

Chemical Process Utilities
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Module No # 12
Lecture No # 60
Heat transfer in Insulation Materials

Now let us talk about the heat transfer in insulation material in this particular lecture under the areas of chemical process utilities. Now before we go into the detail of this particular content let us have a brief outlook that what we covered in the previous lecture. We discussed about the brief history of thermal insulation. We had a brief discussion about the purposes of thermal insulation. We talked about the temperature ranges for insulation application in this. We discussed about the various type of insulating materials.

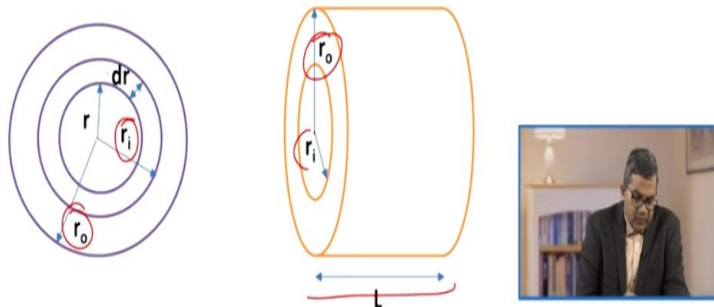
Apart from this we discussed about the heat transfer modes like conduction, convection, radiation. Now in this particular lecture, we are going to cover about the heat transfer aspect through the cylindrical insulating material. We will discuss about the heat transfer through spherical insulating materials. We will discuss about the critical thickness of insulation especially for cylinder and for spheres. So, let us talk about the heat transfer in cylindrical insulating material.

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Heat transfer in cylindrical insulating materials

Cylinders

- Let us consider a long cylinder of length L , inside radius r_i and outside diameter r_o as shown in the following figure.

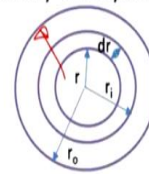


Now cylinders they are very common in the chemical engineering operation. So, let us consider a long cylinder of length L. Now inside radius is r_i and outside radius is r_o and it is you can see this is a side view and this is the front view of this one this is the r_o r_i and the total radius is r. Now this is the differential radius small amount of radius.

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- The cylinder is exposed to a temperature difference of $T_i - T_o$, the length of the cylinder is very large as compared with the diameter of the cylinder. Assume that the heat will flow only in the radial direction i.e., the space co-ordinate r needed to specify the system.
- The area of heat flow in the cylinder will be;

$$A_r = 2\pi rL$$



According to Fourier's law of heat transfer through conduction in small element dr will be given as;

$$q_r = -kA_r \frac{dT}{dr}$$



Now cylinder is exposed to the temperature difference of T_i to t_o , the length of the cylinder is very large compared with the diameter of the cylinder. So, assume that the heat will flow only in the radial direction that is the space coordinates r need to specify the system. So, the area of heat flow in the cylinder will be $A_r = 2\pi rL$. Now according to the Fourier's law of heat transfer through conduction in small element this dr will be given as $q_r = -k A_r dT$ over dr.

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The area of heat flow in the cylinder will be;

$$A_r = 2\pi rL$$

According to Fourier's law of heat transfer through conduction in small element dr will be given as;

$$q_r = -kA_r \frac{dT}{dr}$$

○ or, it can be written as;

$$q_r = -k2\pi rL \frac{dT}{dr}$$

The special boundary conditions will be

$T=T_i$ at $r=r_i$ and

$T=T_o$ at $r=r_o$

On rearranging the above equation and integrate it from T_i to T_o and r_i to r_o we have;

$$\frac{q_r}{-k2\pi L} \int_{T_i}^{T_o} dT = \int_{r_i}^{r_o} \frac{r}{dr}$$



Or, it can be written as $q_r = -k2\pi rL$ because already we have given this area so $q_r = -k2\pi rL \frac{dT}{dr}$ over dr . Now the spatial boundary conditions will be $T = T_i$ and $r = r_i$ and $T = T_o$ at $r = r_o$. So, if we rearrange this particular equation and integrate it from T_i to T_o , we can write this equation with respect to the q_r over $-k2\pi L$ integration dT from T_i to T_o . Or, it can be represented as this is equal to integration r over dr from r_i to r_o .

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or, it can be written as;

$$q_r = -k2\pi rL \frac{dT}{dr}$$

The special boundary conditions will be

$T=T_i$ at $r=r_i$ and

$T=T_o$ at $r=r_o$

On rearranging the above equation and integrate it from T_i to T_o and r_i to r_o we have;

$$\frac{q_r}{-k2\pi L} \int_{T_i}^{T_o} dT = \int_{r_i}^{r_o} \frac{r}{dr}$$

- After integration, the heat transfer rate in the cylindrical materials can be found by the following equation;

$$q = \frac{k2\pi L(T_i - T_o)}{\ln \frac{r_o}{r_i}}$$

The thermal resistance in this case can be found as;

$$R_{th} = \frac{\ln \frac{r_o}{r_i}}{k2\pi L}$$



Now after integration, the heat transfer rate in the cylindrical material this can be found by this particular equation. That is $q = k2\pi L (T_i - T_o) / \ln r_o / r_i$. Now the thermal resistance in this particular case can be written as $R_{th} = \ln r_o / r_i / k2\pi L$.

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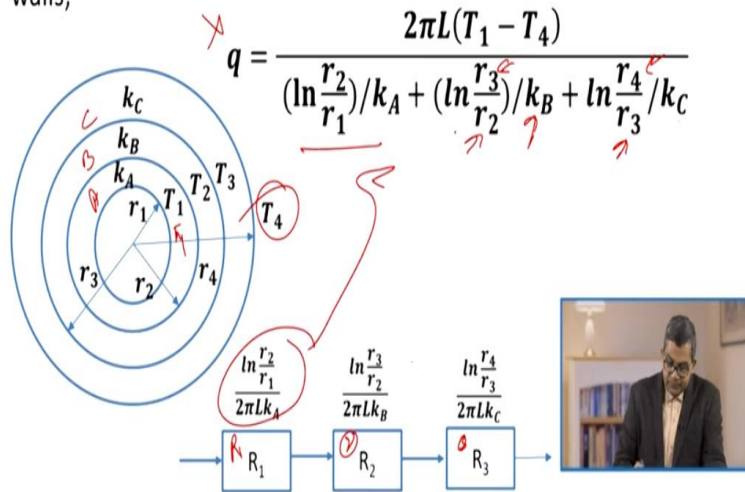
After integration, the heat transfer rate in the cylindrical materials can be found by the following equation;

$$q = \frac{k2\pi L(T_i - T_o)}{\ln \frac{r_o}{r_i}}$$

The thermal resistance in this case can be found as;

$$R_{th} = \frac{\ln \frac{r_o}{r_i}}{k2\pi L}$$

This thermal resistance concept can be used for multilayer cylindrical walls;



Now this thermal resistance concept can be used for multilayer cylindrical walls. Now here you see that, this is the typical figure of a multilayer cylindrical wall, here we are having different layers. Now here if you see that r_1, r_2, r_3, r_4 . So, there are 4 different radius apart from these different materials like A, B, and C. So, the generic equation can be written as $q = 2\pi L (T_1 - T_4)$. This is the T_1 the inner temperature and this one is the T_4 .

This over $\ln r_2$ over r_1 over $k_A + \ln r_3$ over r_2 over $k_B + \ln r_4$ over r_3 over k_C . Now these are in the series if you recall that in previous lecture, we have already studied about this one. So, the resistance to the first layer, second layer and third layer and this can be like this.

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This thermal resistance concept can be used for multilayer cylindrical walls;

$$q = \frac{2\pi L(T_1 - T_4)}{(\ln \frac{r_2}{r_1})/k_A + (\ln \frac{r_3}{r_2})/k_B + \ln \frac{r_4}{r_3}/k_C}$$

Problems


Question 1: A thick wall tube made up of stainless steel with inner diameter of 4cm and outer diameter of 8 cm. The thermal conductivity of the stainless steel is 19 W/m.K. It is covered with a insulation of thickness 4cm ($k= 0.17$ W/m.K). The temperature at outside of the insulation was 200°C. The inside wall of the pipe is maintained at 550°C temperature. Calculate the heat loss per unit length of the pipe and tube insulation interface temperature?

Now let us discuss first problem now here a thick wall tube made up of stainless steel with inner diameter of 4 centimeter and outer diameter of 8 centimeter. The thermal conductivity of the stainless steel is 19 watt per meter Kelvin. It is covered within insulation of a thickness 4 centimeter and that is $k = 0.17$ watt per meter Kelvin. The temperature at outside of the insulation is around the 200 degree Celsius.

The inside wall of the pipe is maintained at 550-degree Celsius temperature. Now here you need to calculate the heat loss per unit length of the pipe and tube insulation interface temperature.

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Given inner radius of the tube
 $r_i = 2 \text{ cm} = 0.02 \text{ m}$
 outer radius of the thick wall tube (r_o) = 4cm = 0.04m
 The pipe is covered with 4cm thick insulation
 $r_2 = r_o + t = 4 \text{ cm} + 4 \text{ cm} = 8 \text{ cm} = 0.08 \text{ m}$
 The only 1-D radial heat transfer in the pipe
 The heat loss per unit length of the pipe



$$\frac{q}{L} = \frac{T_i - T_o}{\frac{1}{2\pi} \left[\frac{\ln(r_o/r_i)}{k_s} + \frac{\ln(r_2/r_o)}{k_i} \right]}$$

$T_i = 550^\circ\text{C} = (550 + 273) = 823 \text{ K}$
 $T_o = 200^\circ\text{C} = (200 + 273) = 473 \text{ K}$
 $k_s = 19 \text{ W/m.K}$
 $k_i = 0.17 \text{ W/m.K}$

$$\frac{q}{L} = \frac{823 - 473}{\frac{1}{2\pi} \left[\frac{\ln(0.04/0.02)}{19} + \frac{\ln(0.08/0.04)}{0.17} \right]}$$

Now it is given that inner radius of the tube $r_i = 2$ centimeter and that is equal to 0.02 meter the outer radius of the thick wall tube $r_o = 4$ centimeter 0.04 meter. Now let us draw the figure

this is r_1 and this one is r_i . Now the pipe is covered with 4 centimeter thick insulation. So, $r_3 = r_1 + t$ and that is equal to 4 centimeter + 4 centimeter and $r_3 = 8$ centimeter which is 0.08 meter.

Now there is only one directional radial heat transfer in the pipe. The heat loss per unit length of the pipe is q over $L = T_i - T_o$ upon 1 upon $2 \pi \ln r_1$ over r_i upon $+$ $\ln r_3$ over r_1 upon $+$ $k_i L$. Now in this particular equation $T_i = 550$ degree Celsius this is equal to $550 + 273$ it is 823 Kelvin. T_o is 200 degree Celsius which is $200 + 273$ that is 473 Kelvin $k_s = 19$ watt per meter Kelvin and $k_i = 0.17$ watt per meter Kelvin. So, q upon $l = 823 - 473$ upon 1 upon $2 \pi L \ln$ 0.04 0.02 upon $19 + L \ln$ 0.08 over 0.04 upon 0.17 .

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Given;

The inner radius of the tube

$$r_i = 2 \text{ cm} = 0.02 \text{ m}$$

outer radius of the thick wall tube (r_o) = 0.04 m

the pipe is covered with 4 cm thick insulation materials

$$\text{then } r_3 = r_o + t = 4 + 4 = 8 \text{ cm}$$

there is only 1-D radial heat transfer in the pipe

the heat loss per unit length of the pipe is given as;

$$q = \frac{2\pi L(T_i - T_o)}{(\ln \frac{r_o}{r_i})/k_s + (\ln \frac{r_3}{r_o})/k_i}$$

$$T_i = 550 \text{ } ^\circ\text{C} = (550 + 273) = 823 \text{ K}$$

$$k_s = 19 \text{ W/mK}$$

$$T_o = 200 \text{ } ^\circ\text{C} = (200 + 273) = 473 \text{ K}$$

$$k_i = 0.17 \text{ W/mK}$$

On putting all these values in the above equation we have;

$$\frac{q}{L} = \frac{2\pi(823 - 473)}{(\ln \frac{0.04}{0.02})/19 + (\ln \frac{0.08}{0.04})/0.17}$$

$$\frac{q}{L} = 54.163 \text{ W/m}$$

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Now the interface temp between outside tube wall and the insulator can be found as

The heat per unit length for overall system should be same heat transfer per unit length of this interface


$$\frac{q}{L} = \frac{T - T_o}{\ln(r_3/r_o)} = 54.163$$

$$\Rightarrow \frac{T - 473}{\ln(0.08/0.04)} = 54.163$$

$$\frac{T - 473}{2.07 + 0.17} = 54.163$$

$T = 508.148 \text{ K}$

Ans



And q upon L is equal to which comes out to be 54.163 watt per meter that is the answer. Now the interface temperature between outside tube wall and the insulation can be found as the heat per unit length for overall system should be same as heat transfer per unit length of this interface. So again, coming back to the figure, this is $T - T_o$ this is r now q over $L = T - T_o$ upon $\ln r_3$ over r_o upon $2 \pi k_i$ and that is 54.163 .

Which is we have already obtained and that is $T - 473$ upon $\ln 0.08 / 0.04$ upon 2π into 0.17 and that is 54.163 . So, while calculating then we got this $T = 508.148$ Kelvin and that is our answer.

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Now the interface temperature between outside tube wall and the insulation can be found. As the heat per unit length for overall system should be same heat transfer per unit length of the interface.

$$\frac{q}{L} = \frac{2\pi(T - T_o)}{(\ln \frac{r_3}{r_o})/k_i}$$

On putting the value of the know parameter we have;

$$54.163 \text{ W/m} = \frac{2\pi(T - 473)}{(\ln \frac{0.08}{0.04})/0.17}$$

On solving this equation, we have
 $T = 508.148 \text{ K}$

Problems

Question 2: What will be the thickness of insulation, if the temperature of inner side is 300°C and temperature at outer side is 38°C. The thermal conductivity of the insulation is $k=0.057 \text{ W/m.K}$ and inner radius is given as $r_1=0.035 \text{ m}$. if the heat transfer per unit length of the cylinder (q/L) is 60 W/m?

Now let us talk about the second question. Now here what will be the thickness of insulation, if the temperature of inner side is 300 degree Celsius and temperature at outer side is 38 degree Celsius? The thermal conductivity of the insulation is k this is which is $K = 0.57 \text{ watt per meter Kelvin}$ and the inner radius is given as $r_1 = 0.035 \text{ meter}$. Now if heat transfer per unit length of the cylinder that that is q/L is 60 watt per meter.

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$r_1 = 0.035 \text{ m}$ $T_1 = 300^\circ\text{C} = 300 + 273 = 573 \text{ K}$
 $r_2 = ?$ $T_2 = 38^\circ\text{C} = 38 + 273 = 311 \text{ K}$

The heat transfer per unit length of the cylinder $(\frac{q}{L}) = 60 \text{ W/m}$


We know Heat transfer per unit length for cylinder

The thermal conductivity of the insulator $k = 0.057 \text{ W/m.K}$

$$60 = \frac{573 - 311}{\frac{1}{2\pi} \left[\frac{\ln(r_2/0.035)}{0.057} \right]}$$

$$\frac{r_2}{0.035} = e^{1.5634}$$

$r_2 = 0.161713$



Now let us solve this particular problem now here it is given that $r_1 = 0.035 \text{ meter}$. We do not have any clue about r_2 $T_1 = 300 \text{ degree Celsius}$ and that is equal to $300 + 273$ and that comes out to be 573 Kelvin. So let us draw the figure first that is r_1 , r_2 , T_1 and T_2 . So, T_2 is equal to it is given that

38 degree Celsius so $38 + 273$ it comes out to be 311 Kelvin. Now the heat transfer per unit length of the cylinder that is q over $L = 60$ watt per meter.

So, we know the heat transfer per unit length for cylinder so q upon $L = \frac{T_1 - T_2}{\ln \frac{r_2}{r_1}} \frac{2\pi}{k}$ that is equation number 1. The thermal conductivity of the insulation that is k is equal to which is given at $k = 0.057$ watt per Kelvin. Now if you substitute these values in this particular equation, we will have $60 = \frac{573 - 311}{\ln \frac{r_2}{0.035}} \frac{2\pi}{0.057}$ and this is $\ln \frac{r_2}{0.035} = \frac{262}{60} \frac{2\pi}{2.793}$ and $r_2 = 0.035$ that is equal to e to the power 1.5634 and 2 comes out to be 0.161713.

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Given;

$$r_1 = 0.035 \text{ m}$$

$$T_1 = 300^\circ\text{C} = 300 + 273 = 573\text{K}$$

Heat transfer per unit length of the cylinder

$$q/L = 60 \text{ W/m}$$

as we know heat transfer per unit length of the cylinder can be written as;

$$\frac{q}{L} = \frac{2\pi(T - T_o)}{(\ln \frac{r_2}{r_1})/k}$$

The thermal conductivity of the insulator is $k = 0.057 \text{ W/mK}$

On putting above values in the above formula we get;

$$60 = \frac{2\pi(573 - 311)}{(\ln \frac{r_2}{0.035})/0.057}$$

On solving we get;

$$r_2 = 0.161713 \text{ m}$$

$$\begin{aligned}
 &\text{The thickness of insulator will be} \\
 &= r_2 - r_1 \\
 &= 0.16713 - 0.035 \\
 &= 0.13213 \text{ m} \quad \text{Ans}
 \end{aligned}$$

The thickness of insulation will be $r_2 - r_1$ and that is $0.16713 - 0.035$ and that is 0.13213 meter and that is our desired answer.

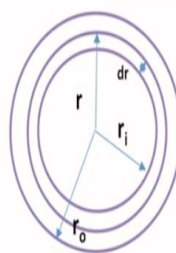
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**The thickness of the insulation will be = $r_2 - r_1$
 = $0.16173 - 0.035$
 = 0.13213 m**

Heat transfer in spherical insulating materials

Spheres

- Let us consider a sphere of inside radius r_i and outside diameter r_o and taking a small element at any radius r (dr) for calculation as shown in the following figure.



Sphere



Now let us talk about the heat transfer in spherical insulating material. So first in this category is the sphere. So let us consider a sphere this is the sphere of inside radius is given as r_i and outside diameter or radius is given as r and taking a small element of any radius and that is dr this one for calculation as per this particular figure.

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- If T_1 be the temperature at inner part of the sphere and T_2 be the temperature at outside surface and assume that T_1 is greater than T_2 .
- The rate of heat flow according to Fourier's law is given as;

$$Q = -k(4\pi r^2) \left(\frac{dT}{dr} \right)$$

If $A = 4\pi r^2$ = area of heat transfer

k = thermal conductivity of the spherical materials

On rearranging the above equation we have;

$$\frac{dr}{r^2} = -\frac{k(4\pi)}{Q} dT$$



Now if T_1 be the temperature at the inner part of this sphere and T_2 be the temperature of the outside surface and assume that T_1 is greater than T_2 that is the rate of heat flux according to the Fourier law is given as $q = -k \frac{dT}{dr}$ where A is we can write at A is equal to $4\pi r^2$ and that is the area of heat transfer k is the thermal conductivity of the spherical material. So, if we rearrange this particular equation then we will have dr over r^2 = $-k$ into 4π upon $Q dT$.

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For Sphere;

The rate of heat flow according to Fourier's law is given as;

$$Q = -k(4\pi r^2) \left(\frac{dT}{dr} \right)$$

If $A = 4\pi r^2$ = area of heat transfer

k = thermal conductivity of the spherical materials

On rearranging the above equation we have;

$$\frac{dr}{r^2} = -\frac{k(4\pi)}{Q} dT$$

Boundary conditions;

$$r=r_1, T=T_1$$

$$r=r_2, T=T_2$$

$$\int_{r_1}^{r_2} \frac{dr}{r^2} = -\frac{k(4\pi)}{Q} \int_{T_1}^{T_2} dT$$

After integration and putting these values we have

$$Q = \frac{(T_1 - T_2)}{\frac{1}{4\pi k} \left[\frac{1}{r_1} - \frac{1}{r_2} \right]}$$



So let us adopt the boundary condition $r = r_1$ and $T = T_1$ and $r = r_2$ and $T = T_2$. So, if we integrate d over r square from the limits r_1 to r_2 then it is equal to $-k$ into 4π upon q integration from T_1 to T_2 d T . Now after integration and putting the values we have $Q = T_1 - T_2$ over 1 upon $4\pi k$ into 1 upon $r_1 - 1$ upon r_2 .

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Boundary conditions;

$$r=r_1, T=T_1$$

$$r=r_2, T=T_2$$

$$\int_{r_1}^{r_2} \frac{dr}{r^2} = -\frac{k(4\pi)}{Q} \int_{T_1}^{T_2} dT$$

After integration and putting these values, we have

$$Q = \frac{(T_1 - T_2)}{\frac{1}{4\pi k} \left[\frac{1}{r_1} - \frac{1}{r_2} \right]}$$

Or it can be written as;

$$Q = \frac{4\pi r_1 r_2 k (T_1 - T_2)}{[r_2 - r_1]}$$

Where,

$r_m = \sqrt{r_1 r_2}$ is the mean radius or geometric mean for sphere.

$$\Rightarrow Q = \frac{4\pi r_m k (T_1 - T_2)}{[r_2 - r_1]}$$



Our conduction heat transfer through a sphere can be written as $Q = \frac{T_1 - T_2}{\frac{1}{4\pi k} \left[\frac{1}{r_1} - \frac{1}{r_2} \right]}$. Now it is the ratio of temperature difference to the thermal resistance to heat transfer between the radius r_1 and r_2 . Or, you can write as $Q = 4\pi r_1 r_2 k (T_1 - T_2) / (r_2 - r_1)$. Now where $r_m = \text{square root of } r_1, r_2$. This is the mean radius or geometric mean for sphere. So if we write this particular thing into this equation it can become the $Q = 4\pi r_m k (T_1 - T_2) / (r_2 - r_1)$.

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Or, conduction heat transfer through the sphere can be written as;

$$Q = \frac{(T_1 - T_2)}{\frac{1}{4\pi k} \left[\frac{1}{r_1} - \frac{1}{r_2} \right]}$$

It is the ratio of temperature difference to the thermal resistance to heat transfer between the radius r_1 and r_2 .

Or it can be written as;

$$Q = \frac{4\pi r_1 r_2 k (T_1 - T_2)}{[r_2 - r_1]}$$

Where,

$r_m = \sqrt{r_1 r_2}$ is the mean radius or geometric mean for sphere.

$$\Rightarrow Q = \frac{4\pi r_m k (T_1 - T_2)}{[r_2 - r_1]}$$

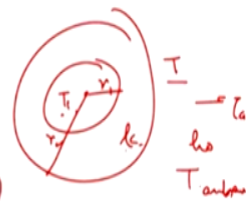
Problems

Question 3: If a spherical ball of steel of inner radius 2cm and outer radius of 4cm is filled with hot matter and the temperature of it was 275°C. The thermal conductivity of the steel is 7.68 W/m.K. If it is exposed to ambient temperature (25°C), the heat loss will be?

The convective heat transfer coefficient is 0.20 W/m².K.

Now let us discuss another problem which is related to the spherical issue. Now if a spherical ball of steel of inner radius 2 centimeter and outer radius of 4 centimeter is filled with hot matter and the temperature of it was say 275 degree Celsius. The thermal conductivity of the steel is 7.68 watt per meter Kelvin. Now if it is exposed to ambient temperature 25 degree Celsius the heat loss would be calculated and the convective heat transfer coefficient is given as 0.20 watt per meter square Kelvin.

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$$\begin{aligned}
 r_1 &= 0.02 \text{ m} & k_s &= 7.68 \text{ W/mK} \\
 r_2 &= 0.04 \text{ m} & h_o &= 0.20 \text{ W/m}^2\text{K} \\
 T_1 &= 275^\circ\text{C} & &= 275 + 273 = 548\text{K} \\
 T_{\text{ambient}} &= 25^\circ\text{C} & &\rightarrow T_a = 298\text{K}
 \end{aligned}$$


$$Q = \frac{T_1 - T_a}{\left[\frac{1}{4\pi k_s} \left(\frac{1}{r_1} - \frac{1}{r_2} \right) + \frac{1}{A_o h_o} \right]} \quad \text{--- (1)}$$

$A_o = \text{outside surface area of the sphere}$

$$\begin{aligned}
 A_o &= 4\pi r_2^2 \\
 &= 4\pi \times (0.04)^2 \\
 A_o &= 0.02011 \text{ m}^2
 \end{aligned}$$

So, let us take up this take this problem so this is your sphere where we are having the r_1 r_2 and t 1 t and this one is k and h naught and t ambient. So, this is a sphere now it is given that $r_1 = 0.02$ meter, $r_2 = 0.04$ meter, k_s is sphere = 7.68 watt per meter, Kelvin h naught = 0.20 watt per meter square Kelvin, $T_1 = 275$ degree Celsius. So, if we convert it into the Kelvin, it can it do it needs to be added with 273 and then T_1 comes out to be 548 Kelvin.

$T_{\text{ambient}} = 25$ degree Celsius, if $25 + 273$ it comes out to be $T_a = 298$ Kelvin. Now the heat transfer from inner surface at T_1 to the outer surface at T will be through the conduction and from outside from our surface at T to m b and t a will be transferred by the convection so both will take place simultaneously. So let us write the equation $T_1 - T_a$ upon 1 upon $4\pi k_s$ into 1 upon $r_1 - 1$ upon $r_2 + 1$ upon $A_o h_o$ and that is equation number 1.

Now A_o is outside surface area of the sphere which is equal to $4\pi r_2^2$ square which is equal to 4π into 0.04 square and $A_o = 0.02011$ meter square.

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Given;

$$r_1 = 0.02 \text{ m}$$

$$r_2 = 0.04 \text{ m}$$

$$k_s = 7.68 \text{ W/mK}$$

$$h_o = 0.20 \text{ W/m}^2\text{K}$$

$$T_1 = 275^\circ\text{C} = 275 + 273 = 548\text{K}$$

$$T_{\text{ambient}} = 25 + 273 = 298\text{K}$$

$$Q = \frac{(T_1 - T_a)}{\frac{1}{4\pi k_s} \left[\frac{1}{r_1} - \frac{1}{r_2} \right] + \frac{1}{A_o h_o}}$$

$$\begin{aligned}
A_o &= \text{outside surface area of the sphere} \\
&= 4\pi r^2 \\
&= 4\pi(0.04)^2 \\
&= 0.02011 \text{ m}^2
\end{aligned}$$

On putting all values in the above heat transfer equation, we will get;

$$Q = \frac{(548 - 298)}{\frac{1}{4\pi \times 7.68} \left[\frac{1}{0.02} - \frac{1}{0.04} \right] + \frac{1}{0.02011 \times 0.20}}$$

$$Q = 0.998 \text{ W}$$

$$Q = \frac{548 - 298}{\left[\frac{1}{4\pi \times 7.68} \left[\frac{1}{0.02} - \frac{1}{0.04} \right] + \frac{1}{0.02011 \times 0.20} \right]}$$

$$Q = 0.998 \text{ W}$$

Now if we substitute all given values in equation given equation then $Q = 548 - 298$ upon $\frac{1}{4\pi \times 7.68}$ into $\left[\frac{1}{0.02} - \frac{1}{0.04} \right] + \frac{1}{0.02011 \times 0.20}$ and that comes out to be $Q = 0.998$ watt and that is our desired answer.

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Optimum thickness of insulation

It can be obtained by economical approach. On increasing in the thickness of insulation there is reduces in the loss of heat, thus saving in the operating cost but at the same time the cost of insulation will be increase with increases in the thickness.

The optimum thickness of insulation is one on which the total annual cost of insulation is minimum.

Now let us talk about the optimum thickness of insulation. Now it can be obtained by economical approach on increasing in the thickness of insulation there is a reduction in the loss of heat. Thus, saving in the operating cost but at the same time the cost of insulation will be increased with increase in the thickness. The optimum thickness of insulation is one on which the total annual cost of insulation is minimum.

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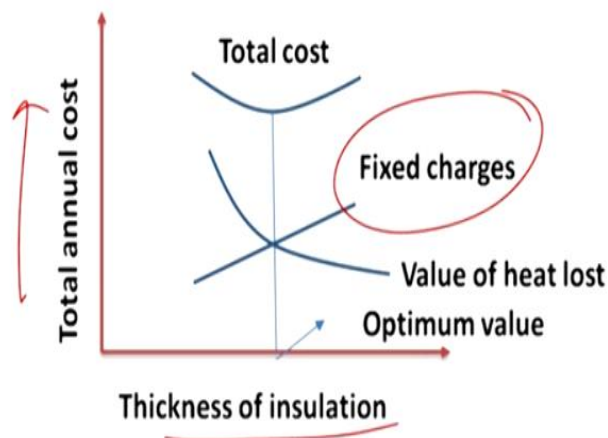


Figure showing optimum thickness of insulation

Now here you see that the optimum insulation thickness now here the total annual cost and the thickness of insulation. So, you need to find out the optimum value based on the fixed charge and the value of heat loss and this is again a well-known phenomenon.

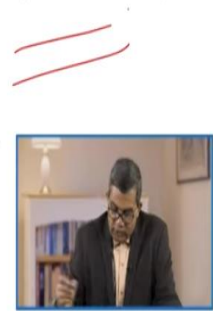
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Critical thickness of insulation for cylinders

The insulation on the external surfaces of the pipelines and vessels to reduce the heat loss to the ambient atmosphere e.g., in steam piping, carrying refrigerant etc.

The greater insulation will result in less in heat loss, which always not be true.

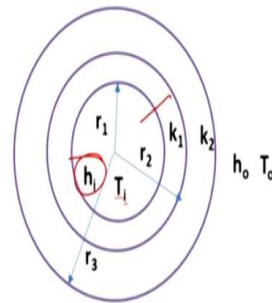
Let us consider a long cylindrical pipe carrying steam at T_i of inner radius r_1 and outside radius r_2 . It is wrapped with an insulating material of thermal conductivity k_2 to a radius r_3 . Let heat transfer coefficient at this radius is h_o .



Let us talk about the critical thickness of insulation for cylinder. Now for the insulation on the external surface of the pipeline and the vessel to reduce the heat loss to the ambient temperature and that is in the steam piping carrying the refrigerant etc. So, the greater insulation will result in less in heat loss which always not be true. So let us consider a long cylinder pipe carrying the steam at T_1 of the inner radius r_1 and outside the radius r_2 . It is wrapped with an insulating material of the thermal conductivity k_2 to a radius r_3 . So let heat transfer coefficient at this radius is h naught.

(Refer Slide Time: 24:33)

Let h_i be the heat transfer coefficient at the inner surface as shown in the figure.



The rate of heat transfer can be given as;

$$q = \frac{2\pi L(T_i - T_o)}{\frac{1}{r_1 h_i} + \frac{\ln \frac{r_2}{r_1}}{k_1} + \frac{\ln \frac{r_3}{r_2}}{k_2} + \frac{1}{r_3 h_o}}$$



Now h_i be the heat transfer coefficient at the inner surface which is as reflected in this particular figure. Now the rate of heat transfer can be given as $q = 2 \Pi L$ into $T_i - T$ naught over 1 upon $r_1 h_i + \ln r_2$ over r_1 over $k_1 + \ln r_3$ over r_2 over $k_2 + 1$ over $r_3 h$ naught.

(Refer Slide Time: 25:05)

Let h_i be the heat transfer coefficient at the inner surface as shown in the figure.

The rate of heat transfer can be given as;

$$q = \frac{2\pi L(T_i - T_o)}{\frac{1}{r_1 h_i} + \frac{\ln \frac{r_2}{r_1}}{k_1} + \frac{\ln \frac{r_3}{r_2}}{k_2} + \frac{1}{r_3 h_o}}$$

Let Q be the function of r_3 and the other parameters being kept constant, it will rise up to a maxima for a certain value of r_3 and the value is called critical radius of insulation.

On simplifying the above equation we have;

$$q = \frac{(T_i - T_o)}{\frac{1}{2\pi L} \left[\frac{1}{r_1 h_i} + \frac{\ln \frac{r_2}{r_1}}{k_1} + \frac{\ln \frac{r_3}{r_2}}{k_2} + \frac{1}{r_3 h_o} \right]}$$

$$R_{Total} = \frac{1}{2\pi L} \left[\frac{1}{r_1 h_i} + \frac{\ln \frac{r_2}{r_1}}{k_1} + \frac{\ln \frac{r_3}{r_2}}{k_2} + \frac{1}{r_3 h_o} \right]$$



So let Q be the function of r_3 and the other parameter being kept constant it will rise up to a maxima of a certain value of r_3 and the value is called the critical radius of insulation. So, if we simplify this particular equation, we will have $q = \frac{T_i - T_o}{\frac{1}{2\pi L} \left[\frac{1}{r_1 h_i} + \frac{\ln \frac{r_2}{r_1}}{k_1} + \frac{\ln \frac{r_3}{r_2}}{k_2} + \frac{1}{r_3 h_o} \right]}$ and by this way we can calculate the R_{Total} and that comes out to be our total is equal to $\frac{1}{2\pi L} \left[\frac{1}{r_1 h_i} + \frac{\ln \frac{r_2}{r_1}}{k_1} + \frac{\ln \frac{r_3}{r_2}}{k_2} + \frac{1}{r_3 h_o} \right]$.

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On simplifying the above equation, we have;

$$q = \frac{(T_i - T_o)}{\frac{1}{2\pi L} \left[\frac{1}{r_1 h_i} + \frac{\ln \frac{r_2}{r_1}}{k_1} + \frac{\ln \frac{r_3}{r_2}}{k_2} + \frac{1}{r_3 h_o} \right]}$$

$$R_{Total} = \frac{1}{2\pi L} \left[\frac{1}{r_1 h_i} + \frac{\ln \frac{r_2}{r_1}}{k_1} + \frac{\ln \frac{r_3}{r_2}}{k_2} + \frac{1}{r_3 h_o} \right]$$

All the parameter in the last equation are constant except r_3 , which is depending upon the thickness of insulation required for minimum amount of heat transfer.

For minimum value of critical radius of insulation can be obtained on differentiating the above equation and put equal to zero.

$$\frac{dR_{Total}}{dr_3} = 0 = \frac{1}{2\pi L} \left[0 + 0 + \frac{1}{k_2} \cdot \frac{1}{r_3} + \frac{1}{h_o} \left(-\frac{1}{r_3^2} \right) \right]$$

$$\therefore \frac{1}{k_2} \cdot \frac{1}{r_3} = \frac{1}{h_o} \left(\frac{1}{r_3^2} \right) \Rightarrow r_3 = \frac{k_2}{h_o} = r_c$$



Where r_c is the critical radius of insulation

So, the all the parameter in the last equation they are constant except r_3 , which is depending upon the thickness of insulation and required for minimum amount of heat transfer. For minimum value of critical radius of insulation, it can be obtained on differentiating this particular equation and put equal to 0. So, by this way if we substitute all these things, it can become $r_3 = k_2$ over h_o = r_c where r_c is the critical radius of insulation. So, by this way you can calculate the critical radius of insulation.

(Refer Slide Time: 26:38)

For minimum value of critical radius of insulation can be obtained on differentiating the above equation and put equal to zero.

$$\frac{dR_{Total}}{dr_3} = 0 = \frac{1}{2\pi L} \left[0 + 0 + \frac{1}{k_2} \cdot \frac{1}{r_3} + \frac{1}{h_o} \left(-\frac{1}{r_3^2} \right) \right]$$

$$\therefore \frac{1}{k_2} \cdot \frac{1}{r_3} = \frac{1}{h_o} \left(\frac{1}{r_3^2} \right) \Rightarrow r_3 = \frac{k_2}{h_o} = r_c$$

Where r_c is the critical radius of insulation

The last equation is the critical radius of insulation for the cylinder.

- ✓ If the critical radius of insulation is greater than the outer radius of pipe, then adding insulation up to r_c will increase the heat loss from the pipe.
- ✓ The addition of the insulation thereafter will reduce the heat loss from the pipe.
- ✓ When the critical radius of insulation is less than or equal to the outer radius of pipe or container then addition of insulation will immediately reduce the heat loss from the pipe.



Now the last equation is the critical radius of insulation for the cylinder. Now if the critical radius of insulation is greater than the outer radius of the pipe then adding insulation up to r_c will increase the heat loss from the pipe. The addition of the insulation there after reduces the heat loss from the pipe. When the critical radius of insulation is less than or equal to the outer radius of the pipe or container then addition of insulation will immediately reduce the heat loss from the pipe.

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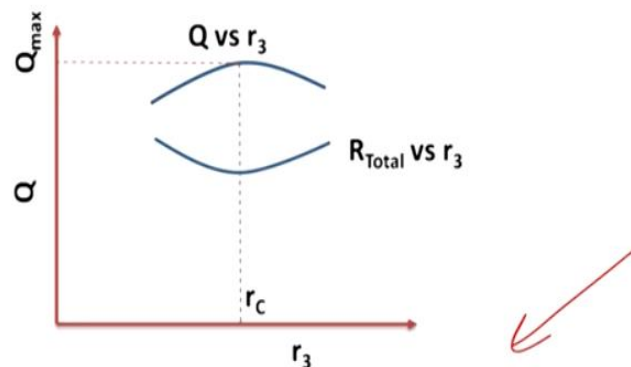


Figure showing relationship in thickness of insulation and Q and r_3 .

Now this is the figure which reflects the relationship in thickness of insulation and Q and r_3 .

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Problems

Question 4: What will be the critical radius of insulation for materials (asbestos, $k=0.20 \text{ W/m.K}$) surrounding the pipe and exposed to the room temperature at 25°C with h_o is $2.5 \text{ W/m}^2.\text{K}$. Calculate the heat loss from a 230°C of 60mm diameter pipe when covered with the critical radius of insulation and without insulation. Would any fibre glass insulation having thermal conductivity of 0.03 W/mK cause decrease in heat transfer?

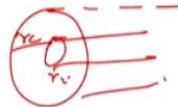
Now let us talk about problem now here the problem statement says that what will be the critical radius of insulation for material that is asbestos in this case where $k = 0.20$ watt per meter Kelvin. Surrounding the pipe and exposed to the room temperature at 25 degree Celsius with h naught is 2.5 watt per meter square Kelvin. Now you need to calculate the heat loss from a 230 degree Celsius of a 60 millimeter diameter pipe when covered with the critical radius of insulation and without insulation.

Would any; fiber glass insulation having the thermal conductivity of 0.03 watt per meter Kelvin cause decrease in heat transfer.

(Refer Slide Time: 28:14)

$$\begin{aligned}
 k_{as} &= 0.20 \text{ W/m.K} \\
 h_o &= 2.5 \text{ W/m}^2.\text{K} \\
 T_o &= 25^\circ\text{C} = 25 + 273 = 298 \text{ K} \\
 T_f &= 230^\circ\text{C} = 230 + 273 = 503 \text{ K} \\
 r_c &= \frac{k}{h_o} = \frac{0.20 \text{ W/m.K}}{2.5 \text{ W/m}^2.\text{K}} \\
 r_c &= 0.08 \text{ m}
 \end{aligned}$$

Ans

$$\begin{aligned}
 r_i &= \frac{60 \text{ mm}}{2} \\
 &= 0.03 \text{ m} \\
 \frac{Q}{L} &= \frac{2\pi (T_i - T_o)}{\ln \frac{r_o}{r_i} \frac{k}{L} + \frac{1}{r_o h_o}} \\
 &= \frac{2\pi (503 - 298)}{\ln \left(\frac{0.08}{0.03} \right) \frac{0.20}{L} + \frac{1}{0.08 \times 2.5}} \\
 \frac{Q}{L} &= 130.05 \text{ W/m}
 \end{aligned}$$


So let us solve this problem it is given that k for asbestosis 0.20 watt per meter Kelvin, h naught is given as 2.5 watt per meter square Kelvin. t naught is given as 25 degree Celsius and that comes out to be 273 that is equal to 298 Kelvin, $T_i = 230$ degree Celsius and that is $230 + 273$ this comes out to be 503 Kelvin. Now we know the critical radius of insulation for the cylinder is given by $r_c = k$ upon h naught. So, $r_c = 0.20$ watt per meter Kelvin upon 2.5 watt per meter square Kelvin and $r_c = 0.08$ meter that is one answer.

Now the diameter of the bare cylinder now here you see now the diameter of the bare cylinder is given as $r_1 = 60\text{mm}$ upon 2 and that is equal to 0.03 meter. Now heat transfer with insulation that is Q over $L = 2 \pi (T_i - T_{\text{naught}})$ upon $\ln r_c$ over r_1 upon $k + 1$ over r_c over h naught and if you substitute the value $503 - 298$ upon $\ln 0.08$ over 0.03 over $0.20 + 1$ upon 0.8 into 2.5. Now upon solving it comes out to be Q over $L = 130.05$ watt per meter. Now without using insulation now the heat will flow through the outer surface of the bare cylindrical pipe to the ambient atmosphere

(Refer Slide Time: 30:29)

Given;

$$k_{as} = 0.20 \text{ W/mK}$$

$$h_o = 2.5 \text{ W/m}^2\text{K}$$

$$T_o = 25^\circ\text{C} = 25 + 273 = 298\text{K}$$

$$T_s = 230^\circ\text{C} = 230 + 273 = 503\text{K}$$

$$r_1 = 60/2 = 30\text{mm} = 0.03 \text{ m}$$

$$r_c = k/h_o = 0.20/2.5 = 0.08 \text{ m}$$

$$q = \frac{(T_i - T_o)}{\frac{1}{2\pi L} \left[\frac{\ln \frac{r_c}{r_1}}{k_{as}} + \frac{1}{r_o h_o} \right]}$$

$$q = \frac{(503 - 298)}{\frac{1}{2\pi L} \left[\frac{\ln \frac{0.08}{0.03}}{0.20} + \frac{1}{0.08 \times 2.5} \right]}$$

$$q = 130.05 \text{ W/m}$$

$$\frac{Q}{L} = (2\pi r) h (T_o - T_i)$$

$$= 2\pi \times 0.03 \times 2.5 \times (503 - 298)$$

$$= 96.604 \text{ W/m}$$

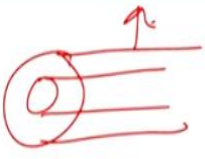
% increase in the heat transfer

$$= \frac{Q_{\text{heat with ins}} - Q_{\text{without ins}}}{Q_{\text{without ins}}} \times 100$$

$$= \frac{130.05 - 96.604}{96.604} \times 100 = 34.622\%$$

$k = 0.03 \text{ W/mK}$

$$r_c = \frac{k}{h}$$

$$= \frac{0.03}{2.5} = 0.012 \text{ m}$$


If you see here it will go to the ambient atmosphere at 25 degree Celsius. Now this is a case of convection convective heat transfer so in that case you can write $2 \pi r$ into h into $T_{\text{naught}} - T_i$ which is 2π into 0.03 into 2.5 into $503 - 298$ and that comes out to be 96.604 watt per meter. Now the percentage increase in the heat transfer that is equal to Q heat transfer within with insulation - Q without installation over Q without insulation multiplied by 100 .

And that is $130.05 - 96.604$ divided by 96.604 into 100 and this comes out to be 34.622% that is the answer. Now if a given fiber glass insulation, then $k = 0.03$ watt per meter Kelvin and the critical rate radius of insulation r_c would be k over h and that comes out to be 0.03 upon 2.5 which is equal to 0.012 meter. Now the value of r_c is less than the outside radius of the pipe and that is 0.03 . So, addition of any fiber glass insulation would cause a decrease in heat transfer. So that is the issue.

(Refer Slide Time: 32:37)

$$\frac{Q}{L} = (2\pi r) h (T_o - T_{am})$$

$$\frac{Q}{L} = 2\pi \times 0.03 \times 2.5 \times (503 - 298)$$

$$\frac{Q}{L} = 96.604 \text{ W/m}$$

$$\text{Percentage increase in the heat transfer} = \frac{Q_{\text{heat with insulation}} - Q_{\text{without}}}{Q_{\text{without insulation}}}$$

$$\text{Percentage increase in the heat transfer} = \frac{130.05 - 96.604}{96.604} \times 100 = 34.62\%$$

$$K = 0.03 \text{ W/mK}$$

$$r_c = k/h$$

$$= 0.03/2.5 = 0.012 \text{ m (answer)}$$

Critical thickness of insulation for spheres

For sphere the heat transfer equation can be written as;

$$Q = \frac{(T_1 - T_2)}{\left[\frac{1}{4\pi r_1^2 \cdot h_i} + \frac{1}{4\pi r_1 r_2 k_1} [r_2 - r_1] + \frac{1}{4\pi r_2 r_3 k_2} [r_3 - r_2] + \frac{1}{4\pi r_3^2 \cdot h_o} \right]}$$

$$R_{Total} = \left[\frac{1}{4\pi r_1^2 \cdot h_i} + \frac{1}{4\pi r_1 r_2 k_1} [r_2 - r_1] + \frac{1}{4\pi r_2 r_3 k_2} [r_3 - r_2] + \frac{1}{4\pi r_3^2 \cdot h_o} \right]$$

Let r_1, r_2 are the inner and outside dia of the sphere and r_3 be the outer radius for insulation, r_2 can be considered as inner radius for insulating materials.



Now let us talk about the critical thickness of insulation for spheres for spheres the heat transfer equation can be written as this particular equation. And when we talk about the r_{total} this can be written as this particular equation number 2. Now let r_1 and r_2 are the inner and outside diameter of the sphere and r_3 be the outer radius of the insulation and r_2 can be considered as inner radius for insulating material.

(Refer Slide Time: 33:05)

Critical thickness of insulation for spheres

For sphere the heat transfer equation can be written as;

$$Q = \frac{(T_1 - T_2)}{\left[\frac{1}{4\pi r_1^2 \cdot h_i} + \frac{1}{4\pi r_1 r_2 k_1} [r_2 - r_1] + \frac{1}{4\pi r_2 r_3 k_2} [r_3 - r_2] + \frac{1}{4\pi r_3^2 \cdot h_o} \right]}$$

$$R_{Total} = \left[\frac{1}{4\pi r_1^2 \cdot h_i} + \frac{1}{4\pi r_1 r_2 k_1} [r_2 - r_1] + \frac{1}{4\pi r_2 r_3 k_2} [r_3 - r_2] + \frac{1}{4\pi r_3^2 \cdot h_o} \right]$$

Let r_1, r_2 are the inner and outside dia of the sphere and r_3 be the outer radius for insulation, r_2 can be considered as inner radius for insulating materials.

On differentiating above equation for R_{Total} with respect to r_3 and taking all the parameter constant and put equal to zero. We have;

$$\frac{dR_{Total}}{dr_3} = 0 = -\frac{1}{4\pi k_2 r_3^2} - \frac{2}{4\pi h_o r_3^2} \Rightarrow r_3 = \frac{2k_2}{h_o} = r_c$$

The above equation gives the critical radius of thickness for the spheres.

Where, k_2 is the thermal conductivity of the insulating material and h_o is the convective heat transfer coefficient for insulating materials.



So, if you differentiate the above equation for r total with respect to r_3 and taking all the parameter constant and put equal to 0 then we have this r_3 is equal to our critical radius of thickness is equal to r_3 and that comes out to be $2k_2$ upon h naught. So, this equation this particular equation gives the critical radius of thickness for the sphere. Now where k_2 is the thermal conductivity of the insulating material and h naught is the convective heat transfer coefficient for the insulating material. Now let us discuss about another problem.

(Refer Slide Time: 33:42)

On differentiating above equation for R_{Total} with respect to r_3 and taking all the parameter constant and put equal to zero. We have;

$$\frac{dR_{Total}}{dr_3} = 0 = -\frac{1}{4\pi k_2 r_3^2} - \frac{2}{4\pi h_o r_3^2}$$

$$\Rightarrow r_3 = \frac{2k_2}{h_o} = r_c$$

Problems

Question 5: If a sphere of inner diameter 40 mm having inner temperature $T_i = 200^\circ\text{C}$, is surrounded insulation. The thermal conductivity of the insulating material k is 0.017 W/m.K . The sphere is exposed to ambient atmosphere at 30°C temperature, with $h_o = 0.20 \text{ W/m}^2\text{.K}$. then, calculate the heat lost with and without the insulation and percentage increase/decrease in the heat loss and the critical thickness of the insulation?

Now if a sphere of inner diameter having a 40 mm having the inner temperature $T_i = 200$ degree Celsius is surrounded by insulation. The thermal conductivity of the insulating material k is 0.017 watt per meter kelvin and the sphere is exposed to ambient atmosphere at 30 degree Celsius temperature, with $h_{\text{naught}} = 0.20$ watt per meter square Kelvin. Then you need to calculate the heat loss with and without the insulation and the percentage increase and decrease in the heat loss and the critical thickness of the insulation.

(Refer Slide Time: 34:25)

$$\begin{aligned}
 \text{Radius of Sphere } r &= \frac{40 \text{ mm}}{2} = 20 \text{ mm} \\
 T_i &= 200^\circ\text{C} = 200 + 273 = 473 \text{ K} \\
 r_c &= \frac{2k}{h_o} = \frac{2 \times 0.017 \text{ W/mK}}{0.20 \text{ W/m}^2\text{K}} \\
 T_{\text{ambient}} &= 30^\circ\text{C} = 30 + 273 = 303 \text{ K} \\
 r_c &= 0.17 \text{ m} \\
 Q &= \frac{T_i - T_{\text{ambient}}}{\frac{1}{4\pi r_c k} (r_c - r) + \frac{1}{4\pi r_c^2 h_o}} \\
 &= \frac{473 - 303}{\frac{1}{4\pi \times 0.02 \times 0.02} \times 0.17 \times (0.17 - 0.02) + \frac{1}{4\pi \times (0.17)^2 \times 0.2}} \\
 Q &= 0.7717 \text{ W}
 \end{aligned}$$

So let us solve this particular problem now here the radius of sphere is given $r = 40 \text{ mm}$ $0.2 = 20 \text{ mm}$. Now here $T_i = 200$ degree Celsius which is equal to $200 + 273$ that comes out to be 473 Kelvin . Now the if sphere is surrounded with the insulating material then $r_c = 2 \text{ k upon h naught}$ which is 2 into $0.017 \text{ watt per meter kelvin upon } 0.20 \text{ watt meter square Kelvin}$ and $r_c = 0.17 \text{ meter}$ that is the first answer.

Now T_{ambient} is given as 30 degree Celsius or $30 + 273$ that comes out to be 303 kelvin . So the rate of heat transfer in sphere with insulation that is $Q = T_i - T_{\text{ambient}}$ over $1 \text{ upon } 4 \pi r_c k$ into $r_c - r + 1 \text{ upon } 4 \pi r_c^2 h_o$ and that is $473 - 303$ upon $1 \text{ upon } 4 \pi$ into 0.02 into 0.016 into 0.17 into $0.17 - 0.02 + 1 \text{ upon } 4 \pi$ into 0.17 into 0.2 and the Q comes out to be 0.7717 watt and that is the answer.

(Refer Slide Time: 36:32)

Given;

Radius of sphere (r) = $40\text{mm}/2 = 20 \text{ mm} = 0.02 \text{ m}$

$T_i = 200 \text{ oC} = 200 + 273 = 473\text{K}$

$r_c = 2k/h_o = 2 \times 0.017 \text{ W/mK} / (0.20 \text{ W/m}^2\text{K})$

$r_c = 0.17 \text{ m}$

$T_{\text{ambient}} = 30\text{oC} = 30 + 273 = 303\text{K}$

On putting these values in the heat transfer equation

$$Q = \frac{(473 - 303)}{\left[\frac{1}{4\pi \times 0.02 \times 0.017 \times 0.17} [0.17 - 0.02] + \frac{1}{4\pi \times (0.17)^2 \times 0.2} \right]}$$

$$Q = 0.7717 \text{ W}$$

Without using insulation

$$Q = h_0 A (T_i - T_{\text{amb}})$$

$$= h_0 \times 4\pi r^2 \times (T_i - T_a)$$

$$= 0.20 \times 4\pi \times (0.02)^2 \times (473 - 303)$$

$$Q = 0.1709 \text{ W}$$

% Change in the heat transfer with / without using insulation

$$= \frac{Q_{\text{with I}} - Q_{\text{without I}}}{Q_{\text{without I}}}$$

$$= \frac{0.7717 - 0.1709}{0.1709} \times 100$$

$$= 351.55\%$$

$h_0 = 0.20 \text{ W/m}^2\text{K}$
 $T_a = 30 + 273 = 303 \text{ K}$

Ans

Now the heat transfer in sphere without using insulation so $Q = h_{\text{naught}} A (T_i - T_{\text{ambient}})$ which is $h_{\text{naught}} \times 4 \pi r^2 (T_i - T_{\text{naught}})$ and that is $0.20 \times 4 \pi \times 0.02^2 \times (473 - 303)$ where $h_{\text{naught}} = 0.20 \text{ watt per meter square Kelvin}$ $T_a = 30 + 273$ which is equal to 303 Kelvin . So, $Q = 0.1709 \text{ watt}$ now the percentage change in the heat transfer with or without using insulation.

So, this is Q with insulation minus Q without insulation upon Q without insulation and that comes out to be $0.7717 - 0.1709$ upon 0.1709 into 100 and that is equal to 351.55% and that is our desired answer. So, in this particular lecture we discussed about the various aspects of heat transfer, insulating material, and solved and we discussed the various cases like cylindrical aspect and then spherical aspect.

(Refer Slide Time: 38:29)

Without any insulation:

$$Q = h_o A (T_i - T_{ambient})$$
$$Q = h_o \times 4\pi r^2 \times (T_i - T_{ambient})$$

On putting the values of the parameter, we have:

$$Q = 0.20 \times 4 \times \pi 0.02^2 \times (473 - 303)$$

$$Q = 0.1709 \text{ W}$$

% Change in the heat transfer with/without using insulation can be found by the following equations.

$$\% \text{ change in the heat transfer} = \frac{Q_{\text{With insulation}} - Q_{\text{without insulation}}}{Q_{\text{Without insulation}}} \times 100$$

$$\% \text{ change in the heat transfer} = \frac{0.7717 - 0.1709}{0.1709} \times 100$$

$$\% \text{ change in the heat transfer} = 35.55\% \text{ (answer)}$$

References

- Richard T. Bynum, Insulation Handbook, McGraw-Hill Companies, Inc., (2014), ISBN: 0-07-134872-7, DOI: 10.1036/0071414614.
- Alireza Bahadori, Thermal Insulation Handbook for oil, gas and petrochemical industries, Elsevier (2013), ISBN: 978-0-12-800010-6.

For your convenience we have included couple of references and if you wish you can have a look of all those references for further study. Thank you very much.