{yi} = -(y-y_0) \left(\frac{I_{yy} M_z + I_{yz} M_y}{I_{yy} I_{zz} - I_{yz}^2} \right) + (z-z_0) \left(\frac{I_{yz} M_z + I_{zz} M_y}{I_{yy} I_{zz} - I_{yz}^2} \right)$$

Special Case: $I_{yz} = 0$

$$\Delta_{yi} = -(y-y_0) \frac{M_z}{I_{zz}} + (z-z_0) \frac{M_y}{I_{yy}}$$

Now from here I get that $d^2 \Delta y / dx^2 = (I_{yy} M_z + I_{yz} M_y) / (I_{zz} I_{yy} - I_{yz}^2)$ and $E d^2 \Delta z / dx^2 = -(I_{yz} M_z + I_{zz} M_y) / (I_{yy} I_{zz} - I_{yz}^2)$.

So, here found these 2 now going back to the expression for the stress σ_{xx} will get it as $\sigma_{xx} = -y \Delta_{yi} + z \Delta_{zi}$. Here and I comes because it is minus $y \Delta_{yi}$ plus $z \Delta_{zi}$ into E times $d^2 \Delta y / dx^2$ that negative sign comes here. Here this is minus E times $z \Delta_{zi}$ plus $y \Delta_{yi}$ by $d^2 \Delta z / dx^2$ and hence this negative sign does not propagate into here. So, that is the expression was stress.

Now, let us look at special cases let us look at the case where I_{yz} is 0. Special case where I_{yz} is 0 then your expression was σ_{xx} becomes $\sigma_{xx} = -y \Delta_{yi} + z \Delta_{zi}$. This is the same expression that we got in your it is same expression that we got in your for σ_{xx} except that u and v roles are change to y and z . Now except that u and v roles are change to y and v , now u is y v is z . So, this M_z by I_{zz} as a negative sign from see that M_z by I_{zz} as a negative sign in here. So, this same as what we got there. So, it is consistent now.

The second special case that we are going to consider is when there is only along one direction case 2.

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The image shows a series of handwritten equations on a whiteboard background. At the top, there are two equations for the normal stress components σ_{xx} and σ_{yy} in a rotated coordinate system, both expressed as $\frac{d^2}{dx^2}$ terms. The first equation is $\sigma_{xx} = \frac{I_{yy} M_z + I_{yz} M_y}{I_{yy} I_{zz} - I_{yz}^2} + (z - z_0) \frac{I_{yz} M_z + I_{zz} M_y}{I_{yy} I_{zz} - I_{yz}^2}$. Below this, a 'Special case' is noted where $I_{yz} = 0$, leading to the simplified equation $\sigma_{xx} = -(y - y_0) \frac{M_z}{I_{zz}} + (z - z_0) \frac{M_y}{I_{yy}}$. A second case is noted as 'Case 2' where $I_{yz} \neq 0$ but $M_y = 0$, resulting in $\sigma_{xx} = -(y - y_0) \frac{I_{yz} M_z}{I_{yy} I_{zz} - I_{yz}^2} + (z - z_0) \frac{I_{zz} M_z}{I_{yy} I_{zz} - I_{yz}^2}$.

I_{yz} not equal to 0, but M_y is 0 applied force along only one direction, but I did not apply it about the principal direction now σ_{xx} would be minus y minus y naught M_y is 0. So, I have I_{yy} divided by $I_{yy} I_{zz}$ minus I_{yz} squared into M_z plus z minus z naught into I_{yz} into M_z divided by $I_{yy} I_{zz}$ minus I_{yz} squared. So now, this is where you have only one moment M_z moment, but the stress where is both along y and z direction.