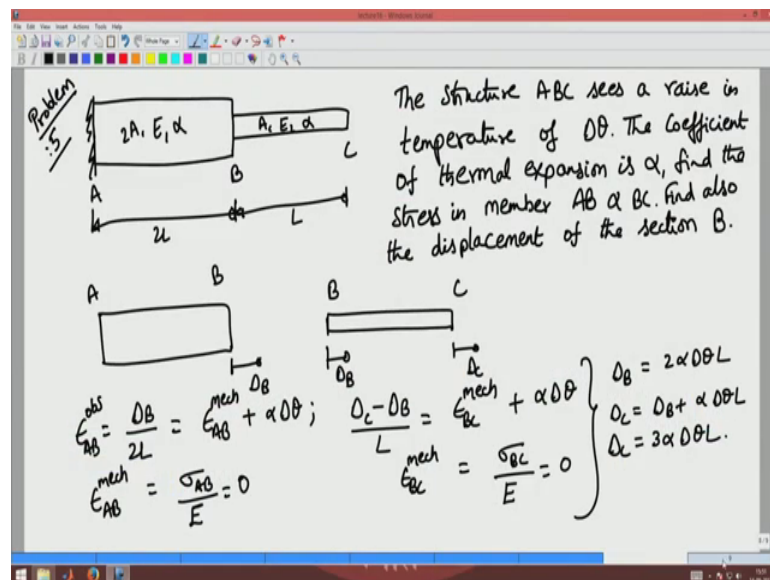


**Mechanics of Material**  
**Dr. U. Saravanan**  
**Department of Civil Engineering**  
**Indian Institute of Technology, Madras**

**Displacement due to uniaxial loading, temperature and bending**  
**Lecture – 47**  
**Stepped shaft subjected to raise in temperature**

Now, having seen this; next let us move on to thermal stresses.

(Refer Slide Time: 00:26)



So, I have the same stepped shaft A, B, C,  $2A$ ,  $E$ ,  $A$  of cross section Young's modulus  $E$ . This length is  $2L$  and this length is  $L$ ; this problem 5. These are subjected to raise in temperature of  $\Delta\theta$ . Structure ABC sees a raise in temperature of  $\Delta\theta$  and the coefficient thermal expansion is  $\alpha$  for both. The coefficient of thermal expansion is  $\alpha$ , find the stress in member AB and BC.

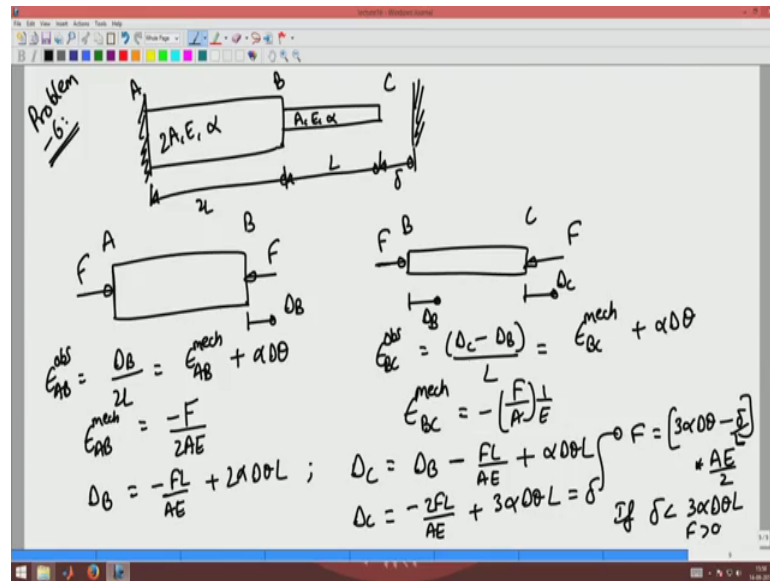
Now, how will you solve this problem? There is no applied force here. Just the temperature of the structure increases by  $\Delta\theta$ . Apart from the stress, I want to find also the displacement of the section B. I want to see by how much this section B moves and I want to find what will be the stresses in member AB and BC. Now, what can you say? When temperature raises, A is fixed? So, it cannot move. B will move by  $\Delta_B$ . This AB, BC, B moves by  $\Delta_B$  and C moves by  $\Delta_C$ .

There is no force applied. So, what will be the observed strain? Observed strain would be  $\frac{\Delta B}{2L}$  (Refer Time 03:52) of the member. This will be equal to  $\epsilon_{\text{mechanical}} + \alpha \Delta \theta$ , which is the thermal strain along the direction, axial direction for AB is mechanical strain in member AB. Similarly, for BC the strain would be  $\frac{\Delta C - \Delta B}{L}$ . That is coming from a strain displacement relationship difference B moves by  $\Delta B$ . C moves by  $\Delta C$ . So, the strain would be difference between displacement of C and B.

So, there is  $\frac{\Delta C - \Delta B}{L}$  by the length of the member which is L. This will be equal to the mechanical strain in BC plus  $\alpha \Delta \theta$  which is again this strain in member BC to the thermal effects. Now, since there is no force applied in AB, what will be the mechanical strain AB? Mechanical strain AB from the constitutive relation would be the stress in AB by the Young's modulus E. Since, there is no force applied in member AB; this stress is going to be 0.

Similarly, the mechanical strain in member BC would be the stress in BC by the Young's modulus. I am applying no force in this member BC. So, the stress in member BC would be 0 and this will also be 0. From this I get  $\Delta B$  to be equal to  $2\alpha \Delta \theta L$  and  $\Delta C$  would be  $\Delta B + \alpha \Delta \theta L$  which will be  $3\alpha \Delta \theta L$ . That is  $\Delta C$ . That is the change in cross section does not matter. The total length of the member is  $3L$ . The elongation at point C would be  $3L$  times  $\alpha \Delta \theta$ . Now, let us solve the final problem of this lecture which will be problem number 6.

(Refer Slide Time: 06:30)



This is same as problem 5 except that I have restrained at C. Just like in problem 3, I have this distance given by delta; this is A, B, C; this as  $2A$  as state of cross section  $E$  as Young's modulus;  $\alpha$  is a question of thermal expansion  $A$ ,  $E$   $\alpha$  for BC. This has a length  $2L$  and this has a length of  $L$ . BC as length of  $L$ . Now, I heat it. Now, what happen? Until delta, the temperature change is such that the total elongation of the member is delta. There would not be any force coming in; this will be same as problem 5.

Now, after the gap closes there will be mechanical stress arising. Because there will be a compressive force coming at C which will propagate and it will change the entire dynamics of the problem. So, basically how do you solve this problem? You assume again as we did in problem 3. That the gap is closed to the change in temperature and then what you do is you draw a free body diagram AB, BC. There is a compressive force  $F$  applied here. There arises another compressive force  $F$ .

There will be by continuity at B, there should be a compressive force  $F$ . Here and  $F$  here too; so, since I assumed  $F$  here and I do not know what this  $F$  is. I have to find the  $F$  such that the displacement of point C is delta. They find  $F$  such that the displacement of point C is delta not more than delta. Now, again I write the same equations. I assume delta B this moves by delta B. These moves by delta B and these moves by delta C. Same

things I write as before. This observed strain in member AB is  $\frac{\Delta B}{2L}$ . That will be equal to the mechanical strain in AB plus  $\alpha \Delta \theta$ .

Similarly, the observed strain in member BC would be  $\frac{\Delta C - \Delta B}{L}$  which will be equal to the mechanical strain in BC plus  $\alpha \Delta \theta$ . Now, the mechanical strain in member AB would be  $-\frac{F}{2AE}$ . There will be a mechanical strain in member AB.  $\frac{F}{A}$  is if stress in member AB, the stress by strain  $\frac{F}{2A}$  will be the strain in member AB.  $\frac{F}{2A}$  will be the stress in member AB and that stress divided by the Young's modulus will give me the strain in member AB. Similarly the mechanical strain in BC is given by  $\frac{F}{A} \frac{1}{E}$ . The stress in member BC divided by the Young's modulus of member BC.

Now, substituting this back in there, I get  $\Delta B$  to be  $-\frac{FL}{AE} + 2L\alpha \Delta \theta$  and I get  $\Delta C$  to be  $\Delta B + \frac{FL}{AE} - \frac{FL}{AE} + \alpha \Delta \theta$  into  $L$ . Substituting for  $\Delta B$ . This will be  $-\frac{2FL}{AE} + 3\alpha \Delta \theta$  into  $L$  would be  $\Delta C$ . We know from the comparability condition that the displacement of point C cannot exceed  $\Delta$ . So, this will be equated to  $\Delta$  and from this equation we obtain  $F$  as  $\frac{3\alpha \Delta \theta L - \Delta AE}{L}$ . From this you get  $F$  as  $\frac{3\alpha \Delta \theta L - \Delta}{2L} AE$ .

We will get  $F$  as that and from here is clear that if  $\Delta$  is less than  $3\alpha \Delta \theta L$ , then  $F$  would be positive and that is a case that we want. If  $F$  is become negative then what happens is, it is not possible.  $F$  cannot be a tensile stress in member BC. When the temperature increases the members can be only in compression and it cannot be in tension.

So, you from the physical argument you see that  $\Delta$  has to be less than  $3\alpha \Delta \theta L$  and that is a condition when  $F$  will be greater than 0. If  $F$  have to be less than 0, if  $\Delta$  where to be less than  $3\alpha \Delta \theta L$ . Then the force  $F$  would be less than 0. Not possible physically. Possible physically hence limit  $F$  to be equal to 0.

(Refer Slide Time: 13:33)

Handwritten derivations on a whiteboard:

$$\epsilon_{AB}^{obs} = \frac{D_B}{2L} = \epsilon_{AB}^{mech} + \alpha \Delta \theta$$

$$\epsilon_{AB}^{mech} = \frac{-F}{2AE}$$

$$D_B = \frac{-FL}{AE} + 2\alpha \Delta \theta L$$

$$\epsilon_{BC}^{obs} = \frac{D_C - D_B}{L} = \epsilon_{BC}^{mech} + \alpha \Delta \theta$$

$$\epsilon_{BC}^{mech} = -\left(\frac{F}{A}\right) \frac{1}{E}$$

$$D_C = D_B - \frac{FL}{AE} + \alpha \Delta \theta L$$

$$D_C = \frac{-2FL}{AE} + 3\alpha \Delta \theta L = \delta$$

$F = \left[ \frac{3\alpha \Delta \theta - \frac{\delta}{L}}{\frac{2}{AE}} \right]$   
 If  $\delta < 3\alpha \Delta \theta L$  then  $F < 0$ , not possible physically hence limit  $F = 0$

So, that is how you solve this problem. Just like what we did for problem 3; same arguments here to solve for problem 6. So, what we have seen in today's class is some 6 different (Refer Time 13:53) problems involving actual members. The first 3 were all the same type, where in you have only 4 separate on a homogenous bar (Refer Time 14:03) which are different cross sectional areas. In problem 4 we saw a bar, which is inhomogeneous made of two different materials and in problem 5 and 6; we looked at effect of thermal strains or what is the effect of change in temperature on these structures?

Thank you.