

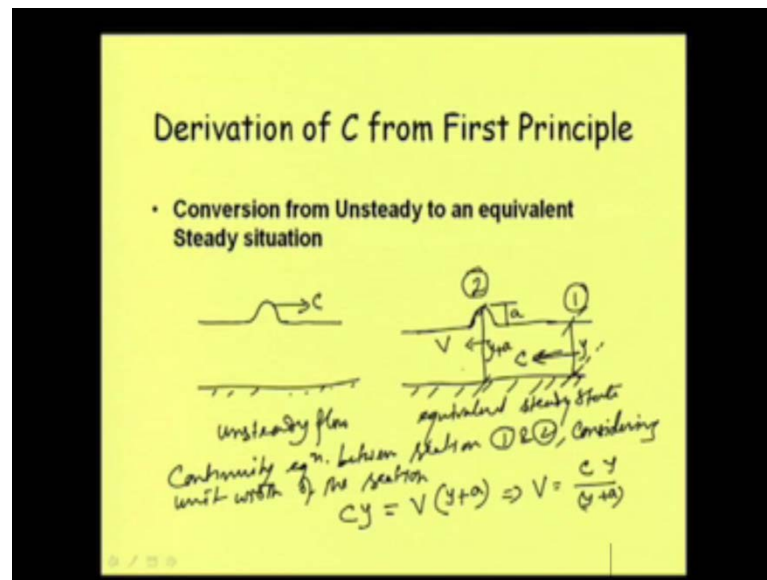
Hydraulics
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Module No. # 07
Unsteady Flow
Lecture No. # 01
Unsteady Flow Part-2

To handle this, we need to see that how we can simulate these wave flow and then how we can take protective measure, preventive measure. So, for all those understanding wave is very important and as such we started with what are the different types of wave, how we can classify waves. And then, as I am just saying that, the how the wave propagate that is very important for our various requirements, practical requirement, that is why the speed of wave propagation is also necessary. And there comes the term that we call as celerity, well.

What we mean by celerity is that, it is the speed of wave with respect to the fluid media, well. If we just simply say that celerity is the speed of the wave, then it is not complete, because we need to say that it is in reference to the fluid media. If the fluid media is **it** at rest, then of course the speed of the wave, absolute speed of the wave and celerity will be same. But, if the fluid is also moving and then over that fluid the wave is moving, then celerity is the speed of the wave with respect to the fluid media. And for analyzing these wave, say what is the celerity, to have an expression for the celerity, when we try to analyze it at unsteady flow, we face some complexity and this unsteady flow therefore we try to convert to an equivalent steady flow. So, that it becomes convenient for our analysis.

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And in the last class, we did **so how we can** we could see how we can convert this to an equivalent unsteady flow and we are starting from equivalent steady flow and we are starting from that in this class, well. Say this is a wave forming here, a solitary wave, single wave and the bed is there and **by say and** let us first consider that this is a steel water may be in a tank and by moving a paddle, we have created a wave, a single wave is moving like that and it is moving with a speed c , well and this is a unsteady flow, **this is a unsteady flow**.

Now, to convert this to a steady flow situation, as I did explain in the last class, that like a walker as the belt is moving upstream or say when we walk the belt moving the opposite direction in a walker and that is why although **our** that we are working on a walker, but we are not moving forward. And then someone can observe us that how we are behaving when we are walking, but we are in a steady position, **we are in a static position**. So, those advantages we can have here, like the belt move in the opposite direction in a walker, we can put a opposite direction the velocity C , which is the actual velocity of the wave.

Then, what will happen that this is also moving in a velocity C , wave is also moving in a velocity C in this downstream direction. And as now this fluid media is moving in the opposite direction with velocity C and wave which was moving in the downstream

direction with a velocity C . So, relative velocity of this will become 0 and then it will be remaining in this position and now, we can observe it carefully well.

Now, let us see how we can analyze it. Say this depth b at this section, suppose at this section depth is y and so amplitude of the wave is say a , this is the amplitude of the wave. And so what will be the depth here? Depth in the wave portion where we have the wave this will be say y plus a . Well and when we talk about velocity, then C is the velocity at this section, say section one. And if I talk about the section two, then what will be the velocity, say velocity is V , because this velocity will not be equal to the velocity C , because depth here is changing.

So, let us write this velocity as V , well. Now, we can write a continuity equation and from that continuity equation we can find that how we can express this V and C , how we can relate this V and C . Well, how we can write the continuity equation, say if we considered this channel to be say rectangular and suppose we are considering unit width of the channel, so this **is** let me just write here, this is a equivalent steady state. And now let us see the continuity equation how we can write, say continuity equation. Between sections say 1 and 2, between section 1 and 2 how we can write and that we are writing considering unit width of the section, **unit width of the section**.

Well, we are considering unit width of the section, then what will be the discharge in continuity equation state, that here the discharge and here discharge will be equal discharge at section 1 and section 2, will be equal, fine. Now, discharge is equal to the velocity at this point one section 1 and the area **area** is equal to y into its width.

In fact, if we considered width, then width will be coming, but we are considering width to be equal to 1, so it will be C into y , so with what we can write that C into y is equal to here, we are talking the velocity as V . So, V and depth here is equal to y plus a **y plus a** . And from this what we can write that V is equal to $C y$ divided by y plus a . Let us keep this expression here and now we can write another expression, this is from continuity equation we are getting this relation, that is b we can express in this form, well, but we can have another expression from the consideration of say energy equation.

Now, what will be the energy at this point, it will be y 1 plus, that means at section 1 it will be y 1 plus, sorry y , we are writing y , y plus C square by twice g . And here because

velocity is C here and here it will be y plus a plus V square by twice g and let us write that expression, well.

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Derivation of C from First Principle
 Energy equation between section ① & ②

$$y + \frac{C^2}{2g} = (y+a) + \frac{V^2}{2g}$$

$$y + \frac{C^2}{2g} = y+a + \frac{C^2}{2g} \left(\frac{y}{y+a} \right)^2$$

$$a = \frac{C^2}{2g} \left[1 - \left(\frac{y}{y+a} \right)^2 \right]$$

$$= \frac{C^2}{2g} \left[\frac{y^2 + 2ay + a^2 - y^2}{(y+a)^2} \right]$$

$$C^2 = 2ga \left[\frac{y^2 + 2ay + a^2}{a(y+a)} \right]$$

$$C = \sqrt{2gy}$$

And we can write that energy equation, **energy equation** between section 1 and 2, of course when we are writing energy equation between section 1 and 2, **and** we are saying that energy at this section at that section are equal, what we mean that there is no energy loss in between that assumption is inherent there. Well, now let us write that expression say y plus C square by twice g, that means V square by twice g. V mean velocity square by twice g, this is equal to depth in the section, two is y plus a plus say V square by twice g, let me write one step V square by twice g. Now, what this V is we know that V is equal to C, then y by y plus a.

So, we can just replace it in this form, that is y plus C square by twice g is equal to y plus a plus we can write that C square this in place of C square by y square by y plus a whole square. So, **so** V square we can write that V square by twice g will be V and we can write C square into y square by y plus a whole square, **ok**.

Well, this is the expression and from this let us try to write because our interest is to get an expression for C. And here what is not known and what we want to try is the C and what is our unknown thing is y, a here, the expression n. And at the same time this expression we are writing **for a very** for a wave where the amplitude is very small, I mean small amplitude wave. **As we just** if we recall our last class, then we were talking

about one expression that C is equal to root over $g y$, for rectangular channel we obtained that and that was for small amplitude wave.

So, here also we are considering that this depth is considerably large than the amplitude a , well, let us just separate this term and see how we can write it. This y and y will of course get cancel and let me write first a in terms... a is equal to $\frac{C^2}{2g}$ C square by twice g , C square by twice g is here. So, we can bring C square by twice g and then we can write $1 - \frac{y^2}{y^2 + \frac{C^2}{2g}}$ well. And this can be written as, say let us break up y^2 C square by twice g , our intension is to see that, if because in the expression of C , in fact we do not have the a term, root over say $g y$, that was that, that is what we got in last class. So, let us see, by we are starting from the first principle and we are trying that yes if if we can get this expression and here we do not have a term, so let us see how we can do that.

This we can write say $y^2 + \frac{C^2}{2g}$ and then this will be say we can break up y^2 plus twice a plus twice $a y$ square plus twice $a y$ plus a square then minus y^2 square. Well, here we are in a position to simplify now, well, so what we can do that from here let us write one expression for C . So, C is equal to, you can write that C is equal to twice $g a$ will be coming C square, let me write C square is equal to twice $g a$ and then this will be just, we can write in the reverse direction, reciprocal of this one. This will be say $y^2 + \frac{C^2}{2g}$ plus twice $a y$ plus a square, this is there and here what will be having this and this is getting cancel already and here we have twice $a y$ plus a square.

So, that twice $a y$ plus a square we can write here as a , keeping common and we are writing twice y plus a , well. Now, this a and this a we can cancel at this point and let us see how we can write this expression well.

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Derivation of C from First Principle

$$C = \sqrt{2g \cdot \left(\frac{y^2 + 2ay + a^2}{2y + a} \right)} \xrightarrow{0}$$

$$C = \sqrt{gy} \sqrt{\frac{2y + 4a}{2y + a}}$$

$$C = \sqrt{gy} \sqrt{\frac{2y + a + 3a}{2y + a}} \quad \text{as } a \ll y$$

$$C = \sqrt{gy} \sqrt{1 + \left(\frac{3a}{2y + a} \right)} \quad \therefore \frac{3a}{2y + a} \text{ is negligible.}$$

$$C = \sqrt{gy} \quad , \quad C = \sqrt{gD} \quad \text{Hydraulic depth}$$

So, we can write C square is equal to now root over twice g, **twice g** and entire things we can put under root sign, root over twice g and then here, it will become say y square plus twice a, then twice y plus a. Let me start from this expression, again y square plus twice a y plus a square divided by a, twice a plus a this a.

And a is getting cancelled, so what we are writing that twice g and in this part, we are writing that expression, well plus a square, well. So, now, here as we know that a square is say, a itself is very small, so this a square term we can put equivalent to 0 or say it is negligible. So, if it is negligible now what we can write that, C is equal C square no, it is C, because we have written already in terms of root over.

So, c is equal to say our target is to get this term g y, so we are writing g y means from here, we are bringing a y common, we are bringing a y common here. In fact, we had the term a y, a y plus a square, **right**, so y we are brining common and 2 we are taking to that side. So, what we can write root over g y, then here we can write, so as one y has come, so it will become twice y 2 is going inside and then plus 4 a 2 is going and this is coming, so it will be twice y plus a.

Well, now this we can further simplify in a way that this is equal to root over g y and let me write it in this form, that twice y plus a, fine, here also let me write twice y plus a. Then, in fact, we need to write plus thrice a into write plus thrice a, well.

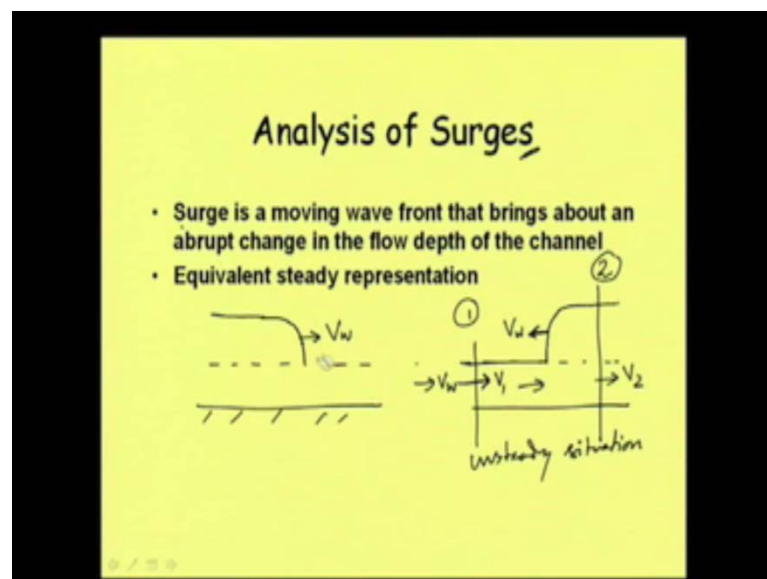
So, this twice y plus a , $2y + a$ that we can have one and this will become thrice a by this expression. And so let us write C is equal to $\sqrt{g y}$ then you can write $\sqrt{g}$ over $1 + \frac{3a}{2y + a}$. Now, this expression, $\frac{3a}{2y + a}$, a is very small and here, in the denominator, we have $2y$.

So, it is quite a large expression and $2y$ as y is very large than as compared to a , so $\frac{3a}{2y}$ this expression will become a very small term divided by a very large term, so this we can now neglect. So, if we neglect this term say as a is very very small, as a is very very small as compared to y , therefore $\frac{3a}{2y + a}$ is say negligible, $\frac{3a}{2y + a}$ is negligible. And now, just neglecting this part it will become C is equal to $\sqrt{g y}$.

Well, so that is the expression that we can derive, what we got in our last class, again starting from the first principle we could see that for a small amplitude wave we can have the expression for C as $\sqrt{g y}$. And if it is a suppose nonrectangular channel, then what we do, that y will not represent these things properly.

So, what we write that C is equal to $\sqrt{g D}$, what D is, D is the hydraulic depth, D is the hydraulic depth. So, using this hydraulic depth, in fact for rectangular channel this will become y , but for trapezoidal channel it will be A/t . So, using this expression also we can get the value of C , well.

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So, after that let us see that, well for a wave of this type, for a wave of this type solitary wave of this kind we can have an expression for C , but if we have a surge, if we have a surge and how to analyze this surge, whether the C value will be same as or the same expression whether we can use or not. Well, **that** first we should know what is surge, this is also in unsteady flow, this is important, I mean important topic that is surge, we need to do lot of analysis in fact on surges. And but here we will be just doing some limited exercise on surge, that you can see that surge is a moving wave front that brings about an abrupt change in the flow depth of the channel.

So, basically what we mean by surge is that, say this is the bed and normal flow is suppose moving here and somehow a wave is coming like that, it is the moving wave front, that is why we called this is a wave front, this wave front and say then it is more. So, this water is moving like that otherwise also and then we have a moving wave front, this wave front is moving with a velocity say V_w , this wave front is moving with a velocity V_w and **this can be** this we referred as a surge. In fact, it can be in the other way also say your water level is here, **water level is here** and water itself is moving in this direction suppose and somehow due to closure of gate, **the** you have suddenly closed the gate.

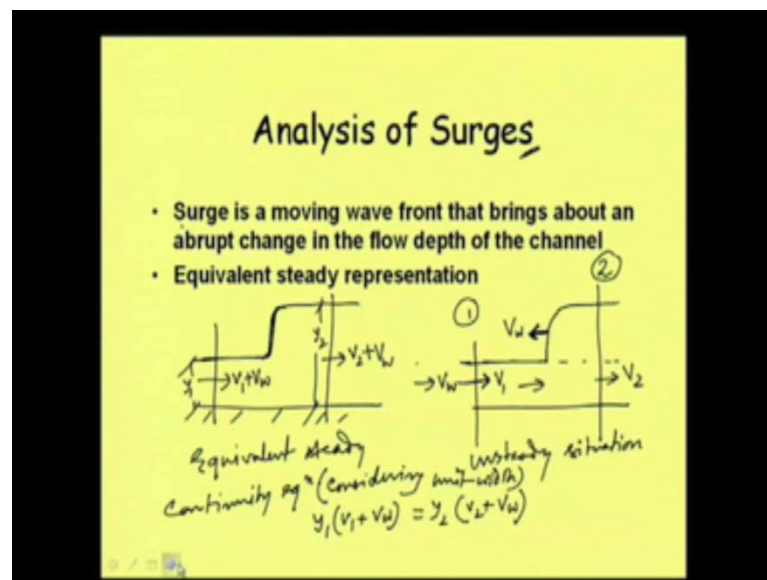
So, water level here is rising and then the wave can be moving in the opposite direction also, this is say wave moving upstream and this is a wave moving downstream. So, whatever may be the situation, we called such moving wave front, which is moving and creating a abrupt change in the depth, say depth earlier was like this and there is a abrupt change, if the depth changes gradually like this, then we will not call this as a charge, but here depth is changing abruptly and that is why we called this as a charge and surge. So, this surge also we can express in the form of say equivalent steady state for its analysis. Well, let us see how we can represent this in the form of an equivalent flow.

Well, let us consider this one, anyone we can consider, but let us consider this one, suppose this is say 1 and this is section 2, so say 1 and 2. Why we are considering because this is both in the same direction, here it is in the opposite direction, that will give us an opportunity to handle a case where the flow and waves are moving in the opposite direction, till now we have not discussed that sort of situation.

So, suppose the velocity here is V_1 and velocity here will be changing. Velocity here means in the entire section say V_2 , well, now V_w is the velocity which is moving in the opposite direction, this is a unsteady situation, at next movement of time this wave will be moving further, this wave will be moving further and say we will not find it here. So, let us see how we can do this to keep in a steady position.

Well, what we can do in this, we can apply an additional velocity in the opposite direction to the speed of the wave, well. So, please just see we are meaning that opposite direction to the speed of the wave, but this speed of a wave is not the celerity, celerity will be the relative speed, so **we are** we need to apply a velocity y in the opposite direction to the speed of the wave, otherwise it is moving with a velocity V_1 . Now, if you apply another velocity say V_w , if you apply another velocity say V_w in this part, then total velocity at this point will become V_w plus V_1 and here also it will become V_2 plus V_w . And then, velocity of this in this direction will become 0, because it is moving in this direction and **then at** that is why the these things is not in a position to move further, it will be remaining in the same position.

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Well, so let us represent this and let us see how we can derive. I am now rubbing this portion and this equivalent steady state position we can keep here, we can draw here, say it will be like this. Now, we have here the velocity will be V_1 plus V_w and here the

velocity will be V_2 plus V_w and of course, there will not be any velocity of the wave, it is not moving rather.

So, this is basically we can say equivalent steady situation. Well, now, again for this surge, just like we were writing earlier, we can write continuity equation and momentum equation. So, continuity equation we can write here, say continuity equation and let us put some depth value here, say depth here is y_1 and depth here is say y_2 , y_2 well, now what is continuity equation?

So, again considering unit width of the channel, considering unit width, we should mention this one, considering unit width this will become say y_1 into V_1 plus V_w is equal to y_2 into V_2 plus, sorry it is not V_3 , it is V_w V_2 plus V_w , well, so that is our continuity equation. And this continuity equation can give us or from **or from** this continuity equation, we can express y_1 in terms of y_2 and we can do those things and then what is this V_1 plus that is also interesting.

In fact, if from this point when wave speed or absolute speed of the wave is say it is moving with a speed V_w and then the fluid is moving in the opposite direction V_1 , then what is its relative speed? Its relative speed will be V_1 plus V_w , because both are moving in the opposite direction.

So, **it will be** it is in fact it will appear that it is moving faster, when V_1 is in this direction, V_w in this opposite direction. So, wave speed, relative wave speed will be V_1 plus V_w and this relative wave speed in fact we call as C . So, this V_1 plus V_w is nothing but C , well that we can write that equation.

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So,
continuity
equation we
have seen
and then let

Continuity and Momentum Equation of Surges

Continuity Eqⁿ: $y_1(V_1 + V_w) = y_2(V_2 + V_w)$

Momentum Eqⁿ: $\frac{1}{2} \rho g y_1^2 - \frac{1}{2} \rho g y_2^2 = \rho y_1(V_1 + V_w)(V_2 - V_1)$

Celerity $C = V_1 + V_w$

$\frac{1}{2} \rho g y_1^2 \left(1 - \frac{y_2^2}{y_1^2}\right) = \rho y_1(V_1 + V_w) \left[\frac{y_2(V_1 + V_w)}{C} - \frac{y_2(V_2 + V_w)}{C}\right]$

$\Rightarrow \frac{1}{2} g y_1^2 \left(1 - \frac{y_2^2}{y_1^2}\right) = y_1(V_1 + V_w) \left[\frac{1}{y_2} - \frac{1}{y_1}\right]$

me write the continuity equation again and let me keep the diagram here, quickly, say it is V_1 plus V_w , sorry V_2 plus V_w and this is V_1 plus V_w , that we have and depth here is y_1 , this is y_2 . Now, the continuity equation we have already described, so y_1 plus y_1 into V_1 plus V_w is equal to y_2 into V_2 plus V_w . Now, we need to write the momentum equation, we need to write the momentum equation, so for momentum equation, for writing the momentum equation, we need to see what the forces are acting. So, the pressure force from this direction and the pressure force from that direction and then the momentum, change in momentum between this point and that point.

So, pressure diagram we can draw like that and as we know, we have discussed that part a lot, so pressure here we can write as half of ρg into y_1 square, because pressure here is nothing but ρg into y_1 or $w y_1$, we can write **in** it as w or we can write ρg . So, writing in any form we can get it say $\rho g y_1$ and then area of this triangle will be half of $\rho g y_1$ plus multiplied by the way y , so it will become half of $\rho g y$ square. So, momentum equation what we can write, the force from this side that we can write, this is continuity equation and now, we are writing momentum equation. So, momentum equation we can write here, say half of $\rho g y_1$ square that is the pressure force from this side and minus half of $\rho g y_2$ square that is the pressure force from that side, that is equal to change in momentum, rather rate of change in momentum, so what we can write that mass flowing per unit time and change in velocity.

So, mass flowing per unit time how we can write, that discharge flowing per unit time, well discharge as it is not changing from here to here, because no other flow is being added, nor the flow has been taken out, so we can write it in terms of discharge of this pass. Because this is known to us, what is depth y_2 that is of course **known**, not known to us, because after coming of the wave this is happening, but this y_1 will be generally known to us.

So, let us write the discharge in terms of this one, that we can write discharge in fact is equal to y_1 into V_1 plus V_w is the say velocity and area is actually y_1 into width, but width is 1. So, this is what the volume flowing we can say and then this volume flowing if we multiplied by ρ , then it become the mass flowing, so this is what the mass flowing. And then V square or say, sorry, not V square, this is the mass flowing and the change in velocity. So, change in velocity is equal to in fact, it is V_2 plus $w V_w$ minus

V_1 plus V_w , so ultimately the resulting will be V_2 minus V_1 , so that is what the change in flow velocity, this is our momentum equation.

Well, from this momentum equation we can further derive some of the relation; I mean which is required for finding the expression for C in case of surge. And well before that let us write the expression for C here, this is another equation, that is C is equal to we have, we can write that C is equal to say V_1 plus V_w , that we have already explained how it is.

So, this is equal to C , celerity C that is the expression for celerity C . And this expression celerity C we can further say starting from the momentum equation, we can derive it in a different form and let us see how we can do that. Well, now, we need to mention one point here that we got one expression for C is equal to root over $g y$ and this equation is called lagrange's equation of celerity, this equation, C is equal to root over $g y$, this equation is called lagrange's equation of celerity.

Well and now, let us see what will be the expression for C in case of surge, in terms of y_1 and y_2 . Well, in general, we can have it as V_1 plus V_w , but **we** then we do not know what V_w is and so we need to have it in a different form, like that earlier we got in terms of depth y , so let us see what we can do. Starting from this again, starting from this momentum equation, we can write that this is equal to say ρ , we can cancel in each part. Then let me take common here say half of g , then y_1^2 square, say half of $g y_1^2$ square if I keep here, then it become 1 minus y_1^2 square by y_2^2 square, well. And on this side we can take say y_1 is here and then V_2 minus V_1 is there, so what is the V_2 is the velocity, so velocity and this expression actually y_1 plus V_1 plus V_w , this expression. This expression is nothing but, this is showing how much is the discharge I am writing this as Q , this is Q means unit discharge, because we are talking about discharge through unit width.

So, this is equal to Q and what is our V_2 or V_1 , V_2 is nothing but Q by say y_1 , because V_2 into y_1 is equal to y_2 is equal to Q and V_1 is equal to Q by y_1 , because that we know, that is again from continuity equation we know that $V_1 y_1$ is equal to $V_2 y_2$, that is also known to us. So, in fact, this V_2 can be written as, V_2 can be written as Q by y_2 , means Q is equal to V_1 plus V_w , Q is equal to $y_1 V_1$ plus V_w divided by y_2 . So, that can be written, well, so if we bring this Q common here, let me write it in

this from, here say y_1 plus V_1 plus V_w and then this Q , we can let us keep ρ still here, because here also ρ , ok discharge will be coming.

So, this discharge is nothing but say we can again write this part as y_1 into V_1 plus V_w that is what the discharge we are writing here bringing common. And then inside this will be saying 1 by that means Q , we are bringing out this Q is nothing but this expression and then, here it will be 1 by y_2 minus 1 by y_1 , well. And as we can see very clearly that this term and this term is same.

So, we can just because we are just writing for discharge only, so this will be square, so this can be written as half of $g y_1$ square and 1 minus y_1 square by y_2 square is equal to, this now we can write y_1 square and then we can write here as say V_1 plus V_w square, then within bracket we are putting say 1 by y_2 minus 1 by y_1 .

Now, let us see how we can further simplify this expression here, that is the V_1 plus V_w this is nothing but C . So, from that we can put the value here as C square, say y_1 square and this y_1 square we can cancel and then we can just rewrite this expression in a simple form like that.

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The image shows a handwritten derivation on a yellow background. At the top, it says "Continuity and Momentum Equation of Surges". Below this, the derivation proceeds as follows:

$$C^2 = \frac{\frac{1}{2}g \frac{(y_1+y_2)(y_1-y_2)}{y_1^2}}{\frac{(y_1-y_2)}{y_1 y_2}}$$

$$= \frac{1}{2}g \left(\frac{y_2}{y_1} (y_1+y_2) \right)$$

$$C^2 = g y_1 \left(\frac{1}{2} \frac{y_2}{y_1} \left(1 + \frac{y_2}{y_1} \right) \right)$$

$$C = \sqrt{g y_1} \sqrt{\frac{1}{2} \frac{y_2}{y_1} \left(1 + \frac{y_2}{y_1} \right)}$$

C square we have already replaced this part, that means this we are writing as C , this one this is nothing but C , so putting that, what we can write C square is equal to say half of g , half of g , then we can write say y square, y_1 square minus y_2 square, that we can write

y_1 plus y_2 into y_1 minus y_2 and this is divided by y_1 square. And then this, the denominator part we can write say y_1 minus y_2 divided by $y_1 y_2$, that means this part, this is become y_1, y_2 , then y_1 minus y_2 , so this is coming here. And this is becoming y square, y_2 square, then this y_1, y_2 square minus y_1 square, that we are writing as this, I mean this one say y_1, y_2 and y_1 plus y_2 . Now, from here what we can do, this is equal to half of g , then we can write y_2 by y_1 .

So, this y_1 and this y_1 is getting cancelled and we can write this as y_2 by y_1 , y_2 by y_1 , y_2 by y_1 into say it will be y_1 plus y_2 , that will be the expression. And we can of course further simplify from this part, we can see that our target is always to get $\frac{1}{2}$ the expression in terms of root over $g y$ and then whether we can have it in further simplified form.

So, C square, this is equal to, we can bring one y from here, one from one y_1 from here, so it is equal to say $g y_1, 1 y_1 y$ bringing from here and then the other part we are writing in a different way, say half we are writing here and say this y_2 by y_1 is there, y_2 by y_1 and then as $1 y_1$ we have brought here, this will be 1 plus y_2 by y_1 , well.

So, that is the expression we are getting and as you can see, that, $\frac{1}{2}$ this will be y_1 . So, C square is equal to this part, then if we just try to take C , then we will be getting C is equal to root over $g y_1$, then root over say half of y_2 by y_1 and 1 plus y_2 by y_1 .

Well, now in this expression normally if we refer to our earlier diagram, this say y_2 will not be known to us, because it is coming, this wave is coming and the y_1 will be known to us. Of course, so to get the value of C , then say generally we are getting the expression in terms of y_2 by y_1 and here it is $g y_1$ and this y_2 we need to know in many case.

So, this y_2 $\frac{1}{2}$ sorry, $\frac{1}{2}$ this should have been y_2 square by y_1 square, yes, we are taking common y_1 square here and as such it will be y_2 square by y_1 square and this is y_2 square by y_1 square, $\frac{1}{2}$. And that is why we are getting this expression in this form like that one, this one and so this is coming in this form, well, fine.

So, that way C is equal to root over $g y_1$ and this expression we are getting in terms of y_2 by y_1 . And this is the expression normally we use for computing surge, surge means a celerity in surge. And then this help us $\frac{1}{2}$ in various in solving various numerical problems, small numerical problems, we can solve by using this particular expression, well.

[FL] [FL] expression for C 2 variable continuity and momentum equation [FL] 39 [FL]
39 [FL] [FL]

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Typical Problem of Surge Analysis

- Water flows in a rectangular channel at a depth of 2m with a velocity of 1m/s. If discharge in the channel is suddenly trebled what will be the depth of flow?

$$(V_1 - V_w)y_1 = (V_2 - V_w)y_2 = (1 - V_w)2$$

Let us take a problem, typical problem. In fact, we will not **we will not** be solving the problem as such, but we will just show how the steps need to be followed and how we can get the result. So, the problem suppose it is like that the water flows in a rectangular channel at a depth of 2 meter, with a velocity of 1 meter per second, well, say this is the channel and here, water is flowing, first I am drawing by dotted line is flowing with a depth of 2 meter, this depth is 2 meter, this is a typical problem taken from the book of Rangaraju open channel flow.

So, this is say depth is 2 meter and the velocity of flow is 1 meter per second, well and if discharge in the channel is suddenly trebled what will be the depth of flow? So, here it was a depth of flow, suppose in the discharge if we suddenly trebled, then what will be the depth of flow? And suppose depth of flow is increasing like that and this will in fact continue to increase, this will continue to increase, this will continue to increase and then wave is moving in this direction and after some time the depth will be increasing.

Now, here this is in fact **our say** we can put as y_2 and this is our y_1 , of course we can write either way also and then velocity here is say V_1 , velocity here is V_2 and then wave velocity let us put as V_w . Then how we can write the continuity equation and

momentum equation for this case and what we know here is the depth y_2 and this V_2 is known, velocity is 1 meter per second and depth is say 2 meter.

So, that part is known and other things are not known and what we know is the discharge, what was earlier flowing is just trebled. So, this discharge what will be getting here $y_1 V_1$, say considering unit width, what will be getting $y_1 V_1$ that will be three time of that of the say $y_2 V_2$, well.

So, how we can write the continuity equation again to first make it steady, what we can do to make it steady? We can apply a velocity opposite to this V_w , so we will be applying here V_w . And then if we apply V_w , what will be the velocity here, ultimately this velocity will be changing to say V_1 minus V_w , after applying this one and this will be changing to, this velocity will be changing to V_2 minus V_w .

Well and then continuity equation we can write say V_1 minus V_w into y_1 is equal to V_2 minus V_w into y_2 , so that is what we can write the continuity equation. Now, here, we can put the value of V_2 and y_2 , so what we can write that this is nothing but say V_2 is equal to 2, so 2, sorry V_2 is equal to 1 minus V_w into 2. So, this equation will give us some information and then we can write the momentum equation, **we can write the momentum equation** say.

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$$\frac{1}{2} \rho g (y_1^3 - y_2^3) = \rho (v_2 - v_w) y_2 (v_2 - v_1)$$

$$\frac{1}{2} \rho g (y_1^3 - 4) = \rho (1 - v_w) 2 (1 - v_1) \quad \text{--- (2)}$$

$$v_1 y_1 = 3 v_2 y_2 = 3 \times 1 \times 2 = 6$$

$$y_1 = 2.45 \text{ m.}$$

So, momentum equation can be written as say half of **well...** let me give a number to this equation, say this equation is 1, then momentum equation is equal to half of ρg say y_1 square minus y_2 square is equal to ρV_2^2 minus V_w . Here, this is the velocity, then we are getting y_2 and I mean this part is actually the discharge and then it is V_2^2 minus V_1^2 that is what we are getting. And then this expression also we can simplify, **simplify** means we can put the value like half of say ρg y_1 square minus y_2 square, means 4, this is equal to ρ , you can write this as ρ , then V_2^2 minus V_w that we can again write as say V_2^2 was our 1 minus V_w .

And this y_2 is already known to us, so **this will** this is 2, so **this** two depth is, we got the depth as, sorry we got the depth as 2 meter. So, that we can put here, say 2 and then this V_2^2 minus V_1^2 , again this we can write as 1 minus V_1^2 , now this is say equation 2.

Well, that what information we have, **we have** a relationship between, what information we have that you can refer to the slide, we have one information like that $V_1 y_1$, which is the discharge, which was the discharge after the charge is coming, that is $V_1 y_1$. This is the actual discharge what is coming here and this discharge is trebled or three times of that $V_2 y_2$, so we can write it like that.

$V_1 y_1$ is equal to say three time of $V_2 y_2$ and this value we can have that is equal to 3 into say one is the velocity into to the depth 2, so this is equal to 6. So, that way we can have, I am just writing the numerical value, not writing the unit here, so this is one expression and then we have this expression. And solving these expressions we can get ultimately the value of y_1 , because our target is to know the value of y_1 and so if we know this value of y_1 our problem is solved. And to get the value of V_1 we have these equations, say this is one equation and then, here of course we have this unknown V_w and this is one equation where we have this unknown V_w .

So, V_w and y_1 are **the** unknown that we can solve by trial and error method and we can get say y_1 is equal to 2.45 meter. This is just a solved problem already in the book of rangaraju and just I am taking here, just to show how the surge problem can be solved, well. Then, we will be taking up the next topic rather the equation of unsteady flow, well.

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Equations of Unsteady Flow

• Continuity equation $\frac{\partial A}{\partial t} + \frac{\partial Q}{\partial x} = 0$
 $\frac{\partial A}{\partial t} + A \frac{\partial V}{\partial x} + V \frac{\partial A}{\partial x} = 0$ (where $Q = A \cdot V$)

• Equation of motion (Deduced by Barre' De' Saint Venant (1871))

• Dynamic equation of unsteady flow in Open Channel (Shallow water wave equation, i.e., vertical acceleration is negligible)

• The equation can be derived by two approach

1. Energy approach
2. Starting from Newton's equation of motion

Also, equation of unsteady flow that we know, that already we have discussed some of the equations of unsteady flow when we were discussing our earlier discussion on say governing equation of open channel flow. For unsteady state, we were discussing about the continuity equation, **the continuity equation** that as we know it is say $\frac{\partial A}{\partial t} + \frac{\partial Q}{\partial x}$ is equal to 0, that we could get. And this of course we can write as say $\frac{\partial A}{\partial t} + \frac{\partial Q}{\partial x}$, if it is Q is written as A into V this can be written as say $A \frac{\partial V}{\partial x} + V \frac{\partial A}{\partial x}$ is equal to 0, well.

So, here, I am not taking up again this continuity equation, that you can refer or rather we will be knowing by referring to our earlier classes. And then, the two governing equations are required basically for solving the problem of unsteady flow and then, one of the most popular equation, of course continuity equation is there, then another equation that we take is the equation of motion. And this can be of course we use momentum principle or energy principle to get this equation of motion and for some case we use say continuity and momentum equation in couple for solving the problem, sometimes we use continuity and energy equation for solving the problem, depending on the situation where suppose energy is, energy loss is there, there we go for momentum couple, continuity momentum couple.

So, that way these considerations are there, of course in this class we are not going for all those details, but we will be just discussing the equation of motion that was given, that

was first deduced by barre de saint vennant and popularly known this equation as saint vennant equation. And that is say 1879, long back this equation was derived, well and this is a dynamic equation of unsteady flow in open channel and for what condition it is the shallow water wave equation? **Shallow water wave equation?**

That means, why we are giving this as shallow water wave equation, because when this equation was derived this vertical acceleration was considered to be negligible, so vertical acceleration is negligible.

And then we should know that for what condition we can apply this and derivation of this equation not this equation, this is continuity equation, derivation of the equation of motion can be done by two approach, one is energy approach and another is that we can start from newton's equation of motion. So, by both this approach we can have the derivation and here, we will be discussing how by energy approach we can derive the equation in a simple way, **ok**.

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Writing energy eqⁿ between ① & ②

$$z_1 + y_1 + \frac{V_1^2}{2g} = z_2 + y_2 + \frac{V_2^2}{2g} + \text{loss } h_L$$

$$\text{loss } h_L = \text{friction loss } (h_f) + \text{accⁿ loss } (h_a)$$

$$h_L = h_f + h_a$$

of friction slope S_f

$$\frac{h_f}{\Delta x} = S_f$$

$$h_f = S_f \Delta x$$

Diagram showing two sections 1 and 2 of a channel. Section 1 has elevation z_1 and depth y_1 . Section 2 has elevation z_2 and depth y_2 . The channel bed is at elevation z_b . The flow is from left to right. The length between sections is Δx . The velocity at section 1 is V_1 and at section 2 is V_2 . The total head at section 1 is $z_1 + y_1 + \frac{V_1^2}{2g}$ and at section 2 is $z_2 + y_2 + \frac{V_2^2}{2g}$. The head loss between sections is h_L .

$$dV = \frac{\partial V}{\partial t} dt + \frac{\partial V}{\partial x} dx$$

$$\Rightarrow \frac{dV}{dt} = \frac{\partial V}{\partial t} + \frac{dx}{dt} \frac{\partial V}{\partial x}$$

$$= \frac{\partial V}{\partial t} + V \frac{\partial V}{\partial x}$$

local accⁿ

And then, let us see what is the energy equation, say if this is the flow and this is going like that, well let me take some space, because we will have to write here, say this is section 1 and section 2, so section 1 and 2, well. In this section, 1 and 2 let us take a small length, **let us take a small length** and let us write this as say as this is small, let us write this as say Δx , this length is and that term is here, **that term is here**. So, this depth is say z_1 and this depth is say z_2 that is the elevation head up to the bed. And then up to

this bed this is y_1 , we are considering slope to be small and that is why we are not writing $y_1 \cos \theta$ or those term we are writing straight way it is y_1 .

And then here this energy is V^2 by twice g , V_1^2 by twice g energy head up to that point. And then here, in the second section **section 2**, this is the y_2 and the V^2 by twice g is suppose that much, V^2 by twice g , V_2^2 by twice g . And then we can draw the energy gradient line as this one energy gradient line, as this one and there is definitely some energy loss, **this we refer as...**

So, when we draw it parallel to the datum then we will be finding that there is a head loss and this head loss we can write as h_L . And in fact, this head loss is having two components, one is that, one is that its friction loss, that is known to us because we did discuss about this friction loss during our discussion of gradually varied flow itself, but here there will be another component. Because, in case of unsteady flow that local acceleration exists, local acceleration exists just to recall briefly. Say, when we say V , then it is a velocity, which is a function of x and T , of course in steady flow it become a function of a it **it** is not a function of T , but in unsteady this become a function of T .

Now, when we talk about, so this change in V say dV , that we can write as $\frac{dV}{dt}$ into dt plus $\frac{dV}{dx}$ into dx , **sorry** $\frac{dV}{dx}$ into dx . Now, if we write that it is a function of x and t , so if we just write it as $\frac{dV}{dt}$, **$\frac{dV}{dt}$** , then we are getting $\frac{dV}{dt}$ plus say this $\frac{dV}{dx}$ into dx , so $\frac{dV}{dx}$ divided into $\frac{dV}{dx}$. And this $\frac{dV}{dx}$ is nothing but V , so now perhaps you can recall that we did discuss earlier also $\frac{dV}{dx}$ is equal to V , $\frac{dV}{dx}$. And then this is called local acceleration, this is called convective acceleration.

Now, in case of say steady flow, this term is not existing, so that problem becomes little simpler, but here we have this term. So, this local acceleration exist **local acceleration exist**. So, because a acceleration is there **in any** whether this fluid or in a solid body, if acceleration is there that is a mass moving and that mass is having some acceleration means, some force is being utilized to have that acceleration, otherwise that acceleration will not be there. So, some force is being utilized to have this acceleration and when some force is being utilized and things are moving, then there must be some work done, force is applied and it is moving, so some distance has been moved.

So, some work done will be there and some work done is there means then some energy loss is there. So, we can say that in this sort of flow there is two types of loss, one is h_f and other is h_a , so this two laws will be there, this h_a is say loss due to acceleration.

Well, now if we write the energy equation, so writing energy equation between say 1 and 2, between 1 and 2, what we can have, between 1 and 2 this we can write say z_1 plus y_1 plus V_1^2 square by twice g is equal to z_2 plus y_2 plus V_2^2 square by twice g plus h_L , well, plus h_L or say we can say loss h_L . Now, this loss as I have explained that let me write here say loss h_L is equal to say friction loss, friction loss that we write as h_f and plus the acceleration loss, acceleration loss that is say h_a .

So, our expression become, now of course in this last term we need to put this two, so this is equivalent to h_f plus h_a , already we have written here, now we need to have an expression for these two. So, h_L is equal to, we know that it is h_f plus h_a . Now, how we can get the h_f , because friction slope we know that s_f , if friction slope is s_f , if friction slope is say s_f , then we know that h_f after that, that is friction loss divided by Δx Δx is equal to s_f or we can say that s_f the slope into distance, s_f into this Δx will give us the h_f .

So, friction slope may be this like that and we can have s_f up to certain point h_f and then this slope is actually s_f and then other part of loss is due to say this acceleration. So, that is cleared to us, that we have discussed earlier also, so in place of h_f by Δx , sorry in place of h_f , we can write that h_f is equal to s_f into Δx , well, now that is for our next acceleration lost is there, how we can calculate that that?

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$acc^{\Delta} \frac{\partial v}{\partial t}$ exist.
 unit wt of fluid, then mass = $\frac{weight}{g} = \frac{1}{g}$.
 Force utilized to produce this acc.
 $mass \times acc^{\Delta}$
 $= \frac{1}{g} \frac{\partial v}{\partial t}$.
 distance moved by this unit wt of fluid = ∂x
 $\therefore$ work done = $\frac{1}{g} \frac{\partial v}{\partial t} \partial x$
 $h_a = \text{Energy loss} = \frac{1}{g} \frac{\partial v}{\partial t} \partial x$
 $\therefore h_L = h_f + h_a = S_f \partial x + \frac{1}{g} \frac{\partial v}{\partial t} \partial x$.

So, acceleration $\frac{\partial v}{\partial t}$, local acceleration $\frac{\partial v}{\partial t}$ exist here. So, if this is the acceleration, then **if this is the acceleration then** the mass suppose if we considered that unit weight of fluid **unit weight of fluid**, then mass is equal to say weight by actually weight by the g , so this is here as weight is equal to 1.

So, this is equal to 1 by g and force utilize **force utilize** to produce this acceleration, force utilize to **produced to** produce this acceleration that is equal to mass into acceleration, **mass into acceleration**, so that we can write as 1 by g into $\frac{\partial v}{\partial t}$. So, this is what force required, force utilized, then this force is working for how much distance, this force is working and then acceleration is being there and then the fluid is moving, this mass is moving from here to here, so the distance of say Δx it is being moving.

So, what is the work done? And distance moved **distance moved** by this unit mass, by this unit weight rather by this unit weight of fluid is equal to Δx , that is what we are considering. Therefore, the work done, how much work is being done? Work done is equal to 1 by g $\frac{\partial v}{\partial t}$ into Δx , **$\frac{\partial v}{\partial t}$ into Δx** . Well, so this is the work done and what this work done is that is the energy loss **energy loss**. So, energy loss is equal to; that means, 1 by g $\frac{\partial v}{\partial t}$ into Δx .

So, finally, how we can write the head loss, so this **this** energy loss is nothing but h_a . So, this energy loss due to acceleration that is the work done due to produce that acceleration

and that is the energy loss we can write like that. Therefore, say what we can write that head loss h_L is equal to h_f what we can write, h_f plus h_a **h_f plus h_a** and that h_f we can write s_f into Δx and then this h_a we can write that is the acceleration loss 1 by g and $\frac{dv}{dt}$ into Δx .

So, putting this value of h_L in our equation of energy this one, then we can get a simplified expression and then manipulating with that expression finally we will be able to derive equation of motion and that we will be doing in our next class. And then from that we will be also trying to see how this equation can be solved and then by solving this equation how we can get solution to our real life problem of open channel flow. So, thank you very much.