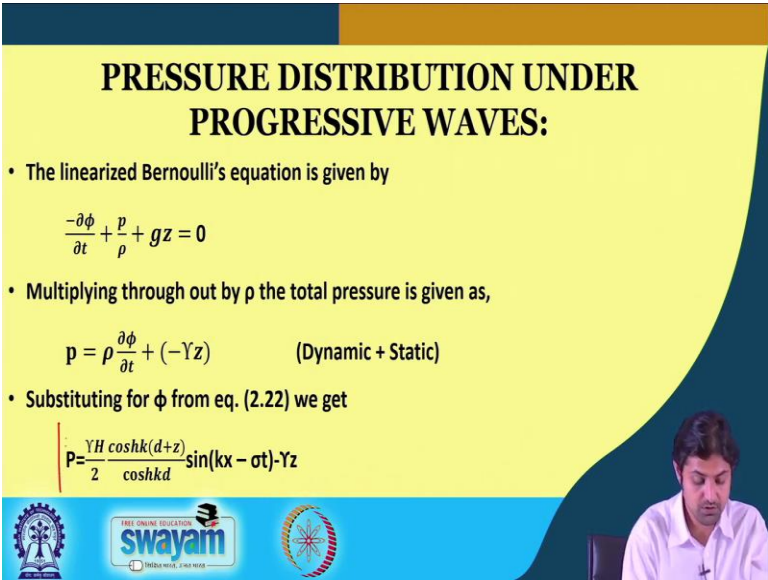


Hydraulic Engineering
Prof. Mohammad Saud Afzal
Department of Civil Engineering
Indian Institute of Technology-Kharagpur

Lecture # 63
Introduction to wave mechanics (Contd.)

Welcome back student to the last lecture of this module and also the last lecture of this course of hydraulic engineering, it has been a pleasure interacting with you. So, to go ahead and get started with this topic of pressure distribution under progressive waves.

(Refer Slide Time: 00:43)



PRESSURE DISTRIBUTION UNDER PROGRESSIVE WAVES:

- The linearized Bernoulli's equation is given by
$$\frac{-\partial\phi}{\partial t} + \frac{p}{\rho} + gz = 0$$
- Multiplying through out by ρ the total pressure is given as,
$$p = \rho \frac{\partial\phi}{\partial t} + (-\gamma z) \quad (\text{Dynamic} + \text{Static})$$
- Substituting for ϕ from eq. (2.22) we get
$$p = \frac{\gamma H}{2} \frac{\cosh k(d+z)}{\cosh kd} \sin(kx - \sigma t) - \gamma z$$

The slide also features logos for IIT Kharagpur, Swayam, and a circular emblem at the bottom.

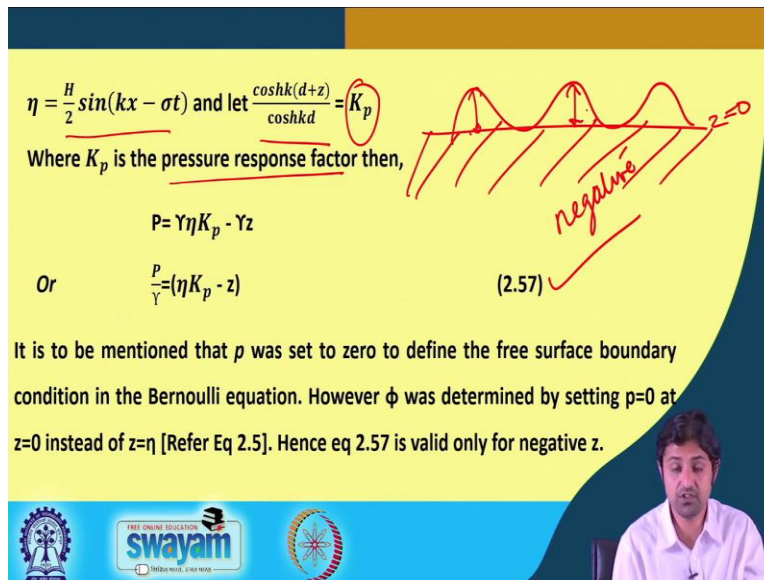
So, you remember we talked about linearized Bernoulli's equation, this equation is given by - $\frac{\partial\phi}{\partial t} + \frac{p}{\rho} + gz = 0$. We avoided that term because of linearization. Now, if you multiply this throughout by ρ the above equation, then the pressure can be given as you see, if we take beyond the other side it can be written as $\rho \frac{\partial\phi}{\partial t} + p = -\gamma z$.

So, let me take this so, we have multiplied by ρ so it becomes - $\rho \frac{\partial\phi}{\partial t} + p$ because ρ gets canceled here + $\rho g z$ that and this can be written as γz . So p can be written as if this goes on the other side, this becomes $\rho \frac{\partial\phi}{\partial t}$ and this one becomes - γz is it and

this is the same equation here. So becomes $p = \rho \frac{\partial \phi}{\partial t} - \gamma z$ or $+$ of $-\gamma z$ said this is the dynamic pressure.

And this is the static component depending upon only the water depth now, if we substitute for ϕ was the velocity potential in this equation, what do we get? p will be so $\frac{\partial \phi}{\partial t}$ will be written as $\frac{\gamma H}{2} \frac{\cosh k(d+z)}{\cosh kd} \sin kx - \sigma t - \gamma z$ so this is the pressure equation.

(Refer Slide Time: 02:49)



$\eta = \frac{H}{2} \sin(kx - \sigma t)$ and let $\frac{\cosh k(d+z)}{\cosh kd} = K_p$
 Where K_p is the pressure response factor then,

$$p = \gamma \eta K_p - \gamma z$$

 Or
$$\frac{p}{\gamma} = (\eta K_p - z) \quad (2.57)$$

It is to be mentioned that p was set to zero to define the free surface boundary condition in the Bernoulli equation. However ϕ was determined by setting $p=0$ at $z=0$ instead of $z=\eta$ [Refer Eq 2.5]. Hence eq 2.57 is valid only for negative z .

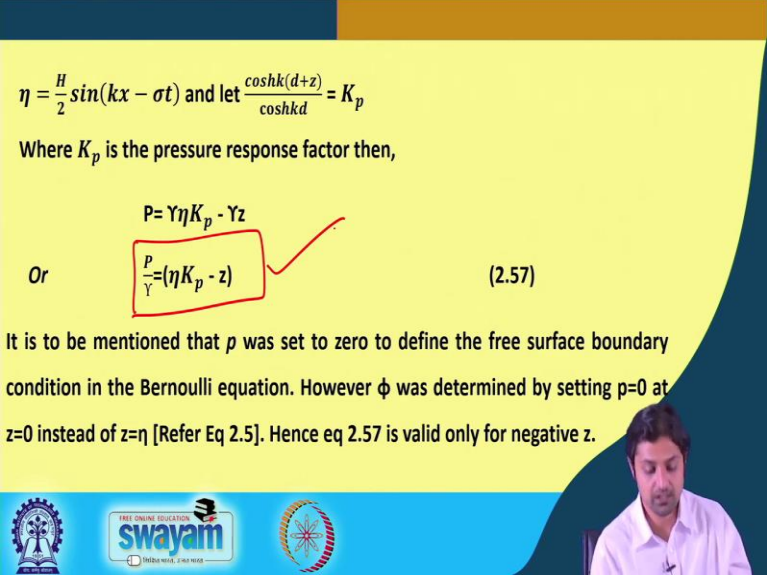
The slide also features a diagram of a water surface profile with a wavy line representing the surface. A vertical line is drawn from the surface to the bottom, labeled 'negative' in red. The bottom boundary is labeled 'z=0'.

We already know that η can be written as $\frac{H}{2} \sin kx - \sigma t$ and let us assume that $\frac{\cosh k(d+z)}{\cosh kd}$ into $d + z$ divided by $\cosh kd$. If we write as K_p substitute then the p this one can be written as $\gamma \frac{H}{2}$ this will be K_p or $\frac{H}{2} \sin kx - \sigma t$ is η . So, we can write and K_p we say that K_p is pressure response factor, then we can simply write p as $\gamma \eta$ into $K_p - \gamma z$ or p by γ can be return as $\eta K_p - z$.

Now, it has to be mentioned that P was set to 0 to define the free surface boundary condition in Bernoulli's equation if you remember, however, ϕ was determined by setting $p = 0$ as is that = 0 instead of $z = \eta$. Hence this means this particular equation is valid only for negative z that if you want to suppose this is the you know freeze this is the you know freezer. So, this is that = 0. So, the above equation is valid only in this region below. We cannot apply this here in this

domain the pressure no, because it was because we had derived phi with certain approximations assumptions.

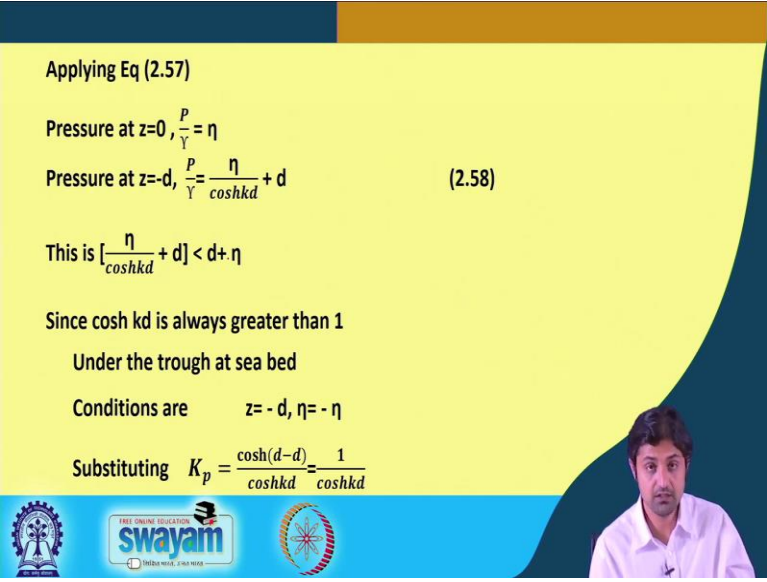
(Refer Slide Time: 04:36)



$\eta = \frac{H}{2} \sin(kx - \sigma t)$ and let $\frac{\cosh k(d+z)}{\cosh kd} = K_p$
 Where K_p is the pressure response factor then,
 $P = \gamma \eta K_p - \gamma z$
 Or $\frac{P}{\gamma} = (\eta K_p - z)$ (2.57)
 It is to be mentioned that p was set to zero to define the free surface boundary condition in the Bernoulli equation. However ϕ was determined by setting $p=0$ at $z=0$ instead of $z=\eta$ [Refer Eq 2.5]. Hence eq 2.57 is valid only for negative z .

So, p by gamma is ηK_p and I think this is one such equation which should be remembered K_p is $\cosh k(d+z)$ divided by $\cosh kd$ and η we already know it is $\sin kx - \sigma t$ or H by $2 \sin kx - \sigma t$.

(Refer Slide Time: 04:56)

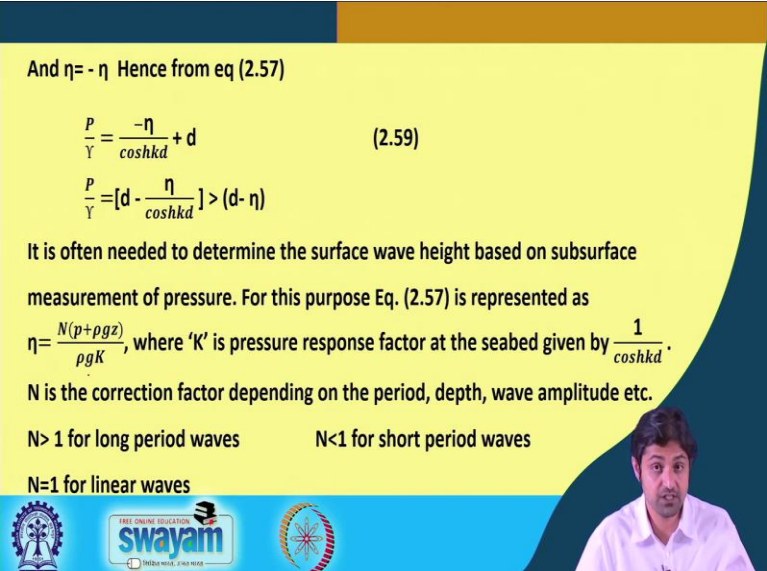


Applying Eq (2.57)
 Pressure at $z=0$, $\frac{P}{\gamma} = \eta$
 Pressure at $z=-d$, $\frac{P}{\gamma} = \frac{\eta}{\cosh kd} + d$ (2.58)
 This is $[\frac{\eta}{\cosh kd} + d] < d + \eta$
 Since $\cosh kd$ is always greater than 1
 Under the trough at sea bed
 Conditions are $z = -d, \eta = -\eta$
 Substituting $K_p = \frac{\cosh(d-d)}{\cosh kd} = \frac{1}{\cosh kd}$

Now, if you apply this equation 2.57 so, pressure at $z = 0$ is going to be p by gamma = η and pressure at $z = -d$ so, this is free surface and this is at bottom $z = -d$ at bottom. So, this means, if you η by $\cosh kd + d$ we know that it is definitely less than $d + \eta$ because $\cosh kd$ is always

greater than one since $\cos$ so, under the trough at sea bed the conditions are $z =$ at trough wave trough conditions are $z = -d$ and $\eta = -\eta$. So, if we substitute that K p is going to be $\cos d - d$ divided by $\cos h k d$ or 1 by $\cos h k d$.

(Refer Slide Time: 06:06)



And $\eta = -\eta$ Hence from eq (2.57)

$$\frac{p}{\gamma} = \frac{-\eta}{\cosh kd} + d \quad (2.59)$$

$$\frac{p}{\gamma} = \left[d - \frac{\eta}{\cosh kd} \right] > (d - \eta)$$

It is often needed to determine the surface wave height based on subsurface measurement of pressure. For this purpose Eq. (2.57) is represented as

$\eta = \frac{N(p + \rho g z)}{\rho g K}$, where 'K' is pressure response factor at the seabed given by $\frac{1}{\cosh kd}$.

N is the correction factor depending on the period, depth, wave amplitude etc.

$N > 1$ for long period waves $N < 1$ for short period waves

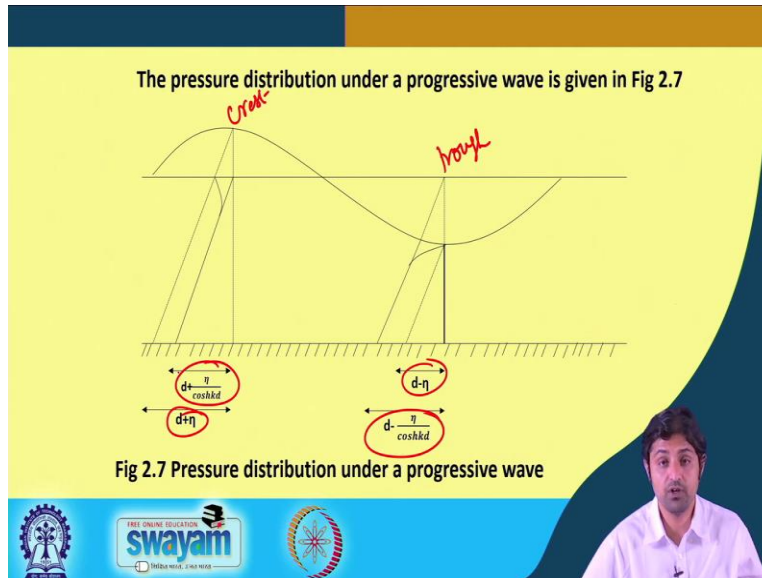
$N = 1$ for linear waves

Logos for Swayam and other educational institutions are at the bottom.

And n in $\eta = -\eta$ therefore, we will get p by $\gamma = -\eta$ by $\cos h k d + d$ which means that p by γ is $d - \eta$ by $\cos h k d$ will always be greater than $d - \eta$ because this is greater than one it is often needed to determine the surface wave height based on sub surface measurement of the pressure. So, for this message for this purpose equation 2.7 can be represented as. So, if we have sub surface measurement techniques available.

So, we can actually you know calculate the n where n is the correction factor depending upon the period depth wave amplitude sector this is for the people who are interested more in practical. So, n is has been found that should be greater than one for long period waves and n should be less than one for short period waves and $n = 1$ for linear waves as we have seen already.

(Refer Slide Time: 07:20)



So, the pressure distribution under progressive wave is given by this is crest wave crest, so, pressure distribution under wave crest and pressure distribution wave trough to this is the pressure distribution under a progressive wave. So, these terms is important $d + \eta$ $d - \eta$ by $\cosh kd$ and $d +$. So, in questions you can be given for example, this curve and asked to label water what is this quantity and other things.

(Refer Slide Time: 08:16)

GROUP CELERITY:

- When a group of waves or a wave train travels its speed is generally not identical to the speed with individual waves within the group travel. If any two wave trains of the same amplitude, but slightly different wavelengths or periods, progress in the same direction, the resultant surface disturbance can be represented as the sum of the individual disturbances. For waves propagating in deep or transitional waters, the group velocity is determined as follows.

$$\eta_T = \eta_1 + \eta_2 = a \sin(k_1 x - \sigma_1 t) + a \sin(k_2 x - \sigma_2 t) \quad (2.60)$$

$$\eta_T = 2a \cos \left[\left(\frac{k_1 - k_2}{2} \right) x - \left(\frac{\sigma_1 - \sigma_2}{2} \right) t \right] \cdot \sin \left[\left(\frac{k_1 + k_2}{2} \right) x - \left(\frac{\sigma_1 + \sigma_2}{2} \right) t \right]$$

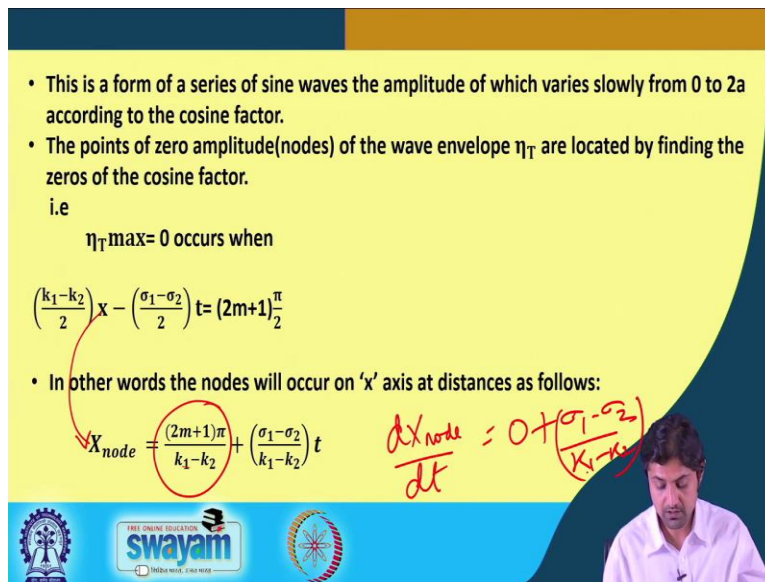
Now, there is something called group celerity, a very important concept. So, when a group of waves or a wave train travels its speed is generally not identical with the speed of the individual waves. So, if there is a group that is traveling, its speed is not going to be the same as it was

traveling alone analogy is if you run alone and if you run along with the group of people taking everyone together the speed will be different.

So, if any 2 wave trains have the same amplitude, but the same but slightly different wavelengths or periods progress in the same direction, the result in surface disturbance can be represented as the sum of individual disturbances based on the principle of superposition, so for wave train getting in deeper transitional water the group velocity is determined as follows. So, as I said, the superposition of η_1 and η_2 says we can simply write combined η , T is $\eta_1 + \eta_2 = A \sin k_1 x - \sigma_1 t + a \sin k_2 x - \sigma_2 t$.

Because we have assumed that the same almost same amplitude different phases. So, using the trigonometry we write it is $2a \cos \left(\frac{k_1 - k_2}{2} x - \frac{\sigma_1 - \sigma_2}{2} t \right) \sin$ of this term, this is what we get using the trigonometry. So the left hand side is $k_1 - k_2$ by $2 x - \sigma_1 - \sigma_2$ by $2 t$ into t .

(Refer Slide Time: 10:02)



- This is a form of a series of sine waves the amplitude of which varies slowly from 0 to $2a$ according to the cosine factor.
- The points of zero amplitude (nodes) of the wave envelope η_T are located by finding the zeros of the cosine factor.
i.e.
 $\eta_T \max = 0$ occurs when

$$\left(\frac{k_1 - k_2}{2} \right) x - \left(\frac{\sigma_1 - \sigma_2}{2} \right) t = (2m+1) \frac{\pi}{2}$$

- In other words the nodes will occur on 'x' axis at distances as follows:

$$X_{\text{node}} = \frac{(2m+1)\pi}{k_1 - k_2} + \left(\frac{\sigma_1 - \sigma_2}{k_1 - k_2} \right) t$$

Handwritten red notes: $\frac{dX_{\text{node}}}{dt} = 0 + \frac{(\sigma_1 - \sigma_2)}{(k_1 - k_2)}$

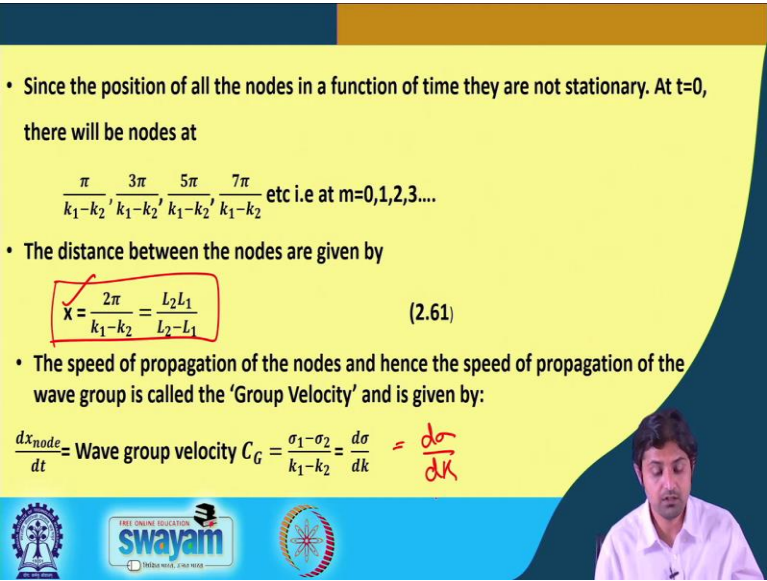
Logos at the bottom: Swamiji, swayam, and a circular logo.

So, this is a form of a series of sin waves the amplitude of which very slowly from 0 to $2a$ according to the cosine factor. So, we say this is the amplitude of the wave and this is the phase and the amplitude varies from 0 to $2a$ or depending upon the, what the phase is here. So the point of 0 amplitude or nodes, because it will very slowly from 0 to $2a$ and there will be $2a$ as well they

will be 0 as well. So, the point of 0 amplitude are called nodes. They can be located by finding the 0s of the cosine factor.

Because if this is 0 that is $\eta T \max = 0$ occurs when $k_1 - k_2$ when this the term within the cos is π by 2 or a multiple of π by 2. In other words, the nodes will occur on x axis at a distance as follows. If you see you try to do that if you rearrange we can get x node here = x is here, just rearrange it will be $2m + 1 \pi$ by 2 will get cancelled from each side it will be $k_1 - k_2 + \sigma_1 - \sigma_2$ by $k_1 - k_2$ into T.

(Refer Slide Time: 11:41)



- Since the position of all the nodes in a function of time they are not stationary. At $t=0$, there will be nodes at

$$\frac{\pi}{k_1 - k_2}, \frac{3\pi}{k_1 - k_2}, \frac{5\pi}{k_1 - k_2}, \frac{7\pi}{k_1 - k_2} \text{ etc i.e at } m=0,1,2,3,\dots$$
- The distance between the nodes are given by

$$x = \frac{2\pi}{k_1 - k_2} = \frac{L_2 L_1}{L_2 - L_1} \quad (2.61)$$
- The speed of propagation of the nodes and hence the speed of propagation of the wave group is called the 'Group Velocity' and is given by:

$$\frac{dx_{node}}{dt} = \text{Wave group velocity } C_G = \frac{\sigma_1 - \sigma_2}{k_1 - k_2} = \frac{d\sigma}{dk} = \frac{d\omega}{dk}$$

Since the position of all nodes in the function is a function of time and they are not stationary at $t = 0$ there will be nodes that so as we see the equate this at time $t = 0$. So, we will see there will be nodes at π divided by $k_1 - k_2$ divided and then there will be node at 3π divided by $k_1 - k_2$ if we start putting $m = 0, 1, 2, 3$ and the distance between the node is given by 2π by divided by $k_1 - k_2$ or $L_1 L_2$ divided by $L_2 - L_1$.

So, you can be asked to find out the distance between the nodes and this is an important result that you can remember the speed of propagation of the nodes and hence, the speed of propagation of wave group is called the group velocity already so, what we have obtained is we have obtained in the distance between the nodes. So, now, if we find out the speed of these

nodes, we can find out the speed of the propagation of the wave group and this particular velocity is called as group velocity.

So, if we find the x node by dt is the wave group velocity C_G . So, if you go to see x node what was x node was here and if you differentiate the x node by dt, this term on differentiation will be $0 + \frac{\sigma_1 - \sigma_2}{k_1 - k_2}$ divided by $k_1 - k_2$. And this is what is told here $\sigma_1 - \sigma_2$ divided by $k_1 - k_2$ or $d\sigma$ by dk .

(Refer Slide Time: 13:31)

But $\sigma = K.C = \frac{2\pi L}{T} = \frac{2\pi}{T}$

$C_G = \frac{d(KC)}{dk} = C + k \frac{dc}{dk} = C + \frac{K.dC}{dL} \left(\frac{1}{\frac{dk}{dL}} \right)$ (Manipulation with terms)

Since $k = \frac{2\pi}{L}$

$C_G = C + \frac{2\pi.dC}{L.dL} \left(\frac{1}{-\frac{2\pi}{L^2}} \right)$

$C_G = C - L \frac{dC}{dL}$ (dispersion relationship)

Since $C^2 = \frac{g}{k} \tanh(kd)$

Substituting and on simplification we get

But, σ is what K into C , $K.C$, σ can be written as K into C 2π by L into L by T . So, C_G will be $d\sigma$ instead of σ we write K into C and if we differentiate this we are going to get so differentiation by no I mean if there are differentiation of a b $a b$ is $ad db dt + b + a + b da dt$. So, we have used this rule change rule and we often $c + k dc dk$ C remains C here and K in So, what we do we write k remain same instead of $dc dk$ we write $dc dl$ into 1 by $dK dL$.

So, we are actually doing some manipulation here with terms here. And since $k = 2\pi$ by L C_G will be $C + kV$ write to $\frac{2\pi}{L} \frac{dC}{dL}$ into 1 -, so, into 1 divided by -2π by L Squire or $C_G = C - L \frac{dC}{dL}$. Since $C^2 = \frac{g}{k} \tanh(kd)$ from dispersion relationship and if we substitute this C here and do dC by dL as well.

(Refer Slide Time: 15:23)

$$\frac{C_G}{C} = n = \frac{1}{2} \left[1 + \frac{2kd}{\sinh 2kd} \right] \quad (2.62)$$

For deep waters $\frac{2kd}{\sinh 2kd}$ is zero

Hence $C_G = \frac{1}{2} C_0$

$$C_G = \frac{1}{2} \frac{L_0}{T} = \frac{1}{2} C_0 \quad (2.63)$$

The Group velocity is one half of the phase velocity in deep waters. Further it should be noted that variables if associated with a suffix '0' refer to deep-water conditions. For example C_0 is deep water celerity.

We will get C_G by $C = n$, where n is half into $1 + 2kd$ divided by $\sinh 2kd$. So the derivation you do not have to worry about that much but this equation is important or C_G can be written as group velocity will be C by 2 into $1 + 2kd$ divided by $\sinh 2kd$ this equation is very important. Do remember you must remember this equation so for deep water $2kd$ divided by $\sinh 2kd$ is 0. Therefore C_G group velocity is C not by 2 C not is, these were solidity of a single wave. An important result that the group velocity in deep water is wave velocity of similarity by 2.

So, group velocity is one half of the phase velocity in deep waters. Further it should be noted that the variables associated with suffix 0 refers to deep water condition, wherever we have ref put 0 that means deep water condition. And Porter celerity you already remember 1.56 times the time period.

(Refer Slide Time: 16:44)

Table 2.2 Variation of Asymptotic Functions		
Function	Asymptotes	
	Shallow waters	Deep Waters
$\sinh kd$	kd ✓	$\frac{e^{kd}}{2}$ ✓
$\cosh kd$	1 ✓	$\frac{e^{kd}}{2}$ ✓
$\tanh kd$	Kd ✓	1 ✓

In shallow waters,
since $\sinh 2kd = 2kd$

$$C_G = C = \sqrt{gd} \quad (2.64)$$


There is a table that shows the sum total variations so $\sinh kd$ in shallow water this kd whereas in deep water it is e to the power kd by 2 $\cosh kd$ in shallow water is none and $\cosh kd$ in deep water e to the power kd by 2 $\tanh kd$ kd in shallow water and deep water it is one this we have already discussed once before also in a different format but yes this is a thing so in shallow water $\sinh 2kd$ becomes $2kd$. Therefore C_G is going to be you look at this equation $\sinh 2kd$ will be $2kd$ so this $2kd$ gets canceled. So it will be $1 + 1$ to 2 into half of so C_G will become C and that equal to under root gd .

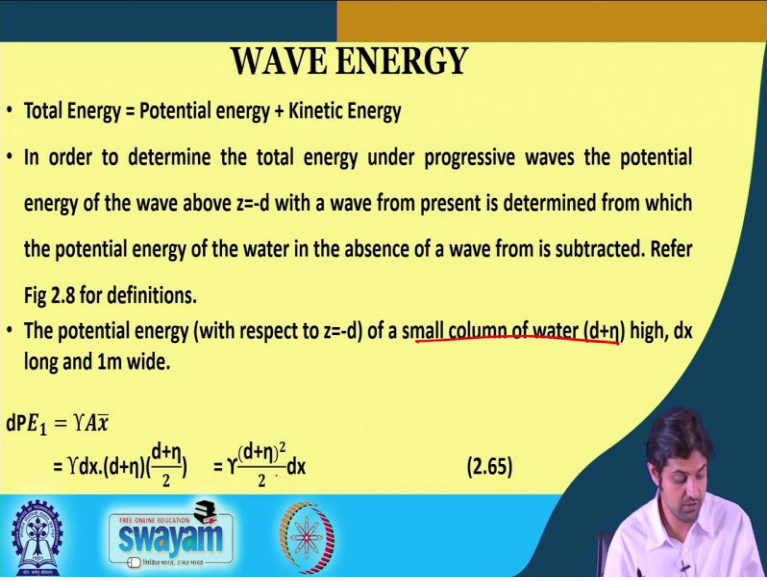
(Refer Slide Time: 17:42)

Hence in shallow water the group and phase velocities are same and is a function of only depth of water and in deep waters, the C_G is a function of wave length. Because of this, in deep waters, the longer waves (Long L) travel faster and produce the small phase differences resulting in wave groups. These waves are said to be dispersive or propagating in a dispersive medium, i.e., in a medium where their celerity is dependent on wave length.



So in shallow water the group velocity same as the face velocities all this celerity of the wave. So deep water it is C not by 2 whereas $CG = C$ shallow waters and in for the normal for the intermediate water you can use this equation $C = CG = C$ by 2 into $1 + 2kd / \sin h2kd$. This is actually for all the waters but intermediate waters, because deep water in shallow water we have some approximations, but intermediate waters we can use the same formula.

(Refer Slide Time: 18:44)



WAVE ENERGY

- Total Energy = Potential energy + Kinetic Energy
- In order to determine the total energy under progressive waves the potential energy of the wave above $z=-d$ with a wave from present is determined from which the potential energy of the water in the absence of a wave from is subtracted. Refer Fig 2.8 for definitions.
- The potential energy (with respect to $z=-d$) of a small column of water $(d+\eta)$ high, dx long and 1m wide.

$$dPE_1 = \gamma A \bar{x}$$

$$= \gamma dx \cdot (d+\eta) \left(\frac{d+\eta}{2} \right) = \gamma \frac{(d+\eta)^2}{2} dx \quad (2.65)$$



Now what is wave energy? We have discussed about almost everything. So, we have discussed about the particle trajectories then we have discussed about you know this group velocity now we must go towards wave energy. So, total energy potential energy + kinetic energy. So, in order to determine the total energy and a progressive wave the potential energy of the wave above $z = -d$ with a wave from present is determine from which the potential energy of the water in absence of the wave is subtracted.

So, how do we determine total energy and the way we determine the total energy and we total energy or the way when we subtract it with the potential the water in the absence of the waves so, we get the energy in presence of waves only. So, the potential energy with respect to $z = -d$ of a small column of water $d + \eta$ high dx long and 1 meter wide can be written as, so if we have a small column of water $d + \eta$ high, where dx is length and 1 meter wide potential energy will be $\gamma a \times \bar{x}$ area will be $d + \eta$ into $d + \eta$ by 2 into dx .

So, the potential energy will be $\gamma d + \eta^2$ whole squared by 2 multiplied by dx . So, the potential energy of a small column of water.

(Refer Slide Time: 20:22)

- The average potential energy per unit surface area (sometimes called the average potential energy density) is

$$\overline{PE}_1 = \frac{\gamma}{2LT} \int_t^{t+T} \int_x^{x+L} (d + \eta)^2 dx dt \quad (2.66)$$

Using $\eta = a \sin(kx - \sigma t)$ then Eq. (2.66) becomes

$$\overline{PE}_1 = \frac{\gamma}{2LT} \int_t^{t+T} \int_x^{x+L} (d^2 + 2ad \sin(kx - \sigma t) + a^2 \sin^2(kx - \sigma t)) dx dt$$

On simplification

$$\overline{PE}_1 = \frac{\gamma d^2}{2} + \frac{\gamma a^2}{4} \quad (2.67)$$


The average potential energy per unit surface area is going to be integration of γd^2 by 2 into L so, we have to average over the whole wave period and also average over the entire wavelength. And using the equation below you see, we integrated and after integration if we use $\eta = a \sin kx - \sigma t$ we and then we integrate and simplification we will get potential energy total potential energy is going to be γd^2 squared by 2 + γa^2 squared by 4.

(Refer Slide Time: 21:06)

- Which is the average potential energy per unit surface area of all the water above $z = -d$
- The potential energy in the absence of wave would be

$$\overline{PE}_2 = \frac{\gamma}{2LT} \int_t^{t+T} \int_x^{x+L} d^2 dx dt = \frac{\gamma d^2}{2} \quad (2.68)$$

- The average potential energy density, $\overline{PE}$ which is attributable to the presence of the progressive wave on the free surface, is

$$\overline{PE} = \overline{PE}_1 - \overline{PE}_2 = \text{Average Potential Energy}$$

$$= \frac{\gamma d^2}{2} + \frac{\gamma a^2}{4} - \frac{\gamma d^2}{2}$$


However, this is the average potential energy per unit surface area of all the water above $z = -d$. Now, we should also calculate the potential energy and absence of the wave and the wave is not there, when the wave is not there then there will be no η in this term you see there was η here. So, now, this would not be there when there is no wave and we do the same procedure for finding the total potential energy and this comes to be $\frac{\gamma d^2}{2}$.

And the total energy due to the presence of the wave will be the total energy - the energy that are - the energy when the wave is not there. So, this will become the average potential energy this one came to be $\frac{\gamma d^2}{2} + \frac{\gamma a^2}{4}$ and this one came to be $\frac{\gamma d^2}{2}$.

(Refer Slide Time: 22:06)

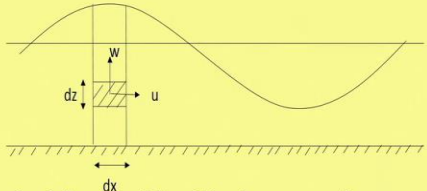
$$\overline{PE} = \frac{\gamma a^2}{4} \quad (2.69)$$


Fig.2.8 Definition sketch for potential and kinetic energy under progressive wave

Kinetic Energy

The kinetic energy, $KE = \frac{1}{2}mv^2$, where 'm' is the mass of the fluid and 'v' is the resultant velocity. For 2D wave flow

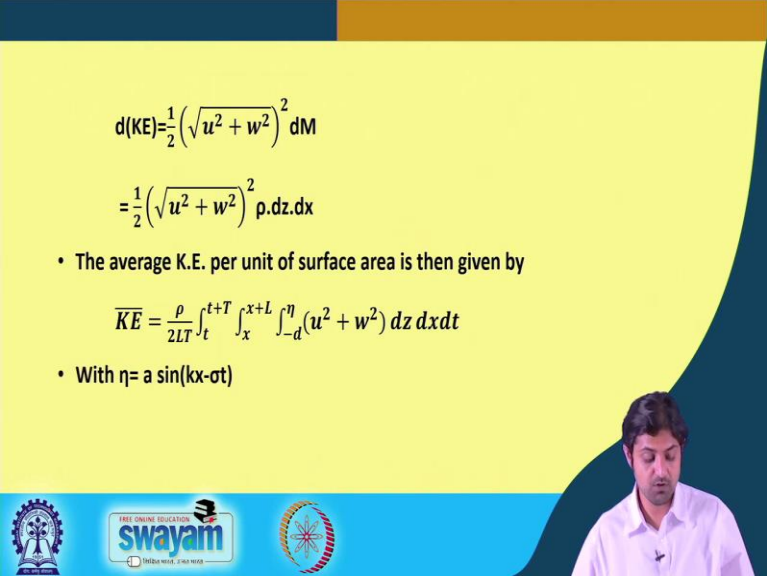




And this gives us the potential energy due to waves is $\frac{\gamma a^2}{4}$ where a is the wave amplitude? You have seen how it is derived, but results are more importantly you must remember the potential energy due to the waves is written as $\frac{\gamma a^2}{4}$. So, this was the assumption we have assumed, using this small particle we and by integrating over the entire wavelength and entire wave period we have obtained the potential energy.

So, the method was total potential energy with wave - the energy water potential energy without waves gave us due to waves alone. Now we will also need to find kinetic energy it is very simple kinetic energy is half mv^2 squared, where m is the mass of the fluid and v is a result and velocity.

(Refer Slide Time: 23:08)



$$d(KE) = \frac{1}{2} (\sqrt{u^2 + w^2})^2 dM$$

$$= \frac{1}{2} (\sqrt{u^2 + w^2})^2 \rho \cdot dz \cdot dx$$

- The average K.E. per unit of surface area is then given by

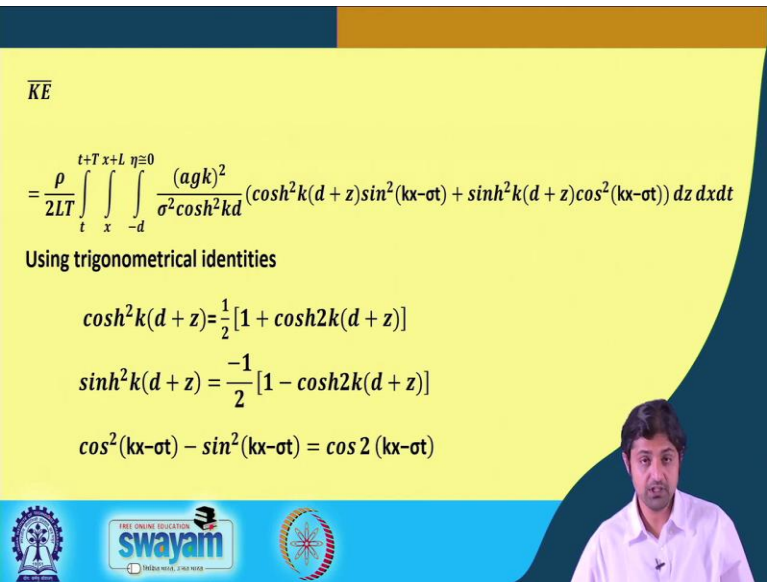
$$\overline{KE} = \frac{\rho}{2LT} \int_t^{t+T} \int_x^{x+L} \int_{-d}^{\eta} (u^2 + w^2) dz dx dt$$

- With $\eta = a \sin(kx - \sigma t)$



For 2 dimensional wave flow, we know it is half under route u squared + w squared into dM can be written as rho into dz dx for that definition here,, these are dx and under route u squared + w squared, so the average kinetic energy per unit of surface area, if we integrate it over the entire wavelength and wave period will come out to be it is a complex into I mean.

(Refer Slide Time: 23:35)



$$\overline{KE}$$

$$= \frac{\rho}{2LT} \int_t^{t+T} \int_x^{x+L} \int_{-d}^{\eta \approx 0} \frac{(agk)^2}{\sigma^2 \cosh^2 kd} (\cosh^2 k(d+z) \sin^2(kx - \sigma t) + \sinh^2 k(d+z) \cos^2(kx - \sigma t)) dz dx dt$$

Using trigonometrical identities

$$\cosh^2 k(d+z) = \frac{1}{2} [1 + \cosh 2k(d+z)]$$

$$\sinh^2 k(d+z) = \frac{-1}{2} [1 - \cosh 2k(d+z)]$$

$$\cos^2(kx - \sigma t) - \sin^2(kx - \sigma t) = \cos 2(kx - \sigma t)$$



It is so many terms, but on you know, applying the simplification of trigonometry, we can get if we apply these simplifications, you will get these slides so you will have more you know, it will be easy to understand. But more important are the results.

(Refer Slide Time: 23:56)

$\cos^2(kx - \sigma t) + \sin^2(kx - \sigma t) = 1$

$\sinh 2kd = 2 \sinh kd \cdot \cosh kd$

And $\sigma^2 = gk \tanh kd$

It can be shown $\overline{KE} = \frac{\gamma a^2}{4}$ (2.70)

Total energy $E = \overline{PE} + \overline{KE}$

$E = \frac{\gamma a^2}{2}$ (2.71)

The average total energy per unit surface area is the sum of the average potential and kinetic energy densities often called as specific energy density.

So we can show that kinetic energy is gamma a squared by 4 potential energy was also gamma a squared by 4. Therefore, the total energy is going to be due to the waves alone is potential energy + kinetic energy, the total energy is gamma a squared by 2. So, the average this is an important result again so the kinetic energy value the potential energy and the total energy these equations you must remember gamma a squared by 4 and total energy is gamma squared by 2.

So, the average total energy per unit surface area is the sum of average potential and kinetic energy density is often called as a specific energy density. You can also be asked what is specific energy density for example.

(Refer Slide Time: 24:53)

WAVE POWER

- Wave energy flux is the rate at which energy is transmitted in the direction of wave propagation across a vertical plane perpendicular to the direction of the wave advance and extending down the entire depth. The average energy flux per unit wave crest width transmitted across a plane perpendicular to wave advance is

$\bar{P}$ = Wave power = Average energy flux per unit wave crest width

$$\bar{P} = \bar{E} n C = \bar{E} C_g \quad (2.72)$$

When $n = \frac{1}{2} \left[1 + \frac{2kd}{\sinh 2kd} \right]$

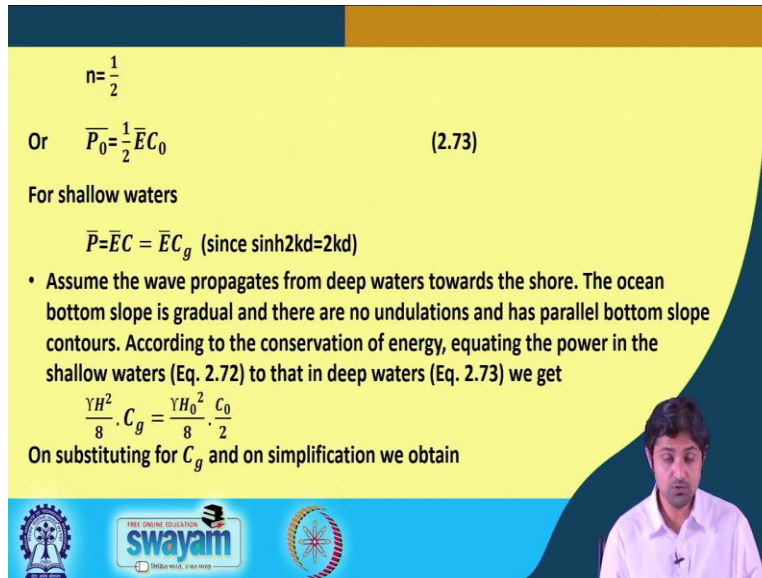
For Deep waters $\frac{2kd}{\sinh 2kd} = 0$ and $C_g = \frac{1}{2} C_0$



So, now we have studied wave energy it is very obvious that we study wave power wave energy flux is the rate at which energy is transmitted in the direction of wave propagation across a vertical plane perpendicular to the direction of wave advance and extending down the entire. So, the average energy flux per unit wave crest with transmitted across the plane perpendicular to the wave advances is wave power. And it is given as e into CG .

This is important CG is group velocity and e is the energy that we just derived. So, the power is given as e into CG or in if you want to write it in terms of celerity. It is e bar n into CG u did you saw that n was this so, the wave power is nothing you reject. You just need to remember the formulas e bar into CG where e bar was γa^2 by 2. So, for deep water you know that CG was half c not.

(Refer Slide Time: 26:11)



$n = \frac{1}{2}$
 Or $\bar{P}_0 = \frac{1}{2} \bar{E} C_0$ (2.73)
 For shallow waters
 $\bar{P} = \bar{E} C = \bar{E} C_g$ (since $\sinh 2kd = 2kd$)
 • Assume the wave propagates from deep waters towards the shore. The ocean bottom slope is gradual and there are no undulations and has parallel bottom slope contours. According to the conservation of energy, equating the power in the shallow waters (Eq. 2.72) to that in deep waters (Eq. 2.73) we get

$$\frac{\gamma H^2}{8} \cdot C_g = \frac{\gamma H_0^2}{8} \cdot \frac{C_0}{2}$$
 On substituting for C_g and on simplification we obtain

$n = \frac{1}{2}$ so, power is going to be half into C not for shallow water it will be into C_g because C_g is C only if you assume that the wave propagates from deep water towards the shore and the ocean bottom slope is gradual and there are no undulations and as parallel bottom slope because, you see the wave power is going to be conserved if the wave moves from 1 depth to the other. Because you see this if there is no loss, it is average energy flux per unit wave crest rate.

And if we apply the conservation of wave power. So, you see this is any depth. So, γ is gamma h^2 by 8. So, this becomes gamma h^2 by 8 and C_g is C not. So, with the wave propagates from deep water to let us say any depth whether intermediate or shallow. So, wave power is going to be conserved correct. So, in deep water, it will be gamma h^2 by 8 h not indicates the wave height in deep water.

multiplied by we have already seen that this is going C_g is C not by 2 and this will be equal to gamma h^2 by 8 this is the way high at any depth where we want to calculate multiplied by C_g , this is what this equation is all about this equation so we are conserving power from deep water to any water depth. And if we substitute for C_g as C by 2 into $1 + 2kd$ by $\sinh 2kd$.

(Refer Slide Time: 28:25)

$$\left(\frac{H}{H_0}\right)^2 = \frac{C_0}{C} \frac{1}{\left[1 + \frac{2kd}{\sinh 2kd}\right]}$$

Or
$$\frac{H}{H_0} = \sqrt{\frac{C_0}{C} \cdot \frac{1}{2n}} = K_s \quad (2.74)$$

Where $n = \frac{1}{2} \left[1 + \frac{2kd}{\sinh 2kd} \right]$

- The above equation giving the ratio between wave height at any depth in shallower waters and the deep water height. This relationship obtained without considering the irregular variation in the sea bottom contours is called as shoaling coefficient.

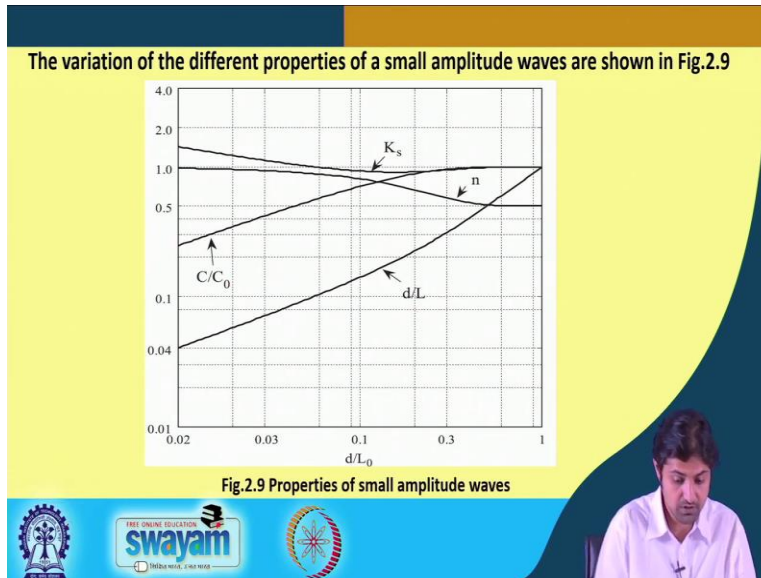
Shoaling
Very important Equation
You must remember

We are going to obtain $\frac{H}{H_0} = \frac{C_0}{C} \frac{1}{1 + \frac{2kd}{\sinh 2kd}}$ or we can obtain $\frac{H}{H_0} = \sqrt{\frac{C_0}{C} \cdot \frac{1}{2n}}$ because this is n this is n by I mean this is a $2n$. Therefore, $\frac{H}{H_0} = \sqrt{\frac{C_0}{C} \cdot \frac{1}{2n}}$ this is called K_s where $n = \frac{1}{2} \left[1 + \frac{2kd}{\sinh 2kd} \right]$. So, the above equation is very important again this represents of phenomena which is called shoaling. And this gives the ratio between wave height at any depth in the shallower waters compared to the deep water wave height.

And this relationship is obtained without considering the irregular variation in the sea bottom. And this ratios under root of $\frac{C_0}{C} \cdot \frac{1}{2n}$ is called shoaling coefficient or chaos. So, until now, you saw that we had been able to obtain relationship between the water velocities and only kinematics, but this is the only equation that we have studied that if we know the wave height in deep water we will also be able to calculate the height it any depth to z .

So, a very important equation which you must remember the shoaling coefficient and the root $\frac{C_0}{C}$ not by C into 1 by and where C not is the, speed in the deep water which is 1.56 times t . So, there are some, you know formulas to remember, but, remember only the simple ones, the ones that I have already told you. So, by equating the wave power, we have been able to obtain the wave height the wave height transformation if the wave propagates from 1 depth to the other depth.

(Refer Slide Time: 30:53)



So, the variation of different properties of a small amplitude waves are shown in this figure you do not need to pay too much attention just we have plotted d by L , C by C not k , s and n which you already know s is the shoaling coefficient.

(Refer Slide Time: 31:10)

MASS TRANSPORT VELOCITY

When waves are in motion, the particles upon completion of each nearly an elliptical or circular motion would have advanced a short distance in the direction of propagation (Fig.2.10). Consequently there is a mass transport in the direction of progress of the wave. The mass transport velocity at any depth z below S.W.L is given as

$$\bar{U}(z) = \left(\frac{\pi H}{L}\right)^2 \frac{C \cosh 2k(d+z)}{2 \sinh^2 kd} \quad (2.75)$$

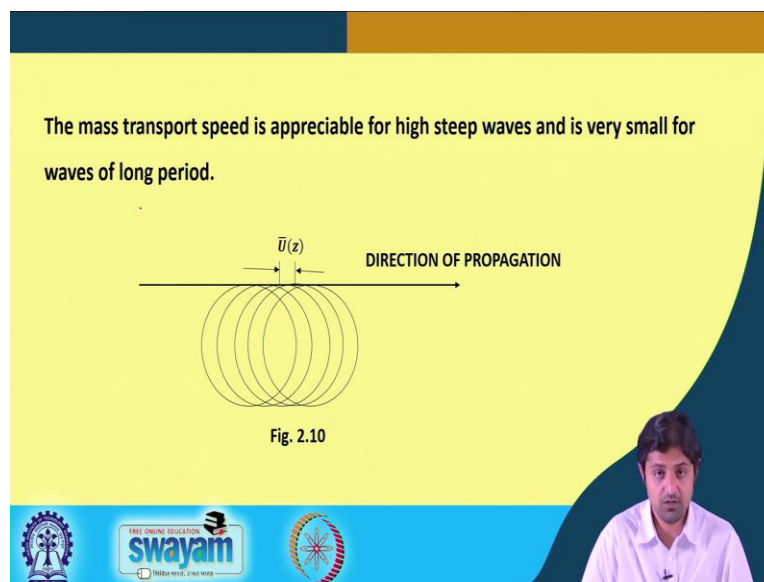
Outside the scope

So, this is the last topic the derivation is outside the scope, but what you must understand is that when waves are in motion, the particles upon completion of each nearly an elliptical or circular motion would have an advanced a short distance in the direction of propagation of waves, you can check it from those equations as well. Therefore, if they move ahead that means that the

mass associated with them has already moved forward correct. This mass transport is happening in the direction of the progress of the wave.

And the mass transport velocity is given by $\frac{1}{2} \frac{h^2}{L^2} \frac{C}{\sin^2 kd} + z$ divided by $\sin^2 kd$. So, this is outside the scope formula I do not expect you to know, remember this particular equation, but more importantly the message is to convey messages that you must understand that the mass transport happens and then the wave motion is there. Of course, you must remember that it is a function of edge squared for example, mass transport is the function of h^2 or you know is related to how I mean the end of the vein which is proportional to one quantity.

(Refer Slide Time: 32:38)



So, the mass transport speed is appreciable for high steep waves and very small for waves of long period you can see this equation. So, if it is a long wave, the mass transport is very less because, so if period is long the length is long. It is the high steep wave which means which is directly proportional to h^2 . So, the mass transport will be high for long the higher waves.

So, this was the last topic of hydraulic engineering which we have finished now, and with this I would like to close the lecture and also this course. If you have further doubts, please do contact us and the forum or I will be appearing in some live sessions. Also, I do not know if you have something after the this lecture, but if you have you can send email to my teaching assistants, or

also post the question and forum. I wish you good luck for you are assignment for this particular week. And also the final exams. Thank you so much for listening. Have a great year.