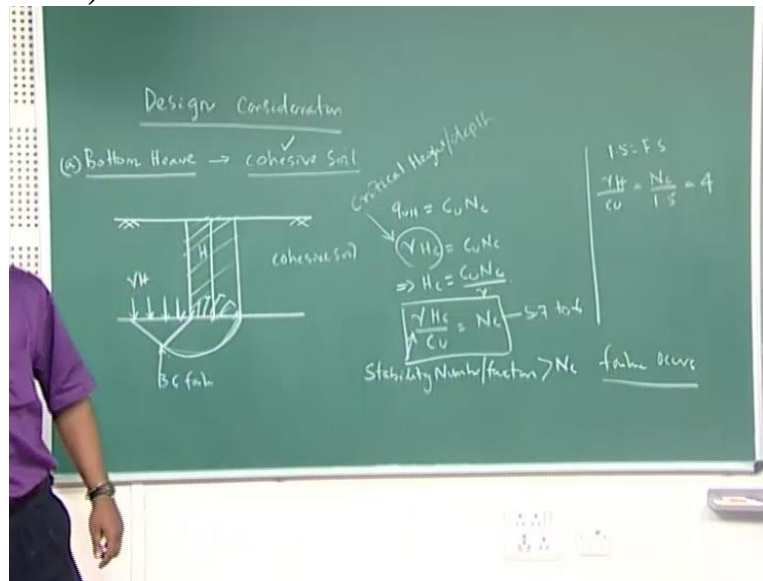


Application Of Soil Mechanics
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Lecture # 11

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As we discussed last class about the design consideration of braced excavation. First one is your bottom heave formation or bottom heave. It occurs generally in cohesive soil. Let us say, this is a cohesive soil and this part is your ground surface, and this is your height H of the excavation of height H and this is overburden γH , and this you can say that bearing capacity failure. Then this comes as a heave. For homogenous soil, clay q ultimate, for clay q ultimate is equal to $C_u N_c$, C is your $(())$ cohesion. And for critical depth, γH_c is equal to $C_u N_c$ – this is your critical depth, that means H_c is equal to $C_u N_c$ by γ . And you can write it down like this γH_c by C_u which is equal to N_c , generally the value of N_c is 5.7 to 6. So γH_c by C_u , it is called stability number. If stability number or stability factor, greater than N_c then failure occurs.

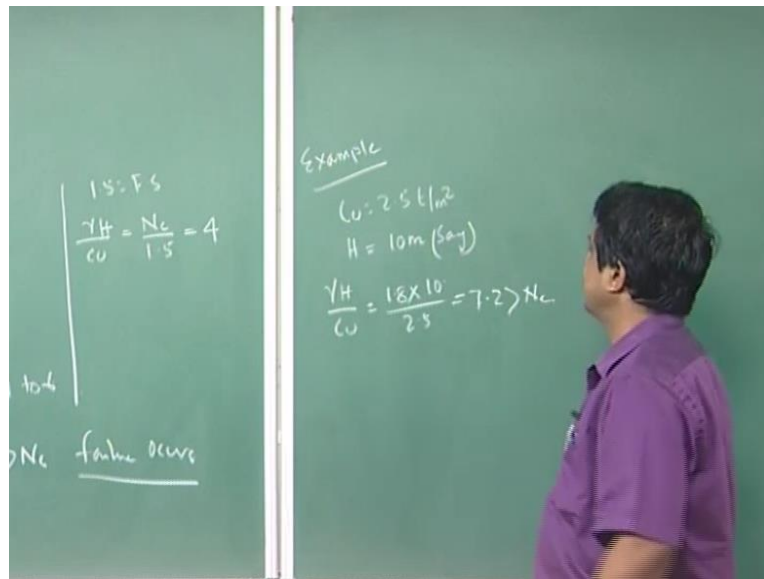
For a factor of safety of say, 1.5, factor of safety of 1.5, you can write out γH by C_u which is equal to N_c by 1.5 which is equal to 4. Now what is it mean, if we look at they are, if you remember well last class we discussed about the one of the design criteria or design consideration is about your bottom heave. This bottom heave generally occurs in what kind of

soils, generally it occurs in case of cohesive soil. How the bottom heave has been formed, as you go more the deep, more depth you cut vertical cut means below the ground surface then what happen this overburden pressure will pressure. Because of this increasing overburden pressure, below the cut what will happen this soil will fail by means of bearing capacity. Once this soil will fail, then nearby soil will be pushed, so that there will be a heave or meson, in the exavations. So this is your exavations.

This shaded area is your completely exavations; and in this exavations, once there is a heave formation, heave means the soil from the bottom will come insight your underground exavations. Once this thing has been occurred, what will happen, whatever the structure constructed here like Metrorail underground, so it will also fails. So to start with this, understand this phenomena, let us say for this cohesive soil, this is a cohesive soil, what is the bearing capacity? For cohesive soil bearing capacity is, purely cohesive soil, there is no pile $C N_c$ or $C u N_c$. C is your (()) cohesion. Then this $C u N_c$ is nothing, you have to equate it to critical height. So that means, it is not in a kind of critical height, if you equate it into this will be your γH_c , critical depth or critical height. So this $C u N_c$ depends upon your critical depth.

Now from there critical height is coming H_c is equal to $C u N_c$ by γ . If I take this all the terms γH_c by $C u$, this is called stability factor. γ is C by $C u$, this is called stability factor, which is called to N_c that means this N_c value is generally for ah bearing capacity factor for cohesion value for purely cohesive soil, it is 5.7 to 6. That means γH_c by $C u$ is your stability number or stability factor, which is if it is this stability number or stability factor, if it is greater than N_c , that means failure occurs for cohesive soil. Failure occurs means, what will happen, there will be a bottom heave formation, that means this is the condition the stability number or factor, it should be less equal to N_c . It should not greater than your bearing capacity factor for cohesive soil.

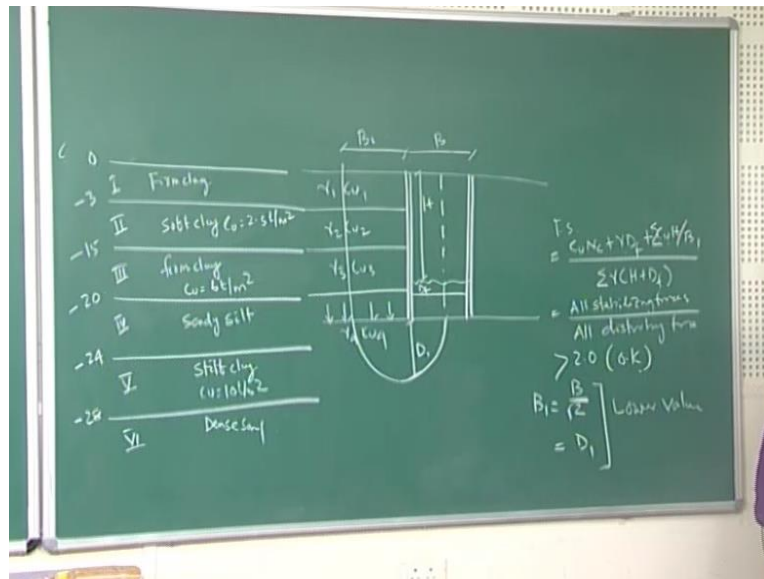
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Now for example, in (()) soil C_u is equal to 2.5 ton per meter square. And H generally cot, typical example I'm taking Calcutta metro H is equal to ten meter say height of cot excavation. So γH by C_u which is equal to γ is equal to 1.8 into H is equal to 10 by 2.5, which is equal to 7.2 greater than N_c . That means, if there is your underground construction, underground construction in Calcutta soil, there is a chance that bottom heave will be formed, bottom heave formation will be there. So this is your first criteria for design consideration that is your bottom heave. Then another example, this is you can say that this is a uniform soil, suppose this soil is purely uniform there is no layer soil that means say constant value of C_u is there. This is your calculation.

Now if I go for second example, so how do you prevent before I solve this second example, how do prevent? The prevent will be, you have to deep water, you have to deep water from the cohesive soil, so that water depth will go below your for below this depth, so that it will become harder slightly harder, so that bearing capacity failure may be avoided.

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So example two, there are six layers of soil. As I said, this is not a uniform soil layer. So layer one is your firm clay. Layer two is your soft clay, C_u is equal to 2.5 ton per meter square. Layer three again it is firm clay, C_u is equal to six ton per meter square. Then layer 4 is your sandy silt; and layer 5 is your stiff clay, C_u is equal to ten ton per meter square. And layer six is equal to your dense sand. Now there is a chance that there is a cut off to sand silt that means vertical cut off, you do the vertical ground excavation, you go for if these are your all your soft soil at what depth you can go for your vertical excavation, where you are getting a kind of hard stratum. This is sandy silt or dense sand, you can go here.

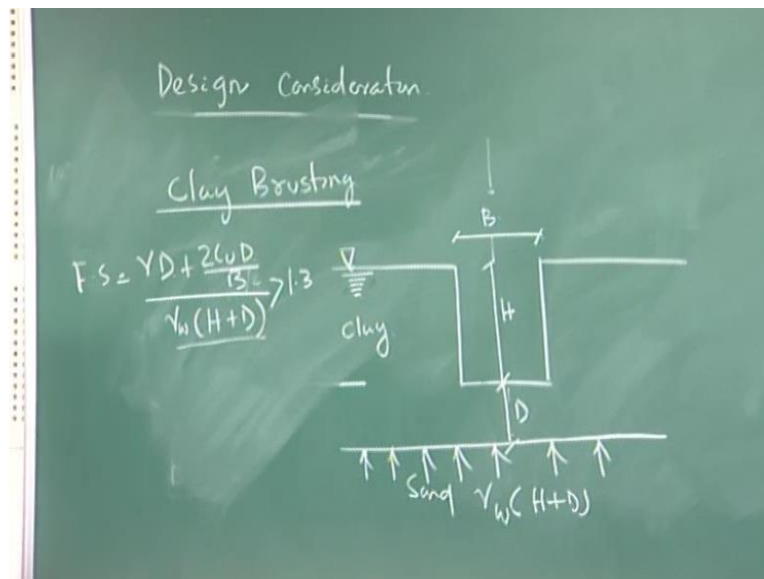
So if I draw with this there is a vertical cut in excavation up to sandy silt. Let us say with this sandy silt say, this is your D_f and this is your kind of you can write H and let us we put it layer by layer, layer 1, layer 2, layer 3. Layer one is equal to γ_1 , $C_u 1$; γ_2 , $C_u 2$; γ_3 , $C_u 3$ then from they are it is starts like this. Then let us say this is my case of D_1 , then this is γ_4 and $C_u 4$. Then if it is coming in this way up to the middle, the bearing capacity failure, I am showing up to this middle like this. So let us say the failure envelope from here, you can extend up to B_1 , and here it will be completely B . Now factor of safety is equal to $C_u N_c$ plus γD_f plus $C_u H$ by B_1 by γH plus D_f . So that means this is your all stabilizing forces divided by all disturbing forces. Then what will happen, the factor of safety greater than 2.0, it will be ok.

If the factor of safety is coming out to be for against your bottom heave, if it is greater than two point zero then it is ok. So what we are basically doing, we are taking a influence line, influence of failure envelope here up to a distance B_1 ; and this is B , here it is extend B_1 . How do calculate B_1 , so B_1 is equal to B by root two and D_1 , from there it is your lower value. If we look at here, first with check your stability number and factor, it should be greater than N_c , so that if it is greater than N_c then failure will occur, based on that you can calculate your factor of safety. For finding out factor of safety, let us say this is an exavation, there are one, two, three, four, five, six number of layers and at two positions or fourth number of layer this is sandy silt. And sixth position is your dense sand, so that means your exavation, you can extend from here to here or exavation you extend from here to here. That means the base of your exavation till exavation where you are doing up to that depth it should be ensure that up to that depth at that depth, there is a hard stratum line, that means this is your hard stratum line – sandy silt or dense sand.

So what happen, I'm taking a this is my involvement D_1 is your influence area based on your bearing capacity, so once your are getting then there will be a depth of foundation, this will be also given, height also given, B also given, only you have to find it out B_1 and D_1 . So D_1 one will be come, it will come based on your bearing capacity calculation. Then once you get D_1 one then you can check your factor of safety. Your factor safety is equal to there are 5 layer; 1, 2, 3, 4, 4 layers, that means $C_u 1 N_c 1$, $C_u 2 N_c 2$ all for you calculate plus $\gamma D_f - \gamma$ into depth of foundation, depth of these depth γD_f plus $C_u H$ by B_1 . This $C_u N_c$, this one is your $C_u N_c$, and $C_u H$ by B_1 - this summation of $C_u H$ by B_1 by γH plus D_f divided by γH plus D_f .

If you look at here, all stabilizing forces dividing by all disturbing forces, from there you have to find it out your factor of safety is equal to 2.0. And B_1 you are going to calculate, B_1 is equal to B by root 2 or D_1 . B_1 is equal to as it is given B and D , so B by root two or D_1 that means which is lower. Lower value of B_1 , you are supposed to take it. This is for design consideration of bottom heave. Then next part is your clay brusting. How to calculate factor of safety for your bottom heave, this has been done.

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Then for clay brusting, what is the condition for clay brusting. Clay brusting means clay soil sample will come out along with the water. If there is a clay layer of shallow depth, then there is a water table, then water table is a ground surface, then below the shallow depth of clay if there is a kind of sandy soil, sand or sandy soil or sand then there is chance of clay brusting. In these case, the factor of safety, how comes the clay brusting will come, the sand will give upward movement. If we look at here, this is your clay of a shallow depth of the clay layer is there, then here there is a sand layer, so once you start excavation that means you completely excavate, excavate and small part above your sand you are there, you stopping there. What will happen this along with this water, it will make upward force, so what will happen mixture of sand and clay, it will come up in the excavation. So you have to stop the clay brusting. Clay brust means it will brust out and puncture and the clay will come out from the excavation, that is the meaning.

So what is the factor of safety you should take it, factor of safety is equal to $\gamma D + \frac{2cuD}{B}$ divided by $\gamma_w(H+D)$ which is equal to greater than one point three. γD , γ times into D – γ times into depth of D plus two $C u D$, two times $C u D$ into B , it is nothing but $C u D$ by B by two. So this B by two, this two, because this half of the part will be taken into consideration. So once this half of part is taken into consideration, so B by two that means these two ((Refer Time: 19:58)) there. So two $C u D$ (Refer Time: 20:00) by B then for upward thrust, this is your upward thrust, upward thrust will be γ_w into H plus D . γ_w

w is your unit weight of water and H plus D is your this height up to this height, it is applying your upward thrust. So this factor of safety would be greater than one point three for design consideration of clay brusting, that means each case we have to check this whether this factor of safety is satisfying or not. If it is not satisfying, then this design has to be changed that means the depth has to be changed or other criteria the thrust has to be provided very close to each other.