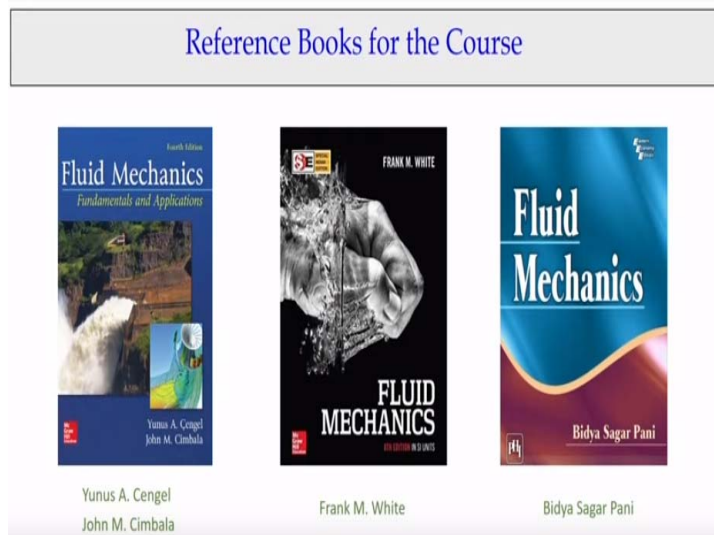


Fluid Mechanics
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Lecture - 13
Fluid Statics Applications: Example Problems

Welcome all of you to Fluid Mechanics course. Today we are going to solve the problems on fluid statics.

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Before starting that again I repeat that these are the three books we follow to solve fluid mechanics problems. But today I will focus on the fluid mechanics problems in GATE exam and Engineering Service Exam.

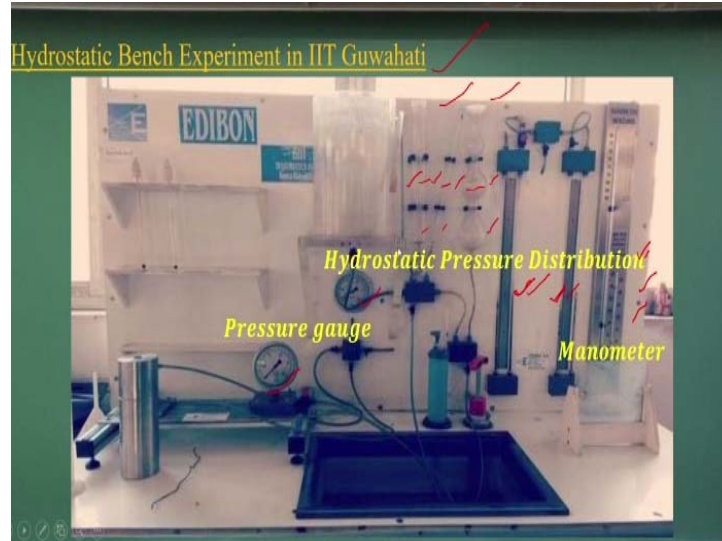
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Contents of Lecture

1. Hydrostatic Bench Experiment
2. Formulae
3. Problems

Looking that today I will cover with a introductions to hydrostatic bench experiment. Then some formulaes, then we will solve 10 problems from GATE exam and Engineering Service Exam.

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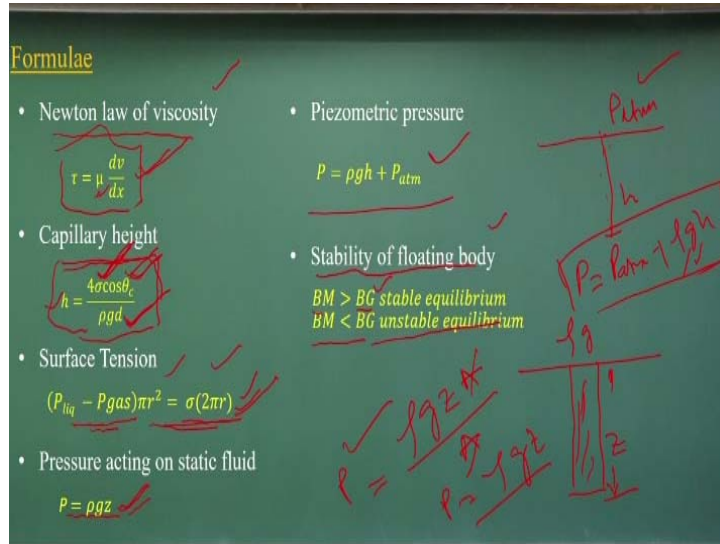


Now let us look at the hydrostatic bench experiment setup, which is there in IIT Guwahati. So this type of experimental setups which is called this hydrostatic bench experiment setup, you can see the pressure gauge, you can see the pressure gauge. You can see this mercury manometers. So these are mercury manometers are there. These are U-tube manometers are there.

And you can have conduct different experiments using this pressure gauge as measurements, the manometer measurement, and U-tube manometers. Not only that, there is the experiment setups to prove the Pascal's laws that the pressure in a horizontal surface remains the constant. That what you can see there is a different shape of the containers are there.

So when you fill up the fluid if it is at the rest you will have the same horizontal plane will be developed irrespective of whatever the shape of the containers. That is the hydrostatic if they are connected it. This is what we discuss more detail while teaching the hydrostatics, basic hydrostatics concepts and we also derive the equations for that.

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Now let us I just write the formulae, okay. And just to repeat the things what we learnt in fluid basic properties and the fluid statics that the Newton's laws of viscosities we established the relationship between shear stress and the velocity gradient.

Newton law of viscosity

$$\tau = \mu \frac{dv}{dx}$$

μ =dynamic viscosity

Similar way also we derived the capillarity height in terms of the diameter of the capillarity tube.

Capillary height

$$h = \frac{4\sigma \cos \theta_c}{\rho g d}$$

θ_c = angle of contact

σ = surface tension force

d= diameter

h=capillary height

The surface tension force when we equate with a pressure difference and the area where it is acting it the force, both the side the force equating what you have done it the force the net force acting on this part is taking care of the force due to the surface tensions.

Surface Tension

$$(P_{liq} - P_{gas})\pi r^2 = \sigma(2\pi r)$$

That what is here and as you know very basic things, when you consider z as a at the free surface level is zero.

As z increases in the downwards the pressure will be

$$P = \rho gz$$

So that what it indicates of a linear pressure distribution when fluid is at the rest. But, if you consider that the at the atmospheric P equal to P atmospheric pressures and at the height h what will be the pressures which is very simple is

$$P = \rho gh + P_{atm}$$

ρ is the density,

g is acceleration due to gravity.

And next one what we know it, how a floating body's stability we analysis with respect to BM and the BG the distance between the buoyancy to metastatic points, the buoyancy to the center of gravity, that is what will be show us that whether the body is of a floating bodies is a stable or unstable conditions. That what we will get it.

$$BM > BG \text{ stable equilibrium}$$

$$BM < BG \text{ unstable equilibrium}$$

So let me repeat these things that very simple things as we discuss the Newton laws of viscosity which establish the relationship between shear stress and the velocity gradient. Similar way we derive the capillarity height will be a functions of contact angles, surface tensions, and the d, d stands for here the diameter of the capillarity tube. Or you can equate the force acting due to the pressure difference and the surface tension forces that what we equated.

And very simple, what will be the pressure distribution in a fluid which is at the rest the static fluid will be the weight of the fluid divide by the area.

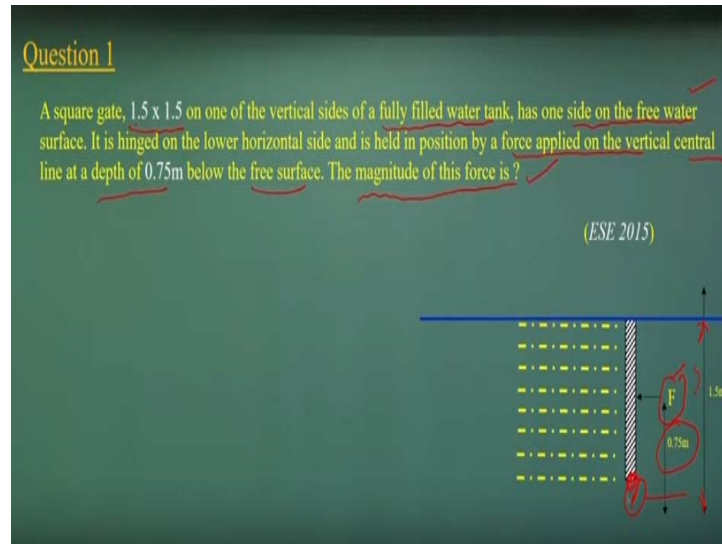
$$P = \frac{\rho gzA}{A}$$

$$P = \rho gz$$

We will come it or simple way, if I am to know it, the if it is a z is a total depth of a or depth of a fluid and ρ is density g is acceleration due to gravity, the weight will be the ρgzA divide by the area I get the pressures the weight per unit area, that what I get the pressure.

Simple way $P = \rho g z$. But when you consider P equal to atmospheric then we have considered this part. So very simple way we can compute pressure distributions when fluid is at rest conditions.

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Let us start to solve the problems, these very easy problems that there is a square gate of a dimensions of 1.5 meter into 1.5 meters. One of the vertical sides of a fully filled water tank has one side on the free surface. It is hinged on the lower horizontal sides. Here it is a hinged it and is held in a positions by force applied on the vertical the central line at a depth of 0.75 meter below the free surface.

[A square gate, 1.5 x 1.5 on one of the vertical sides of a fully filled water tank, has one side on the free water surface. It is hinged on the lower horizontal side and is held in position by a force applied on the vertical central line at a depth of 0.75m below the free surface. The magnitude of this force is?]

So this is 1.5 meters and 0.75 meters below means 0.75 meter from the bottom, from the hinge. This is what 0.75 meters, total is 1.5 meters. So what could be the magnitude of this force? What could be this force part. So this is the force. You can easily solve these problems. The problem is that we need to know hydrostatic pressure distributions. Then we can compute the force due to the hydrostatic distribution.

Once I know what is the force is acting because the fluid is at the rest and where it acts the force that the locations. If I know the force, the center of pressures or the force where is acting it, if I know that to the force magnitudes or the at the locations where

the force acts then I can take a moment at the hinge locations to compute what will be the force component.

Flow Classification:

Static fluid

Control volume is static

Homogeneous fluid

So the problems wise it is a very easy problems to solve it. Only we need to draw the pressure diagrams, compute the force due to this pressure diagrams and we need to find out where this force acts, the center of pressures, where the force act. Then we try to take the movement at the hinge locations as you know it the sum of the moments should equal to zero if in case of the hinge conditions.

That the conditions we use it to compute the F value. That is very simple things. Let us have F as we used to do the flow classifications. Here is fluid is rest. Need not to draw any control volumes. But if you want to draw a control volumes to draw the pressure diagram for that we can do it but I am not highlighting this the control volume this case.

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Pressure Distribution:

- Atmospheric pressure on water surface $P_{atm} \approx 0$
- Hydrostatic pressure distribution valid
- Pressure distribution varies linearly with depth

Net Force exerted by fluid = $(\frac{1}{2}) \times 1.5 \rho g \times 1.5 \times 1.5$

$$F_{fluid} = \frac{1.5^3}{2} \rho g$$

Point of application of this force from bottom = $(\frac{1}{3}) \times 1.5$

Taking Moment about hinge

$$(1.5/3) \times F_{fluid} = F \times 0.75$$

$$(1.5/3) \times 1.5^3/2 \rho g = F \times 0.75$$

$$F = 11.036 \text{ KN}$$

Now the pressures at the water surface levels will be the atmospheric pressures, will be the atmosphere pressures and we can consider this atmospheric pressure is close to the zero okay that as compared to the pressure distributions.

$$P_{atm} = 0$$

This the correct the pressure distribution varies linearly with respect to the depth. That is what will be the pressure distributions.

Net Force exerted by fluid = $(\frac{1}{2}) \times 1.5 \rho g \times 1.5 \times 1.5$

$$F_{\text{fluid}} = \frac{1.5^3}{2} \rho g$$

The a triangular pressure distributions diagrams we will get it and we need to compute what is the force because of these pressure diagrams. The average pressures multiplied into the area that is what will be the net force due to the fluid at the rest. That what will come it, average pressures into the area of the gate. That is what will be the this is the force will act due to the fluid at the rest and that what will act it at one third distance from the base.

Point of application of this force from bottom = $(\frac{1}{3}) \times 1.5$

Taking Moment about hinge

$$(1.5/3) \times F_{\text{fluid}} = F \times 0.75$$

$$(1.5/3) \times 1.5^3/2 \rho g = F \times 0.75$$

$$F = 11.036 \text{ KN}$$

As you know in a triangular pressure distribution diagrams the resultant force act at a one third distance from the bottoms or two third distance from the free surface. So one third distance locations that what will be act it the fluid F we know it what is the distance from this. So we just take a moment about the hinge to compute what will be the F, the force into distance, force into distance. That is what is moment we take it the finally it comes out to be 11 KN.

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Question 2

The force "F" required at equilibrium on the semi-cylindrical gate shown below is

(GATE)

Flow classification:
 Fluid is homogeneous
 Density is constant
 Fluid is static

Forces acting on gate:

1. Horizontal force by water on gate
2. Vertical force by water on gate
3. Force "F" required for equilibrium

Now let us we another GATE questions we can solve it with as it is a diagrams given here. There is a semi circles cylindrical gate is there and force F is acting here and there

is a hinge at this point. So we need to compute it if this is a free surface. This is the two meter depth of the water is there. What could be the force is required if the hinge at this point. This is what the questions.

[The force “F” required at equilibrium on the semi-cylindrical gate shown below is]

Now if you look it, we can have a flow classifications here because fluid is at rest, density is a constant and we can consider is a homogeneous and what we need to compute for this case if you look it this is a curved surface. So because of that there will be horizontal force acting on this. There will be horizontal force act on this. Also the vertical force is going to act on that.

Flow classification:

Fluid is homogeneous

Density is constant

Fluid is static

So there are the two force component will come it. One is a horizontal force and other is vertical force. And another F which is applied to here. So we will try to find out what could be this force component to compute, so that this will not rotate it. So we need to compute what is F is acting on this if there is a two force component, one is a horizontal force because the fluid at the rest.

Forces acting on gate:

1. Horizontal force by water on gate
2. Vertical force by water on gate
3. Force “F” required for equilibrium

Also will be the vertical force F_v will act on that. So these force will take a moment about this hinge and that moment taking moment of these three force components will help us to compute what will be the F component. This is what the basic idea to solve these problems.

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Question 2

Horizontal force = $P(dA \cos \theta)$
 $= P_{gauge} \times \text{Vertical Projection at Curved Surface Area}$
 $F_H = 0.5 \times 2 \times 19.62 = 19.62 \text{KN}$

Horizontal force = $P(dA \cos \theta)$
 Vertical force = $P(dA \sin \theta)$

Now to compute horizontal forces, what is going to act it. So it is very easy that the places what will get it that what will be the force into vertical projections of the curved surface area. That is what we derived earlier. So we can compute it what will the force will act on this as the surface the pressure distributions where is like this, we can find out the pressures at the centroid locations.

$$\text{Horizontal force} = P(dA \cos \theta)$$

$$= P_{gauge} \times \text{Vertical Projection at Curved Surface Area}$$

$$F_H = 0.5 \times 2 \times 19.62 = 19.62 \text{KN}$$

And multiply this area of the vertical projections area of the curved surface that is what is come it which will be the force acting on that. But that force will act to one third distance from this bottoms. That since it is a 2 meter height you have a 2 by 3 meter distance from this B locations. This is what the horizontal force what is acting it.

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Question 2

Vertical force on portion AC = weight of liquid contained in the shaded area acting vertically downward through CG of shaded area = F_{V1}

Vertical force on portion BC = weight of liquid contained in the shaded area acting vertically upward = $F_{V2} - F_{V1}$

Net vertical force (acting upon the CG of the shaded area) = $F_{V2} - F_{V1}$

$$F_V = \frac{\pi r^2}{2} \times h \times \rho g = \frac{\pi \times 1^2}{2} \times 1 \times 1000 \times 9.81 = 15.41 \text{ KN}$$

"F" for equilibrium taking moment about hinge "O"

$$F \times 1 + F_V \times \frac{4R}{3\pi} - F_H \left(1 - \frac{2}{3}\right) = 0$$

$$F \times 1 = 19.62 \times \left(1 - \frac{2}{3}\right) - 15.41 \times \frac{4 \times 1}{3\pi} = 0$$

Similar way if I need to compute the how much vertical force is acting on this. So we can find out if this is my free surface. This is the area, the shaded part will give a vertical force component of F_{V1} . But F_{V2} will be the, all the shaded part will be the F_{V2} part. The subtracting this part that what will be the net force what will be act vertically upward directions.

Vertical force on portion BC = weight of liquid contained in the shaded area acting vertically upward = $F_{V2} - F_{V1}$

As you know it this F_{V2} will be the higher than F_{V1} as the more area of the liquid displaced by this curved surface. So let me compute it. The vertical force on portion of AC that what with the weight of the liquid contained in the shaded area acting vertically downward through CG. That is F_{V1} . Similar way if you look at what is the force is acting on the BC surface part that what with the weight of the liquid contained in the shaded part okay, which is acting vertically upwards.

Net vertical force (acting upon the CG of the shaded area) = $F_{V2} - F_{V1}$

That what will be the F_{V1} value and the net force will come it the difference between F_{V2} and F_{V1} . That is the net force will be acting it. So we can find out the net force will be act it the shaded part of this part only. So that means you just find out the cylindrical area what is the dimension of cylindrical area, volume of the cylindrical area into the specific weight of the water. That is what the ρg .

$$F_V = \frac{\pi r^2}{2} \times h \times \rho g = \frac{\pi \times 1^2}{2} \times 1 \times 1000 \times 9.81 = 15.41 \text{ KN}$$

That what will comes out to be 15.41 KN which is the vertical force, the net vertical force acting on this gate parameter. Now if I take a moment at the hinge locations.

“F” for equilibrium taking moment about hinge “O”

$$F \times 1 + F_V \times \frac{4R}{3\pi} - F_H \left(1 - \frac{2}{3}\right) = 0$$

$$F \times 1 = 19.62 \times \left(1 - \frac{2}{3}\right) - 15.41 \times \frac{4 \times 1}{3\pi} = 0$$

So these are the some of the moment about the hinge should equal to zero. That the concept we have used it. Then we will get it F into 1 that is what will value will come it which becomes zero, the force becomes will be the zero value.

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Question 3

Cross-section of an object submerged into a fluid consists of a square of side 2m and triangle as shown in the figure. The object is hinged at point P that is 1m below the fluid free surface if the object is to be kept in the position as shown in the figure, the value of x should be (GATE, 2005)

Flow classification:
 Fluid is homogeneous
 Density is constant
 Fluid is static

If the object is in position, then net moment about “P” should be zero.

The diagram shows a cross-section of an object submerged in a fluid. The object consists of a square base with a side length of 2 m and a triangular top. The object is hinged at point P, which is 1 m below the fluid free surface. The horizontal distance from the right edge of the square to the hinge is x. The forces F_H and F_V are shown acting on the object.

Now let us come to the another questions number 3, the cross sections of object submerged into a fluid consists of a square side of 2 meters and the triangle as shown in the figure. Object is hinged at the point P is 1 meter below the fluid free surface if object is to be kept in this position as shown in the figure, the value of x should be what is the x value so that this will be at a same position, the equilibrium positions.

[Cross-section of an object submerged into a fluid consists of a square of side 2m and triangle as shown in the figure. The object is hinged at point P that is 1m below the fluid free surface if the object is to be kept in the position as shown in the figure, the value of x should be]

This is the hinge locations, the but what is the basic concept of this submerged object. If you look it that there will be horizontal force will be act from these sides. Also horizontal force will go into act from this side. But those will be cancelled out, the same amount of horizontal force will act from this side. Also same amount will be horizontal force FH 1, FH 2 if I consider both will be cancelled out.

What will be the difference? There will be the vertical force will act on this side, also this side F_{v1} , F_{v2} and there is a distance from these locations. So if I know these two forces and their center pressures are the, the line of actions of the vertical force and what is the distance from the hinge. Taking the moment at the hinge, we can compute it what will be the x distance the triangle should be there so that the moment will be the zero.

Flow classification:

Fluid is homogeneous

Density is constant

Fluid is static

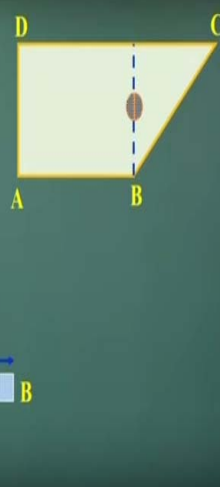
That means, the positions will be the same position at the equilibrium positions will be there. Now as object is in a positions that means, the net moment about the P should be zero, that the concept.

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Question 3

Pressure Distribution:

- Atmospheric pressure on water surface
- Hydrostatic pressure distribution valid



In plate AB:

$$F_{v1} = \rho g h \times A = \rho g \times 2 \times 2 \times 1 = 4\rho g$$

Now let us we compute it what will be the vertical force in the AB part. It is a very simple is the pressure distributions is uniform here and we know rho g into A will be the force component. That what will come it

$$F_{V_1} = \rho g h \times A = \rho g \times 2 \times 2 \times 1 = 4\rho g.$$

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Question 3

In plate BC.

$$F_{V_2} = \rho g \times \text{Volume of water above plate}$$

$$F_{V_2} = \rho g \times \frac{1}{2} \times 2 \times x \times 1$$

Equating Moments

$$\sum M_P = 0$$

$$F_{V_1} \times 1 = F_{V_2} \times \frac{x}{3}$$

(Moment due to F_{H_1} and F_{H_2} about P=0)

$$4\rho g = \rho g x \times \frac{x}{3}$$

$$x = 2\sqrt{3} \text{ m}$$

Similar way,

In plate BC

$$F_{V_2} = \rho g \times \text{Volume of water above plate}$$

$$F_{V_2} = \rho g \times \frac{1}{2} \times 2 \times x \times 1$$

Now we are equating the sum of the moment at the origins that will be,

$$\sum M_P = 0$$

$$F_{V_1} \times 1 = F_{V_2} \times \frac{x}{3}$$

(Moment due to F_{H_1} and F_{H_2} about P=0)

$$4\rho g = \rho g x \times \frac{x}{3}$$

$$= 2\sqrt{3} \text{ m}$$

The CG of this part at this point which is a one by third of the x distance. So that way we can take him a moment at the two locations at the hinge locations and when you get this moment we will get x value of this one. So if you look at these problems, it is very easy problems. Only you have to resolve the force components.

The first you resolve to find out what is the horizontal force is acting it in different surface if this two surface are canceling out, then you look the vertical force

components and their line of actions. So if you know the vertical force where is acting it and the vertical line of actions take a moment about the hinge, then you will get the what will be the x value. That is the basic concept here.

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Question 4

In an inclined manometer shown in the figure below, the reservoir is large. Its surface may be assumed to remain at fixed elevation. A is connected to a gas pipeline and the deflection noted on the inclined glass tube is 100 mm. Assuming $\Theta = 30$ and the manometric fluid as oil with specific gravity of 0.86, the pressure at A is? (GATE, 2004)

Flow classification:
 Fluid is homogeneous
 Density is constant
 Hydrostatic fluid

Assumptions:
 manometer leg diameter > 12 mm
 for no capillary rise and fall

No connection to gas pipeline A is connected to gas pipeline

Now let us come it to a manometer problems. So there is a inclined manometer shown in the figure below. Reservoir is large. That is the, its surface maybe assumed to be remain as a fixed elevations. A is connected to a gas pipeline. The deflection is noted on the inclined gas tube. This is what the inclined gas tube is 100 millimeters the theta the angle of inclined manometers theta equal to 30 degrees and manometric fluid as oil with a specific gravity of 0.86.

[In an inclined manometer shown in the figure below, the reservoir is large. Its surface may be assumed to remain at fixed elevation. A is connected to a gas pipeline and the deflection noted on the inclined glass tube is 100 mm. Assuming $\Theta = 30$ and the manometric fluid as oil with specific gravity of 0.86, the pressure at A is?]

What is the pressure at A point which is a GATE 2004 questions. So that way let we it is a fluid in static problems. So the NCC constants fluid can consider is homogeneous. Now let us have a the assumption is that considering this manometric lake what we have that diameter should be more than 12 millimeters so that there is no capillarity effect.

Flow classification:

Fluid is homogeneous

Density is constant

Hydrostatic fluid

Because of the capillarity there should not be the rise and fall of the manometric liquid for this case. So this is what the assumptions for this problems.

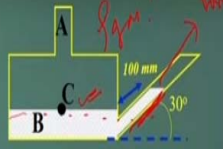
Assumptions:

manometer leg diameter > 12 mm for no capillary rise and fall

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Question 4

Pressure distribution:
 Hydrostatic Pressure
 No pressure variation from C to A due to gas



Pressure at C,

$$\frac{P_c}{\gamma_w} = Gh + \frac{P_{atm}}{\gamma_w}$$

$$= 0.86 \times 100 \times \sin 30 + \frac{P_{atm}}{\gamma_w}$$

$$\frac{P_c - P_{atm}}{\gamma_w} = 0.86 \times 50$$

$$\frac{P_c - P_{atm}}{\gamma_w} = 43 \text{ mm}$$

$$\frac{(P_c)_{gauge}}{\gamma_w} = 43 \text{ mm of water}$$

As there is no pressure variation from C to A due to gases (small to moderate heights)

$(P_c) = (P_A)$
 $(P_A)_{gauge} = 43 \text{ mm of water}$

Now what I doing it to equate the pressures to compute what will be the pressures acting on this. So if you look it that there is no pressure variations between the C to A. This is the gas part. Assuming it that since the density of gas is very less. So let us assume it there is not significant difference, variations of the pressure at the P and C levels. If it is that case, the PC the pressure at these locations, we can compute it as at this point the pressure is equal to the atmosphere pressures.

Pressure at C,

$$\frac{P_c}{\gamma_w} = Gh + \frac{P_{atm}}{\gamma_w}$$

$$= 0.86 \times 100 \times \sin 30 + \frac{P_{atm}}{\gamma_w}$$

$$\frac{P_c - P_{atm}}{\gamma_w} = 0.86 \times 50$$

$$\frac{P_c - P_{atm}}{\gamma_w} = 43 \text{ mm}$$

$$\frac{(P_c)_{gauge}}{\gamma_w} = 43 \text{ mm of water}$$

So the PC is equal to be the height of this manometric liquid, the vertical height that what will come it the $100 \times \sin 30$ that will be showed as the vertical height and the specific gravity if I multiplied it, it is talking about in terms of millimeters, in terms of millimeters as equivalent of water how much the pressures is acting on that.

That is what is atmospheric pressures divide by the unit weight of the waters. So that way it is equivalent to water we have done it. So that way the gauge pressure the pressure difference between the PC minus P atmospheric which is the gauge pressure will come out to be 43 mm of the water value.

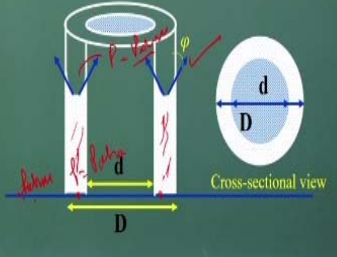
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Question 5

Two coaxial glass tubes forming an annular with small gap are immersed in clear water. The inner and outer diameter are d and D respectively. What is capillary rise of water in the annular. If σ is the surface tension of water in contact with air and ϕ is the angle of contact between water and glass tube? (ESE)

Flow classification:
 Fluid is homogeneous
 Density is constant
 Hydrostatic fluid

Assumptions:
 Due to adhesion of water to wall of vessel, the meniscus turns upwards making an angle of ϕ .



Now let us go to the question number 5 which talking about the capillarity and the surface tensions. So this is what the Engineering Service exam paper where the two coaxial glass tubes forming a annular with a small gap okay. There will be annular but the gaps are small immersed in a clear waters. The inner and the outer diameters are small d and the capital D respectively.

[Two coaxial glass tubes forming an annular with small gap are immersed in clear water. The inner and outer diameter are d and D respectively. What is capillary rise of water in the annular. If σ is the surface tension of water in contact with air and ϕ is the angle of contact between water and glass tube?]

What is a capillary rise of water in this annular if the σ is a surface tension of the water in contact with air and the ϕ is the angle of contact between the water and the glass tubes. So these are simple derivations to find out a relationship between capillary rise with the surface tensions and the angle of contact for annular with having inner and the outer diameters of smaller d and the capital D .

This is a very easy concept that as you had derived in the theory classes that whenever you put it any small tubes, annular tubes in a liquid, what we get it that the outside you have P equal to atmospheres here also will have the P equal to be the P atmosphere because when fluid is at that the rest any horizontal plane if you take it the pressure should be equal. So that is what this is the horizontal reference plane.

Flow classification:

Fluid is homogeneous

Density is constant

Hydrostatic fluid

The fluid outside since is it at the atmospheric pressures, the fluid which is inside in this capillary tube also will be the atmospheric pressures. So P will be the atmospheric pressures. If is that is the conditions, here also P equal to P atmospheric pressures. That means, the weight of this liquid which is capillary raised from the surface that what will be balanced by the surface tension force as we derived in the theory class.

Assumptions:

Due to adhesion of water to wall of vessel, the meniscus turns upwards making an angle of ϕ .

This very basic concept, the fluid due to the adhesion of water to wall the that is what is upwards making angle of ϕ degree.

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Question 5

Checking equilibrium condition in y direction

Upward force = downward force

$$(T_1 + T_2) \cos \varphi = \gamma_w * \left(\frac{\pi}{4}\right) * h * (D^2 - d^2)$$

$$T_1 = \sigma \pi D$$

$$T_2 = \sigma \pi d$$

$$\sigma \pi (D + d) \cos \varphi = \gamma_w * \left(\frac{\pi}{4}\right) * h * (D + d) * (D - d)$$

$$h = \frac{4 \sigma \cos \varphi}{\gamma_w (D - d)}$$

Now I have just equating this since is a equilibrium conditions in the so upward force is equal to the downward force.

Upward force = downward force

$$(T_1 + T_2) \cos \varphi = \gamma_w * \left(\frac{\pi}{4}\right) * h * (D^2 - d^2)$$

$$T_1 = \sigma \pi D$$

$$T_2 = \sigma \pi d$$

The upward force is a surface tension force part, that what will act for a two different diameters. That what will give you this component as the upward force.

So we can compute the downward force which is the weight of the fluid. That what we confined by this the capillary rise. That what will be

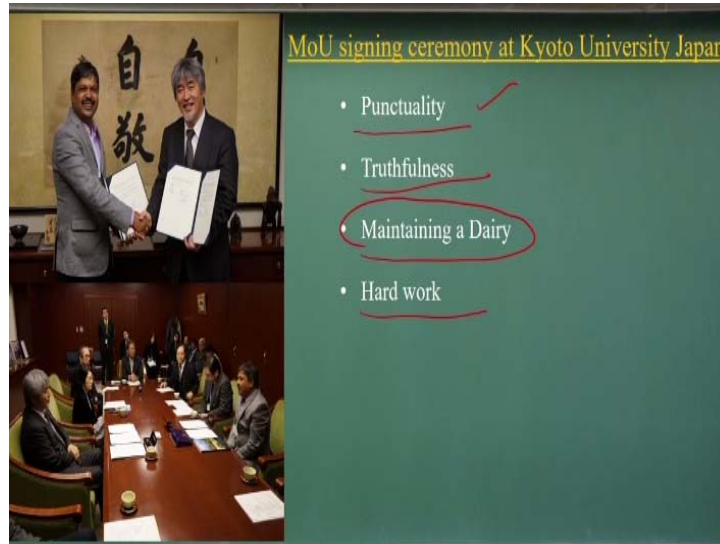
$$\sigma \pi (D + d) \cos \varphi = \gamma_w * \left(\frac{\pi}{4}\right) * h * (D + d) * (D - d)$$

$$h = \frac{4 \sigma \cos \varphi}{\gamma_w (D - d)}$$

That what will give us the weight which is the weight of the fluid acting downwards, the upper part. So if I just rearrange these terms the finally, I will get this ones.

That is what very basic way I will get it the relations between the capillarity height angle of contact and these two are the diameter of annular systems where you will have a and sigma stands for surface tensions. This is a simple derivation what we have done it.

(Refer Slide Time: 28:16)



Now let us before coming to another 5 questions to solve this is what the photographs what you can see it, I attended this MoU ceremonies held at Kyoto University in Japan. What I am to see that if I try to understand it how, what the success story behind a Japanese which is to develop after the World War II, I can visualize they have the three human characteristics that what helped them to improve their economic conditions when after the World War I. One is no doubt is hard work, truthfulness, and the punctuality.

But another things what I want to tell you that we always not have a habit to maintain a diary. But the any of Japanese if you look it, they are very good in maintaining a diary. That is the reasons they are look it, keep it their brain is free. So they are very particular to maintain a diary, the planning the activities very systematic ways.

So always if you look a Japanese, he always maintain a diary to noting it the calendars, work plan, job activities, all they noted on these and they carry the diary wherever locations they go it. So that what is another characteristics what I observed it while I interacting with Japanese groups, with whom I have been working on rainfall data analysis in northeast regions.

So what am I to say that in a fluid mechanics or any of the subjects, we always try to remember the formulaes. Please do not remember the formulaes, you try to maintain a diary for that. So slowly, you can understand those equations and try to apply this the formulaes in the right place. So as a overall the design of the course if you look it that

always I encourage all of you to derive the simple equations, instead of remembering this total formula.

That should be the idea when you solve the fluid mechanics problems. Let us solve another five questions on fluid at the rest conditions.

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Question 6

Two pipelines, one carrying oil (mass density = 900 kg/m^3) and the other water, are connected to a manometer as shown in the figure. By what amount the pressure in the water pipe should be increased so that the mercury levels in both the limbs of the manometer becomes equal? (mass density of mercury = 13550 kg/m^3 and $g = 9.81 \text{ m/s}^2$) (GATE, 2003)

Flow classification:
 Fluid is heterogeneous
 Hydrostatic fluid
 No mixing of fluids

Assumptions:
 When pressure is applied at a point in a fluid, the pressure increases uniformly at each point on the fluid (Pascal's law)

The question number 6, that is what two pipelines one carrying oil. The mass density of the oil is $900 \text{ kg per meter cube}$. Other one is water. It is connected to a manometer as shown in the figures. By what amount of pressure in the water pipe should be increased so that the mercury levels in the both limbs of the manometers becomes equal.

[Two pipelines, one carrying oil (mass density = 900 kg/m^3) and the other water, are connected to a manometer as shown in the figure. By what amount the pressure in the water pipe should be increased so that the mercury levels in both the limbs of the manometer becomes equal? (mass density of mercury = 13550 kg/m^3 and $g = 9.81 \text{ m/s}^2$)]

The mass density of mercury is given here which is $13,550 \text{ kg/m cube}$, g is the acceleration due to the gravity. Now let me sketch it. So initial conditions what you have? You have oil, you have the water; it is connected to the manometers, mercury manometers which is having a $20 \text{ centimeter rise}$ along this horizontal plane. This is a 3 meters . This is what 1.5 meter .

As we increase the pressures, the mercury manometers limbs will be the horizontal. That means, there will be a this 20 centimeter if you can understand it will be make it 10 centimeter in this side and also the 10 centimeter from this side, then it will come it to a horizontal plane. So it will be 1.6 meters, this side will be the 2.9 meters. There will be rise, there is fall.

Flow classification:

Fluid is heterogeneous

Hydrostatic fluid

No mixing of fluids

That what will be happen it. In this case will be rise it, this case will be fall it. The total mercury will come it this orientations will come when pressure in the tube is increased. So what we are going to do it for these conditions we try to find it how the pressure difference is there over this plane of A dash and the AB dash. From that, we can know it what is the additional pressure is applied here to make it the surface horizontal. So the very basic concept here just to try to understand it.

Assumptions:

When pressure is applied at a point in a fluid, the pressure increases uniformly at each point on the fluid (Pascal's law)

So pressure is applied at a point, so pressure increases uniformly at each point of the fluid. So that is what the Pascal's laws. That is what the Pascal's law.

(Refer Slide Time: 33:29)

Question 6

Let the pressure increased be P_0 so that mercury level in each limb becomes equal

If, x is decreased from left limb, then level of right limb increase by x
Both level are equal with respect to the datum shown

$$\Rightarrow x = 0.2 - x \Rightarrow x = 0.1\text{m}$$

Case I:

Pressure at the datum AA' should be equal $P_A = P_{A'}$

$$\frac{P_{oil}}{\gamma_w} + G_{oil} \times 3 = \frac{P_w}{\gamma_w} + G_w \times 1.5 + 0.2 \times G_m$$

$$\frac{P_{oil}}{\gamma_w} - \frac{P_w}{\gamma_w} = 1 \times 1.5 + 0.2 \times 13.55 - 0.9 \times 3 = 1.51\text{ m}$$

Now we are applying for the first case. As I said it to remain it the perfect levels the x will be decreased from the left limb obviously, and there will be the right limbs will be the increased by the x value. So x will be come out to be 0.1 meters.

$$x = 0.2 - x \Rightarrow x = 0.1\text{m}$$

Now I may equating the pressures P, P dash for this case. So I have the pressure at this point, pressure at this point on these horizontal surface in these manometers I am to compute what will be the pressure difference between this.

Pressure at the datum AA' should be equal $P_A = P_{A'}$

$$\frac{P_{oil}}{\gamma_w} + G_{oil} \times 3 = \frac{P_w}{\gamma_w} + G_w \times 1.5 + 0.2 \times G_m$$

Let be consider pressure at this point is P oil. At this point is P water. So P oil, then the specific gravity into the height.

$$\frac{P_{oil}}{\gamma_w} - \frac{P_w}{\gamma_w} = 1 \times 1.5 + 0.2 \times 13.55 - 0.9 \times 3 = 1.51\text{ m}$$

Similar way we can multiply it for water case as well as the mercury case. So if you rearrange it the pressure difference between the oil and the waters divide by the unit weight of the waters will get these values, will get this value which is equal to 1.51 meter.

(Refer Slide Time: 34:54)

Question 6

Case II:

$$P_A = P_B$$

$$\frac{P_{oil}}{\gamma_w} + G_{oil} \times 2.9 = \frac{P_w + P_B}{\gamma_w} + 1.6 \times G_w$$

$$\frac{P_{oil}}{\gamma_w} - \frac{P_w}{\gamma_w} + 0.9 \times 2.9 - 1.6 = \frac{P_B}{\gamma_w}$$

$$1.51 + 0.9 \times 2.9 - 1.6 = \frac{P_B}{\gamma_w}$$

$$\frac{P_B}{\gamma_w} = 2.52\text{ m}$$

$$P_B = 2.52 \times 9.81 \times 1000 = 24.7\text{kPa}$$

The diagrams illustrate a differential manometer with two limbs containing oil and water, and a U-tube containing mercury. The top diagram shows the initial state with a 0.2m difference in mercury levels. The bottom diagram shows the state after pressure is applied, with a 2.9m difference in mercury levels. The manometer is labeled with 'oil', 'water', and 'mercury'.

Now the second case what we will consider when it is the mercury levels at the same level okay after increasing the pressure at this point. So that what will be equal to,

$$P_A = P_B$$

$$\frac{P_{oil}}{\gamma_w} + G_{oil} \times 2.9 = \frac{P_w + P_B}{\gamma_w} + 1.6 \times G_w$$

$$\frac{P_{oil}}{\gamma_w} - \frac{P_w}{\gamma_w} + 0.9 \times 2.9 - 1.6 = \frac{P_B}{\gamma_w}$$

$$1.51 + 0.9 \times 2.9 - 1.6 = \frac{P_B}{\gamma_w}$$

$$\frac{P_B}{\gamma_w} = 2.52 \text{ m}$$

$$P_B = 2.52 \times 9.81 \times 1000 = 24.7 \text{ kPa}$$

And since this component is known to us you can compute the P_B value will be 24.7 kilo Pascal. Basically try to understand it, there is a two conditions we have, the initial conditions where the manometric liquids are the different levels and then is a final conditions when we apply the additional force at this point.

So only we have applied very basic equations that in a horizontal surface whenever you take it the pressure on that horizontal surface is the same or equal pressure will act on the horizontal surface when fluid is at the rest. That the conditions what we applied it to compute what will be the additional force is acting at the water to make it the mercury level is perfectly horizontal.

(Refer Slide Time: 36:33)

Question 7

A ship has a metacentric height of 0.3 m and its period of rolling is 20 seconds. The relevant radius of gyration is nearly? (ESE, 2015)

Flow classification:
Fluid is homogeneous
Hydrostatic fluid

Assumptions:

- The ship rotates about its longitudinal metacentric axis
- The ship can be considered as a pendulum with centre of rotation as metacentre

Now take it the question number 7. There is a ship of metacentric height of 0.3 meters. Its period of rolling is 20 seconds. The relevant radius of gyrations is nearly or what is

the value of relevant radius of gyrations. That is what is in Engineering Service question in 2015. So as you know that there is a metacentric axis. It has known the metacentric height and it is also know it what is the time periods of rolling this ship part.

[A ship has a metacentric height of 0.3 m and its period of rolling is 20 seconds. The relevant radius of gyration is nearly?]

Flow classification:

Fluid is homogeneous

Hydrostatic fluid

Assumptions:

- The ship rotates about its longitudinal metacentric axis
- The ship can be considered as a pendulum with centre of rotation as metacentre

These are just sketched to say it the weight, the metacentric height and all the things. So the ship rotates about its longitudinal metacentric axis and it is considered as a pendulum okay as a pendulum. It has a center of rotations at the meta centers. So at the metacentric levels, this is what having the simple pendulum oscillations happening it.

(Refer Slide Time: 37:49)

Question 7

The ship can be considered as a pendulum with centre of rotation as metacentre

Restoring moment = $I\alpha$

$$-wGM \sin \theta = I \frac{d^2\theta}{dt^2}$$

$$\frac{d^2\theta}{dt^2} = \frac{-wGM\theta}{I} \quad \theta \approx \text{small angle}$$

This formula is in the form of harmonic motion of equation

$$\frac{d^2\theta}{dt^2} = -\omega^2 \theta$$

$$\omega = \sqrt{\frac{wGM}{I}}$$

So if it is that, let me draw the free body diagrams. That means if it is the metacentric height here, this is the object is moving like this, okay? The oscillating is like a pendulum. If that we have a restoring momentum is moment of inertia into accelerations. It will be acting, what is the force torque momentum is working it that is what unit weight sin theta into GM.

Restoring moment = $I\alpha$

$$-w\overline{GM} \sin \theta = I \frac{d^2\theta}{dt^2}$$

$$\frac{d^2\theta}{dt^2} = \frac{-w\overline{GM}\theta}{I} \quad \theta \approx \text{small angle}$$

This formula is in the form of harmonic motion of equation

$$\frac{d^2\theta}{dt^2} = -\omega^2 \theta$$

$$\omega = \sqrt{\frac{w\overline{GM}}{I}}$$

And that what if you rearrange it in terms of angular oscillating component will get this part and as a harmonic components part if you look it and finally we will get it the omega in terms of unit weight GM and I is moment of inertia.

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Question 7

Time Period = $\frac{2\pi}{\omega} = \frac{2\pi}{\sqrt{\frac{w\overline{GM}}{I}}} = 2\pi \sqrt{\frac{I}{w\overline{GM}}}$ $r = \text{radius of gyration}$

$T = 2\pi \sqrt{\frac{mr^2}{mg\overline{GM}}} = 2\pi \sqrt{\frac{r^2}{g\overline{GM}}}$

$20 = 2\pi \sqrt{\frac{r^2}{9.81 \times 0.9}}$

$r = \frac{20}{2\pi} \times \sqrt{9.81 \times 0.9} = 9.45 \text{ m}$

(Given)
 $T = 20 \text{ seconds}$
 $\overline{GM} = 0.9 \text{ m}$

$$T = 20 \text{ seconds}$$

$$\overline{GM} = 0.9 \text{ m}$$

So the return periods or the time periods will

$$\text{Time Period} = \frac{2\pi}{\omega} = \frac{2\pi}{\sqrt{\frac{w\overline{GM}}{I}}} = 2\pi \sqrt{\frac{I}{w\overline{GM}}} \quad r = \text{radius of gyration}$$

$$T = 2\pi \sqrt{\frac{mr^2}{mg\overline{GM}}} = 2\pi \sqrt{\frac{r^2}{g\overline{GM}}}$$

$$20 = 2\pi \sqrt{\frac{r^2}{9.81 \times 0.9}}$$

$$r = \frac{20}{2\pi} \times \sqrt{9.81 \times 0.9} = 9.45 \text{ m}$$

And it is making angle theta then what are the restoring momentum moment and what is the moment due to this oscillation. That what we are equating it to find out what will be the r value, what will be the r value.

(Refer Slide Time: 39:53)

Question 8

A three fluid system is connected to a vacuum pump. The specific gravity value of the fluids are given in the figure. The gauge pressure value (in KN/m^2) of P_1 is ? Take $\gamma_w = 9.81 \text{ KN/m}^3$? (ESE)

Flow classification:
 Fluid is heterogeneous
 Hydrostatic fluid
 No mixing of fluids

Pressure at point A = P_{atm}

$$P_1 + \gamma_w S_1 \times h_1 + \gamma_w S_2 \times h_2 = P_{atm}$$

$$P_1 + 9.81 \times 0.88 \times 0.5 + 9.81 \times 0.95 \times 0.5 = P_{atm}$$

$$P_1 - P_{atm} = -8.97 \text{ KN/m}^2$$

$$(P_1)_{gauge} = -8.97 \text{ KN/m}^2$$

Now take it the question number 8, which is a three fluid system connected to a vacuum pump okay, where there is no pressures on this. So that is what the vacuum pump. Specific gravity values are given in these figures. Okay that is a S 1 is 0.88, 0.95 and the water which is specific gravity equal to 1. Then this gauge pressure value at P 1 what will be the pressure at the P 1 value if you consider the unit weight of the waters 9.81 kilometer per meter cube.

[A three fluid system is connected to a vacuum pump. The specific gravity value of the fluids are given in the figure. The gauge pressure value (in KN/m^2) of P_1 is ? Take $\gamma_w = 9.81 \text{ KN/m}^3$]

This is very simple problems that if I take a horizontal surface here the pressure is atmospheres I can compute the pressure at this point also will be the atmosphere. So I know this present at this point is atmospheric pressure. I just equate it. If I compute the pressures from these vertical directions what is the pressure is coming that should be equal to the atmospheric pressure. That what is done it here.

Flow classification:

Fluid is heterogeneous

Hydrostatic fluid

No mixing of fluids

Pressure at point A = P_{atm}

$$P_1 + \gamma_w S_1 \times h_1 + \gamma_w S_2 \times h_2 = P_{atm}$$

$$P_1 + 9.81 \times 0.88 \times 0.5 + 9.81 \times 0.95 \times 0.5 = P_{atm}$$

$$P_1 - P_{atm} = - 8.97 \text{ KN/m}^2$$

$$(P_1)_{gauge} = - 8.97 \text{ KN/m}^2$$

P_1 is pressure at this point. As we go down the unit weight specific gravity into the height, the pressures of this fluid one then this fluid two, the unit weight, the specific gravity S_2 into h_2 should equal to the atmospheric pressure, should equal to the atmospheric pressure. Just equating that we will get the gauge pressure will be the negative of 8.79 kilometer per meter square.

So this is very easy problems. Only you have to find out where you have to equate the pressures. Where you have to take the horizontal lines. So that way you can equate the problems and solve the problems. If you do not take properly the horizontal surface to equate the pressures at two locations, then you try to do the mistakes. That what I have to tell it.

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Question 9

A droplet of radius R is split into n -smaller droplets of equal size. Find the work required. Given that surface tension is equal to σ . (ESE)

Flow classification:
Fluid is homogeneous
Hydrostatic fluid

Assumptions:
Assume the droplet to be spherical because the surface area is minimum thereby the surface energy is minimum. Minimum surface energy leads to most stable state.

Diagram: A spherical droplet with radius R .

Another this is a very interesting problems is that a droplet of radius R split into n small droplets okay. So bigger droplets is split it into n number of small droplet of equal size.

Find the work required given that the surface tensions is equal to the sigma value. So that means a bigger radius R is there and which is a split it to the n small number of droplets. And that is what is happened to go for more surface areas.

[A droplet of radius R is split into n-smaller droplets of equal size. Find the work required. Given that surface tension is equal to σ .]

As its go for the more surface areas, it is need to do the work against that surface area increase of the surface area there will be more surface tension force will be act as we increase the surface area. So that is what we are trying to look it if a bigger droplet of radius R split into n number of smaller droplets then how much of extra area, surface area we are generating it and because of the extra surface area, the how much force is required to give it to split into the n number of droplets.

Flow classification:

Fluid is homogeneous

Hydrostatic fluid

That the concept here and most of the concept what we consider as equivalent to a spherical balls and surfaces in minimum that what is surface energy is minimum concept what is considered that is what is a stable consider for the any droplet.

(Refer Slide Time: 43:38)

Question 9

We know that surface tension is work done per unit increase in surface area.

Volume of droplet of radius 'R' = Net volume of n smaller droplets of radius 'r'.

$$\frac{4}{3}\pi R^3 = n \times \frac{4}{3}\pi r^3$$

$$r = \left(\frac{R^3}{n}\right)^{\frac{1}{3}} = \frac{R}{n^{\frac{1}{3}}}$$

Increase in surface area = $4\pi r^2 \times n - 4\pi R^2$

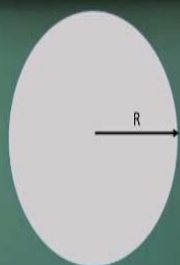
$$= 4\pi(nr^2 - R^2)$$

$$= 4\pi\left[n \times \left(\frac{R}{n^{\frac{1}{3}}}\right)^2 - R^2\right]$$

$$= 4\pi R^2\left[\frac{1}{n^{\frac{1}{3}}} - 1\right]$$

$\sigma = \frac{\text{Work done}}{\text{Increase in area}}$

$\text{Work done} = \sigma \times 4\pi R^2\left[\frac{1}{n^{\frac{1}{3}}} - 1\right]$

$$= 4\sigma\pi R^2\left[\frac{1}{n^{\frac{1}{3}}} - 1\right]$$


The first is that let us since the bigger droplet it is divided into n number of smaller droplet the volume should be equal okay. Of the spherical volumes what you are getting it that should be equal it. That what for the if this small r is for the smaller droplet and

bigger R represent the radius of the bigger droplet that then we will get it the volume and this side and is multiplied to find out for the n number of droplet conditions.

Volume of droplet of radius 'R' = Net volume of n smaller droplets of radius 'r'.

$$\frac{4}{3}\pi R^3 = n \times \frac{4}{3}\pi r^3$$

$$r = \left(\frac{R^3}{n}\right)^{\frac{1}{3}} = \frac{R}{n^{\frac{1}{3}}}$$

The increase in the surface area into the surface tensions that what will give us the work done for that. That is what we have computed to compute the work done part. That just we need to compute increase in the surface area. And after knowing this increasing of surface area into the surface tension force will give us the work done part. So the basically these problems does not have a much concept wise.

$$\begin{aligned} \text{Increase in surface area} &= 4\pi r^2 \times n - 4\pi R^2 \\ &= 4\pi(nr^2 - R^2) \\ &= 4\pi \left[n \times \left(\frac{R}{n^{\frac{1}{3}}}\right)^2 - R^2 \right] \\ &= 4\pi R^2 \left[n^{\frac{1}{3}} - 1 \right] \\ \sigma &= \frac{\text{Work done}}{\text{Increase in area}} \end{aligned}$$

$$\begin{aligned} \text{Work done} &= \sigma \times 4\pi R^2 \left[n^{\frac{1}{3}} - 1 \right] \\ &= 4\sigma\pi R^2 \left[n^{\frac{1}{3}} - 1 \right] \end{aligned}$$

Only to equate the volume of droplets and n number of small droplet volumes. Then find out what is the increase of surface area. As we know that this much of work needs to be done it to split the bigger droplet to the smaller, n number of smaller droplet because this much of additional surface force is acting. So that wave force surface tension into the area will give us the work done component.

(Refer Slide Time: 45:51)

Question 10

A cylinder 0.15 m in diameter and 0.375 m high containing water is rotated about its vertical axis at a speed of 320 rpm, so that a portion of water spills out.

If the cylinder is now brought to rest, what would be the depth of water in it?

Flow classification:

Fluid is homogeneous

Hydrostatic fluid

Forced vortex flow



Now let me come it to very simple problems which this is the last questions what we are going to discuss is that there is a cylinders of 0.1 meter diameters, 0.375 meters high containing the water. It is rotated about the vertical axis at the speed of 320 rpm, rotations per minute so that a portion of water spills out. Okay, so if you consider a cylinder like this and you start rotating with a uniform speed of 320 rotation per minute. As you know it, it will create the free surface profile like this.

[A cylinder 0.15 m in diameter and 0.375 m high containing water is rotated about its vertical axis at a speed of 320 rpm, so that a portion of water spills out.

If the cylinder is now brought to rest, what would be the depth of water in it?]

Flow classification:

Fluid is homogeneous

Hydrostatic fluid

Forced vortex flow

So the water will be spilled. As the water spill it if it is making the cylinder is brought to the rest, what could be the depth of the water in it? So this is just a force vortex problems. Already we have derived what could be the forced vortex flow distributions part. We are just using these formulae to solve this problem.

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Question 10

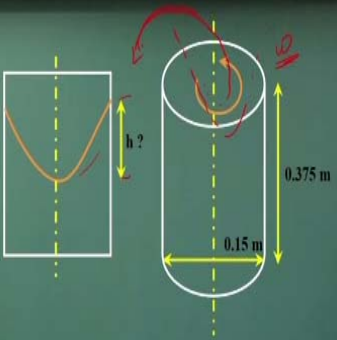
Cylinder is brought to rest:
 $N = 320$ rpm
radius of cylinder $= (0.15/2) = 0.075$ m

angular velocity $= \frac{2\pi N}{60} = 33.51$ rad/s
 $h = \frac{\omega^2 r^2}{2g} = \frac{33.51^2 \times 0.075^2}{2 \times 9.81} = 0.322$ m

volume of paraboloid $= (1/2) \times$ enclosing cylinder
 $= (1/2) \times h \times \pi r^2$
 $= 2.845 \times 10^{-3} \text{ m}^3$

Volume of vessel when full of water
 $= H \times \pi r^2$
 $= 6.6268 \times 10^{-3} \text{ m}^3$

Remaining water in tank
 $= \text{volume of vessel} - \text{volume of paraboloid}$
 $= 3.78 \times 10^{-3} \text{ m}^3$



When cylinder is brought to rest the above water will fill the cylinder and depth
 $= \frac{3.78 \times 10^{-3}}{\pi \times 0.075^2} = 0.214$ m

Now the first what is that if n is rotations per minute and you compute the radius, Cylinder is brought to rest:

$$N = 320 \text{ rpm}$$

$$\text{radius of cylinder} = (0.15/2) = 0.075 \text{ m}$$

$$\text{angular velocity} = \frac{2\pi N}{60} = 33.51 \text{ rad/s}$$

That what will give us the angular velocity in terms of radian per seconds. As we are discussing it that if this is the cylindrical object, which will rotate with the omega angular velocity, you will have free surface profiles like this.

$$h = \frac{\omega^2 r^2}{2g} = \frac{33.51^2 \times 0.075^2}{2 \times 9.81} = 0.322 \text{ m}$$

The height h will have a relation with the angular velocity and the radius. That is what we derived in a forced vortex case. That what will it comes out to be 0.322 meters. As you know it volume of paraboloid is half of enclosing cylinders. So we know the volume that part. That means this much of volume vessels will pull water conditions and this is the volume will be spilled out.

The remaining water will be this much of volume. So divide by the surface area will get the depth what will be the remaining. Again I am to just conceptually talk about these when we are rotating a cylinder which is filled with the waters, as we have rotated with angular velocity of omega, then what will happen it, it will create a free surface like this of height h.

The remaining amount of this is the amount of the water will be spilled out from the surface. So as you know this what will be the h surface will be generated and we also know how much of volume water will be spilled out from these original amount of water we know it. Remaining amount of the volume of water we know. From there we can compute what will be the depth which is volume divided by the surface area.

volume of paraboloid = $(1/2) \times$ enclosing cylinder

$$= (1/2) \times h \times \pi r^2$$

$$= 2.845 \times 10^{-3} \text{ m}^3$$

Volume of vessel when full of water

$$= H \times \pi r^2$$

$$= 6.6268 \times 10^{-3} \text{ m}^3$$

Remaining water in tank

$$= \text{volume of vessel} - \text{volume of paraboloid}$$

$$= 3.78 \times 10^{-3} \text{ m}^3$$

When cylinder is brought to rest the above water will fill the cylinder and depth

$$= \frac{3.78 \times 10^{-3}}{\pi \times 0.075^2} = 0.214 \text{ m}$$

That what will be condition. So with this, let me conclude these lectures by solving these 10 problems. Thank you.