

Waste to energy conversion
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Lecture – 24
Gas Cleanup – 1

Good morning. Now we will start discussion on a new module Gas Cleanup. As you know most of the waste to energy conversion processes let say incineration, gasification, pyrolysis, anaerobic, digestion, etcetera produce significant amount of gas streams. We have already discussed incineration, gasification and pyrolysis and we will discuss on the anaerobic digestions in later on modules and the gas produced through this processes contain different type of molecules or the compositions varies and this can be used in different applications also and for that applications.

So, to meet the quality we need to remove some gas components from this produced gas like say example if you want to use say syngas produced through gasification process through different routes. So, different quality parameter of the gas is required for chemical synthesis we have to remove all impurities, but for thermal applications we do not need to clean to that extent. So, this is one way to meet the specification of any downstream applications we need to clean up the gas another important point is that in many cases these gases exit into the environment where as the gas contains many polluting components also which make health impact.

So, to reduce that health impact or environmental pollution we need to treat the gas.

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So, in this module we will cover all those aspect how to remove different components of a gas before it is exist to the environment and we will make discussion on typical composition of gas produced through different routes of waste energy conversion.

Processes for removal of unwanted elements from gas and basically particulates removal both particulates and gas molecules removal and gas molecules removal. So, now, we will start with the particulates removal first.

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Typical composition of gas produced through different routes		
Process	Typical Gas composition	Elements to be removed
Incineration	CO ₂ , H ₂ O, NO _x , SO _x , PM, N ₂	NO _x , SO _x , PM, CO ₂
Gasification	CO, H ₂ , CO ₂ , H ₂ S, COS, PM, CH ₄	CO ₂ , H ₂ S, COS, PM
Pyrolysis of biomass and wastes	Hydrocarbons, CO, CO ₂ , H ₂	CO ₂
Pyrolysis of waste plastics	Hydrocarbons, CO, CO ₂ , H ₂ , HCl, dioxins	CO ₂ , HCl, dioxins
Anaerobic digestion	CH ₄ , CO ₂ , H ₂ S, H ₂ O	CO ₂ , H ₂ S, H ₂ O

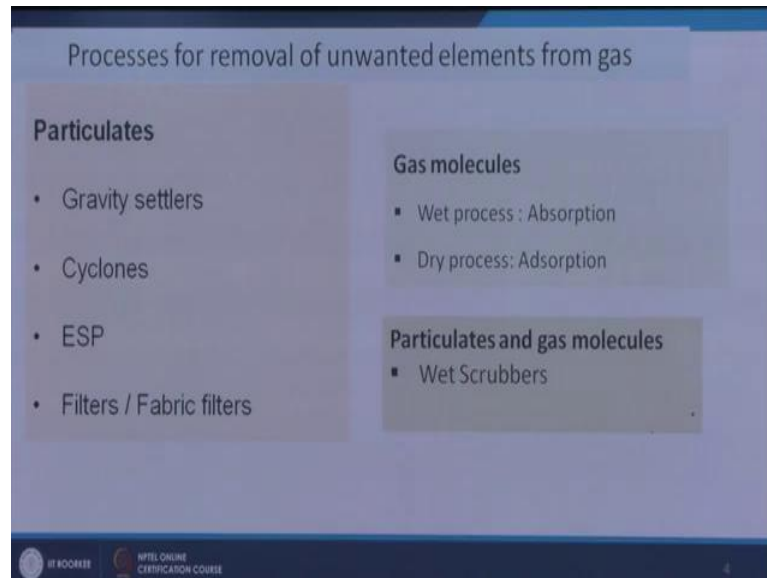
Before that let us see; what are the different types of gases generated in waste to energy conversion processes? So, you have incineration process we have gasification pyrolysis of biomass and waste pyrolysis of waste plastics and anaerobic digestion. So, these are major process which produce a significant amount of gas streams for incineration completely gas stream is produced. So, the typical gas composition is CO₂, H₂, NO_x, SO_x, particulate matter and nitrogen.

So, what we need to remove here we need to remove NO_x, we need to remove SO_x particulate matter and carbon dioxide before it gets entry to the environment similarly for gasification the composition is carbon monoxide hydrogen CO₂, H₂S, COS, PM and CH₄ or methane. So, out of these compositions we need to remove CO₂ H₂S COS and PM particulate matter CO is not needed because this will be used for further applications for chemical synthesis or other applications or if it is used for heat production then CO will be converted to CO₂ that is why CO is not mentioned here and pyrolysis of biomass and waste it produces CO, CO₂ hydrogen and hydrocarbons containing gas.

This hydrocarbons basically C₁ to C₅ or C₅, it gets C₅ gets and then we removed to we need to remove the CO₂ because other will be having some heating values. So, after that finally, CO₂ has to be removed similarly for pyrolysis of waste plastics we will get number of gas components like CO, CO₂, H₂, C₁, dioxins hydrocarbons etcetera and many others depending upon use of additives in the plastics. So, we have to remove CO₂ HCL and dioxins for anaerobic digestion we can get gas; bio gas. So, that will be containing mainly CO₂ and CH₄ apart from this one amount of H₂S and H₂O are normally available. So, we have to removed H₂S CO₂ and H₂O.

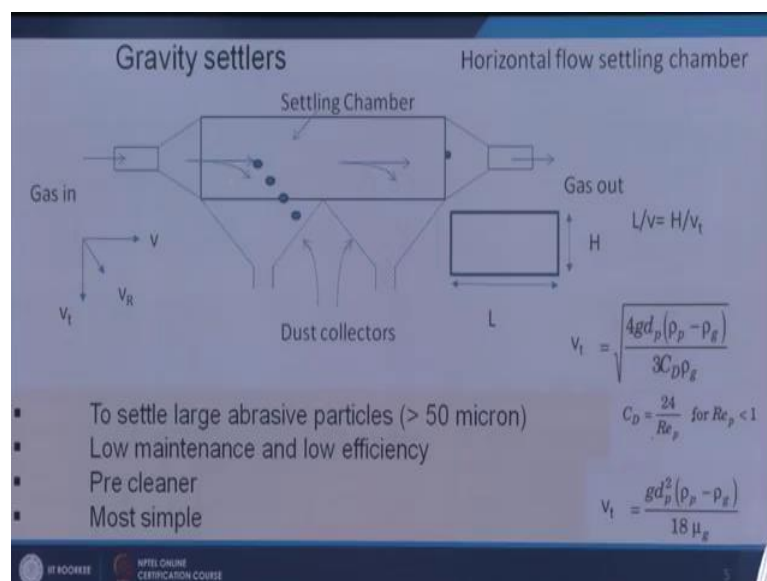
So, these are the elements we need to remove. So, here we see PM and other gas molecules the CO N and COS and H₂S removal from the gasification gas that is Syngas we have already discussed in our gasification module. So, we will concentrate on PM CO₂ removal NO_x and SO_x removal.

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So, for the removal of particulates we have number of equipment's that is gravity settlers cyclones electrostatic precipitators filters there is bag filters and fabric filters. So, these are important devices which are used for the removal of particulate matters from any gas stream for gas molecules with processes absorptions and adsorption best processes are used and particulates and gas molecules wet scrubbers are used both these wet scrubbers can remove both gas molecules as well as the particulates present in the gas stream.

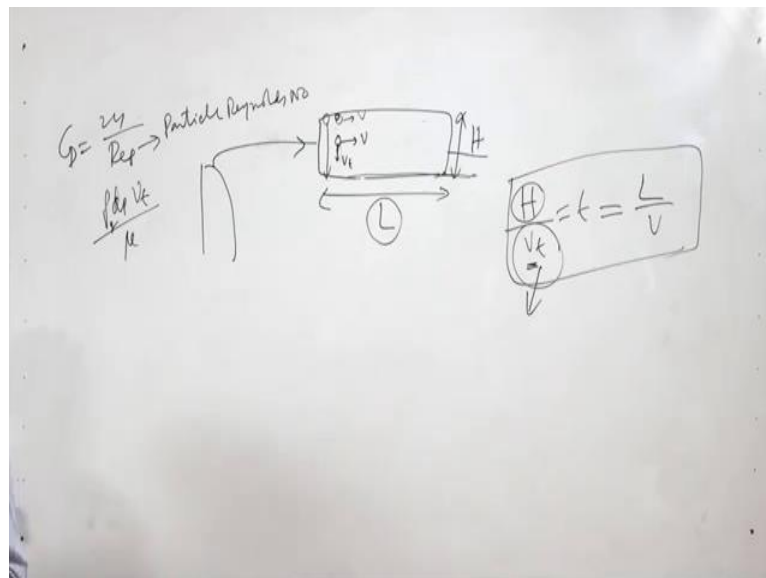
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Now, we will see the gravity settlers which are used to settle the particles from the gas stream. So, here let us see a gas is getting entry into this settling chamber. So, this particle will be having one velocity that is equal to say gas velocity and there will be some relative velocity between gas and particle, so these velocities there in horizontal direction and gravities also working on it in the particle direction. So, it is expensing 2 forces. So, resultant force will be given as the resultant velocity. So, this tangential movement this particle we will have. So, after travelling certain distance it will reach to the bottom of it and it will be collected.

So, this is the mechanism of the separation of particles in a gravity settling chamber now these chambers are not very efficient very spine particles cannot be separated by this chamber very easily and particle size more than 50 micron are normally separated through this that is why this is used as a pre cleaner step, but advantage of this process is that this is a very simple process operation is very simple and its maintenance is very low now we will see how can we design one gravity settler for getting the separation of particulates from a gas stream let us see from a process one gas is coming out. So, we are designing some settler, so where the particles will be settled.

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So, let us say this is the length of the settler and this is the height of the settler. So, this particle any particle if we considered here that will be having on velocity this direction that is v or the gas velocity and that is v_t terminal settling velocity now if a particle is

present here and another particles is present here. So, both are having v and this distance maximum distance is H . So, if we provide certain time that this particle moves in these directions certain distance and during that time it also travels across the vertical direction is equal to H distance. So, this particle will be separated. So, if these 2 particles are having same diameter within this time this particular will also be separated because the distance required to be traveled by this particle is less.

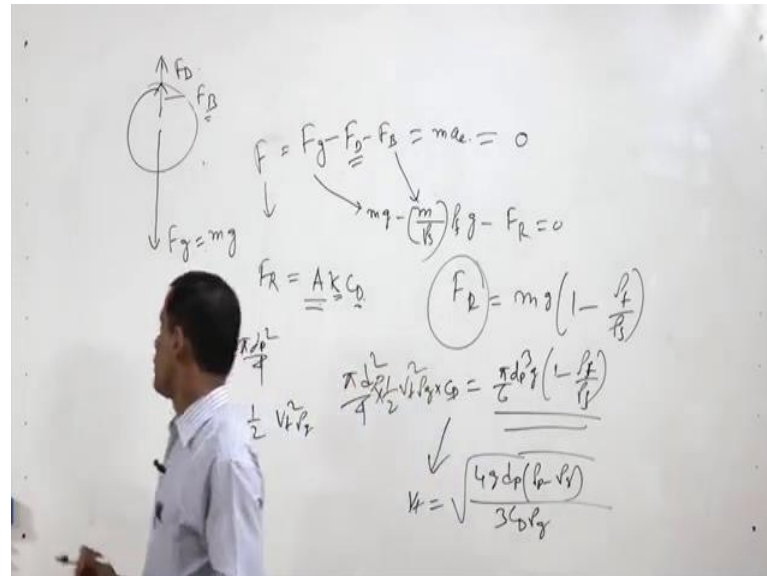
So, we are assuming here the maximum possibility for the separation of all particles let us assume one particle is here. So, it is travelling H distance. So, this H distance is travelling in vertical directions and if I want to separate it from this chamber, so it is necessary. So, within this time this particle must travel this one not more than this if it is not it is more than this then it will not be separate it. So, the boundary condition is that. So, H by V_T that is equal to time required to travel H distance from that is equal to L by V_L by V_V is the velocity of the particle in horizontal directions.

So, this is the condition which will give us the separation. So, now, if you know the V_T then we can get the value of L at which L or at which will H for what value of H will get the separation of the particles; that means, it is giving the dimensions of the chamber now let us see how can we get the value of V_T ; V_T is the terminal settling velocity if we follow a particle from the rest the particle will increase its velocity and at in a constant velocity. So, that contain velocity is vertical directions that is called terminal settling velocity. So, we are assuming the same situation here the particle has reached the terminal settling velocity. So, in this case how can you calculate the terminal settling velocity? You see here V_T is equal to root of $\frac{4 G D^3 (\rho_P - \rho_G)}{3 C_D \rho_G}$.

This is the definition of the V_T it has been derived on the basis of mass force balance on the particles I will discuss just now. So, this is the case we can get the V_T this expression. Now this C_D is a drag coefficient, C_D is the drag coefficient. So, C_D is equal to $\frac{24}{\text{Re}_P}$, the particle Reynolds number. So, C_D is equal to $\frac{24}{\text{Re}_P}$, Re_P is your particle Reynolds number. So, particle Reynolds number that is $\rho_G D V_T$ by μ that is your G , $\rho_G D V_T$ by μ , this is the definition of Re_P . Now if we put this definition of Re_P . So, C_D equal to $\frac{24}{\text{Re}_P}$ by these one then we will get this part then we will get this part.

Now, let us see while from this VT equal to $4 \text{ GDP} \rho \text{ P minus } \rho \text{ G by } 3 \text{ CD} \rho \text{ G}$ is coming let us see one particle is there.

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So, this particle is experiencing one force that is F_g that is equal to m into g mass of this particle into acceleration due to gravity, it will be experiencing some buoyancy force that is F_B , it will be experiencing some drag force F_D . So, F_D is drag force. So, particle is falling opposite directions it will be experiencing one force there is called drag force due to friction basically and this is due to buoyancy or replacement of volume, it will give the fluid will give some of what force also that is F_B . So, now, what is the balance of the forces the force is that F_g minus F_D minus F_B . So, that is equal to resultant force the resultant force f is equal to this one.

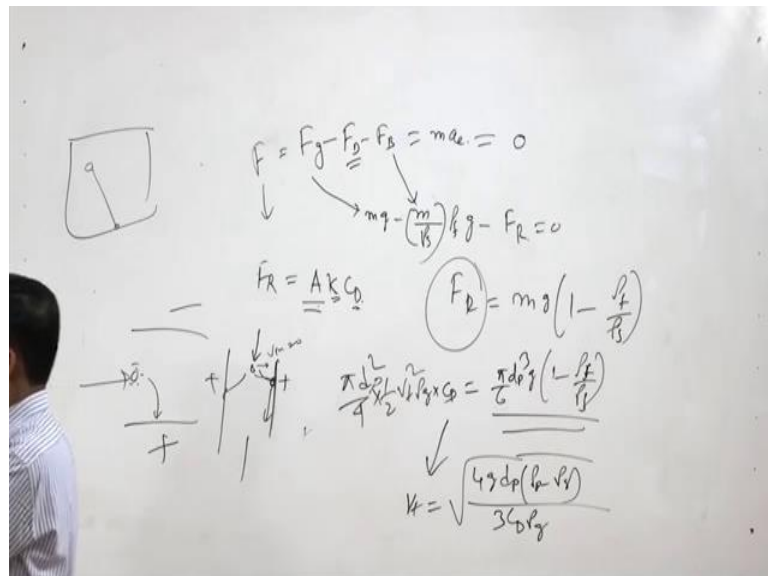
Now, if say as some value then it will give some acceleration to the particles. So, that will be m into a say acceleration, but when it reaches the terminal settling velocity; that means, there is no acceleration. So, that is equal to 0. So, in that steady state we will get F_g minus F_D minus F_B equal to 0. So, we will be getting F_D is equal to F_g minus F_B . So, here getting $m g$ here we see getting $m g$ and this is you are getting m into m into ρ_s into ρ_f into ρ_f F_g that is your this one and this is your, this one and this F_D is equal to say F_r . So, F_D is sometimes called F_r that is kinetic, kinetic force F_r is kinetic force and F_r is equal to this F_r is equal to $A K$ into C_D where A is the characteristics area of the

particles and K is the characteristic kinetic energy of the particle and CD is the drag coefficient.

So, if the particle is spherical one then a value is equal to $5 D P^2$ square by $4 K$ value is equal to half into $V T^2$ square into ρ g into ρ into ρ g. So, this is the K rhos and CD value will put CD value we are having CD . So, if we this put equal to 0. So, Fr is equal to we are getting MgM into g into 1 minus ρF minus ρS . So, this is the expression then if the particle is spherical one. So, m is equal to π by $\pi d^3 \rho_p$ by $6 D P^2 q$ g into 1 minus ρF minus ρS 1 minus ρf then if we you are getting this side and if we now put the Fr is equal to this one a K and CD that is means $\pi D^3 \rho_p$ square by 4 into half $V T^2$ square ρ g into CD then we are getting by this expressions by rearranging will be getting $V T$ is equal to root over root over $4 G D P^2$ into ρ_p minus ρ g divided by $3 C D$ ρ g.

So, this is the expression we are getting from the force balance on the particles. So, we can get the value of $V T$ equal to this much now we are coming to electrostatic precipitator. So, electrostatic precipitator you see what is the mechanism of separation here in the gravity separation gravity settler.

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Handwritten notes on a whiteboard showing force balance equations for a particle in an electric field. The equations include:

$$F = F_g - F_d - F_e = ma = 0$$

$$F_d = mg - \left(\frac{m}{\rho}\right) \rho g - F_e = 0$$

$$F_e = A K G$$

$$F_d = mg \left(1 - \frac{\rho}{\rho_p}\right)$$

$$\frac{\pi d_p^2}{4} \rho_p \frac{V_t^2}{2} = \frac{\pi d_p^2}{4} \left(1 - \frac{\rho}{\rho_p}\right) \rho g$$

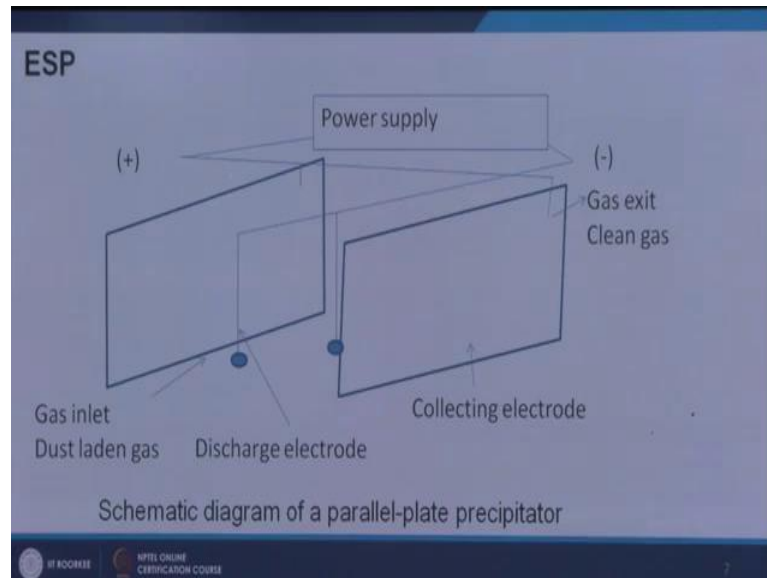
$$V_t = \sqrt{\frac{4 g d_p (\rho_p - \rho)}{3 C \rho g}}$$

There is also a diagram of a particle in a square container.

We had seen that particles is falling and it is reaching to the bottom after certain time, but when will be using electrostatic precipitator the particle will be extracted by some force one is your negative surface another is positive surface. We are sending the

particles through this particle are having negative charge surrounded by it. So, this will be attracted by this surface and once this is reaching this surface it will be settled.

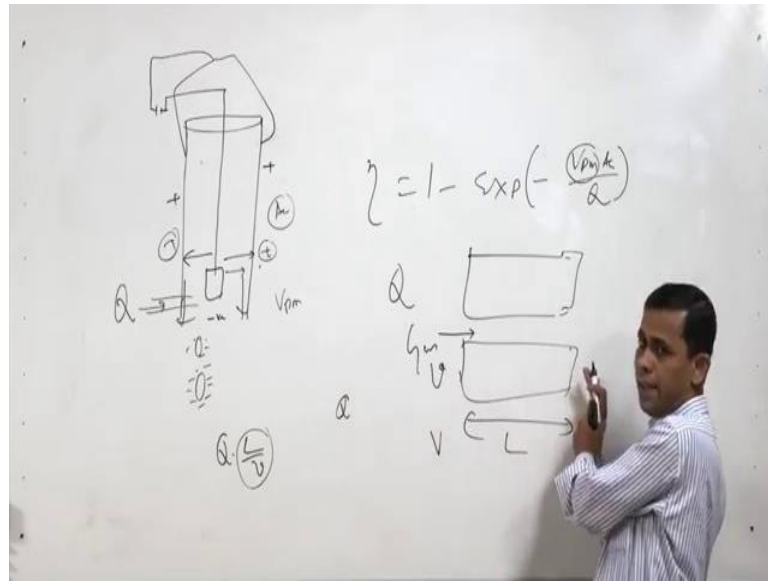
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So, these two are horizontal these may not be horizontal this may be vertical plate also, and electrostatic precipitators are basically of 2 types: one is here this one that is parallel plate types. So, these 2 parallel plates are used. So, to parallel plates are there. So, through this the gas is coming.

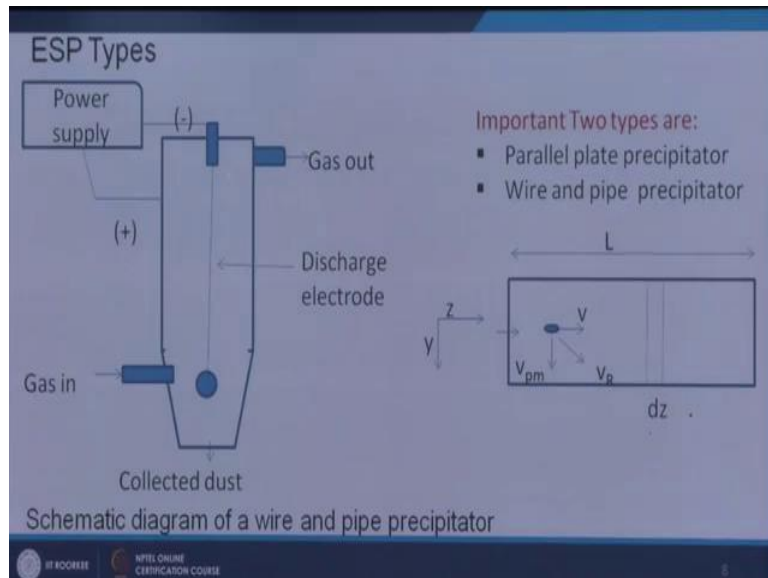
So, this is gas is coming and in between these 2 parallel plates 2 electrodes are there that is your negatively charged and these 2 plates are positively charged. So, that this particle is negatively charged. So, that will be moving toward the 2 plates. So, this is the mechanism of the separation another type of ESP is available that is called your wire and pipe precipitator wire and pipe precipitator.

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So, what happens in this case? Say one pipe is there say we have put here some electrode with negative charge this is with positive charge. So, we have collected here these 2 and this is to this one say positive negative. So, that way we have collected. So, when the gas is coming particle is coming here. So, that will be moving to these directions and settled.

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So, 2 types are 2 types of PSP are available. So, this gas in the gas out the particles will be attracted by the surface due to the negative charge on the pipe this is the mechanism. So, here interesting thing we are getting that if we take this zone. So, one particle is

getting one velocity that is the gas velocity one is your gas velocity the gas when it is coming in it will be having some velocity here and that the charge on the surface of this plate or the pipe will generate some electric field and that field will give some velocity.

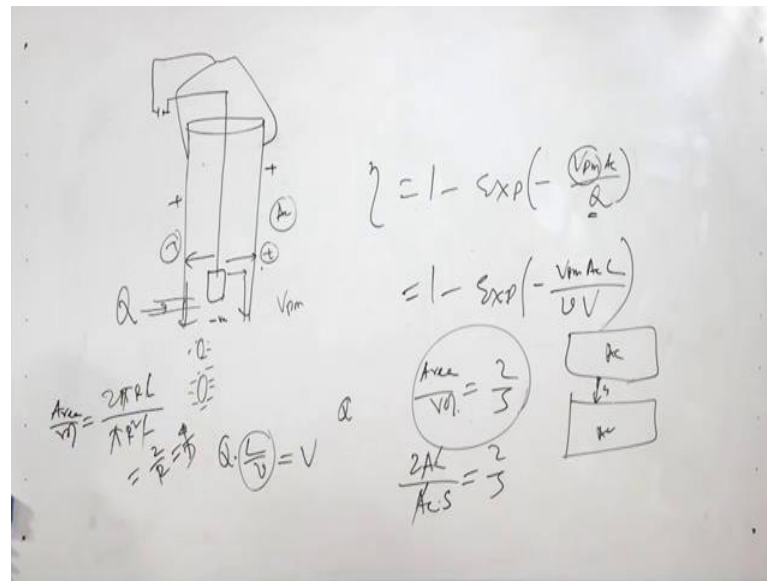
So, this velocity is called drift velocity. So, drift velocity that is v_{pm} it generated and v is available with the gas stream. So, these 2 velocities is having and again one result resultant velocity it will be gaining. So, the particle will move particle will not move directly from this in these directions it will be having some trajectory. So now, what will be the efficiency say if one gas is coming here having different particle size and different particle size as well as the charge is different here the charge is different here.

So, positive charge is similar, here the negative is charge more. So, that particle will be moving faster because V_{pm} will be higher than this particle. So, all particles will not be separated equally. So, there will be some efficiency of separation. So, that efficiency of separation can be explained in terms of efficiency is equal to $1 - \exp(-V_{pm} AC / Q)$, what is that; this is the Q how much gas flow rate is coming?

This is the area of where the particles are collected. So, that is AC ; collection area and V_{pm} that we have discussed that what is the drift velocity the particle is getting now what is the Q ? Q is equal to say we have 2 plates here, similar size plate we have, separated by some distance we are sending gas through this with particles say we have some volume of the precipitator. So, volume of the precipitator will be V and Q is the flow rate. So, now, if this is the L is the distance, L is the distance and v is the gas velocity; small v is the gas velocity. So, what will get Q into l by V , L by V is the time, this is the L and this is small v . So, L by v is the time required to travel the gas molecules from this to this end.

So, that time multiplied by volumetric flow rate that will be the total volume of gas which is passing through these 2 plates that is actually the volume of the ESP, Q into this equal to V , if we replace this expression of Q here.

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So, we are getting, we are getting η is equal to 1 minus exponential 1 minus exponential minus V_{pm} into $A_c L$ divided by 1 is replaced by here V into capital V . So, this is the efficiency of this now what will be the A_c value what will be the A_c ? A_c is the collector area. So, collector area, if it is a plate type then area by volume is equal to 2 by S , how it is we have one 2 plates the distance is s the distance is S .

So, area is equal to 2 into A_c this is A_c and this is A_c . So, 2 into A_c that is collecting the particles and what is the volume A_c into S . So, that is equal to A_c into s . So, that is equal to 2 by s . So, area by volume is equal to 2 by S , but if it is say tubular type of precipitator then what will be the area by volume. So, area by volume in this case the area collecting area is $2\pi r$. So, $2\pi r$ into l distance divided by volume $\pi r^2 l$. So, this is getting. So, we are getting 2 by r or that is equal to 4 by D ; 4 by D . So, that is the case that A_c by V equal to 4 by DC and this is by DC B equal to this 2 by S .

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Efficiency of ESP

Efficiency, $\eta = 1 - \exp\left(-\frac{v_{pm} A_c}{Q}\right)$

Where v_{pm} = drift velocity
 A_c = Collector surface area
 Q = Volumetric flow rate

Or $\eta = 1 - \exp\left(-\frac{v_{pm} A_c L}{v V}\right)$

Where v = Gas velocity
 V = Volume of the precipitator
 L = Length of precipitator

For tubular type precipitator $A_c/V = 4/D_c$
 D_c = Diameter of the collector

For plate type $A_c/V = 2/S$
 S = Distance between two plates

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So, by the geometry or the dimensions of this precipitator we can get the value of A_c/V and we can calculate the performance.

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Now v_{pm} can be replaced as $v_{pm} = \frac{q_p E_c C}{3\pi\mu_g d_p}$

Thus, $\eta = 1 - \exp\left(-\frac{q_p E_c C A_c}{3\pi\mu_g d_p Q}\right)$

Where, E_c = Electric field strength
 d_p = Particle size
 μ_g = Gas viscosity
 q_p = Particle charge
 C = Cunningham correlation factor
 q_p = Particle charge

C can be written as $C = 1 + \frac{2\lambda}{d_p} \left(1.257 + 0.4e^{-0.55d_p/\lambda}\right)$
 where, λ = Mean free path of gas molecules

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And that v_{pm} is another dependent on the E_c , q_p and C under q_p is equal to particle charge E_c is equal to electric field strength and C is equal to Cunningham correlation factor that is again dependent on the mean free path of the gas molecules. So, that if we know things we can calculate the v_{pm} and v_{pm} can be used to calculate the efficiency.

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A MSW based power plant is emitting 45,000 m³/h flue gas. It is proposed to install an ESP with a collection efficiency of 96.8%. Calculate the total area of the collection electrodes. If the collection efficiency is 99.5%, how much additional collection electrode area would be needed? Drift velocity of the particles has been determined experimentally as 0.13 m/s.

Ans.

$Q = 45000/3600 = 12.5 \text{ m}^3/\text{s}$

Efficiency $= 1 - e^{-v_p m A_c / Q}$

For the first case

$0.968 = 1 - e^{-0.13 A_c / 12.5}$

$A_c = 330.96 \text{ m}^2$

Similarly for 99.5 % efficiency

$A_c = 509.45 \text{ m}^2$

Additional area: $509.45 - 330.96$

$= 178.49 \text{ m}^2$

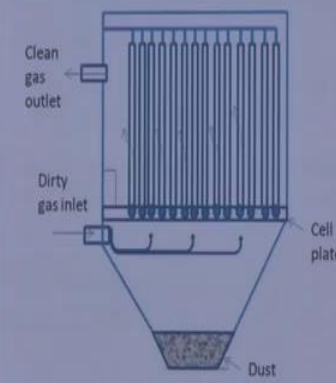
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This is one example a municipal solid waste based power plant is emitting 45,000 meter cube per hour flue gas it is proposed to install and ESP with a collection efficiency of 96.8 percent, calculate the total area of the collection electrodes if the collection efficiency is 99.5 percent, how much additional collection electrode area would be needed drift velocity of the particles has been determined experimentally at 0.13 meter per second.

So, V_p is 0.13 meter per second our Q is equal to 45 meter cube per H. So, that has to be converted to meter cube per second. So, that has been converted to meter cube per second. So, if you use the efficiency expression here. So, V_p value is given Q value is given. So, we can get the value of A_c as efficiency is given. So, first case will get the A_c is equal to 330.96 for the second case, we will getting the A_c equal to 509.45 as the efficiency changing. So, by difference of these 2 A_c is will give the additional area requirement. So, 178.449 were getting here.

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Fabric filters



The diagram illustrates a fabric filter unit. Dirty gas enters from the bottom left through a 'Dirty gas inlet'. It flows upwards through a series of vertical filter bags. Clean gas exits from the top left through a 'Clean gas outlet'. A 'Cell plate' is located at the bottom of the filter bags. Dust is collected at the bottom of the unit, labeled 'Dust'.

Salient features

- Eff – > 99.9 %;
- Particles >0.01-1 micron;
- Low pressure drop;
- Cannot operate in moist environment
- Large & Expensive;
- Competitive with ESP;
- Process temp. below 285 °C
- Woven fabric or felt cloth made of cotton, nylon, polyester, fiberglass, asbestos, etc.

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Now, we will go to discuss on fabric filters or bag filters. So, in fabric filters, dust laden gas comes in the bag filter unit and it passes through these bags and it is purified and clean gas goes out from the unit.

These have some efficiency is later greater than 99.5 percent, this is the highest efficiency of among all the devices used for the separation of the particulates from the gas, but this has low pressure drop and the fabrics are made of cotton, nylon, polyesters, fiberglass or asbestos.

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Mechanism of separation

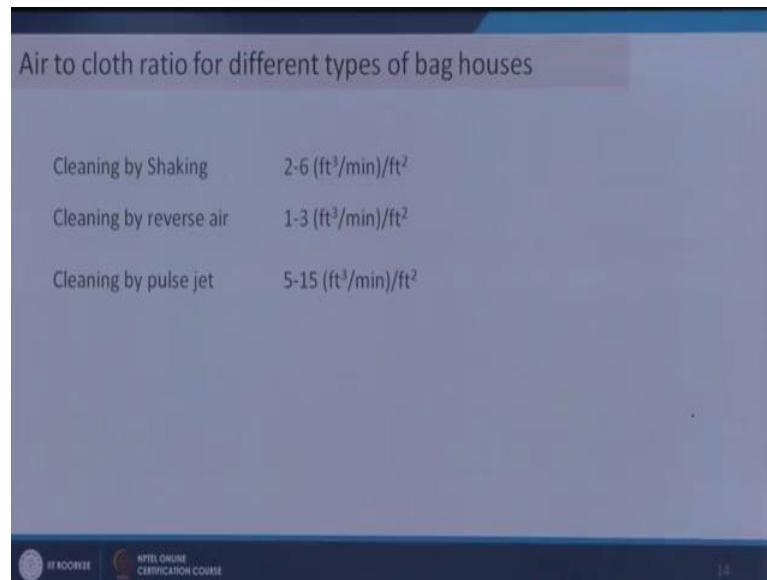
- Inertial collection - Dust particles strike the fibers placed perpendicular to the gas-flow direction instead of changing direction with the gas stream.
- Interception - Particles that do not cross the fluid streamlines come in contact with fibers because of the fiber size.
- Brownian Movement - Submicrometre particles are diffused, increasing the probability of contact between the particles and collecting surfaces.
- Electrostatic forces - The presence of an electrostatic charge on the particles and the filter can increase dust capture.

☐ Baghouses are classified by the cleaning method used. The three most common types of baghouses are mechanical shakers, reverse gas, and pulse jet

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There are 4 types of separation mechanism that is initial collection intersections Brownian movement and electrostatic forces the particles how they are separated in the bag filters or described here and in the bag house when the bag sur field with the dust on the surface of it then it needs to be cleaned.

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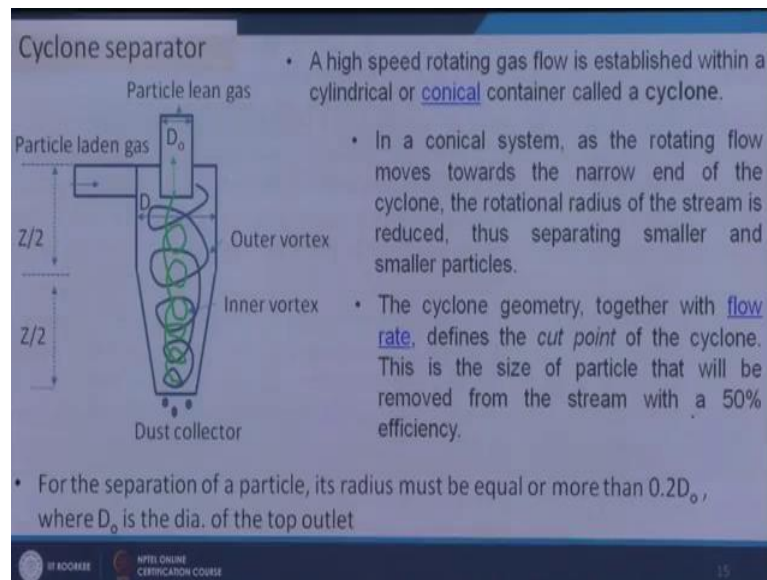


Air to cloth ratio for different types of bag houses	
Cleaning by Shaking	2-6 (ft ³ /min)/ft ²
Cleaning by reverse air	1-3 (ft ³ /min)/ft ²
Cleaning by pulse jet	5-15 (ft ³ /min)/ft ²

And so mechanical shakers reverse gas and pulse jet is used for the cleaning purpose and if you get different types of cleaning then requirement of feed cube per minute per feet square that; that means, the air to cloth ratio how much air can be cleaned by one feet square of this cloth is different. So, it is maximum for pulse jet.

So, pulse jet is the superior among these and not only this the pulse jet can also help the continuous operation of the process. So, this is the most advance advanced methods out of this 3.

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This is the cyclone separator another device which is used in this case particle laden gas is getting entry here and due to high velocity it is entering into the cyclonic on the on the cyclone shape duct. So, when it will a device. So, it will be getting some movement here that is centrifugal force will react on it and this will be and gravity will also act on it. So, this will come in this fashion and it will goes off from the top. So, very fine in particles will goes off the bigger particles will be separate it again the same mechanism the centrifugal force will give more velocity towards this. So, $m \propto r$.

So, m is more means force is more. So, bigger particles will be separated come fast to this surface and we will get separated final particles will not be able to come here and it will goes up and for the separation the condition is that the particle diameter must be more than $0.2 D_o$. So, this is the D_o or the diameter of the outlet pipe. So, this outlet pipe is having $0.2 D_o$ if the particle size is more than that then that can be separated through this cyclone.

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Force balance and characteristics equations

Centrifugal force (outward) = mV_{gr}^2/r Where m = mass of the particle
 r = radius of the particle

Drag force (inward) = $3 \pi \mu_g D_p V_r$ Where D_p = diameter of the particle
 V_r = radial component of the velocity of gas
 μ_g = viscosity of the gas

Laminar gravitational free settling velocity (V_t) = $(\rho_s - \rho_g)gD_p^2/18\mu_g$

Minimum size of particle for separation in cyclone separator

$$(D_p)_{min} = \left[\frac{3.6 A_i^2 D_o \rho_g \mu_g}{\pi Z D \rho_s G} \right]^{1/2}$$

G = mass flow rate of gas
 A_i = area of cross section of gas inlet
 D_o = is the dia. of the top outlet

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So, you have different types of forces works on the particles centrifugal force drag force and gravity force also the expressions are given here and these are the laminar gravitational free settling velocity already we have discussed this things and minimum size of particles for separation in cyclone separator what is the minimum particle size that can be separated from the separator that is that can be calculated to this empirical relationship D_p minimum is equal to $3.6 I^2 D_o \rho G \mu G \pi Z D \rho S$ and G .

This G is equal to mass flow rate of gas. So, this is the mass flow rate of gas is G and then a i area of the cross section of the gas in let again the area is of cross section there is equal to a i next is your D_o we have already explained and D and Z , we have to know. So, this is the diameter of this part the Q cylindrical part diameter is D and the cone shaped part diameter is different from this and we are having the total height is Z . So, Z by 2 is conical part and Z by 2 is the cylindrical part. So, this is the conventional design of the cyclones and if you know the value of Z , we can calculate the D_p minimum which can be separated from these cyclones if these values are known to us.

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Comparison of different PM removal equipment			
Equipment type	Typical particle size	Typical removal efficiency	Remark
Gravity settler	> 50 μm	< 50 %	Need large space, Low pressure loss
ESP	> 1 μm	> 98 %	High initial cost Sensitive to variable dust loading or flow rates
Fabric filter	> 0.01 μm	> 99 %	Filters are susceptible to chemical attack
Cyclone separator	> 5 μm	> 90 %	Inexpensive and less maintenance

Now, this is the slide which give us the comparison of the efficiency of different types of devices like gravity settler ESP fabric filer cyclone separator etcetera we is see different typical your particle size in this which can be handled by this systems and the removal efficiency is also different. So, from this it is very clear the fabric filters is having the maximum efficiency and it can remove very fine particles also, but all the processes are their advantage and disadvantage, up to these in this part of this module. So, we will discuss the rest part in the next module in the next part of this module.

Thank you very much for your patience.