

**Soil Dynamics**  
**Professor. Paramita Bhattacharya**  
**Department of Civil Engineering**  
**Indian Institute of Technology, Kharagpur**  
**Lecture - 6**  
**Single Degree of Freedom System (SDOF) - Part 4**

Hello friends. Today we will continue our discussion on Single Degree of Freedom System.

(Refer Slide Time: 0:35)

**Free Vibration**  
(With Viscous Damping)

**Recapitulation**

➤ For under-damped system:  $z = e^{-\omega_n D t} [A_1 \sin \omega_d t + A_2 \cos \omega_d t]$

$\omega_d = \omega_n \sqrt{1 - D^2}$  — Damped Nat. Freq.  
 $\omega_n$  — Undamped Natural frequency of a system  
 at  $t=0$   $z = z_0$   
 $\dot{z} = \dot{z}_0$

Fig. 6.1 Response of under-damped free vibrating system

➤ Logarithmic decrement:  $\delta = \ln \left( \frac{z_1}{z_2} \right) = \frac{2\pi D}{\sqrt{1-D^2}} = \frac{1}{n} \ln \left( \frac{z_1}{z_{1+n}} \right)$

So, last week we have studied free vibration system under different damping condition. First we have studied if the system is undamped and thereafter we have studied if the system is damped with viscous damping and that time we have three different cases of damped system for viscous damping; one is called the over-damp system, the second one is called critically damped system and the third one was the under-damped system.

So, in under-damp system, system we have seen the general equation for vibration is represented by Z is equal to e to the power minus omega n D t times A1 sin omega Dt plus A2 cosine omega Dt. What is omega D here? Omega D was omega n times square root of 1 minus D square that is how we can calculate omega D.

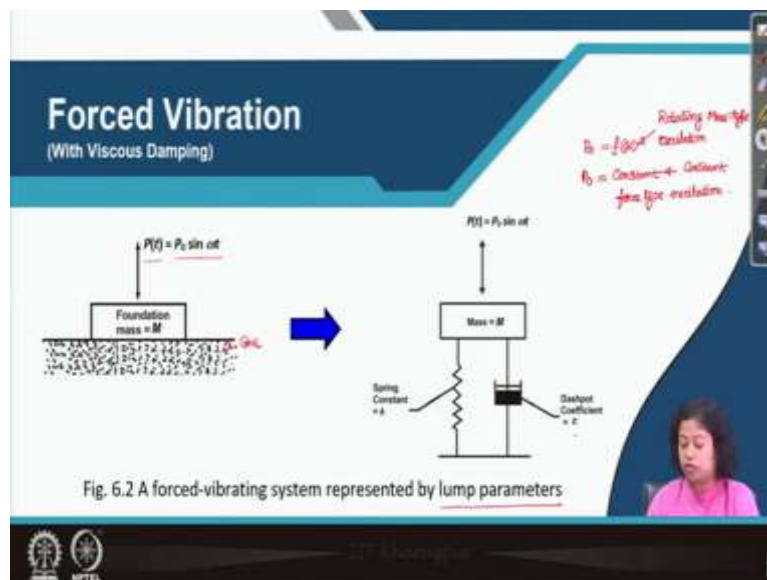
However, this omega D is called damped natural frequency, damped natural frequency. What is omega n? Omega n is called undamped natural frequency of a system and D is the damping ratio. Now, you can see here the response curve for Z versus t for under damped system. So, in these equation there are two unknown terms, one is A1 and the second one is A2. So, how we can calculate or determine A1 and A2?

If we know the boundary conditions, then we can easily calculate  $A_1$  and  $A_2$ . So, how we will set the boundary condition for an example for the vibration which is shown in figure 6.1? If you see at time  $t$  equals to 0, we can see what is the mag, what is the value of  $Z$ . Here we can take this  $Z$  which is probably  $Z_0$  may be defined by  $Z_0$ , so at time  $t$  equals to 0,  $Z$  is  $Z_0$ .

Likewise, at time  $t$  equals to 0, if we know the velocity which is  $\dot{Z}$  we can write  $\dot{Z}$  is equal to  $V_0$ , so the velocity also at this point is  $V_0$ . If we set these two, if we satisfy these two boundary conditions in this equation, we will get the value of  $A_1$  and  $A_2$ . So, you can give a try to get  $A_1$  and  $A_2$  in this way.

Then we have studied the logarithmic decrement which is  $\delta$  here which is the ratio of the two consecutive amplitudes in natural log scale and that can be expressed in terms of damping ratio by this relationship that  $2\pi D$  divided by square root of  $1 - D^2$ .

(Refer Slide Time: 4:44)



Now today we will study forced vibration. So, under forced vibration system is subjected to external loading. So, if you take an example of this foundation having mass  $M$  resting over the soil or ground surface this is our ground surface. So, what we can see here in this case the foundation is subjected to an external force  $P t$  which can be expressed by  $P_0$  times  $\sin \omega t$ .

So,  $\omega$  is the operating frequency of the machine for which this kind of force is applied to the foundation.  $P_0$  is the amplitude of the force. Now, there are two cases, in one case the amplitude  $P_0$  depends upon the frequency or operating frequency of the machine. That means, I can write here as  $P_0$  is a function of  $\omega$ .

In another case, we see that  $P_0$  is constant, it does not depend upon  $\omega$ . So, the second case when  $P_0$  is constant is called constant force type excitation. So, this case is called constant force type excitation. Now, if  $P_0$  is a function of  $\omega$  that means the operating frequency, then we call it as generally these can be happened when two masses in machine are allowed to rotate in opposite direction, that time this kind of situation may be arise.

So, we will see this kind of example later. However, this kind of case is called generally as rotating mass type excitation, as excitation is created, occurred by the allowing rotation of the two masses into different direction if one is rotating in clockwise direction the other will rotate in the anti-clockwise direction or counter clockwise direction.

So, first case we will consider the case for constant force type excitation, that means  $P_0$  is constant, it does not depend upon the operating frequency  $\omega$ . So, this kind of system can be represented by lump parameters like  $k$  and  $c$ ,  $k$  means spring constant and  $C$  is the dashpot coefficient. That means our soil is represented by one spring and one dashpot.

(Refer Slide Time: 8:40)

**Damped Forced Vibration**  
(with Viscous Damping and constant Force type excitation)

Equation of motion of a system subjected to forced vibration with viscous damping is:

$$M\ddot{z} + c\dot{z} + kz = P_0 \sin \omega t$$

Unbalanced force acting on mass 'M' =  $P(t) - kZ - c\dot{Z}$   
 Inertia force =  $M\ddot{Z}$   
 In equilibrium:  $M\ddot{Z} = P(t) - kZ - c\dot{Z} \Rightarrow M\ddot{Z} + c\dot{Z} + kZ = P(t)$

So, in this case first we will see the equation of motion. Here you can see the equation of motion the question you may think or ask that how this equation is coming. So, let us first draw the free body diagram for the mass M, mass M means which represents the foundation so it is resting on the soil.

Now, let us take this is the equilibrium position of the mass, so I am writing equilibrium position by E P. Now, at some time when force is applied to the mass M external force  $P t$  at some time  $t$ , its position is here, so it is going downward direction this time and sign

conventions, as per sign convention which we have followed since beginning downward force means positive, I am writing here if it is upward, then it will be negative.

So, when it is going downward direction because of P t what are the forces or reactions coming from the spring and the dashboard to the mass M? Spring exerts a force of magnitude KZ whereas dashboard exerts a force with magnitude C times Z dot. Now, if we see this free body diagram I am writing here this is the free body diagram of mass M.

Now, if you see what are the unbalanced forces acting on this mass? I am writing here unbalanced forces acting on mass M is or R is unbalanced forces acting on mass in are P0 sin omega t or I can write actually it is better if I write P t, so P t minus KZ minus C Z dot, KZ spring force C Z dot force from the dashboard and P t is the external force acting on the mass M.

Now, what is the inertia force in this case? M Z two dot. So, inertia force should be equal to the unbalanced force, so I can write here, in equilibrium plus or I can I jump to one step better I should write step wise, M Z two dot which is inertia force is equal to the unbalanced force acting in the system.

So, now we can get the general equation of motion which says M Z two dot plus C Z dot plus KZ is equal to P t which is the external force, Z two dot is the acceleration, Z dot is velocity in this case. So, what I have written in equation 1 in this way we can derive. Now, we need to know the general solution for this equation 1.

(Refer Slide Time: 13:47)

The image shows a whiteboard with handwritten mathematical derivations. The equations are as follows:

$$M\ddot{z} + c\dot{z} + kz = P(t) \quad (1) \quad \ddot{z} + c\dot{z} + kz = 0 \rightarrow$$

Particular Solution for Eq (1)

$$z_p = A_3 \sin \omega t + A_4 \cos \omega t = Z_p \sin(\omega t - \phi)$$

$$Z_p = \sqrt{A_3^2 + A_4^2}$$

$$\dot{z}_p = A_3 \omega \cos \omega t + A_4 \omega (-\sin \omega t) = A_3 \omega \cos \omega t - A_4 \omega \sin \omega t$$

$$\ddot{z}_p = A_3 \omega^2 (-\sin \omega t) + A_4 \omega^2 (-\cos \omega t) = -A_3 \omega^2 \sin \omega t - A_4 \omega^2 \cos \omega t$$

Eq (1) as

$$M(-A_3 \omega^2 \sin \omega t - A_4 \omega^2 \cos \omega t) + c(A_3 \omega \cos \omega t - A_4 \omega \sin \omega t) + k(A_3 \sin \omega t + A_4 \cos \omega t) = P(t)$$

$$\left[ (k - M\omega^2)A_3 - c\omega A_4 \right] \sin \omega t + \left[ c\omega A_3 + (k - M\omega^2)A_4 \right] \cos \omega t = P_0 \sin \omega t$$

For that let us come to the board. So, first I am writing the equation  $M \ddot{z} + C \dot{z} + Kz = P \sin \omega t$  this is the equation for which we are interested to find out the solution. Earlier we have determined the general solution for free vibrating system with viscous damping and the equation of motion for the free vibrating system was  $M \ddot{z} + C \dot{z} + Kz = 0$ .

Now, what is the difference between equation 1 and the equation written on the right hand side? This equation is homogeneous equation whereas; the equation 1 has a particular solution because of the non-zero right hand side. So, in such case what we need to do, we will write first that, we will assume general solution, so in this case it is a particular solution for equation 1, so I am writing it as small  $z_p$ , let me write it as small  $z$ , small  $z_p$  is the particular solution for equation 1.

And we can write it as  $A_3 \sin \omega t + A_4 \cos \omega t$  or otherwise we can write it as capital  $Z_P \sin(\omega t - \alpha_P)$ ,  $\alpha_P$  is phase angle, capital  $Z_P$  is the amplitude of vibration. So, if I am interested to write in terms of  $Z_P$ , then I can write  $Z_P$  also in that means capital  $Z_P$  also in terms of  $A_3$  and  $A_4$ . What will be that capital  $Z_P$  is equal to square root of  $A_3^2 + A_4^2$ .

Now, what we need to do? We need to find out the final form. So, here we have assumed  $Z_P$  which is sum of two periodic motion  $A_3 \sin \omega t$  which is a periodic harmonic motion,  $A_4 \cos \omega t$  is another harmonic motion and both have same frequency also. So, now from this that means this one we can write small  $\dot{z}_p$ , small  $\dot{z}_p$  that means velocity component that is equal to  $A_3 \omega \cos \omega t + A_4 \omega \sin \omega t$ .

Then acceleration can be written as  $A_3 \omega^2 \sin \omega t - A_4 \omega^2 \cos \omega t$ . I can rewrite these two once again here, so  $A_3 \omega \cos \omega t - A_4 \omega \sin \omega t$ , likewise this one  $Z_P \ddot{z}_p$  I can write as  $A_3 \omega^2 \sin \omega t - A_4 \omega^2 \cos \omega t$ .

Now, I will use these  $\dot{z}_p$  and  $\ddot{z}_p$  in equation 1. So, we can rewrite equation 1 as  $M \ddot{z}_p - A_3 \omega^2 \sin \omega t - A_4 \omega^2 \cos \omega t + C \dot{z}_p + Kz_p = P \sin \omega t$ , sorry, plus  $C$  times  $A_3 \omega \cos \omega t - A_4 \omega \sin \omega t$  plus we have at third term  $Kz_p$ , so for  $Kz_p$  I can write here as  $K Z_P$  which is, here I can write it as particular solution for equation 1, it will probably look better.

So, now the third term on the left hand side can be written as  $K$  times  $A_3 \sin \omega t$  plus  $A_4 \cos \omega t$  and that is equal to your  $P t$ . So, now what we will do here? If you see what was actually  $P t$ ,  $P t$  is nothing but  $P_0 \sin \omega t$ . So, we can rewrite the expression which I have just written down once again like  $P t$  will be replaced by  $P_0 \sin \omega t$  and all the components of  $\sin \omega t$  will be taken together and the, and all the coefficient component means coefficient, all the coefficient of  $\sin \omega t$  will be taken together and all the coefficient of the  $\cos \omega t$  will be taken together on the left hand side. Whereas, in the right hand side we will write  $P t$  as  $P_0 \sin \omega t$ .

So, let me do that, first I would like to mark the terms having  $\sin \omega t$  here this one and this one. So, now I can write it as  $K - M \omega^2 A_3 \sin \omega t - C \omega A_4$ , now I can use whole multiplied with  $\sin \omega t$  plus same way I will write the coefficient of  $\cos \omega t$  here.

So, the coefficient of  $\cos \omega t$  that is multiplying with  $A_3$  that I am writing first so that is  $C \omega$  this one then I can write the those coefficients which are multiplying with  $A_4$ , that means now I will write plus  $K$ , here I have to write  $A_3$ , so  $K - M \omega^2 A_4$  and entire thing is multiplying with  $\cos \omega t$ . So, that is equal to  $P_0 \sin \omega t$ .

So, from this we know we can easily write the coefficient of  $\sin \omega t$  on the left hand side is equal to the coefficient of  $\sin \omega t$  on the right hand side, that will give us one equation. And the second equation we will give, we will get by equating the coefficient of  $\cos \omega t$  on left hand side and the right hand side. In this way, we will get two equations and we have two unknowns which are  $A_3$  and  $A_4$ , so we will get finally  $A_3$  and  $A_4$  in terms of  $K$ , capital  $M$  and  $C$ . So, let us do that.

(Refer Slide Time: 24:26)

$$(k - M\omega^2)A_3 - C\omega A_4 - P_0 = 0 \quad \text{--- (2a)}$$

$$C\omega A_3 + (k - M\omega^2)A_4 = 0 \quad \text{--- (2b)}$$

$$\frac{A_3}{(k - M\omega^2)} = \frac{A_4}{-C\omega} = \frac{P_0}{(k - M\omega^2)^2 + (C\omega)^2}$$

$$\Rightarrow A_3 = \frac{(k - M\omega^2)P_0}{[(k - M\omega^2)^2 + (C\omega)^2]} \quad A_4 = \frac{-C\omega}{[(k - M\omega^2)^2 + (C\omega)^2]} P_0$$

$$Z_p = \sqrt{A_3^2 + A_4^2} = \frac{P_0 \sqrt{(k - M\omega^2)^2 + (C\omega)^2}}{[(k - M\omega^2)^2 + (C\omega)^2]} = \frac{P_0}{R/k}$$

$$M\ddot{z} + c\dot{z} + kz = P(t) \quad \text{--- (1)} \quad \text{--- } M\ddot{z} + c\dot{z} + kz = 0 \quad \text{---}$$

$$P(t) = P_0 \sin \omega t$$

$$\text{Bentuk Solusi jka } E_1(t) \quad z_p = A_3 \sin \omega t + A_4 \cos \omega t = Z_p \sin(\omega t - \phi)$$

$$Z_p = \sqrt{A_3^2 + A_4^2}$$

$$\dot{z}_p = A_3 \omega \cos \omega t + A_4 \omega (-\sin \omega t) = A_3 \omega \cos \omega t - A_4 \omega \sin \omega t$$

$$\ddot{z}_p = A_3 \omega^2 (-\sin \omega t) + A_4 \omega^2 (-\cos \omega t) = -A_3 \omega^2 \sin \omega t - A_4 \omega^2 \cos \omega t$$

$$\text{Eq (1) as } M(-A_3 \omega^2 \sin \omega t - A_4 \omega^2 \cos \omega t) + c(A_3 \omega \cos \omega t - A_4 \omega \sin \omega t) + k(A_3 \sin \omega t + A_4 \cos \omega t) = P_0 \sin \omega t$$

$$[(k - M\omega^2)A_3 - C\omega A_4] \sin \omega t + [C\omega A_3 + (k - M\omega^2)A_4] \cos \omega t = P_0 \sin \omega t$$

So, first one which we can write is  $K$  minus  $M$  omega square times  $A_3$  minus  $C$  omega  $A_4$  is equal to  $P_0$  or I can take  $P_0$  also on the left hand side in such case I will write it as minus  $P_0$  is equal to 0, give it a name 2a. Next equation, so first equation is formed, now next equation will be from this one.

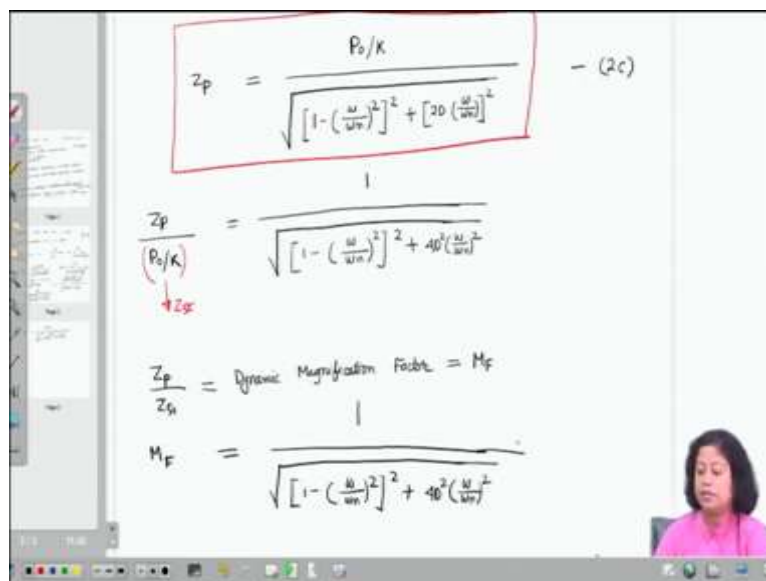
So,  $C$  omega  $A_3$  plus  $K$  minus  $M$  omega square multiplying with  $A_4$ , multiplying by  $A_4$  that is equal to 0. Let us give it 2b, so there are two equations and we have two unknowns. So, from these we can get  $A_3$  and  $A_4$  if we do the cross multiplication. So, easily we can do the cross multiplication and get the solution. So, what will be the final product then?

So, in this way we are getting  $A_3$  is equal to  $K$  minus  $M$  omega square times  $P_0$  divided by  $K$  minus  $M$  omega square whole square plus  $C$  omega whole square and  $A_4$  is equal to  $K$

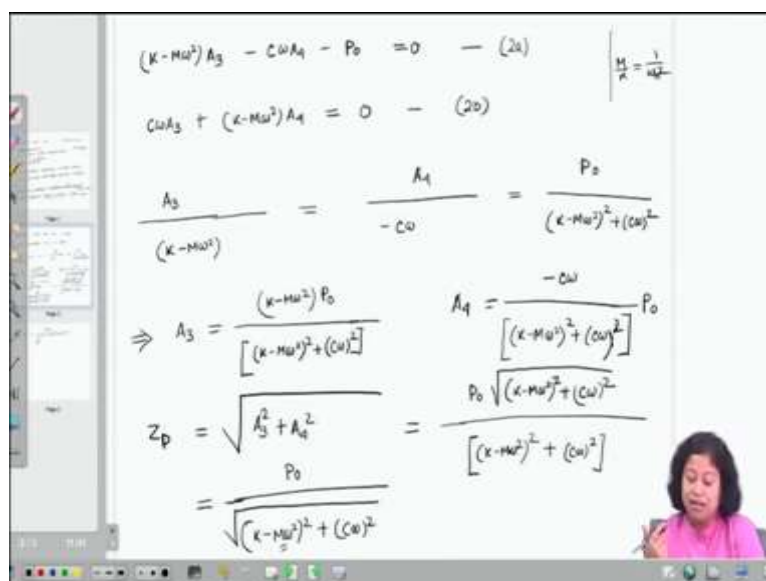
minus, sorry it is not K, it is only minus C. So, minus C omega divided by K minus M omega square whole square plus C omega whole square this whole in multiplying with P0.

So, now we know what is A0, what is A3 and what is A4 in terms of K, M and C and P0. So, from these we can calculate capital ZP which is the amplitude of vibration we already know this is nothing but square root of A3 square plus A4 square. So, it will be your or we can write it as P0 divided by square root of this term. Now, if we take K out of these square root in the denominator, then we can rewrite the same expression that means capital ZP is equal to better I should write it in the next page.

(Refer Slide Time: 28:14)



Handwritten derivation of dynamic magnification factor  $M_F$ . The first equation shows  $Z_p = \frac{P_0/K}{\sqrt{[1 - (\frac{\omega}{\omega_n})^2]^2 + [2D(\frac{\omega}{\omega_n})]^2}}$  labeled as (2c). The second equation shows  $\frac{Z_p}{(P_0/K)} = \frac{1}{\sqrt{[1 - (\frac{\omega}{\omega_n})^2]^2 + 4D^2(\frac{\omega}{\omega_n})^2}}$ . The third equation states  $\frac{Z_p}{Z_{st}} = \text{Dynamic Magnification Factor} = M_F$ . The final equation shows  $M_F = \frac{1}{\sqrt{[1 - (\frac{\omega}{\omega_n})^2]^2 + 4D^2(\frac{\omega}{\omega_n})^2}}$ .



Handwritten derivation of amplitudes  $A_3$  and  $A_4$ . The first equation is  $(k - M\omega^2)A_3 - c\omega A_4 - P_0 = 0$  labeled as (2a). The second equation is  $c\omega A_3 + (k - M\omega^2)A_4 = 0$  labeled as (2b). The third equation shows  $\frac{A_3}{(k - M\omega^2)} = \frac{A_4}{-c\omega} = \frac{P_0}{(k - M\omega^2)^2 + (c\omega)^2}$ . The fourth equation shows  $A_3 = \frac{(k - M\omega^2)P_0}{[(k - M\omega^2)^2 + (c\omega)^2]}$  and  $A_4 = \frac{-c\omega}{[(k - M\omega^2)^2 + (c\omega)^2]}P_0$ . The fifth equation shows  $Z_p = \frac{\sqrt{A_3^2 + A_4^2}}{P_0} = \frac{1}{\sqrt{[1 - (\frac{\omega}{\omega_n})^2]^2 + (2D)^2(\frac{\omega}{\omega_n})^2]}$ .

So, ZP, capital ZP can be written here as P0 by K times square root of I am just going back to the previous equation I will take K out of this square root that means the first term under



square root will be  $1 - \frac{M}{K} \omega^2$ ,  $\frac{M}{K}$  means  $\frac{1}{\omega_n^2}$ ,  $\omega_n$  is the natural frequency of the undamped system. So, basically what I am saying we will get this term which will be  $1 - \omega_n^2$  in this place.

So, this is one way and then in the second term under square root will be  $\frac{C}{K}$  times  $\omega$ . Now,  $\frac{C}{K}$  means we can use the damping ratio and can rewrite this term once again as  $\frac{C}{K}$  means we can write it as  $2D$  divided by  $\omega_n$ . So, let us write it in the next page.

So, what I said I am just trying to write here. So, finally we are getting, sorry so this is our expression, final expression for  $Z_P$ . So, what is  $Z_P$ ? This is the amplitude of vibration. Now,  $P_0$  if the static load is applied to the system of magnitude  $P_0$  then what will be  $\frac{P_0}{K}$ ?  $\frac{P_0}{K}$  will be static deflection of the system. So, now we can write whatever we write, written here if we give a number  $2c$ , then we can write  $2c$  as  $Z$ , capital  $Z_P$  divided by  $\frac{P_0}{K}$  which is equal to square root of  $1 - \omega^2 / \omega_n^2 + 4D^2 \omega^2 / \omega_n^2$ .

Now, as I already said  $\frac{P_0}{K}$  is static displacement, so I can write this term as  $Z_{static}$ , in this way  $Z_P$  by  $Z_{St}$ ,  $Z_P$  is the amplitude of dynamic deflection, whereas  $Z_{St}$  is the static deflection so this ratio is called the dynamic magnification factor, the ratio of the dynamic deflection to the static deflection, maximum dynamic deflection in this case that means amplitude of course is called the dynamic magnification factor which can be represented by  $MF$ . So,  $MF$  is equal to finally  $1$  divided by square root of  $1 - \omega^2 / \omega_n^2 + 4D^2 \omega^2 / \omega_n^2$ .

(Refer Slide Time: 32:19)

**Damped Forced Vibration**  
(with Viscous Damping and constant Force type excitation)

➤ Solution for Eq. (1):

$$Z_p = \frac{P_0/k}{\sqrt{1 - \left(\frac{\omega}{\omega_n}\right)^2 + 4D^2 \left(\frac{\omega}{\omega_n}\right)^2}}$$

➤ The magnification factor:  
or Dynamic magnification factor:

$$M_f = \frac{Z_p}{P_0/k} = \frac{1}{\sqrt{1 - \left(\frac{\omega}{\omega_n}\right)^2 + 4D^2 \left(\frac{\omega}{\omega_n}\right)^2}}$$

The slide includes a video feed of a presenter in the bottom right corner and logos for IITM and IITEL at the bottom left.

So, you can now see in this slide also we get the same thing, here it will be MF, magnification factor or sometime we call it as or dynamic term may be added, dynamic magnification factor.

(Refer Slide Time: 32:46)

**SUMMARY**

In this lecture we discussed the followings:

- ✓ Equation of motion for forced (constant force type excitation) vibrating system with viscous damping
- ✓ Derivation of the response of forced vibrating system with viscous damping
- ✓ Magnification factor or Dynamic magnification factor.

The slide includes a video feed of a presenter in the bottom right corner and logos for IITM and IITEL at the bottom left.

So, finally come to the summary today we discussed the equation of motion for forced vibrating system, forced vibrating system due to constant force type excitation considering viscous damping. Then what we have studied? Then we have studied how to derive the equation of motion for this type of forced vibrating system. Finally, we derived the response and from that the magnification factor or you can call it as dynamic magnification factor.

(Refer Slide Time: 33:34)



So, these are the references which I have used in this discussion. Thank you.