

Application of Soil Mechanics

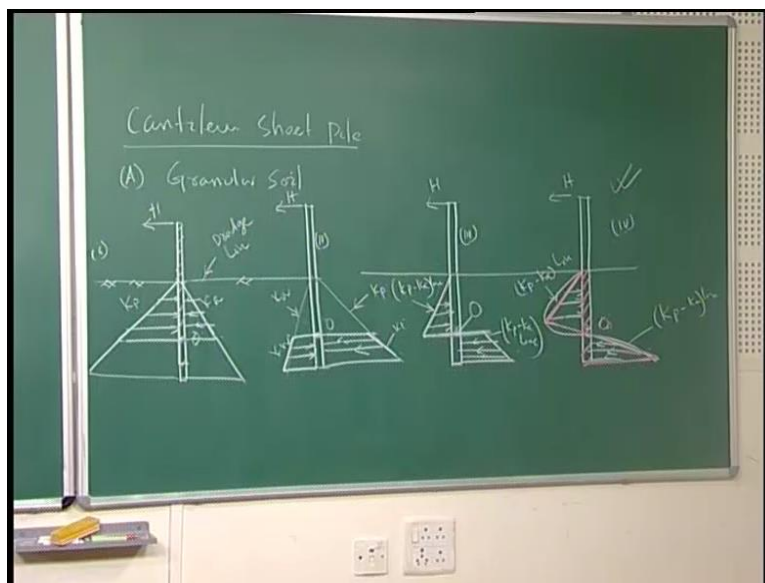
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Lecture – 03

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Now we are doing the derivation for cantilever sheet pile. First case is your for granular soil. Now as I say there will be a point of rotation in case of granular soil for cantilever sheet piles, if this is my point of rotation 'o'. The next stage how this derivation has been derived if I so this is acted upon by horizontal load H , k_p minus k_a line. This is your horizontal force.

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If we look at this diagram - complete diagram, and now if I take it the original what I explained earlier, this is my cantilever wall and there will be like, it is your dredge line. So, it says it will rotate some point at point 'o', this is called pivot point acted upon by horizontal force. So, then as I said earlier if it is rotate if this cantilever wall is rotating at point 'o', so what will happen, the top part, if I divide into two parts, one edge is your above the point of rotation, other is your below the point of rotation. If I say above the point of rotation this wall is moving away from soil. Suppose this is my soil mass, so that means, this part will be active, this is your passive state. And if we look at the bottom, it will be a reverse, and this is your passive state, and this is your active state.

So, generally passive state, we write k_p line; active state we write k_a line or k_a we write it k_a . Now the same principle if I apply here let us consider this is a cantilever sheet pile wall and this is my dredge line, and below this there is soil mass, now this is a point 'o'. Now above this above this dredge line there is nothing. So, what will happen, if this wall cantilever sheet pile wall now it will rotate at point o, it will rotate at point o, that means, if it rotate at point at o, what will happen above these this is the passive state and this is the active state.

Now I can draw this is my k_p line. If I draw the passive earth pressure it will be kind of like this and active earth pressure it will be kind of like this, so that means, I have taken consideration of passive state and active state up to at point o. Now this is the passive

line are passive state of the soil and this is the active state of soil; that means, always remember k_p is greater than k_a - passive state is greater than your active state or passive earth pressure is greater than your active earth pressure. So, that is why these triangle I have taken this your k_p ; that means, passive state or passive earth pressure, it is bigger than this line is your this triangle is your smaller this is your active state.

Now come back to if this is your first diagram, second diagram, third and fourth diagram. Now come back to second diagram; in second diagram, what is supposed to be happen, this is my point o, look at the point o, below point o what will happen. Below the point o, this wall is moving towards and this part is it is this wall is moving away; that means, if I draw a line here somewhere else below this, this is your active state and this is your passive state. Now same concept has been applied here, if I draw it completely below point o that means, this is my active state or active earth pressure will act this is passive earth pressure will act and I will remove the pressure from o to dredge line.

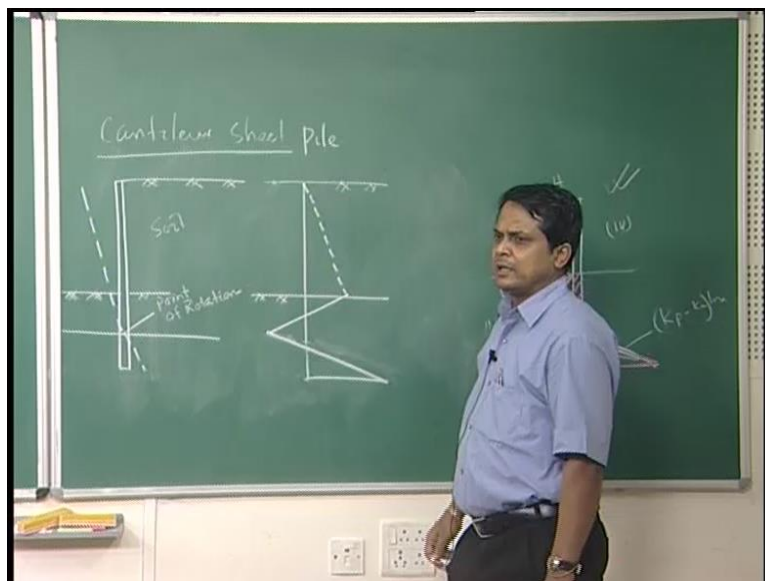
Because this concept below this is different than the concept above your point o. Below this points o, it is different passive state active state, above the point o this is passive state and active state, this is in a reverse. So, above point o, this has been neglected and below point o it is considered. So, this will be your k_a line, and this is your k_p line. Now for complete derivation, it has to be superimposed; both the cases has to be superimposed. Now these has been superimposed what happen this is k_p and this is k_a . So, this will be k_p minus k_a line, and this is your k_p and this is your k_a . In this case this is your also k_p minus k_a line.

So, now, the diagram has been drawn. So, this point is your point o. Now next question you can ask yourself will it with your failure lie, no. Why, because from passive state to active state soil cannot transit in the all sudden transition cannot be occur. Sudden transition means, if we look at at point 'o', all of sudden it is in passive state kept other side then it is moving moving and it is changing then all of sudden it is changing. So, these transition is not acceptable. So, these transition is not acceptable; that means, there will be a smooth transition from one state to other state; one state of failure and other state of failure, there should be a smooth transition. So, that is why it has been drawn. So, that it is slowly, slowly decreasing and it is achieving this other failure transition.

So, now this is your final failure mode of cantilever retaining wall below means in granular soil having a point of rotation o above the base. Now how it looks, it looks like this. Now these are the assumptions for particularly considering not non-linear actual case of this how it should be looks like, it should be a kind of curvilinear, it is a curvilinear it has been approximated to simple straight line or may be linear failure you can say it. So, if I take it this is my final failure surface of this cantilever retaining wall having embedded in granular soil that means, it is starting from one state to other state, there is a smooth transition. This concept has to be used for derivation of cantilever sheet pile wall for derivation of equation; that means, what is the capacity cantilever sheet pile wall in granular soil.

If I remove all one, two, three and keeping only this part final form of this equation. So, we will start this derivation, how the derivation has been made. Now instead of suppose I say there is there might be a soil mass above the cantilever, there might not be a soil mass above the cantilever.

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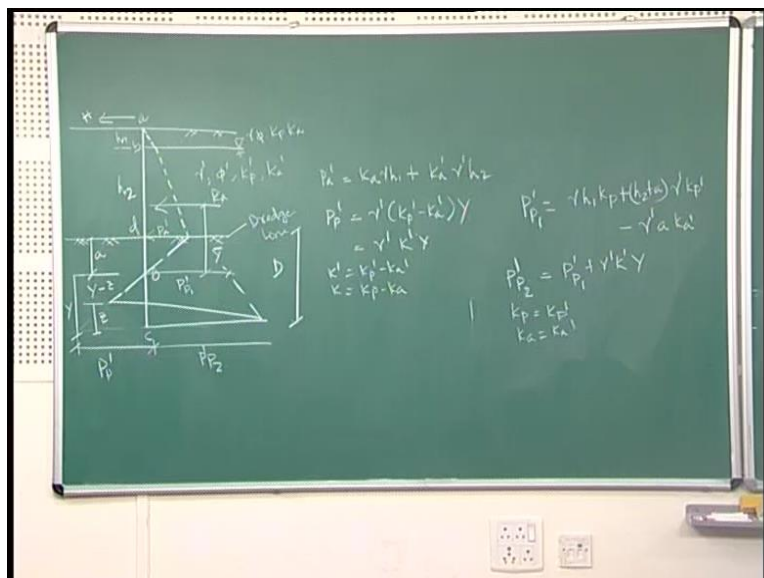
As I said cantilever sheet pile walls are two types one is your free cantilever other is your fixed cantilever, other is a simple cantilever sheet pile. In case of free cantilever, there is nothing in case of this is a typical case of free cantilever. So, both these sides, there is nothing this will the stability will be achieved by means of your embedded tip, but the moment I say that cantilever sheet pile that means, it has been embedded at one end. it

will retain your soil mass. Now if I modify this as only this is case of free cantilever. Now I am saying that only cantilever sheet pile wall, how it looks this is the cantilever sheet pile. Now this is your dredge lane line dredge line, now it rotate like this, now here at other end here, at this end it is retaining soil, because this is not a case of free cantilever sheet pile. So, it is retaining the soil now how the failure surfaces will be there.

If I take this principle of this, look at these derivation of this failure surface below the dredge line for free cantilever sheet wall has been taken. It has been taken, it has been put it here. Now if you consider the top part, as it is retain in this soil mass, it will generate active earth pressure up to this. Now this is the final form of your soil mass, this is the final form of this failure surface of cantilever wall retaining wall, cantilever sheet pile wall, one side it retain your soil mass.

Now you can say that with these conditions what are the most adverse condition may occur while it could derivation the water table may be at the ground surface may be somewhere else at the ground surface. So, there are conditions are there, but this failure surface whatever we derived from free cantilever sheet pile wall that has been applied for your cantilever sheet pile wall now coming back to your complete derivation.

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If I draw it, this is the dredge line. Now below this left, let us say this is my point of rotation. Now let us say at any distance below the surface - ground surface, at the top there is your water table, this is a symbol of water table. Now I am drawing the pressure

distribution diagram a b, now this is your b a. This is the complete failure surface how the derivation has to be done now. If I take it this is my dredge line, this is the water table. So, let us say this property is $\gamma \phi k p$ and $k a$, and below the water table, the property is as let us say [FL].

So, this property, I can write it because water table is there this will be γ' , ϕ' , $k p'$ and k' . Now let us say this distance is h_1 and this distance h_2 and a b, let us name d, this is point o, this is your c, now it will be acted upon by let us say a resultant force, this will be your P_a - active earth pressure prime. Let us say all these forces, this is your resultant force R_a . Particular from this to this, this is your resultant force R_a . It acted upon by it say suppose say at a distance \bar{y} from point o. Now this distance say a, because why I am naming this derivation has to be made for this to find it out what is the capacity what load these wall can take, this is your distance a. Let us say from here to here, this is your distance y. Now these to these, let us say $y - z$ and this is your distance say z, this your c.

So, now, if I put it like this, this to this, let us say it is P_p prime, and this is your say $P_p 2$ prime. And in between, if I take it this pressure distribution you will go like this. So, in between from o to this, I say $P_p 1$ prime. Now this failure surface concept has been taken from once again I am saying from free cantilever sheet pile to cantilever sheet pile wall. And this below this whatever this free cantilever sheet pile, the failure surface it has been adopted and this failure surface is drawn. Now this I put it most adverse conditions what what may possible in most adverse condition may be possible during rainy season, may be this water table fluctuate from ground surface from the below from the dredge line this water surface, water table may be raise to a ground surface.

So, now if this complete of this what were suppose to get where suppose to get what is the capacity and what distance this is your complete distance d, I should know depending upon the capacity how much depth this cantilever sheet pile can be embedded below your dredge line. Or can be put it below your dredge line this is your output this parameter to be require to find it out as well as the capacity h what capacity it can take this two parameters to be find it out. So, k and $k p$ is your Rankine earth pressure coefficient.

So, let us start with this P_a for this diagram complete. If we look at this for this diagram

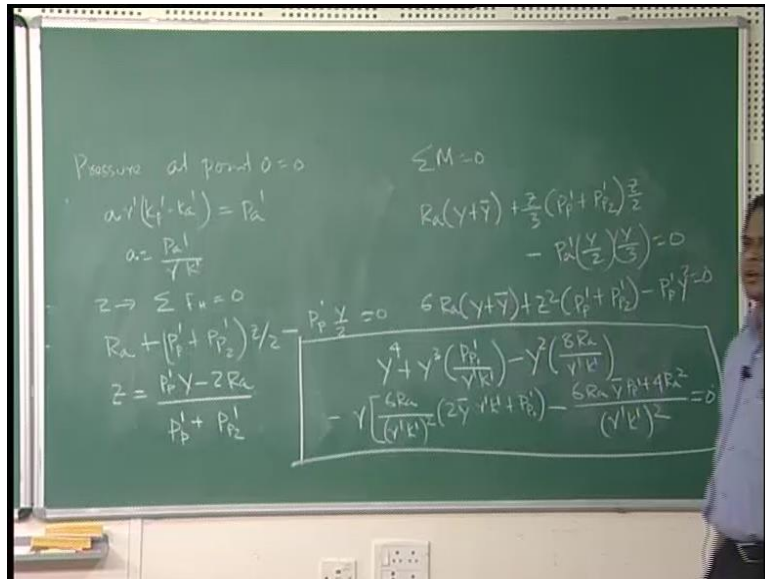
this is your P_a . So, what is your p_a p_a is your active earth pressure from a to up to your dredge line active earth pressure from a to active up to your dredge line. So, P_a is equal to $K_a \gamma h_1$ plus $K_a' \gamma' h_2$. Now what is your P_p ; P_p is your effective passive earth pressure at the base of pile. This is your P_p which is equal to $\gamma' k_p$ minus k_a into y , basically, earth pressure is your γ either k . If we look at how the derivation here earth pressure will be k_a , $k \gamma h$; h is your distance, γ is your unit weight of soil, and k should be either k_a or k_p .

From this concept, it has come here because your water table is lying here below this, this will be somewhat unit weight that is why it is $\gamma' k_p$ is your k_p minus k_a as I derived here. This is a k_p minus k_a , and the distance will be your y . Now it will be $\gamma' k_p y$. So, k_p is nothing but your k_p minus k_a , and k is equal to k_p minus k_a . Now what is your P_{p1} passive earth pressure at point o, what is the value of P_{p1} .

Now P_{p1} is equal to at point o, it will be $\gamma h_1 k_p$ plus h_2 plus a $\gamma' k_p$ minus $\gamma' a k_a$. So, it will be your $\gamma h_1 k_p$ plus $\gamma' k_p h_2$ minus $\gamma' a k_a$. This diagram plus $\gamma' k_p h_2$ minus $\gamma' a k_a$, this is your h_2 plus a up to this how much it is coming minus $\gamma' a k_a$. If we look at a, this part will be your active state $k_a k_p$ and minus this is your active state because this part is also soil is there. So, this part will be active. So, $\gamma' a k_p$.

Now similarly, it can find it out P_{p2} , which is equal to nothing but P_{p2} plus $\gamma' k_p y$ γ' ; $k_p y$, which is your $\gamma' k_p$ and Y is your this distance, it should be added. If the value of ϕ , remember if the value of ϕ for both the persons is same for both the persons is same value of ϕ value then it will you k_p is equal to k_p is equal to k_p and k_a is equal to k_a . Now these at the values you get it, P_a P_a P_a P_p P_{p1} P_{p2} based on your earth pressure distribution diagram know we have to find it out what is the resultant earth pressure that is the resultant earth pressure. So, let us say R_a is equal to resultant of all forces above point o R_a is equal to resultant of all forces above point o above point o the point o is located at a distance a below the your dredge line point o is located at a distance a below your dredge line. So, now, the pressure at point o is zero.

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Now, the pressure at point o is zero. With this concept, pressure at point o is equal to zero; with this concept a gamma prime k p prime minus k a prime is equal to P a prime is equal to P a prime. Now a, it can find it out the distance is equal to P a prime by gamma prime and k prime k prime. Now this distance Z, now what are the other parameter, this distance Z has to be find it before before finding out R a, this distance to be find it out in terms of k a and k p now distance Z you can find it out. So, distance Z can be find it out Z. It can get it by taking summation of force in horizontal direction is equal to zero.

Now R a this force this is acting in this direction R a plus your P p prime P p two prime into Z by two into Z by two if we look at here P p two prime and P p prime P p prime into Z by two. This is a triangular distribution this will act with Z by two plus [FL] minus P p dash minus P p dash minus P p dash. This is your P p dash minus P p dash Y by two is equal to zero. From this you can find it out Z is equal to P p prime Y minus two R a by P p prime plus P p two prime. Now how many unknowns there are two unknowns you do not know Z you do not know R a so; that means, additional equation is required; that means, you take you take moment at the bottom should be zero

So, taking moment at the bottom is equal to zero. Now it will be R a Y plus Y prime plus Z by three P p prime plus P p two prime into Z by two minus P a prime Y by two into Y by three is equal to zero; that means, I have considered there are two unknowns two equation is required. One is your force in horizontal direction is equal to zero; other is

Now it this putting this value of Z putting this value of Z here to here now this will be forth ordered differential equation is on will be derived. Now this forth ordered differential equation, if it write in a form, it will be Y forth plus y cube P p one prime by γ prime k prime minus Y squared eight R a by γ prime and k prime. It will be minus γ six R a by γ prime k prime is whole squared into two Y prime γ prime k prime plus P p one prime minus six R a Y prime P p prime plus four R a squared by γ prime k prime whole squared is equal to zero. This is your final form of equation this is your final form of equation in a fourth order differential equation sorry fourth order equation it is not differential equation it is a fourth order equation.

So, how you can derive it can be derive by means of trial by means of trial and error method, one in you put this values then whether it is becoming zero or not, satisfying or not. You see first what happen, you take a value, you see that whether it is negative or positive depending upon that you take, this second set value. Then it will be it has to be approximated by means of trial and error method, you have to solve it. And with this solution, factor of safety can be provided by two methods, one is you get it; once is get it, the end array value, you can provider to factor of safety by two methods.

$(C) \quad D \rightarrow 20 \text{ to } 40\%$
 OR
 $(II) \quad 1.5(T.S) \rightarrow \frac{p_1}{\bar{p}} \text{ or } \frac{p_1}{p_2}$

One is your the value of the obtain should be increased by twenty to forty percent or second factor of safety, you can take it one point five factor of safety one point five factor of safety. You can take in k_p and or k_a ; that means, while designing at the end, what you are suppose to get the value of D , you are get at the end, suppose to get your value of D how much your depth D . So, how do take the factor of safety either whatever you are getting the point d , when distance this can be increase twenty to forty percent for your factor of safety or you can take one point five factor of safety in k_p and k_a in k_p and k_a . We will solve a problem may be next class.