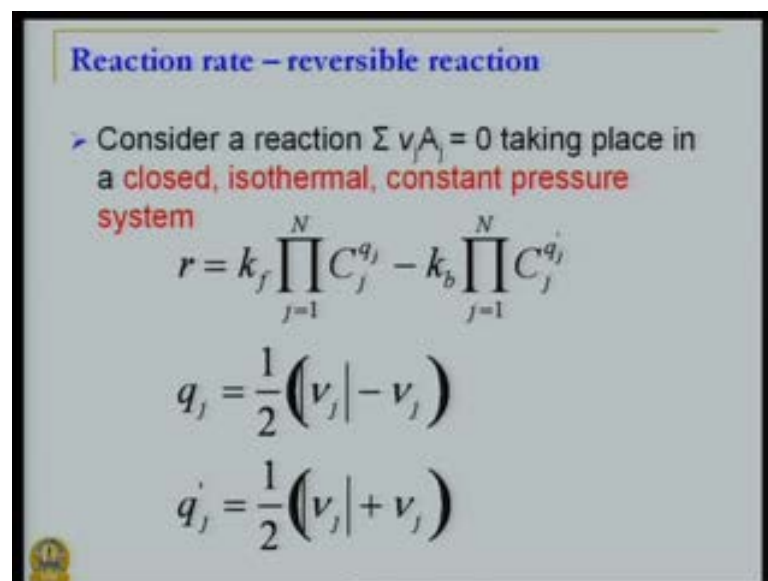


Chemical Reaction Engineering
Prof. Jayant Modak
Department of Chemical Engineering
Indian Institute of Science, Bangalore

Lecture No. # 06
Chemical Reaction Kinetics and Reactor Design

Friends, let us continue our discussion on chemical kinetics, and last time we saw several restrictions that come on the rate of reaction, because of thermodynamic consideration. To recap what we saw last time we said that if the reaction is reversible, then the rate of forward reaction ratio of forward rate constant to backward rate constant is the equilibrium constant. Because of this we do not have freedom of choosing both forward rate constant and backward rate constant independently. Because thermodynamics specifies for us what should be the equilibrium constant. So, if we choose any one of those constants, the other one is automatically fixed. The same applies to power law kinetics, and the orders that we use with respect to forward reaction and reverse reaction. Let us continue this discussion further and see what happens when we have a reversible reaction taking place in the reactor, and to get a feel of how reaction rate changes as these reaction progresses, let us look at in qualitative terms.

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Reaction rate – reversible reaction

➤ Consider a reaction $\sum \nu_j A_j = 0$ taking place in a **closed, isothermal, constant pressure system**

$$r = k_f \prod_{j=1}^N C_j^{q_j} - k_b \prod_{j=1}^N C_j^{q'_j}$$
$$q_j = \frac{1}{2} (\nu_j | - \nu_j)$$
$$q'_j = \frac{1}{2} (\nu_j | + \nu_j)$$

So as we saw last time we start with reaction summation $\sum \nu_j A_j = 0$ taking place in the closed, isothermal, constant pressure system. And let us say that this reaction is reversible reaction. So what we have is forward rate backward rate, so forward rate k_f into product of C_j raise to q_j product overall species. Similarly, backward rate k_b into C_j raise to q_j' , and we also said last time that for law of mass action kinetics q_j and q_j' are link to the stoichiometric coefficient ν_j by these relations; that is q_j is half of mod ν_j minus ν_j , and q_j' is half of mod ν_j plus ν_j .

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Variation of reaction rate with progress of reaction

Consider a reaction $\sum \nu_j A_j = 0$ taking place in a closed, isothermal, constant pressure system

$$r = r_f - r_b = k_f(T) \prod_{j=1}^N C_j^{q_j} - k_b(T) \prod_{j=1}^N C_j^{q_j'}$$

$$C_j = C_{j0} + \alpha \nu_j$$

$$r(\alpha, T) = r_f(\alpha, T) - r_b(\alpha, T)$$

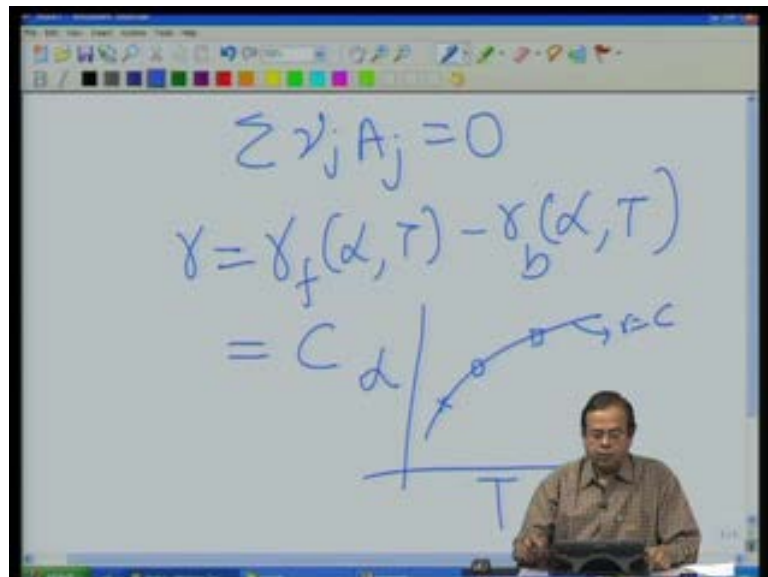
Now let us see how reaction rate varies as the reaction progresses. So, we have these rates of reaction which is forward rate minus backward rate, which is power law kinetics as expressed over here. Let us bring our definition of extent of reaction so C_j is $C_{j0} + \nu_j \alpha$. Now you we have seen in the last class that these rate constants depend on the temperature that is this rate constants k_f and k_b are functions of temperature. We see that concentration is a function of extent of reaction. So concentration is a function of extent of reaction. Now we have rate of reaction explicit function of extent of reaction and temperature both forward reaction as well as reverse reaction.

Now, what happens when the reaction takes place in a closed isothermal system or closed system? We have α that is zero at the start of the reaction and it progressively increases. Now in a non-isothermal system temperature also can change. For an isothermal system temperature is constant but for non-isothermal system temperature

also can change. So the question now we ask ourselves is what happens as reaction progresses? We are not worried about what reactor and so on. We will worry about it in the latter half of this session.

But just say that alpha changes and temperature also may change. So depending on how alpha and temperature changes the rate of reaction been changed. Now how alpha and temperature changes will depend on what reactor we are using how we are operating and so on. At this moment we are just considering for sake of illustration that alpha and temperature is vary, so for different values of alpha different values of temperature how does the rate of reaction change.

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So to see that we see some rate contours here, but before we come to this little bit of background; so let us go back to our reaction and we have our reaction summation $\nu_j A_j$ equal to zero that is our reaction and exercise just now showed us; that we can express r as r_f of α and T minus r_b of α and T . So we have forward rate of reaction backward reaction rate. Now what we want to see is how these rate changes as α and T changes. Now α and T are two variable so if you were to plot rate as a function of α and T one would require a three-dimensional representation α on one axis, temperature on one axis and rate on another axis.

Let us see that is little complicated. So instead what we will do is we will try to see how the rate of reaction varies in a slightly different form. We will try to see the rate of these

reaction contours that is how assuming that r is some constant value C . How does that contour look like in a phase plane of α and T ? So what we are going to see is a two-dimensional representation on one axis y axis we have α or extent of reaction on x axis we have temperature and so given a point; we will try to see how does the rate of constant the contours of constant rate look like in this phase plane.

So what does it mean it means that if i take all those values of α and T for which the rate has a constant value C ; this becomes my contour and join all those points these becomes my contour for rate being constant. So any combination of α and T on this contour all gives rise to the same rate C . So that is a that is how we view this three-dimensional picture into a convert this three-dimensional into a two-dimensional contour contour plot and we are going to see this for variety two different cases; when reaction is endothermic and when reaction is exothermic.

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$$\sum \nu_j A_j = 0$$

$$r = r_f(\alpha, T) - r_b(\alpha, T) = C$$

$$\frac{\partial r}{\partial T} = \frac{1}{RT^2} [E_f r_f - E_b r_b]$$

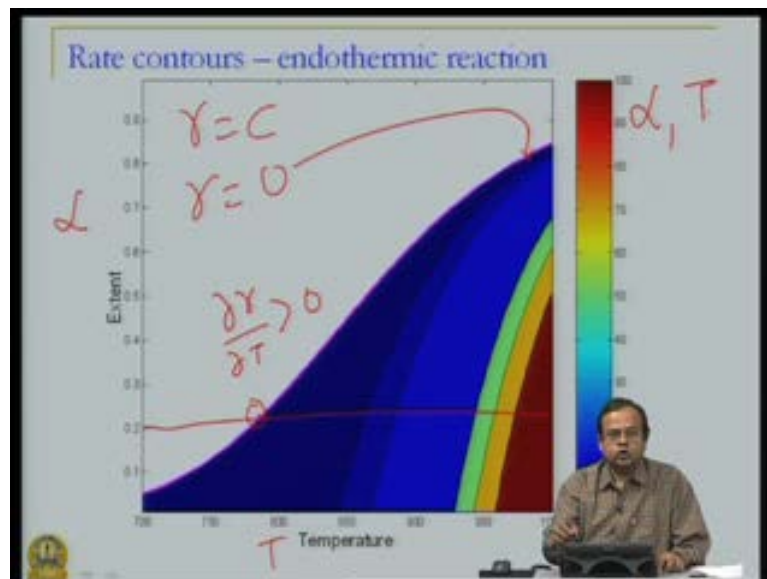
$$E_f - E_b = \Delta H \quad \Delta H > 0$$

Now the background for this is as follows; so we have what we are saying is you are going to see this contours for constant rate and in order to see how these contours vary let us also do one small exercise and take partial of rate with respect to temperature and if you do this differentiation by plugging in power law kinetics into this two rate **into this two rate** forms; we will end-up with this particular form. I leave this to you I leave this as a small exercise for you to do but we get this particular form. What is E and E prime? E is a our we have a kinetic rate constant k_f and which is $A_f e^{-E_f/RT}$ or let us

put or E by $R T r$ to make matters clear let us put f and b over here. So E_f and E_b are the activation energies for forward and reverse reactions respectively.

Now it tells out that going back to our thermodynamics; we can also show that E_f minus E_b must be the heat of reaction ΔH or enthalpies P change. Now this is additional constant pose by thermodynamics where is you have heat of reaction you have activation energy forward and reverse reaction or backward reaction rate reactions and their difference must be ΔH . So now let us go and have a look at how this contours look like first starting with when ΔH is greater than zero or in other words we are looking at endothermic reaction we are looking at endothermic reaction.

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First, let us look at how these rate contours look like and then we will come back to see, what these why these rate contours look something like this; what we see here on the y axis is the extent of reaction α and temperature. We jumped up one and went to exothermic reaction and but let us first complete with endothermic reaction and then go to exothermic reaction. So first let us try to see what does these contours are showing us. So what these different color things that you are seeing is actually the contours for constant rate; recall that we are looking at r equal to constant and what are those values of constant is shown in this color slide, which is on the right hand side.

So brown for example, denotes very high rate of reactions and as I keep saying time and again the numbers do not matter at this moment but qualitative information is what we

are interested. So the rate that is this constant C is decreasing as we are moving down this color slide from brown to dark blue. Now let us try to see what this contours are? The first contour that we can construct is the simplest one, which says that r is zero. What is r is zero? r is zero when the reaction has reached equilibrium and that contour is shown in this violet color line; that is the top-most line over here and which is a contour for r equal to zero that is our equilibrium line.

Now what does it say for endothermic reaction; we have already seen this in our earlier class that as temperature increases the equilibrium extent of reaction increases and this is that particular plot. Now for any other value of C we see that as extent of reaction increases or at a constant rather at a constant extent of reaction. As we increase the temperature the reaction rate is increasing that is if you let us say we just draw horizontal line at α equal to 0.2 then as our temperature is increasing this is a point where reaction rate is zero. So that is an equilibrium condition.

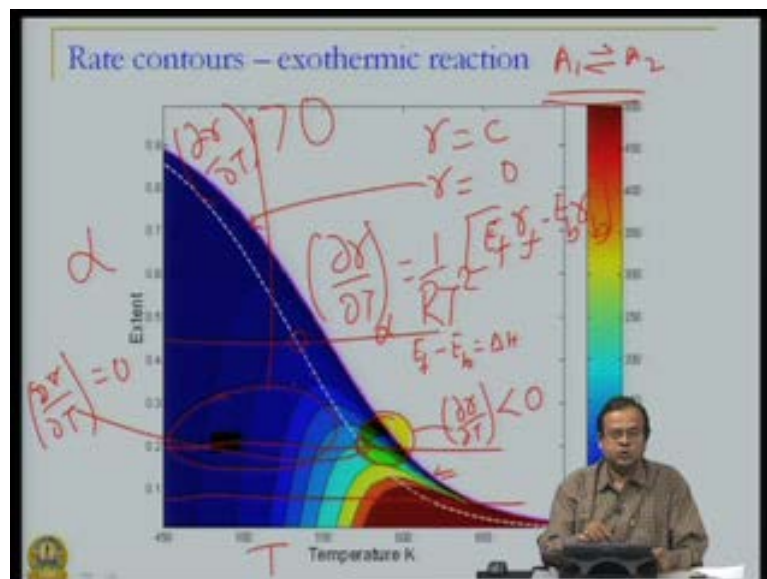
But as our temperature is increasing along this line we see that we are travelling from the color region which is the dark blue to brown through various different transitions; that means the reaction rate is increasing. Now why is this reaction rate increasing that is recall that we what we are seeing here is at a constant value of α ; as we are increasing the temperature the reaction rate goes on increasing now to see why this is happening. Let us go back to our previous exercise that we did and we said that for exothermic for endothermic reaction E_f minus E_b which must be the heat of reaction is positive that means why E_f is greater than E_b .

So now let us consider a scenario where we started the reaction with α equal to zero or with a low value of α . Now initially you expect that R_f forward reaction rate will be higher than reverse reaction rate and E_f is also higher than E_b because reaction is endothermic. What it means is it are ΔT this is understood that this is at a constant value of α is always positive. Because $\Delta r / \Delta T$ is a difference of two terms, the first term is always higher than the second term; why because E_f is higher than E_b prime and r_f is higher than r_b and as a result we have this particular result that $\Delta r / \Delta T$ is always greater than zero.

In other words for a given value of for a given value of α for endothermic reaction $\Delta r / \Delta T$ is greater than zero and what does that mean in terms of this contours for a

given value of alpha as we are increasing temperature as ΔT is positive Δr is also positive that is why the reaction rate will continuously increase and this is what happens when you have endothermic reaction. That is recall all along we are saying that alpha and T for sake of this illustration; we are changing them independent of each other. However that is not always the case because in a vector there will be certain relationship between how extent of reaction changes as or its variation is linked to the variation of temperature. So we have to worry about that link but will come to that in a minute.

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Let us go to the exothermic reaction and for exothermic reaction we see a different scenario what different scenario are we referring to if you look at this contours for example, this contour is always monotonic all these contours are monotonic. Now let us go to the exothermic reaction once again we see that we are saying r equal to constant contours starting with r equal to zero, which is this violet line and recall for exothermic reaction the equilibrium extent reaction decreases as temperature increases and naturally this is that contour. Once again our colour scheme is same we have dark brown, which represents high reaction rates to dark blue which represent lower reaction rate.

Let us go back and write this particular relationship which we saw earlier. Now let us see what **what** happens when you have exothermic reaction. So let me **let me** once again take the same approach of horizontal travel on given value of alpha. Now what do we see here. Notice the color change and that will tell you what **what** is happening to the rate of

reaction. What is **what is** happening here? Low reaction rates are increasing as we are travelling the as we are traveling along this the color is changing from dark blue to light blue; that means the reaction rates are increasing increasing increasing, then beyond certain point the reaction rate.

Now notice the change in color from light green to the dark light light blue to the dark blue. That is the reaction rates are once again decreasing once again decreasing in this range. So what happened there in this range as we increase the temperatures the reaction rates increased but it started decreasing once again that is why there must be a point where the reaction rate is maximum. Now let me illustrate it at yet another level let say that we are looking at this particular value of alpha. And here you can now I once again clearly see that as the temperature is increasing the reaction rates are increasing increasing increasing. But then after some point the reaction rates are decreasing and eventually the reaction rates are going to zero.

Now why is this happening for exothermic reaction? Mathematically we can see in this particular relationship. Now according to our discussion earlier $E_f - E_b$ is ΔH the heat of reaction and this is negative that is why E_f is less than E_b . So in this particular relationship E_f is less than E_b but initially r_f is higher than r_p and so $\frac{dr}{dT}$ is positive as a result of this combination. So in this particular region $\frac{dr}{dT}$ is positive. But what will happen remember our reaction is a reversible reaction of this kind. So initially the rate of A_1 going to A_2 is high but as time progresses as that is as reaction progress A_1 is going to go down and therefore, the rate of forward reaction will go down and the rate of backward reaction will come up.

Now E_f is less than E_b irrespective of where we are but r_f which was initially higher than r_b is now decreasing as the reaction is **reaction is** progressing. As a result there is a **there is a** region where $r_f - E_f$ will be much less than $r_b - E_b$ or in other words $\frac{dr}{dT}$ will be negative. Now the transition from $\frac{dr}{dT}$ positive to $\frac{dr}{dT}$ negative cannot happen abruptly. So there is a point such as this point this particular point where $\frac{dr}{dT}$ is zero. And what we see this white line over here is a tracing of all such points by repeating the same exercise that is you take this particular temperature rate increases increases increases which is maximum starts decreasing. So $\frac{dr}{dT}$ equal to zero.

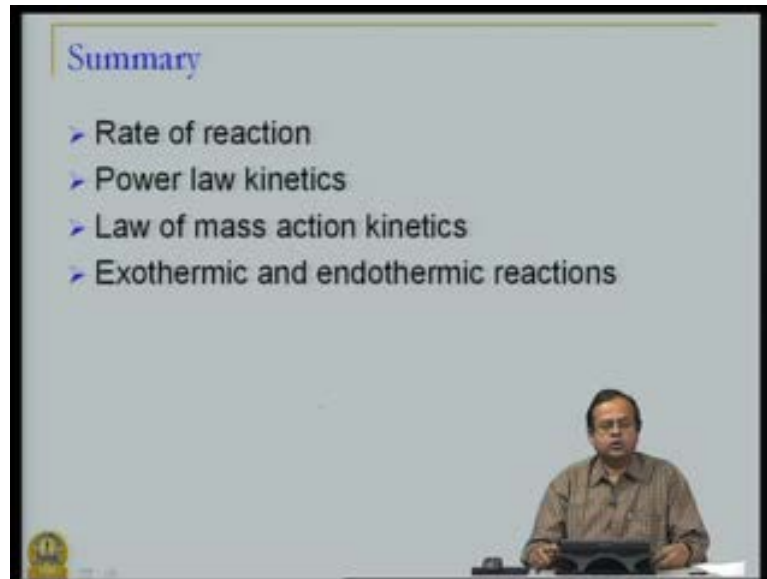
So this is why now if we look at these contours what we see these contours are no longer monotonic; as they were before that is r equal to C is obtained by non-monotonic the contour is non-monotonic now it increases then decreases. Similarly, at all different different contours, so what we have here is very interesting behavior; that the rate increases initially reaches a maximum value. But then it starts decreasing. Now qualitatively why is this happening once again mathematically; we saw why it is happening qualitatively it is **it is** for the following following reason. So if you look at this reaction A_1 going to A_2 reversible reaction.

Initially there is a lot of A_1 so the forward reaction is happening at a faster rate compared to backward reaction rate and as we increase the temperature the rate constants are increasing so for a while the forward rate reaction increases significantly in comparison to reverse and we have an increase in rate of reaction. However there comes a point remember this is an exothermic reaction which determines that as temperature is increased the rate of the equilibrium extent of reaction decreases; as a result after certain increase in temperature the thermodynamic constraints come into picture.

Because now the equilibrium extent of reaction is limited when temperatures are high and therefore, the rate starts decreasing and eventually reaching the zero value; that is this equilibrium line. So this is the conflict between kinetics and thermodynamics which is represented in this contour plot, kinetics wise temperature increases tend to increase the rate of reaction. But thermodynamic point of view for an exothermic reaction increase in temperature tends to decrease the equilibrium constant. Therefore, decrease the equilibrium extent of reaction therefore decrease the rate of reaction and the net result is for a while temperature as a positive influence.

But beyond certain threshold temperature starts actually limiting the reaction and this is true for exothermic reaction whereas, for endothermic reactions there is no such conflict. Both kinetics and thermodynamics are favorably affected by increase in temperature and hence we see these monotonic contours or contours which are always increasing in volume. So with this I want you to keep this information in back of your mind. Because when it comes to design of reactors; we will once again visit this to see how our reactor design for exothermic reactions is influenced by this kind of behavior.

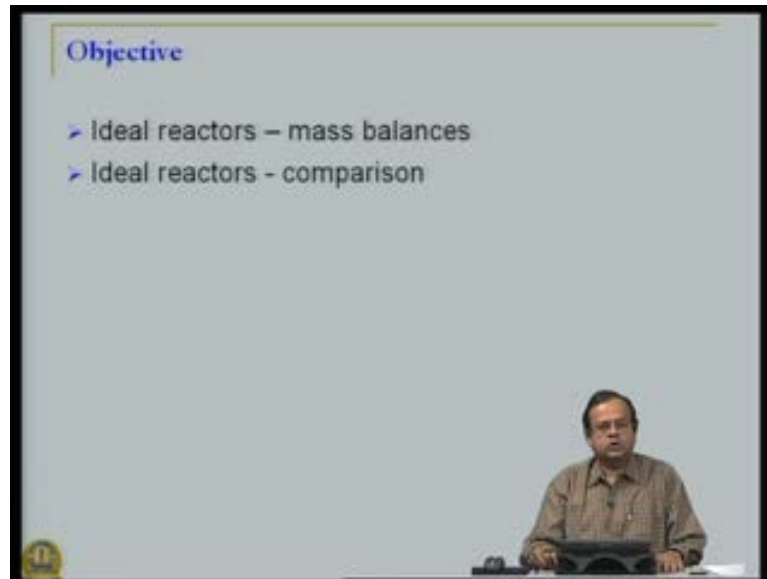
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So to summarize we saw how we define the rate of reaction. For a closed isothermal constant pressure system, we define the rate of reaction as the rate of change of extent of reaction normalized by the volume of the reacting mixture if it is a homogenous reaction. If it is a heterogeneous reaction, we have several choices such as for catalytic reactions we do it by normalizing with respect to the weight of the catalyst. Then we have power law kinetics $r = k_f \prod C_j^{q_j} - k_b \prod C_j^{q_j'}$ forward reaction backward reaction order of reaction overall order of reaction. The rate constant k the simplest manner in which its dependence on temperature is expressed is an erroneous rate expression $k = A e^{-E/RT}$ where E is the activation energy.

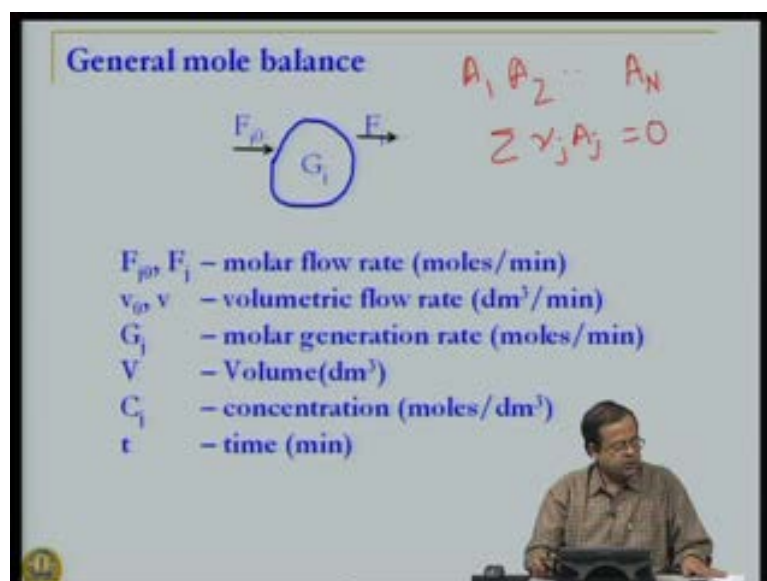
Law of mass action kinetics is a specific case of power law kinetics where the orders q_j are related to stoichiometry through an appropriate relationship and finally, we saw how the rate of reaction changes as α and temperature changes that is the extent of reaction and temperature varies. Once again I emphasize that what we saw these variations were for if we assume α and temperature can vary independently. We now bring in the mole balances or design equations for reactors, which will lead us to how α and temperature varies and this will be the topic of discussion for the remaining of this session; that is design equations for reactors and we will naturally start to begin with ideal reactors and then look at some of the deviations from this behavior at some time in the future.

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So let us now focus on how the rate of how do we design the reactors for by considering the mole balances. So we are still reviewing undergraduate material and I should caution you when I say review some of this material, you may not have seen in this particular form but surely you have seen it in some form or the other. So design equations for reactors. We are going to consider ideal reactors and consider the mass balances and we will follow of this discussion by comparing different kinds of ideal reactors to see how we choose a reactor for certain processes.

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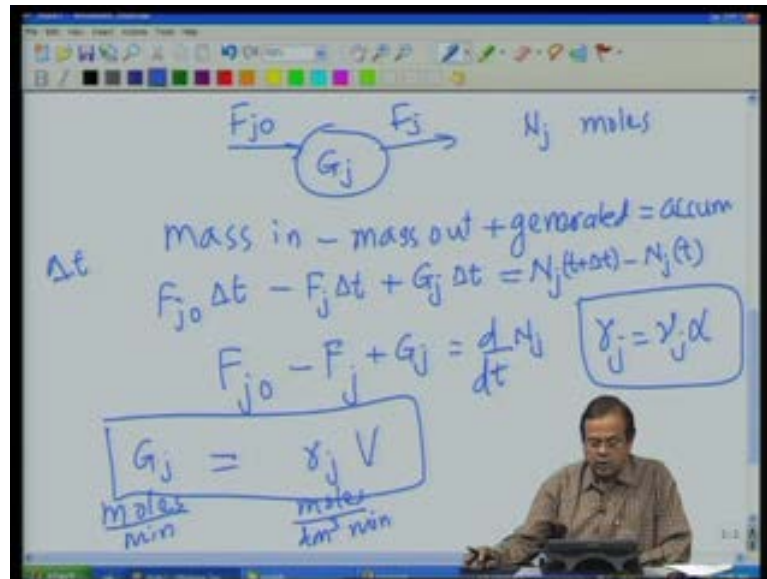
So what we are going to do to begin with is write a simple mole balance for the reacting species and once again we are going to say that we have N species A_1, A_2, \dots, A_N such pieces A_N in which these reaction $\nu_j A_j$ equal to zero is taking place. But these reactions now taking place not in a close system but in an open system. So we have this reactor, we do not know what this reactor is but there is some reactor in which this reaction is taking place and as I said this is open system; so there is a flow coming to the system and flow leaving the system. So there is an entry point and there is an exit point for material to flow in and out of the reactor.

Now before we go to our mass balances few comments about the notation that we are going to follow so that we are all clear about what are the different terms we are talking about. To begin with capital F is the molar flow rate moles per minute and we put subscript j to denote that we are writing molar flow rate of species j and additional subscript 0 for denoting the entry point of the reactor. So F_{j0} for example, is the molar flow rate of species j that is coming into the reactor F_{j1} which is going out of the reactor.

Then small v is the volumetric flow rate what we talked about is the molar flow rate moles per minute now we are talking about volumes per minute. So let say d^3 per minute and again v_0 that is incoming v_1 that is outgoing that means at the entry point v_0 , exit point v_1 . We have something happening in the reactor what is that of course, the reaction so there is a rate at which this species j is undergoing a change and let us write its rate as G_j and G denote that will call rate of generation molar generation generation rate and again it is in moles per moles per minute.

V capital V is the volume of this reactor capital V is the volume of these reactors in which these reaction is taking place. Again when I say volume it is a volume of the reacting mixture, which could be seventy percent eighty percent of the reactor volume but that is how we understand the concept of volume. C_j is the concentrations moles per volume unit so it is nothing but the ratios of corresponding capital F and small f and t is the time let us say.

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Let us do a general mole balance and see how we get this particular mole balance. So let us do this balance for a small volume so that we follow the steps that are inward. So let me emphasize again this is my reactor the rate of generation is G_j whatever is coming is F_{j0} whatever is going out is F_j and we are clear as of whatever different terms that we are going to use one more term that we are going to use is N_j which is the moles so this is in moles mass. Now we do a simple regular mass balance mass in minus mass out plus generated must be what is accumulated in the reactor; that is our standard typical mass balance for any process chemical reactions is no exception, in out minus out plus generated equal to whatever is accumulated.

Let us say that we do this mass balance over a small time step Δt . So in time Δt how was the mass that has come inside the system if F_{j0} is the molar flow rate moles per minute then $F_{j0} \Delta t$ must be the mass of j that is coming in the reactor. What is the mass that is going out of the reactor? It is F_j so during same time interval Δt $F_j \Delta t$ must be the mass that has left the reactor or the system. How much was generated? $G_j \Delta t$. G_j is the rate of generation in the reactor so in time Δt $G_j \Delta t$ must be the moles. Note that all these individual units are in moles moles of species j and how much would have accumulated inside the reactor.

Accumulation inside the reactor is N_j at time $t + \Delta t$ minus N_j at time t . Here all we are saying is this were the moles at time $t + \Delta t$ and if this were the moles at time t

then in time interval Δt this difference is how much has accumulated in the reactor. Now if we divide the whole the both sides by Δt and take limits as Δt goes to zero we get our mass balance equation $F_j - F_{j0} - F_j + G_j = \frac{dN_j}{dt}$ of engine. Since we are dividing this mass balance by Δt , what we have is the now expression in terms of rate each of this unit has each of these term has a dimension of rate now.

The left hand side or let start with right hand side, right hand side is the rate of accumulation of species j $\frac{dN_j}{dt}$ which is the result of what is coming in $F_{j0} - F_j$ what is going out and G_j the generation rate into that must be the the net rate of accumulation. Now we know what inlet outlet is and so on. Let us spend some few minutes on what is this generation rate? Now generation rate we said that it is in moles per moles per minute. If we for example, assume that the working conditions are such that there is no variation inside the reactor variation of temperature or concentration or any quantity that influences the rate of reaction that is temperature is uniform all throughout, concentrations are uniform all throughout and you would have by now guessed; we are now talking of perfectly mixed reactor reactor in which there is very good stirring.

So that there is no variation within the reactors to put at formally there is no special variation of concentrations temperature or any other quantity that influences the rate of reaction if that is the case then our earlier definition of rate of reaction r_j , what were its units were moles per d m cube per minute let us say. The rate of generation of species j recalls that r_j is ν_j into r , where r is the rate of reaction. I keep repeating this thing because I believe certain degree of repetition does not harm anybody. So we have r_j as the rate at which the species j is undergoing reaction and its same throughout the entire volume if that is the case then r_j multiplied by the volume of the reactor must be the rate of generation; the total rate of generation of species j that is G_j . So if there are no special variations then we have this particular G_j which is r_j into V so that that is the balance.

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$$F_{j0} \quad F_j \quad N_j \text{ moles}$$

$$\text{mass in} - \text{mass out} + \text{generated} = \text{accum}$$

$$F_{j0} \Delta t - F_j \Delta t + G_j \Delta t = N_j(t+\Delta t) - N_j(t)$$

$$F_{j0} - F_j + G_j = \frac{dN_j}{dt} \quad \boxed{\nu_j = \nu_j \alpha}$$

$$G_j = \sum_k \nu_k r_k \Delta v_k \quad G_j = \int \nu_j r_k dv$$

$$\Delta v_k \rightarrow 0$$

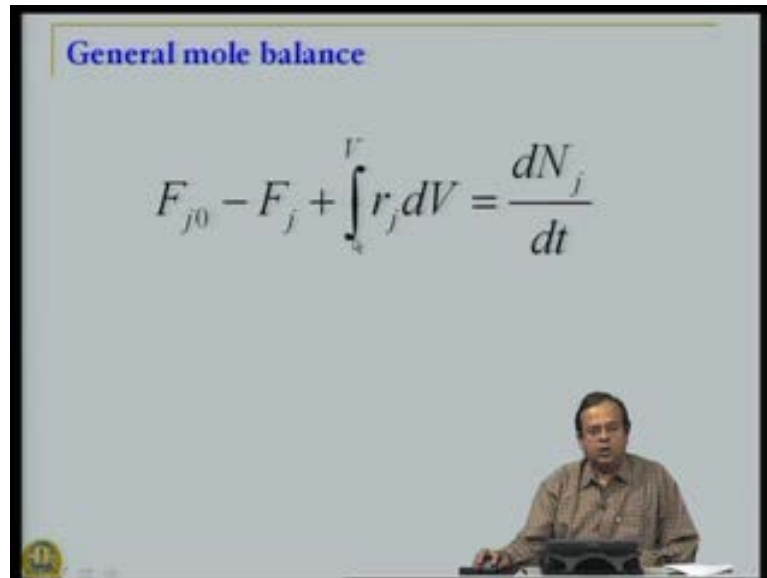
So, now let us go back to our mole balance and let us go back to this particular expression before we actually move to looking at the set of equation. Now this is what we said is the case when there is no special variation but let us say that there is a special variation that is things are not uniform in these reactor. So what we can do is consider small volume elements $\Delta v_1, \Delta v_2, \Delta v_3$. So these are all small volume elements Δv , and in this volume element let us say $\nu_k r_k$ is the rate of reaction **r_k is the rate of reaction**. So in this volume element Δv_k **sorry** Δv_k rather r_k into Δv_k must be the rate of generation in this volume.

But there are so many other elements, so we can we can add-up all the contributions from all these small small volume elements. So let say that summation $r_k \Delta v_k$ over the entire set of volume elements small volume elements this must be now my generation rate G_j . So what we are saying is that we are now looking at this system consisting of small volumes Δv in which things are uniform, this is just for argument say and contribution to the net rate of generation of species j is coming from each of the small volumes and each of the small volume has a contribution r_k into Δv_k , where r_k is the rate in that particular element and Δv_k **sorry** r_j .

Let me write this once again r_j is the rate in that particular volume element times Δv_k . So we can write this as $r_j \Delta v_k$ that is the rate of generation of species j in the element k and volume of that element and summed over all this k . Now once again we can make

these volume elements smaller and smaller and smaller such that Δv tends to zero, then summation of series is converted into integral and what we have is G_j is integral $r_j dV$ that is summed over or integral over the entire volume v is my net rate of generation.

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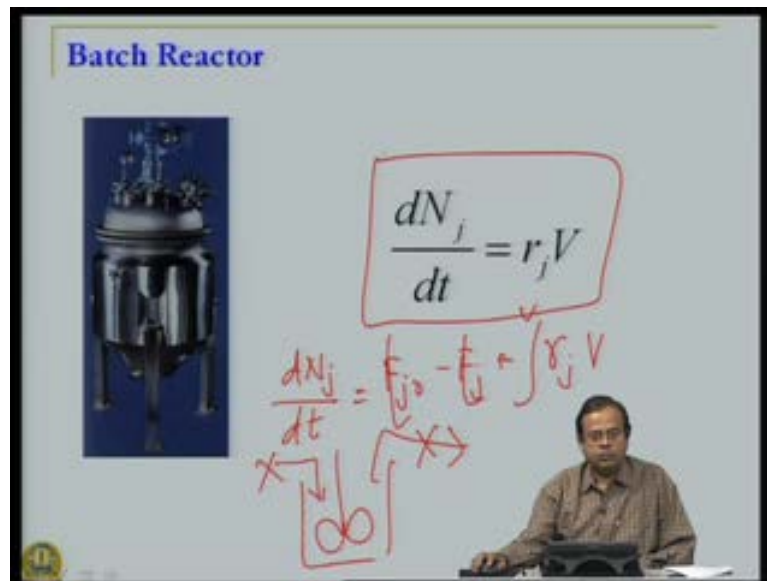


General mole balance

$$F_{j0} - F_j + \int_V r_j dV = \frac{dN_j}{dt}$$

So now let us go back and this is what is that mole balance that we get, that is F_{j0} minus F_j plus integral $r_j dV$ is dN_j/dt . Once again molar flow rates molar flow rates the intrinsic rate of reaction or intrinsic rate of species variation r_j per unit volume times dV summed over the entire volume is the rate of accumulation. Let us now simplify this mass balances for various difference scenarios.

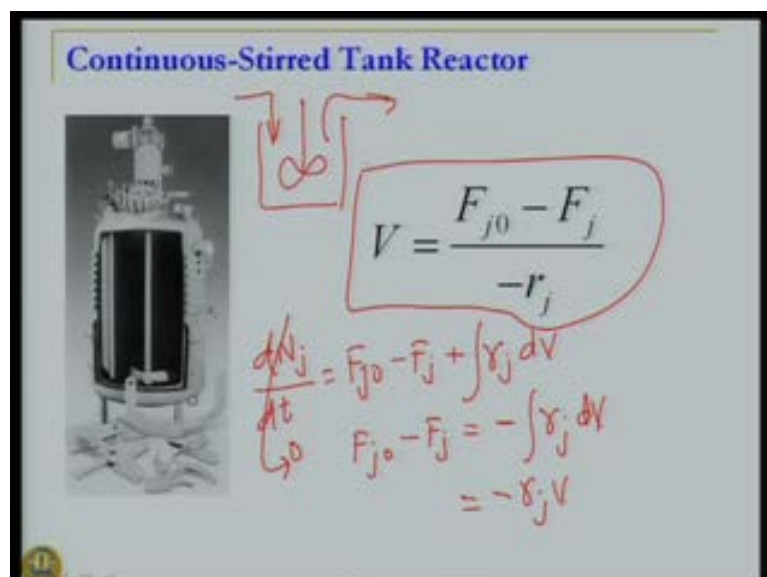
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The slide is titled "Batch Reactor" in blue text. On the left, there is a photograph of a stainless steel batch reactor. To the right of the photo, a man is visible from the chest up, sitting at a desk. The background is a light blue screen with handwritten red equations. The main equation is $\frac{dN_j}{dt} = r_j V$, enclosed in a red box. Below it, the general mass balance equation is written: $\frac{dN_j}{dt} = F_{j0} - F_j + \int \mathcal{R}_j dV$. Red arrows and a large infinity symbol (∞) are drawn around the flow terms, indicating they are zero for a batch reactor.

So going back our mass balance general mass balance equation is this. Let us consider a batch reactor. In a batch reactor we know that there is no in flow, there is no out flow that is why both these terms disappear and stirred tank reactor operated in the batch mode. So conditions are uniform throughout the entire reactor and we have $\frac{dN_j}{dt}$ as r_j into V as our mole balance straight forward exercise.

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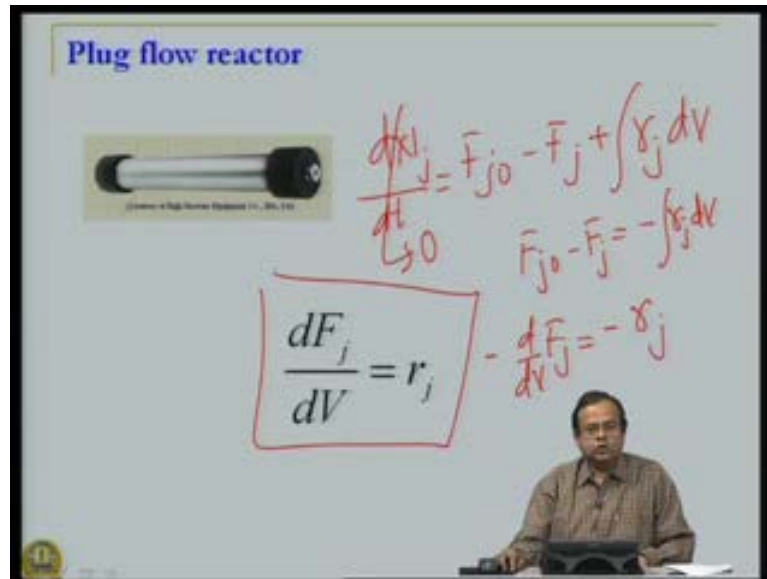


The slide is titled "Continuous-Stirred Tank Reactor" in blue text. On the left, there is a photograph of a stainless steel continuous stirred tank reactor. To the right of the photo, a man is visible from the chest up, sitting at a desk. The background is a light blue screen with handwritten red equations. The main equation is $V = \frac{F_{j0} - F_j}{-r_j}$, enclosed in a red box. Below it, the general mass balance equation is written: $\frac{dN_j}{dt} = F_{j0} - F_j + \int \mathcal{R}_j dV$. Below this, the steady-state equation is derived: $F_{j0} - F_j = -\int \mathcal{R}_j dV = -r_j V$. Red arrows and a large infinity symbol (∞) are drawn around the flow terms, indicating they are not zero for a continuous reactor.

Let us see what happens for a continuous stirred tank reactor operating at steady state that means when steady state is reached. So once again we have we are doing the steady

state balance and for a stirred tank reactors where here is a material coming in material going out, at these rates of F_j zero and F_j at steady state so this is zero. We are left with F_j minus F_j zero minus F_j as minus integral $r_j dV$ but once again we have uniform conditions in the reactor. So this is nothing but r_j into V and we have our mass balance equation for a stirred tank reactor V equal to F_j zero minus F_j by minus r_j .

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What happens for a plug flow reactor? There are various ways of looking at it, but let us go back to our generalized mass balance equation dN_j/dt as F_j 0 minus F_j plus integral $r_j dV$. Recall for a plug flow reactor the fluid moves into the reactor like a plug. So, one part comes in then we have entry of next part it pushes the part further, and there is a continuous movement. There is no mixing or communication between the fluid elements, which are in the reactors. So it is a just like a plug.

So we can simplify this mass balance equation at steady state this is 0, and we have F_j 0 minus F_j , which is minus integral $r_j dV$ and we can differentiate this with respect to V , and express this thing as d/dV of F_j d/dV of this whole quantity F_j 0 is fixed. So d/dV of F_j is nothing but rather minus r_j or dF_j/dV equal to r_j . This is our mass balance equation for a plug flow reactor. We will stop here, and then continue this discussion by looking at how do we compare the performances stirred tank reactor, and plug flow reactor in our next session. **Thank you.**