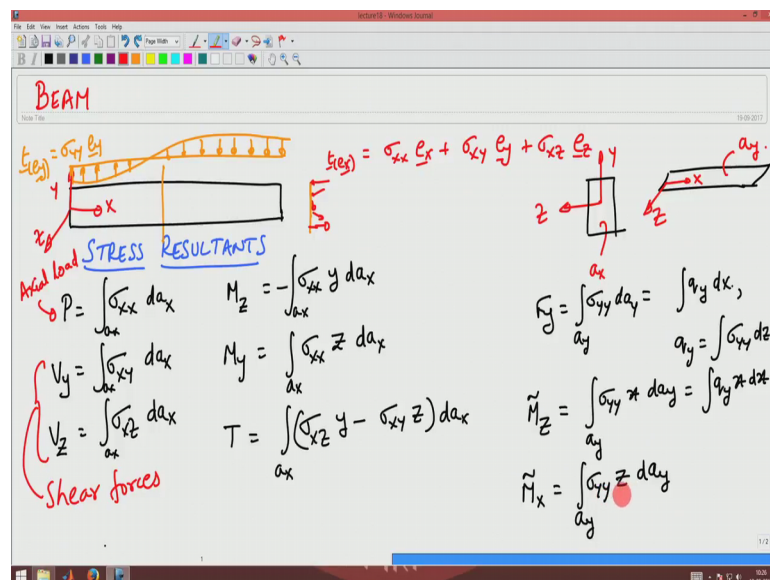


Mechanics of Material
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Displacement due to uniaxial loading, temperature and bending
Lecture - 50
Displacement Field

Welcome to the 18th lecture in mechanics of materials, in the last lecture we started looking at how a beam will deform and what are the stresses that the beam develops, in particular we are looking at the stresses that the beam would have.

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In particular what we did was, we exposed a cut surface or we introduced a cut surface in the beam and we exposed the traction vector that is acting on that beam, the cut surface was essentially a cut surface along the x direction with the normal in the x direction as shown here and then we wrote what are the stress resultants and we wrote the global movements and forces are acting on the beam on various cut surfaces and the boundary of the body.

In particular, we saw that, we said that these are acting only on the top surface of the beam that is on the positive y direction normal along there is some stresses acting on the beam that too there was only a sigma y y component of the stress acting on that surface that is apply loading and then when you introduce a cut in the beam, somewhere

here, we saw that the traction is acting on the beam, we saw that the traction that is acting on the beam will change its magnitude as well as the direction, as shown here.

In general that traction was given by an expression like this, which is a usual expression you get when you have e_x as e normal to the cut. Now, this traction starting over an area given by ax , wherein it is assumed here to be a rectangular cross section with y and z over into like that. That is, it is acting on a cut surface here for example, if you take this as the beam, this cross section area is where the σ_{xx} acts, σ_{xy} acts and σ_{xz} acts.

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This is a beam where loading is like this, loading on a top phase. So, basically what is happening is the beam is bending like this. So, what are the stress resultants for that, the stress resultants are the net force and net moment that will act at the cut surface because of this traction. The net force that is acting in the axial direction is given by P which is a σ_{xx} is $d a_x$, the shear forces V_y and V_z are the shear forces, these are the shear forces this is the axial load.

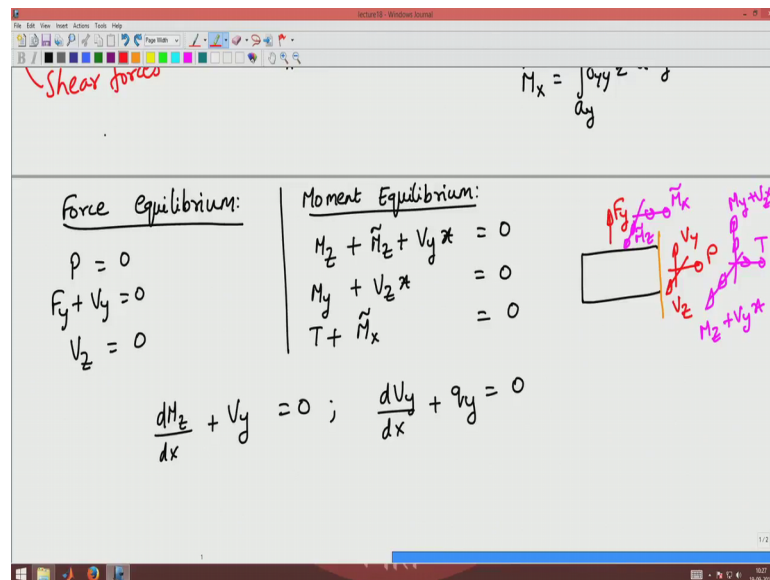
So, basically the shear forces V_y in a cut surface acts like this and the shear force V_z in the cut surface acts like this, the actual force P acts in this direction. So, those are the stress resultants; those are stress force resultants. Similarly, you have stress moment resultants, which is the torsional moment T which is given by this expression in here and then you have the moment M_z acting along this direction given by this expression here,

the moment M_c given by this expression here, which is a moment. So, basically this is y , this is x and this is z . So, M_c moment will produce a deformation something like this, this is a M_z moment deformation.

M_y moment on the other hand will produce a moment like this, you can see, it deforms in the plane. M_z moment produces a moment like this wherein the deformation would be like this. m_z is like this, M_y produces a moment which is like this in the plane, the moment M_y produces in plane deformations and then due to the attraction force acting on the boundary of the body, the y direction wherein that area is given by a_y , it spans in the xz plane, there the net force $F_c f$ is given by this expression, where in we introduce unassembled q_y , this is the integration of this.

σ_{yy} over the width of the cross section that is over this width you are integrating what are stress that is coming in and your net force per unit length is given by q_y here, correspondingly that will produce a moment M_z which is q_y to M_6 and M_x which is σ_{yy} times z into a_y .

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Now, we wrote so the net force and the net moment that is acting on a cut surface of the beam is given here, P acting along the axial direction, V_y acting like this, V_z acting like this F acting like this, F_y acting like this and M_z moment acting like this, M_x moment acting like this and then M_x tilde moment acting along on this phase causing it to twist

like this and then M_z moment which is again acting like to deform the beam like this M_z moment.

So, the net equilibrium equation for the force in a moment is given by here, which we manipulated to get these governing equations for the moment and the shear force and the applied loading. Now, if there is a loading on the z plane, then you will have order F_z force and you will have other moments coming in M_y and M_x will come over there on this phase of the beam.

Basically on this phase of the beam, there are to be some loading acting on it, there will be other stresses that are coming in. So, there will be other stresses that are coming in, if there is some force acting on this surface of the beam, we consider only forces to act on this surface that too only transverse normal to the surface. We did not add any shear stress in this direction or in this direction acting on the surface, we had only normal stress acting on the surface.

That is a basic recommend for a beam to behave like a beam; for a member to behave like a beam. So, basically if it were to bend like this, I have to apply some force here, you can say I am applying some force in this direction for it to bend like that. Then, there will be some other forces and moments coming because of the boundary force, boundary traction is acting on this surface.

So, this is a special case that we are considering, we are considering only first start on the top surface of the beam. If there are force acting in a bottom surface, again you have to include that and you have to rework all the equation that we have derived till now. So, basically this is the governing equation where we stopped in last class, let us proceed further. I am interested in estimating this stresses σ_{xx} in this course, in this lecture.

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$\rho = 0$
 $F_y + V_y = 0$
 $V_z = 0$
 $M_y + V_z \cdot x = 0$
 $T + \tilde{M}_x = 0$
 $M_z + \tilde{H}_z + V_y \cdot x = 0$
 $\frac{dM_z}{dx} + V_y = 0$; $\frac{dV_y}{dx} + q_y = 0$

Estimate the stress σ_{xx} :

Estimate the stress σ_{xx} , this is the aim of this lecture today. So now, as I told you, you add a beam, you add a beam like this.

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$u = -\frac{d}{dx} (y - y_0) e_x + \frac{d^2}{dx^2} e_y$

Plane section normal to the neutral axis remains plane and normal to the neutral axis

Neutral axis: The line about which the stress (σ_{xx}) is zero

$\tan(\theta) = \frac{d}{dx}$
 $\tan \theta \approx \theta$

$\sigma_{xx} = |\theta (y - y_0)|$
 $\sigma_{xx} = -\frac{d}{dx} (y - y_0)$

I am going to represent the beam using a 1 dimensional representation that is I am going to represent the central axis of the beam alone. That is, if this is a central axis of the beam, I am going to represent this beam using the central axis alone. The central axis due to the application of a load, some load acting like this, some load acting like this, would deform some load acting like this, would deform into some curved shape like that.

Now, let us look at a cut surface, this cut surface there that is this surface here, what we are going to assume is, we are going to assume this cut surface how it deforms, all this blue cut surface deforms. So, we are going to assume, how this plane sections will deform, how this blue line is going to deform. So, basically what we are saying is plane sections normal to the neutral axis remain plane and normal to the neutral axis.

Here I use the word neutral axis, what this word neutral axis means is, neutral axis means this red line is a neutral axis here, the line about which the stress is, the stress σ_x is 0. We will see, once we derive we will see why such a axis will exist in a beam, but for now, let us assume that there exists such axis called a neutral axis, our stress goes to 0 and I am giving a cut perpendicular to that neutral axis in the initial configuration or the reference configuration.

After it deforms, what happens is, this blue line will become into some blue line here. So, the tangent to this line at that point, times the line at that point let us say makes an angle θ with the horizontal, measured in the clockwise direction, this is θ measured in the clockwise direction. Let us zoom in here and draw an exaggerated figure. I have the surface, I have tangent to that surface at that point, I have the blue line which is perpendicular to that let us say this makes an angle θ , then the angle made by this, this 90 degrees, the tangent because I assume plane sections remain plane a normal to the neutral axis.

So, initially it was 90 degrees here and then should be 90 degrees here too. So, this angle will become θ , then this displacement along the x direction, this u of x is given by θ into y minus y naught, where y naught is, say I add my coordinate system already like this y, z , this location of the neutral axis is y naught and any other location here as a distance y from the x axis.

So, u of y is θ into y minus y naught. Now, if my vertical deflection here is, this vertical deflection down here is δ , δ is a function of x ; δ is some function of x because you see that, as I bend the beam, the vertical deflection is not same at different points, the vertical deflection varies along the axis of the beam, hence this δ as a function of x .

So, δ is a function of x , then what will this θ be? This θ is going to be, \tan of the θ is going to be $d\delta$ by dx , from you know that slope of a line is given by the

tangent of, the curve at a point is given by the derivative of the function with respect to x . You know that, the tangent at a given point is given by the derivative of the function with respect to the x , so θ is this.

Now, that is a catch though here on what you substitute for θ , we are assuming small deformations. So, $\tan \theta$ is approximated as θ and then here the deformation is in the clockwise, the rotation is in the clockwise direction. In other words, the θ that I will get will be negative in this case, but I want a positive displacement because it is deforming in the positive x direction. Since I want a positive direction, I have to put a absolute sign here, which means the θ that I get will be negative, to make it positive I have to write it as u of x as $-\frac{d\delta}{dx}$ into $y - y_0$, into $y - y_0$ naught this what I will get here.

Now, let us look at different section, let us look at a section at this side, now the tangent to that point here is something like that. Now, the cut surface deforms parallel remains plane and perpendicular the to the normal, so it will be like this, it will be like that. Now, what happens at the surface, that θ that you measure, this is a θ that you get from differentiating δ with respect to x that is a positive θ .

Now, for this positive θ what happens, the deformation is in the negative x direction you can see that right, the deformation is in negative x direction here, it is in this negative x direction this is u of x . So, when δ is positive you are automatically getting that then displacement is not negative (Refer Time: 17:03). So, you have the negative sign put in here, remember y is greater than y_0 , since we are looking at a point above the neutral axis.

If a point is below the neutral axis $y - y_0$ would be negative and it will be positive in this case for positive $\frac{d\delta}{dx}$ which is right because at the bottom you have a displacement u_x star which is the power along the positive x direction, so u_x is given by this expression here. In general, now u the displacement vector is given by $u_x e_x$ that is $-\frac{d\delta}{dx}$ into $y - y_0$ e_x plus $\frac{d\delta}{dx}$ is a function of x into e_y , to be more specific let us write it as δ of y , being a y component or the displacement.