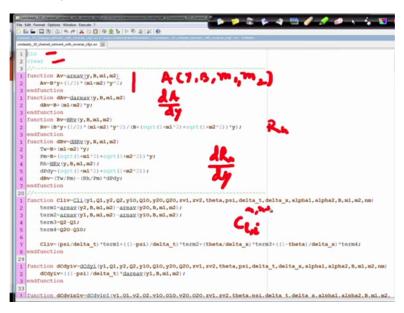
Computational Hydraulics Professor Anirban Dhar Department of Civil Engineering Indian Institute of Technology Kharagpur Lecture 45 Unsteady 1D Channel Flow (Contd.)

So in this case let us start this program with clc which is clear console, clear, clearing all variables. First one is area calculation. Area as a function of y, b, m1. B, m1, m2 these values are fixed values for any section. Only varying thing is y. This is dA by dy. Third one this is hR, hydraulic radius. And forth function this is dRh divided by dy. Fifth function this is CL i N N plus 1.

(Refer Slide Time: 01:22)



Then comes our function which is dc or dc by dy i. This is dc by dy i plus 1 and next one is dc by dQ, this is i. Next one is dc by dQ i plus 1. So we have defined CL i without specifying this L i here I have written this. This is dc L i, y i, dc y i plus 1, dc dQ i, dc dQ i plus 1.

(Refer Slide Time: 02:44)

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7.	□□□□□================================
F	ah _ 10_Jahrwe _ entrois _ whi _ years as _ 10_ 1 as 10_ United to Constant of the State of the of the
	anty, in Characteristics and the second se
20	//
1	function Cliv-Cli (y1,Q1,y2,Q2,y10,Q10,y20,Q20,zv1,zv2,theta,psi,delta_t,delta_x,alpha1,alpha2,B,m1,m2,nm)
2	term1=areay(y2, B, m1, m2) - areay(y20, B, m1, m2);
a	term2=areay(y1, B, m1, m2) - areay(y10, B, m1, m2) ;
4	term3-02-01/
5	term4-020-010;
6	
7	Cliv=(psi/delta t)*terml+((1-psi)/delta t)*term2+(theta/delta x)*term3+((1-theta)/delta x)*term4;
8	endfunction
29	
	function dCdyiv-dCdyi (y1,Q1,y2,Q2,y10,Q10,y20,Q20,zv1,zv2,theta,psi,delta t,delta x,alphal,alpha2,B,m1,m2,nm)
2	dCdyiv=((1-psi)/delta_t)*dareay(y1, B, m1, m2)/
	endfunction
33	- Ant
	function dCdyip1v-dCdyip1(y1, 01, y2, 02, y10, 010, y20, 020, zv1, zv2, theta, psi, delta t, delta x, alpha1, alpha2, B, m1, m2,
1	nm)
2	dCdyiplv=(psi/delta_t)*dareay(y2, B, m1, m2);
	endfunction
1	function dCdQiv-dCdQi (y1,Q1,y2,Q2,y10,Q10,y20,Q20,zv1,zv2,theta,psf,delta t,delta x,alpha1,alpha2,B,m1,m2,nm)
2	dCdQiv-theta/delta x/
3	endfunction AC
40	
	function dcdoiplv-dcdoipl (y1,01, y2, 02, y10, 010, y20, 020, 20, 20, 20, 20, 20, 20, 20, 20,
-	
2	dCdQiply-theta/delta x/
ã.	endfunction
44	//
1	function Mliv-Mli (y1, Q1, y2, Q2, y10, Q10, y20, Q20, zv1, zv2, theta, psi, delta_t, delta_x, alphal, alpha2, B, ml, m2, nm)
2	Av1=arcay(y1, B, m1, m2);
â	Av2=areay(v2, B, m1, m2) /
4	Avio-areav(yi0, B, m1, m2) /
5	Av20-areav(y20, B, m1, m2) /
1	

Now within this again we need to specify this ML i. This is ML i N N plus 1. Next is specification of dM by dy i. This is dm by dy i plus 1.

(Refer Slide Time: 03:21)

<u>d</u> u	a de la constante de
	Tall Format Options Window Decode 2
6	
	aady 10 daareel network with revenue dig Lati (2)
1	
69	
1	function dMdyiv-dMdyi(y1,Q1,Y2,Q2,y10,Q10,y20,Q20,zv1,zv2,theta,psi,delta_t,delta_x,alpha1,alpha2,B,m1,m2,nm)
2	Av1= <u>areay</u> (y1, B, m1, m2) /
3	Rh1- <u>HRy</u> (y1, B, m1, m2) /
4	dAv1= <u>dareav</u> (y1, B, m1, m2) / dBh1=dBy(y1, B, m1, m2) / dBh1=dBy(y1, B, m1, m2) /
5	dRh1= <u>dHRv</u> (y1, B, m1, m2) /
6	T T
7	terml=(Q1/Av1^2)*dAv1;
8	term2=(Q1^2/Av1^3)*dAv1;
9	term3=theta*g/delta_x/
10	
11	term42=(4/3)*Q1*abs(Q1)*dRh1*Rh1^(-7/3)*Av1^(-2))
12	
13	
	endfunction
84	
1	function dMdyiplv=dMdyipl(y1,Q1,y2,Q2,y10,Q10,y20,Q20,zv1,zv2,theta,psi,delta_t,delta_x,alpha1,alpha2,B,m1,m2,
	nan)
2	Av2= <u>areav</u> (y2, B, m1, m2) /
3	Rh2- <u>HRy</u> (y2, B, m1, m2) /
4	dAv2= <u>dareav</u> (y2, B, m1, m2);
5	dRh2= <u>dHRv</u> (y2, B, m1, m2);
6	<pre>dw2=drag(y2, n, m, m2); dw2=drag(y2, n, m, m2); term1=(02/Av2-2)*dAv2;</pre>
7	
8	term2=(Q2^2/Av2^3)*dAv2)
9	term3=theta*g/delta_x/
10	
11	term42=(4/3)*Q2*abs(Q2)*dRh2*Rh2^(-7/3)*Av2^(-2);
12	
13	
	endfunction
99	
1	function dMdQiv=dMdQi(y1,Q1,Y2,Q2,Y10,Q10,Y20,Q20,XV1,XV2,theta,psi,delta_t,delta_x,alpha1,alpha2,B,m1,m2,nm)
.n.	Auf=seau/u1 8 m1 m3):

After this calculation interestingly please note here that we have used this Q abs terms here, Q abs terms here.

(Refer Slide Time: 03:38)

7 un	
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1	월 월 1월
in the	
2	Avi-arcay (yi, B, mi, m2) /
JC	Rh1=HRy(y1, B, m1, m2) /
4	dAv1=dareay(y1, B, m1, m2);
5	dRh1-dHRy(Y1, m, m1, m2);
6	
7	term1=(01/Av1^2)*dAv1;
8	term2=(Q1^2/Av1^3)*dAv1;
0	term3=theta*c_id=theta*y
10	term41=2*01 hbs (01)*0//1*Rh1^(-4/3)*Av1^(-3)/
11	term42=(4/3) 01*abs(07)*dRh1*Rh1^(-7/3)*Av1^(-2);
12	
13	dMdyiv=-((1-psi)/delta_t)*term1+(theta*alpha1/delta_x)*term2-term3-theta*(1-psi)*g*nm^2*(term41+term42);
14	endfunction
84	
1	function dMdyiplv-dMdyipl (y1,Q1,y2,Q2,y10,Q10,y20,Q20,xv1,xv2,theta,psi,delta_t,delta_x,alpha1,alpha2,B,m1,m2,
	nm)
2	Av2= <u>areav</u> (y2, B, m1, m2) /
3	Rh2- <u>HPy</u> (y2, B, m1, m2) t
4	dAv2= <u>dareav</u> (y2, B, m1, m2) /
5	dRh2= <u>dHRy</u> (y2, B, m1, m2);
6	
7	term1=(02/Av2^2)*dav2/
0	term2=(Q2^2/Av2^3) *dAv2/
9	term3=theta-y-delta_x
10	term41=2*Q *abs(Q2)*dAv2*02^(-4/3)*Av2^(-3);
11	term42=(4/1, *Q2*abs(Q2)*dp=2*Rh2^(-7/3)*Av2^(-2);
12	
13	
	endfunction
99	
	function dMdQiv=dMdQi(y1,Q1,y2,Q2,y10,Q10,y20,Q20,zv1,zv2,theta,psi,delta_t,delta_x,alpha1,alpha2,B,m1,m2,nm)
2	AVI- <u>areay</u> (y1, B, m1, m2);
3	Rh1-HEY(Y1, m, m1, m2);
4	term1=Av1^(-1);

These two are Q this is dM by dQ i and this is dM by dQ i plus 1.

(Refer Slide Time: 04:00)

	Straty, 1D advanced entries a weather researce of a local full dama de destruction of a 10 kinetic and a 10 k
	dit Format Options Window Execute ?
QE	G 回 回 回 白 キ オ 英 () 日 安全な トラ 友 (X) () N/ 10 January Antonia Set, Investor (A) In () Charl Management Control (Charles I) to Harved Antonia Set) () States
	W/ Distance of entropy of the set of the
110	
11	
12	
13	
14	
99	
1	function dMdQiv-dMdOi (y1,Q1,y2,Q2,y10,Q10,y20,Q20,zv1,zv2,theta,psi,delta t,delta x,alpha1,alpha2,B,m1,m2,nm)
2	Av1-areay (y1, B, m1, m2) /
3	Rh1=HRy(y1, B, m1, m2);
4	term1=Av1^(-1);
5	term2-Q1/Av1^2/
6	term3=abs(Q1)*Rh1^(-4/3)*Av1^(-2)/
7	
8	dMdQiv=((1-psi)/delta_t)*term1-(theta*alpha1/delta_x)*term2+2*theta*(1-psi)*g*nm^2*term3;
9	endfunction
1	function dMdQiplv-dMdQipl(y1,Q1,y2,Q2,y10,m10,y20,Q20,zv1,zv2,theta,psi,delta_t,delta_x,alpha1,alpha2,B,m1,m2
	, mm)
2	Av2=areay (y2, B, m1, m2) /
3	Rh2=HRy (y2, B, m1, m2) /
4	term1=Av2^(-1);
5	term2-Q2/Av2^2/
6	term3=abs(02)*Rh2^(-4/3)*Av2^(-2);
7	
8	dMdQiplv=(psi/delta_t)*terml+(theta*alpha2/deltaerorta_a*psi*g*nm^2*term3;
9	endfunction
118	
1	function bndv-bndcon(typ, jnum, tv)
2	if(typ-1 4 jnum-3) then
3	bndy-1.43/
4	end
5	if(typ2 & jnum1) then
6	if(tv < 2000) then
7	bndv=50+(100/2000)*tv
8	end

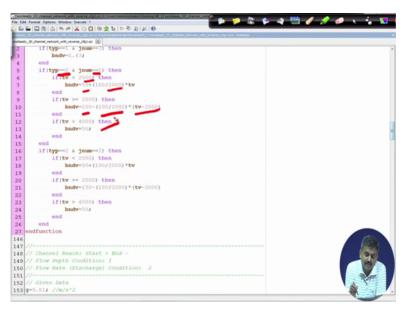
Now after specifying this we need to specify the boundary conditions. So what is this boundary condition function? This is boundary value function. This is boundary condition bndcon. This is type. If type is 1 so we will specify the depth. If type is 2 then we will specify discharge. Then junction number, depending on the junction number we can specify and tv or time value is required in this case.

(Refer Slide Time: 04:34)



So type 1 junction number 3 we have 1 point 43 which is specified flow depth at the end point. Then it is type 2 and junction number 1. This tv is less than 2000 then starting from 50, 50 plus 100 divided by 100 because it is ranging from 50 to 150. So 100 divided by 2000 into tv. This tv is greater than equal to 2000 then 150 minus which is the maximum value, minus 100 divided by 2000 into tv minus 2000. And tv is greater than 4000 then this is fixed value 50 metres cube per second.

(Refer Slide Time: 05:30)



The same thing is specified for junction number 2 which is again boundary junction. So with our initial information let us say this is our g value, eps max, t max, delta t. Delta t is 250

seconds and theta is point 5, psi is point 5. So theta equals to point 5 and psi equals to point 5 and junction number is 4. Boundary junction, we have three boundary junctions. Channel number is 3.

(Refer Slide Time: 06:16)

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0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
<pre>tendy_10_phanest_etimps_wth_entry evense_(spl sol():Deex.WdeexelratorDeatingW_11seaterdy_10_phanest_etimot_wth_entry_etimot_etimot_etimes_</pre>	
Poleady_D_deavel_retwork_with_reverse_dbl.sd [k]	
27 endfunction	
146	
147 //	
148 // Channel Reach: Start + End -	
149 // Flow Depth Condition: 1	
150 // Flow Rate (Discharge) Condition: 2	
151 //	
152 // Given Data	
153 g=9.01/ //m/a*2	
154 global ('g')	
155 eps_max=1e-6;	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	
157 delta_t=250; //8	
159 psi=0.5/	
160 //	
161 junn=4/	
162 bjn=3/	
163 chln=3/	
164 // Chl# Length Width m1 m2 Segment n S0 JN1 JN2	
165 chl_inf=[1 5000 50 0 0 500 0.025 0.0002 1 4	
166 2 5000 50 0 0 500 0.025 0.0002 2 4	
167 3 5000 100 0 0 500 0.025 0.0002 4 3]	
168	
169 jun_inf=[-99999 2 2	
170 -99999 2 2	(5)
171 1 -99999 0 172 -99999 -99999 11;	
172 -99999 -99999 1]; 173 //0: Not Connected	
174 //Positive Sign: lst section of the 1-th channel rech is connected 175 //Negative Sign: N1+1-th section of the 1-th channel rech is connected	
175 //wegative signi Wi+1-th section of the 1-th channel rech is connected 176 jun_con=[1 1 0 0	
176 Jun_con=1 1 0 0	A A A A A A A A A A A A A A A A A A A
177 1 2 0 0	

Now this is our channel information matrix, junction information matrix and then we have this junction connectivity matrix. Alpha for each channel we will consider that alpha is constant and equals to 1. So this value is 1.

(Refer Slide Time: 06:42)

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nsteady_30_sharvel_retrisk_wth_reverse_rfg1.so 12	
64 // Chl# Length Width m1 m2 Segment n S0 JN1 JN2	
165 chl_inf=[1 5000 50 0 0 500 0.025 0.0002 1 4	
166 2 5000 50 0 0 500 0.025 0.0002 2 4	
167 3 5000 100 0 0 500 0.025 0.0002 4 3]J	
168	
169 jun_inf=[-999999 2 2	
170 -99999 2 2	
171 1 -99999 0	
172	
173 //01 Not Connected	
174 //Positive Sign: 1st section of the 1-th channel rech is connected	
175 //Negative Sign: N1+1-th section of the 1-th channel rech is connected	
176 jun_con=(1 1 0 0	
177 1 2 0 0	
178 1 -3 0 0	
179	
180	
181 alpha=ones(chln,1)/	
182	
183 //Derived Information	
184 Lx=chl_inf(1:chln,2);	
185 B-chl_inf(1:chln,3);	
186 ml=chl_inf(1:chln,4);	
187 m2=chl_inf(1:chln,5)) 188 delta_x=chl_inf(1:chln,6))	
189 nm-chl inf(l(chln,7))	
190 S0=chl inf(1:chln, 8) /	Gen
191	
191 192 //Calculated	
193 mnode=Lx./delta_x+1/	
194	
195 //z values	
196 for 1=1 chln	- E
<pre>197 if(jun_inf(chl_inf(1,9),3) > jun_inf(chl_inf(1,10),3)) then</pre>	

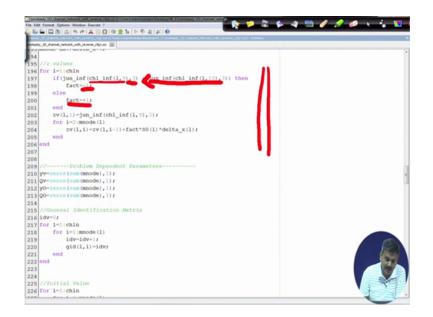
Now we can transfer these values Lx, B, m1, m2, delta x, nm and S not from this channel information matrix directly and mnode we can calculate Lx by delta x plus 1. That will give us mnode or total number of sections for a particular channel.

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entendry_ID_shwnel_netrosh_unity_energie_fig1.60	
164 // Chl# Length Width m1 m2 Segment n S0 JN1 JN2	
165 chl_inf=[1 5000 50 0 0 500 0.025 0.0002 1 4	
166 2 5000 50 0 500 0.025 0.0002 2 4	
167 3 5000 100 0 0 500 0.025 0.0002 4 3]	
168	
169 jun_inf=(-99999 2 2	
170 -99999 2 2 171 1 -99999 0	
172 -99999 -99999 1]; 173 //0: Not Connected	
173 // Wor connected	
175 //Negative Sign: N1+1-th section of the 1-th channel rech is connected	
176 jun_con=(1 1 0 0	
177 1 2 0 0	
178 1 -3 0 0	
179 3 3 -1 -21	
180	
181 alpha=ones (chln, 1) /	
182	
183 //Derived Information	
184 Lx=chl inf(1:chln,2);	
185 B=chl inf(1:chln,3)/	
186 ml=chl_inf(1:chln,4);	
107 m2-chl inf(1:chln, 0)/	
100 delta x=chl inf(1:chln,6)/	
189 nm-chl inf(1:chln,7)/	
190 S0=chl inf(1:chln,8);	(Sec)
191	
192 //Calculated	(9C)
193 mnode=Lx./delta x+1/	A
194	
195 //z values	and the second s
196 for l=l:chln	5
<pre>197 if(jun_inf(chl_inf(1, 0), 3) > jun_inf(chl_inf(1, 10), 3)) then</pre>	

(Refer Slide Time: 07:09)

Now z values, we need to calculate these z values as per our previous calculation thing. That if connectivity this one junction information this channel information L 9. L 9 will give us the starting junction. This is 3, (cha) this junction information is giving the elevation at third column. So starting elevation is more than the ending elevation then this factor is negative because we are starting from that section. Or this factor is positive if this one is less than the ending or elevation of the end section.

(Refer Slide Time: 08:13)



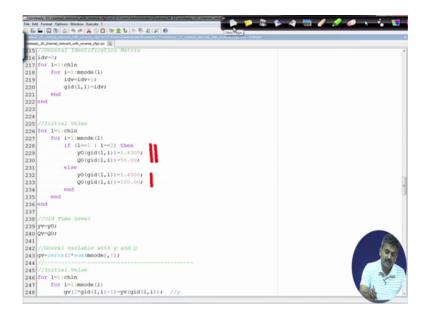
So we need to specify Qv which is Q value at future time level. Yv, Qv, yO or yOld, QOld and we have this general identification matrix gid which we have utilised for our steady state case also.

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z (gentresky, 10. chennel, network, with revenue of 1 to 0 000 per VAdmonstration/Depistop/W-1 (sentresky, 10. chennel, network) File: Edit, Format: Options: Window: Execute: ?	1 1 a
	· · · · · ·
unitedy_30_haved_network_with_revense_figLag32	
2071	
208	
209 //~~~~~ Problem Dependent Parameters~~~~~~	
210 yy=zeros (sum (mnode), 1) /	
211 QV-zeros (sum (mnode), 1) /	
212 yO-zeros (sum (mnode), 1);	
213 QO-zeros (sum (mnode), 1); -	
214	
215 //General Identification Matrix	
216 idv=0;	
217 for l=l:chln	
218 for i=1:mnode(1)	
219 idv=idv+1/	
220 gid(l,i)=idv;	
221 end	
222 end	
223	
224	
225 //Initial-Value	1
226 for l=l:chln	
227 for i=1:mnode(1)	
228 if (1=1 1=2) then	
229 yo (gid (1, i))=1.4300;	
230 Q0 (gid (1, i))=50.007	
231 else	
232 yo (gid (1, i))=1.4300/	
233 QO(gid(1,1))=100.00;	
234 end	
235 end	
236 end	
237	
230 //Old Time Level	
239 97-901	
240 29-201	

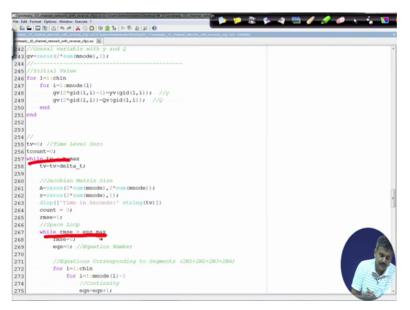
Now in this case we need to specify initial values. This is 50 and 1 point 43 for L that means channel 1 and 2. And this is 100 and 1 point 43 for this channel 3.

(Refer Slide Time: 09:06)



Old time level values we are taking this as guess value. We are starting this. Now we have defined this general variable and we can transfer these values to the general variable. After that we can start our time loop. This is our time loop, this is our space loop.

(Refer Slide Time: 09:36)



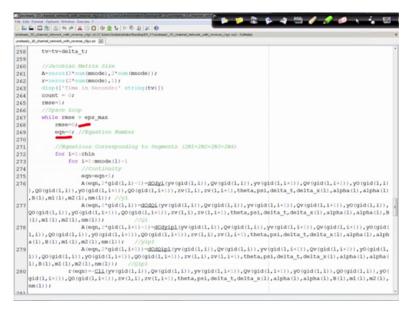
So after starting at tv equals t zero and t count this is time counter equals to zero, after entering we can increase this time value tv equals to tv plus delta t and we can specify over Jacobian matrix A and right hand vector which is r. Time display, time in seconds, count equals to zero, rmse equals to 1 to enter into this space loop.

(Refer Slide Time: 10:08)

🖉 landstady, 10, channel network, with annexes, dpl ice (Cl Ren Melvinistrative bestry, 20, 6 investigation) and (Cl Ren Melvinistrative bestry, 20, 6 investigation	A 1 A A A
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Ready To charged patrons, with resource could be in their Material and Provide W. Howeleady, To charged before the resource could be in Software	
roleady_D_thank_retrick_with_reverse_ifg1.ad [k]	
242 //Gneral variable with y and Q	
243 gv=zeros(2*sum(mnode),1);	
244 //	
245 //Initial Value	
246 for l=1:chln	
247 for i=l:mnode(1)	
248 gv(2*gid(1,i)-1)=yv(gid(1,i)); //y	
249 gv(2*gid(1,i))=Qv(gid(1,i)); //0	
250 end	
251 end	
252	
253	
254 //	
255 tv=0; //Time Level Zero	
256 tcount=0;	
257 while the chamax	
258 tv=tv+delta_t/	
259	
260 //Jacobian Matrix Size	
261 A=zeros(2*aum(mnode), 2*aum(mnode));	
262 r=zeros(2*sum(mnode),1);	
<pre>263 disp(['Time in Seconds:' string(tv)])</pre>	
264 count = 01	
265 rmse=1/	
266 //Space Loop 267 while rmse > eps max	
268 mage / 400 max	100
269 eqn=0/ //Equation Number	
270 eqn=07 77 aquation number	
270 271 //Equations Corresponding to Segments (2N1+2N2+2N3+2N4)	25
272 for 1=1:chln	
273 for i=1:mnode(1)-1	
274 //Continuity	
275 eqn=eqn+1/	
weak address	

After entering into this space loop rmse greater than epsilon max, rmse is equal to zero, equation number equals to zero. Then we can start adding equation number when we will be writing the equations for continuity.

(Refer Slide Time: 10:32)



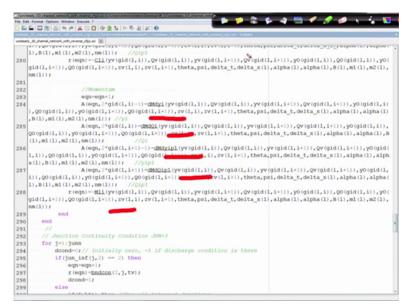
So this is for continuity. Obviously too many (thi) input variables are required for dc dy calculation. So this is first one, this is second one, this is for y i, Q i, y i plus 1, Q i plus 1 and this is minus CL i.

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	■ ■ 2011 (2011) (201
	(2) D. Jahren Jahren, Jahren K. Jahren S. La State Valence and Dessagery (1) Landewy (1) Journe (Jervers Jahren (Jervers Ja
269	eqn=u) // #quation Number
270	
271	//Equations Corresponding to Segments (2N1+2N2+2N3+2N4)
272	for l=1:chln
273	for i=1:mnode(1)-1
274	//continuity
275	egn=eqn+1/
276	A(0qu), (i)-1)=dCdyi(yv(gid(1,i)),Qv(gid(1,i)),yv(gid(1,i+1)),Qv(gid(1,i+1)),V(gid(1,i+1)),V(gid(1,i+1)),V(gid(1,i)),V(gid(1,i+1)),V(gid(1,i+1)),V(gid(1,i))),V(gid(1,i+1)),V(gid(1,i+1)),V(gid(1,i+1))),V(gid(1,i+1))),V(gid(1,i+1))),V(gid(1,i+1))),V(gid(1,i+1))),V(gid(1,i+1))),V(gid(1,i+1))),V(gid(1,i+1))),V(gid(1,i+1))),V(gid(1,i+1))),V(gid(1,i+1))),V(gid(1,i+1))),V(gid(1,i+1))),V(gid(1,i+1))),V(gid(1,i+1))),V(gid(1,i+1))),V(gid(1,i+1))),V(gid(1,i+1))))
), Q0 (gid (1, i)), y0 (gid (1, i+1)), Q0 (gid (1, i+1)), zv (1, i), zv (1, i+1), thata, psi, delta_t, delta_x (1), alpha (1), alpha (1)
	, B(1), m1(1), m2(1), nm(1)); //yi
277	$A(eqn, 2^*gid(1, i)) = acdoi(yv(gid(1, i)), gv(gid(1, i)), yv(gid(1, i+1)), gv(gid(1, i+1)), yo(gid(1, i)),$
	QO(gid(1,i)), yO(gid(1,i+1)), QO(gid(1,i+1)), zV(1,i), zV(1,i+1), theta, (delta_t, delta_t, d
	(1),m1(1),m2(1),nm(1)); ///2
278	A (eqn, 2*gid (1, i+1)-1)=dCdyip1 (yv (gid (1, i)), Qv (gid (1, i)), yv (gid (1, i+1)), Qv (gid (1, i+1)), yo (gid (1, i+1))), yo (gid (1, i+1)), yo (gid (1, i+1)), yo (gid (1, i+1)), yo (gid (1, i+1))), yo (gid (1, i+1))), yo (gid (1, i+1))), yo (gid (1, i+1))), yo (gid (1,
	$1, i)), \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ $
	a(1),B(1),m1(1),m2(1),nm(1)); //yip1
279	$A(eqn, 2^*gid(1, i+1)) = dCdQip1(yv(gid(1, i)), Qv(gid(1, i)), yv(gid(1, i+1)), Qv(gid(1, i+1)), y0(gid(1, i+1)), y0(gid(1, i+1))), y0(gid(1, i+1)), y0(gid(1, i+1))), y0(gid(1, i+1)), y0(gid(1, i+1))), y0(gid(1, i+1)))), y0(gid(1, i+1))), y0(gid(1, i+1)))), y0(gid(1, i+1))), y0(gid(1, i+1)))), y0(gid(1, i+1)))), y0(gid(1, i+1))))))))))))))))))))))))))))))))))))$
	$i)), \\ Q0(gid(1,i)), \\ y0(gid(1,i+1)), \\ Q0(gid(1,i+1)), \\ zv(1,i), \\ zv(1,i+1) \\ theta, \\ psi, \\ delta_t, \\ delta_x(1), \\ alpha(1), \\ a$
	1),B(1),m1(1),m2(1),nm(1)); //Qip1
280	$r(eqn) = -\underline{Cli}(yv(gid(1,i)), Qv(gid(1,i)), yv(gid(1,i+1)), Qv(gid(1,i+1)), yo(gid(1,i)), Qo(gid(1,i)), yo(gid(1,i)), Qv(gid(1,i)), Qv(gid(1,i))), Qv(gid(1,i)), Qv(gid(1,i)), Qv(gid(1,i)), Qv(gid(1,i)), Qv(gid(1,i)), Qv(gid(1,i)), Qv(gid(1,i)), Qv(gid(1,i)), Qv(gid(1,i))), Qv(gid(1,i)), Qv(gid(1,i)), Qv(gid(1,i))), Qv(gid(1,i)), Qv(gid(1,i)), Qv(gid(1,i))), Qv(gid(1,i)), Qv(gid(1,i))), Qv(gid(1,i)), Qv(gid(1,i))), Qv(gid(1,i)), Qv(gid(1,i))), Qv(gid(1,i)))), Qv(gid(1,i)))), Qv(gid(1,i)))), Qv(gid(1,i)))))$
	gid(1,i+1)),Q0(gid(1,i+1)),zv(1,i),zv(1,i+1),theta,psi,delta_t,delta_x(1),alpha(1),alpha(1),B(1),m1(1),m2(1),
	nm(1)) /
281	
282	//Momentum
283	eqn=eqn+l/
284	$ A(eqn, 2^*gid(1, i) - 1) = \underline{dMdyi}(yv(gid(1, i)), Qv(gid(1, i)), yv(gid(1, i+1)), Qv(gid(1, i+1)), y0(gid(1, i+1)), y0(gid(1, i+1))) = \underline{dMdyi}(yv(gid(1, i)), Qv(gid(1, i))) = \underline{dMdyi}(yv(gid(1, i$
), Q0 (gid (1,i)), y0 (gid (1,i+1)), Q0 (gid (1,i+1)), zv (1,i), zv (1,i+1), theta, psi, delta_t, delta_x (1), alpha (1), alpha (1)
	, B(1), m1(1), m2(1), nm(1)); //yi
285	
	$\texttt{QO(gid(l,i)), yO(gid(l,i+1)), QO(gid(l,i+1)), zV(l,i), zV(l,i+1), theta, \texttt{psi, delta_t, delta_x(l), alpha(l), B}}$
	(1),m1(1),m2(1),nm(1)); //Q1
286	
	$1, i)), go(gid(1, i)), yo(gid(1, i+1)), go(gid(1, i+1)), zv(1, i), zv(1, i+1), theta, psi, delta_t, delta_x(1), alpha(1), al$
	a(1),B(1),m1(1),m2(1),nm(1)); //yipi

This is for momentum, for momentum we have this dM by dy which is for y i, Q i, y i plus 1, Q i plus 1, this is minus ML i.

(Refer Slide Time: 11:23)



So after getting this 2 into N1 plus N2 plus N3 number of equations we should try to get the junction conditions. So first one is for d condition which is our condition in this case. Initial is zero if discharge condition zero equals to 1 if discharge condition is there. That means if discharge condition is there for boundary nodes then only we should utilise this otherwise we should omit it. If in junction information j2 that means column 2 if it is equals to 2 that means our discharge is specified.

We should calculate the discharge from boundary condition bndcon function and I will just change this d condition or dcon value to 1.

(Refer Slide Time: 12:35)

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if(jun_con(j,l+1) < 0) then
jn_node=mnode(abs(jun_con(j,l+1)));
A(eqn,2*jd(abs(jun_con(j,l+1)),jn_node))=1;
r(eqn)=r(eqn)+Qv(gid(abs(jun_con(j,l+1)),jn_node));
</pre>

If junction number is greater than bjn that means boundary junction then this r eqn that is equation number that should be zero because we do not have inflow condition from somewhere. So we will have only the variables. So we should start with the zero value.

(Refer Slide Time: 12:54)

Description Description 288 r (eqn (d(1,i+1)), 20 (fi nm(1))) 289 end 290 end 291 /// 292 /// 293 for j=1; junn 294 296 end 292 /// 294 dcond=0/, 295 f(jun,in 296 296 edcond=0/, 297 r (eqn 302 303 ed 304 end 305 end 306 for 1=1; 301 i 303 if (at 311 312 313	en teresen et al ter i collaren Administration Destructive Mal i successed de 2 Consent Catter ・	e 🐃 🥖 🍠 🥔 🤸 🤹 💌
288 r (eqn gd(1,i+1), 20 (g1 nm(1))) 289 end 290 end 291 /// Junction (292 /// Junction (293 for j=1; junn 294 dcond=0/ 295 end 296 eqn=e 297 r (eqn 298 dcond=0/ 299 e1se 300 if (j)u_int 301 e 302 r 303 end 304 end 305 end 306 for l=1; j 307 if (dcond= 308 for l=1; j 310 i 311 i 312 j 313 i	erverse_(fg1.ter(C.CoersVLInvestratorDesktorW_115ztationdy_10_sharver_orterse_cig1.ter) = 5ct0444	
gid(1,i+1),20 (gi nm(1)); 289 end 290 end 291 /// Junction C 292 for j=1;junn 293 for j=1;junn 294 dcond=0;/ 295 fif(jun_in) 296 eqn=e 297 r (eqn=e 298 dcond=0;/ 299 else 300 if(j) 301 e 302 r 303 end 304 end 305 end 306 for 1=1; 310 i 311 i 312 i31	everse_rdpLos 😥	
289 end 290 end 291 // Junction C 292 // Junction C 293 for j=1;junn 294 dcond=0/ 295 fir(jun_in 296 eqn=e 297 r (eqn 298 dcond 301 e 302 r 303 edd 304 end 305 end 306 for l=1; 310 if(ab) 311 i 312 i 313 e 314 e	$\begin{split} (eqn) &= \underline{\texttt{Mli}}(yv(gid(1,i)), qv(gid(1,i)), yv(gid(1,i+1)), qv(gid(1,i+1)), qv(gid(1,i+1)), zv(1,i), zv(1,i+1), theta, psi, delta_t, delta_x(1), alp$	
290 end 291 /// 292 /// 293 for j=1;jun 294 dcond=0;/ 295 if(jun_in 296 eqn= 297 r (eqn 298 dcond=0;/ 299 else 300 if(joun_in 301 e 302 r 303 end 304 end 305 id 306 for i=1; 307 if(dcond= 308 for i=1; 311 i 312 i 313 e		
291 // 292 /// Junction (293 for j=1:junn 294 dcond=0// 295 if(jun_in 296 eqn=e 297 r(eqn 298 dcond 299 else 300 if(j) 301 end 305 end 306 if(cond= 307 if(dcond= 308 for l=1:j 310 if(ab) 311 j 312 j 313 e 315 j		
292 // Junction 293 for j=1:juan 294 for j=1:juan 295 if(jun_in 296 dcond=0; 297 r (eque 298 dcond 299 elae 300 if(j) 301 if(j) 302 r 303 od 304 end 305 end 306 for i=1:j 310 i 313 - 314 - 315 i		
293 for j=1:jum 294 dcond=0;/ 295 if(jum_in 296 eqnee 297 r(eqn 298 dcond=0;/ 300 if(j) 301 eqnee 302 r(eqn 303 add 304 end 305 end 306 for l=1:j 301 if(dcond=) 303 if(add) 314 if(add) 313 if(add)	on Continuity Condition JUN=3	
294 dcond=/u, 295 if(jun_in 296 egne 297 r (eqn 298 elne 300 if(j) 301 e 303 d 304 end 305 end 306 if(dcond=/u) 307 if(dcond=/u) 308 for i=1:1 310 if(a) 311 iii 312		
266 eqnme 297 r (eqn 298 dcond 299 ellse 301 if (j) 303 add 304 end 305 end 306 if (d) 307 if (d) 308 for l=1:1j 310 if (all (all (all (all (all (all (all (al	=0;// Initially zero, =1 if discharge condition is there	
297 r (eqn 298 dcond 299 elze 300 if(2) 301 e 302 r 303 d 304 end 305 end 306 d 309 if(dcond- 310 i 311 i 312 - 313 - 314 - 315 i	n_inf(j,2) == 2) then	
298 dcomb 299 else 300 if(j) 301 e 302 r 303 e 306 e 307 if(dcond- 308 for l=1:j 309 if(lab 311 i 312 - 313 - 314 - 315 i	qn=eqn+1)	
299 else 300 if(j) 302 r 303 d 304 end 305 end 306 if(dcond- 308 fcr1-r_1; 309 if(dcond- 310 if(dcond- 312 313 314 315	(eqn) = bndcon(2, j, tv) / 🍆	
100 if (j) 301 if (j) 302 r 303 end 306 and 307 if (dondd 308 for 1=1; 309 if (and 310 i 311 i 312 iii 313 iii 315 iii	cond=11	
301 e 302 c 303 e 306 e 307 if 308 for 1=1:1 309 if 310 if 311 if 312 if 313 if 314 e 315 if		
302 r 303 d 304 end 305 end 306 307 307 if (dcond-s) 308 for 1-1; j 309 if (ab) 310 i 312 - 313 - 314 - 315 -	f(j>bjn) then //For all internal Junctions	
303 d 304 end 305 end 306 if 307 if (dcond= 308 for 1=1:5 310 if (ab 311 i 312	eqn-eqn+1/	
304 end 305 end 306	r (eqn)=01	
305 end 306 if (dcond= 307 if (dcond= 308 for l=1; j 309 if (ab 310 if 312	dcond=1,	
306 307 if (dcond- 308 for 1-1; j 309 if (ab 310 i 312 313 314 e 315 i 316 317 318 319 319 310 310 310 310 310 310 310 310	nd	
307 if (dcond- 308 for l=1:5 309 if (ab 310 if 311 if 312 if 313 if 314 e 315 if		
308 for l=1:j 309 if (ab 310 i 311 i 312 i 313 i 314 e 315 i		
309 if (ab 310 i 311 312 313 314 e 315 i	ond==1) then	
310 i 311 312 313 314 e 315 i	=1:jun_con(j,1)	
311 312 313 314 315 i	f(abs(jun_con(j,l+1)) > eps_max) then	
312 313 314 e 315 i	$if(jun_con(j, l+1) > 0)$ then	
313 314 e 315 i	jn_node=1/	1
314 e 315 i	A(eqn, 2*gid(abs(jun_con(j, 1+1)), jn_node))=-1/	
315 i	r(eqn)=r(eqn)-Qv(gid(abm(jun_con(j,l+1)),jn_node)))	
	end	
316	if(jun_con(j,1+1) < 0) then	
	<pre>jn_node-mnode(abs(jun_con(j,l+1)));</pre>	
317	A (eqn, 2*gid (abs (jun_con(j, l+1)), jn_node))=1;	
318	r (eqn) = r (eqn) +Qv (gid (abs (jun_con (j,l+1)), jn_node)) /	

Now if this dcon or discharge condition equals to 1 then only we should iterate here. Now if junction condition or (connec) junction connectivity depending on whether it is positive or negative we can identify this starting and end nodes and we can add with r eqn equals to r eqn plus Q values or subtract this one Qv.

(Refer Slide Time: 13:32)

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entendy_10_haved_petroxit_petroxit_pit as (C.VaerokiendedorCentept/_Thanked_10_haved_petroxit_pit(as), Subline protecty_0_haved_petroxit_pit(petrox_hip_entend_fit)		
300	if(j>bjn) then //For all internal Junctions	
301	eqn=eqn+1/	
302	r (eqn)=01	
303	dcond=1;	
304	end	
305	end	
306		
307	if(dcond==1) then	
308	for l=1:jun_con(j,1)	
309	if (abs(jun_con(j,1+1)) > eps_max) then	
310	$if(jun_con(j, l+1) > 0)$ then	
311	jn_node=1/	
312	A(eqn, 2*gid(abs(jun_con(j, 1+1)), jn_node))=-1;	
313	r (con) = r (eqn) - Qv (gid (abs (jun_con (j, 1+1)), jn_node)) /	
314	end 💊	
315	$if(jun_con(j, l+1) < 0)$ then	
316	jn_node=mnode(abr (jun_con(j,l+1)));	
317	A(eqn, 2*gid(abs(jun_con(j, 1+1)), jn_node))=1;	
318	r (eqn) = r (eqn) + Qv (gid (abs (jun_con (j, 1+1)), jn_node));	
319	end 🛀 🖕	
320	end	
321	end	
322	r(eqn) = -r(eqn)t	
323	end	
324	end	
325		
326	//Junction Energy Condition	
327	for j=l:junn	
328		
329	if(jun_inf(j,1) == 1) then	
330	eqn=eqn+1,	
331		
332		
333	if $(jun con(j, 2) > 0)$ then in node1=1; end	

For each junction node or internal junction node or boundary junction node we will have one discharge equation or discharge continuity equation. But if we have flow depth condition specified at the end section of 3 then we do not need any discharge condition there. Then we should omit that point. For junction energy condition if junction information 1 that is first column equals to 1 somewhere so then we should specify this boundary condition value directly and we should directly specify that value into this yv.

(Refer Slide Time: 14:39)

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325	Characterization (N	
326	//Junction Energy Condition	
327	for j=1; junn	
328		
329	if(jun inf(j,)) == 1 then	
330	eqn=eqn+1/	
331		
332		
333	if(jun con(j, 2) > 0) then jn nodel-1, end	
334	if (jun con(j, 2) < 0) then jn nodel-mnode (abs(jun con(j, 2))); end	
335	$A(eqn, 2^*qid(abs(jun con(j, 2)), jn nodel) - 1) = 1)$	
336	$r(eqn) = yv(gid(abs(jun_con(j,2)), jn_nodel)) - bndcon(l, j, tv))$	
337		
338	r (eqn) = -r (eqn) t	
339 //	<pre>/ disp(['Energy Equation Number' string(eqn) string(r(eqn))])</pre>	
340	end	
341	if(jun_con(j, 1) > 1) then	
342	for $1 = \frac{1}{1} = jun_con(j, 1) = \frac{1}{1}$	
343	eqn-eqn+	
344		
345	$if(jun_con(j,2) > 0)$ then $jn_nodel = \frac{1}{2}$ end	
346	$if(jun_con(j,2) < 0)$ then $jn_nodel=mnode(abs(jun_con(j,2)))$; end	
347	λ (eqn, 2*gid (abs (jun_con(j, 2)), jn_nodel) -1) -1/2	
348	r(eqn)=yv(gid(abs(jun_con(j,2)),jn_nodel)))	
349		
350	<pre>if(jun_con(j,1+2) > 0) then jn_node2=1/ end</pre>	
351	$if(jun_con(j,l+2) < 0)$ then $jn_node2=mnode(abs(jun_con(j,l+2)))$; end	
352	$A(eqn, 2*gid(abs(jun_con(j, 1+2)), jn_node2) - 1) = -1)$	(Alternative)
353	r(eqn)=r(eqn)-yv(gid(abs(jun_con(j,l+2)),jn_node2));	Rei L
354		198
355	r (edu) = -r (edu) i	
356	end	
357	end	
358	end	A AN

Now in this case if this condition is not satisfied and junction connectivity this one first column we have more than one entry that means let us say for internal junction we have three nodes available or three channels available. Then we should write at least two energy conditions for that one. So that is why I have written L equals junction connectivity minus 1. That means 1 to 2. That means at least two conditions we should add. We have three connected channels so we will have two conditions.

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	a long of the later is the lat	
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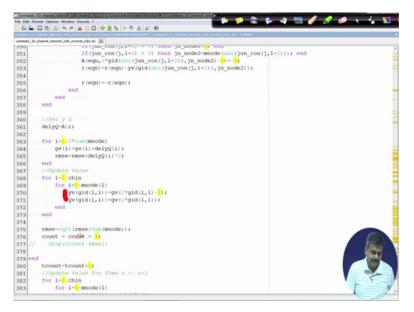
Now after writing this finally what we have to do? We have to calculate this del yQ and we have to add this del yQ with gv. Gv is general variable in our case.

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	, 10. channel, network, with province of glass (10/2) erry(Administration) besition) Well (antrone), 20. channel, petter ormat: Options: Weldow: Execute: ?	
	and option whole broker	
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343	eqn=eqn+	
344		
345	<pre>if(jun_con(j,2) > 0) then jn_nodel=1; end</pre>	
346	<pre>if(jun_con(j,2) < 0) then jn_nodel=mnode(aba(jun_con(j,2))); end</pre>	
347	A(eqn,2*gid(abs(jun_con(j,2)),jn_nodel)- <mark>1</mark>)= <mark>1</mark> /	
348	r(eqn)=yv(gid(abs(jun_con(j,2)),jn_nodel)))	
349		
350	<pre>if(jun_con(j,l+2) > 0) then jn_node2-1; end</pre>	
351	if(jun_con(j,1+2) < 0) then jn_node2=mnode(abs(jun_con(j,1+2))); end	
352	A(eqn, 2*gid(abs(jun_con(j, 1+2)), jn_node2) - 1) = -1/	
353	$r(eqn) = r(eqn) - yv(gid(abs(jun_con(j, 1+2)), jn_node2))$	
354		
355	r(eqn) = -r(eqn) I	
356	end	
357	end	
358	end	
359		
360	//Del y Q	-
361	delyQ=A\r/	
362		-
363	for 1-12*sum(mpode)	
364	av (1) = av (1) + ave y et 1 + 1	
365	end	
366		
367	//Update Value for 1=1;chln	
368	for i=1 mnode(1)	
369	yv(qid(1,i)) = qv(2*qid(1,i)-1) i	
370	yv(gid(1,1))=gv(2*gid(1,1))	
371	gv(gid(1,1))-gv(2-gid(1,1))) end	961
373	end	
374		
375	<pre>rmse=sqrt(rmse/sum(mnode));</pre>	
376	count = count + 1	

Now after adding this we need to update these values because updated values should be transferred to yv and Qv so that we can utilise these values for next iteration. And we should also calculate this rmse because if rmse is less than epsilon max we should terminate this one.

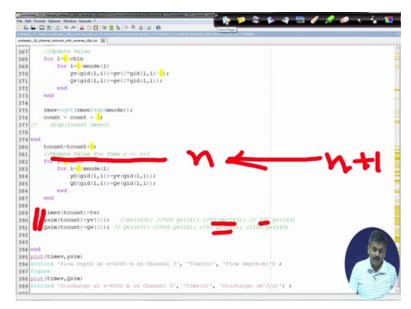
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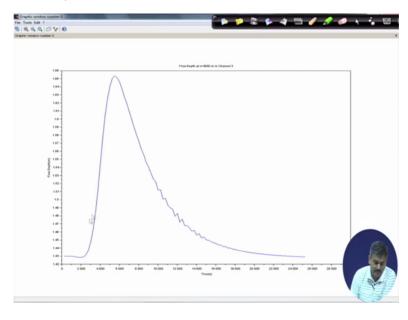
So after termination of this space loop we should update our time loop value because this new time value will be old time value for our case for the next time loop iteration. So update value for time n which is again specifying the value n plus 1 to nth level. And I have stored these values which is yv at 31 which is equivalent to x is equal to 4000 and I can utilise this value for plotting so that I can get the desired plot for this one.

If you have 100 as del x then yv and Qv should be calculated at 143. If it is del x is 43 then yv and Qv should be collected at 283 to get the information about x is equal to 4000.

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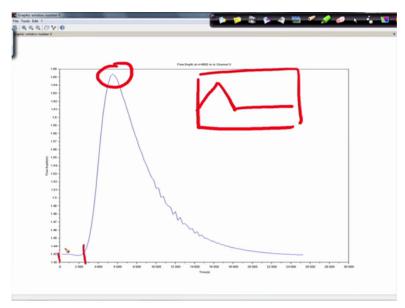
Now at that point if I run this one so time in seconds, so time is increasing so after each convergence in the space loop the time is increasing here. Now in this case we can see that two plots are there. One is for flow depth.



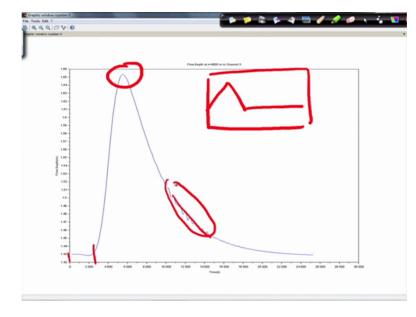
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So what flow depth we are getting? Starting from 1 point 43 here this flow depth is reaching up to 1 point 65 and above. But it is below 1 point 66. And again there is decrease because we have considered one inflow discharge at upstream. So obviously there will be increase in the depth initially with a lag, this much is the lag.

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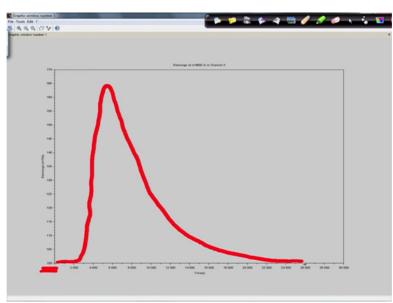
And finally there will be decrease in the depth level. But in this case we can see that some variations are there in depth.



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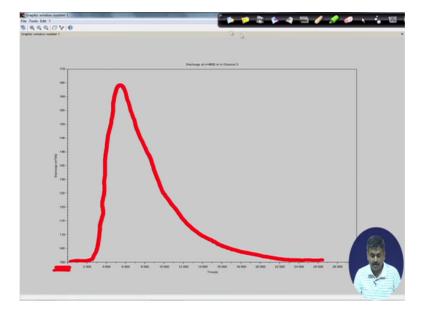
We can change theta and psi values to get different values here for depth. In this case this is a discharge plot. It is starting from 100 because we have specified 100 metre cube in this case. So this is our plot that we have got.

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So interestingly it is reaching up to 165 metre cube per second. And again this discharge values are decreasing here. Initially there is rise in the discharge obviously because of the

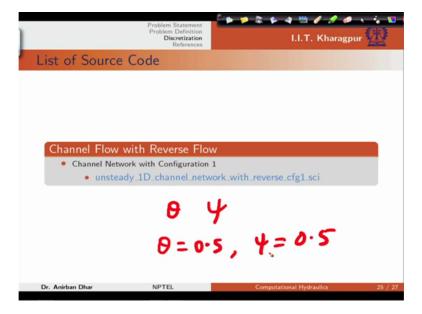
inflow condition, the upstream junction nodes at 1 and 2. But finally discharge values are decreasing again reaching to that 100 metre cube per second value.



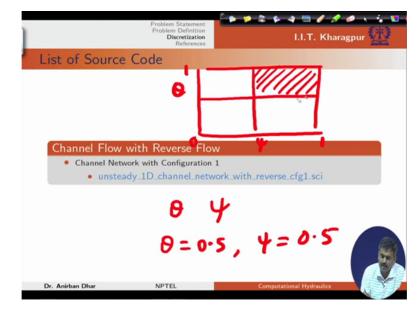
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So this is all about our unsteady channel flow problem. Now you can utilise this source code unsteady 1D channel network with reverse cfg1 because we have used only configuration 1 in this case. And try to simulate the same problem with different theta and psi values. In this case I have utilised theta equals to point 5 and psi equals to point 5 but you can change the values of theta and psi and check the stability of the problem.

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So obviously as per literature this problem this theta and psi if I start from zero to 1 in this case, if this is my psi and this is theta so obviously this part is unconditionally stable part.



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That means if both the values are more than point 5 then I have unconditionally stable situation. But check what is the solution if I change the values or I decrease one value with respect to another? Thank you.