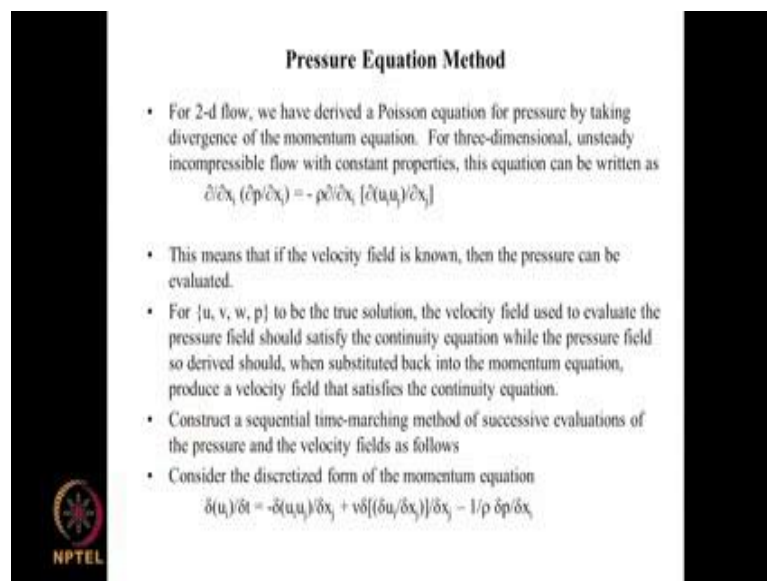


Computational Fluid Dynamics
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Lecture - 39
Artificial compressibility method, Stream function vorticity method

We have seen two methods for incompressible flows in the artificial compressibility method and the stream function vorticity method. Both of these have their own specific limitations the artificial compressibility method can be used for 3-D, but not for time dependent flows the stream function method can be used for time dependent flows, but not for 3-D. We look at pressure equation method which can be use for both 3-D and time dependent flows and, but will explain this method in a specific way and the idea again is to follow the method and work out the details at a later stage.

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Pressure Equation Method

- For 2-d flow, we have derived a Poisson equation for pressure by taking divergence of the momentum equation. For three-dimensional, unsteady incompressible flow with constant properties, this equation can be written as
$$\frac{\partial}{\partial x_i} (\rho \frac{\partial p}{\partial x_i}) = -\rho \frac{\partial}{\partial x_i} [\frac{\partial (u_i u_i)}{\partial x_i}]$$
- This means that if the velocity field is known, then the pressure can be evaluated.
- For $\{u, v, w, p\}$ to be the true solution, the velocity field used to evaluate the pressure field should satisfy the continuity equation while the pressure field so derived should, when substituted back into the momentum equation, produce a velocity field that satisfies the continuity equation.
- Construct a sequential time-marching method of successive evaluations of the pressure and the velocity fields as follows
- Consider the discretized form of the momentum equation
$$\frac{\partial (u_i)}{\partial t} = -\frac{\partial (u_i u_i)}{\partial x_j} + \nu \frac{\partial^2 (u_i)}{\partial x_j^2} - \frac{1}{\rho} \frac{\partial p}{\partial x_i}$$

So, the idea of the pressure equation method is already the germination is there in the stream function vorticity method where, we derived an equation for pressure.

So, we look at a method which is applicable both for time dependent flows and 3-Dimension flows at the same time it is not either for this or for that. In this is based on

the idea of solving an equation for pressure together with the momentum equations and how this equation for pressure is constructed we have already seen, when we discussed stream function vorticity method, in which we said that it is possible to manipulate by taking the divergence of the momentum equation we can derive an equation for pressure and that we showed how to do for 2-D flow for 3-Dimensional unsteady incompressible flow with constant properties the same Poisson equation for pressure can be written in this compact way using the index notation format it is $\frac{\partial}{\partial x_i} \left(\frac{\partial p}{\partial x_i} \right)$ in this term the index i is repeating therefore, this implies sum over the 3 values of i that it can take. So, that that makes it $\frac{\partial}{\partial x} \left(\frac{\partial p}{\partial x} \right) + \frac{\partial}{\partial y} \left(\frac{\partial p}{\partial y} \right) + \frac{\partial}{\partial z} \left(\frac{\partial p}{\partial z} \right)$.

So, that is a Laplace in of p here and on the right hand side we have minus $\rho \frac{\partial}{\partial x_i} \left(\frac{\partial}{\partial x_j} u_i u_j \right)$. So, what do we have on the right hand side density is known property and the velocity field. So, this equation here pressure equation implies as we have seen earlier that, if the velocity field is known then pressure can be evaluated. So, and we also know that for u, v, w, p to be a true solution of fluid flow then the velocity field that is u, v, w which are functions of x, y, z, t used to evaluate the pressure field should satisfy the continuity equation while the pressure field, derived when substituted back into the momentum equation should produce a velocity field that satisfies the continuity equation.

So, we would like to we would need to solve both the continuity equation and the momentum equation. So, if we are evaluating pressure from a velocity field this pressure when substituted in to the momentum equations to get a velocity field, that velocity fields should also satisfy their continuity equation. So, that kind of necessary condition is there for u, v, w, p field to be considered as a true solution of the Navier stokes equations. So, using this idea it is possible to construct sequential time marching method will see and will start with an explicit method of successive evaluations of pressure and velocity which is as follows.

So, you consider the discretized form of the momentum equation. So, we have $\frac{\partial u}{\partial t} + \frac{\partial}{\partial x_j} (u_i u_j) = \nu \frac{\partial^2 u}{\partial x^2} - \frac{1}{\rho} \frac{\partial p}{\partial x_i}$. So, that is the momentum equation you are writing this as

discretized form. So, as to distinguish it from the continuous form is using this delta here and we have taken this term on to the right hand side. So, that we have u_i by u_j equal to $\frac{\partial u_i}{\partial t}$ equal to $\frac{\partial}{\partial x_j} (u_i u_j)$ plus μ the kinematic viscosity times; $\frac{\partial}{\partial x_j} (\frac{\partial u_i}{\partial x_j})$ minus $\frac{1}{\rho} \frac{\partial p}{\partial x_i}$ these $\frac{\partial}{\partial x}$ are difference operators you could be using upwind scheme here, we could be using the centers scheme for this, you could be using central scheme or whatever other scheme that you want to put here.

So, it does not matter what it is you choose the appropriate once for the discretization operators for each of these even here you can use forward first order second order central all those kind of things can be used here, but this is the discretized form of continuity equation. Now we can write this simply as of forward differencing and write this as $u_{i,n+1} - u_{i,n}$ by Δt .

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Pressure Equation Method

- an explicit scheme of solution:

$$u_i^{n+1} - u_i^n = \Delta t [\delta \{-u_i u_j + \nu (\frac{\partial u_i}{\partial x_j}) / \delta x_j\}]^n - \Delta t / \rho (\frac{\partial p}{\partial x_i})^n$$
- Taking divergence to get

$$\frac{\partial (u_i^{n+1})}{\partial x_i} - \frac{\partial (u_i^n)}{\partial x_i} = \Delta t \delta \{[\delta \{-u_i u_j + \nu (\frac{\partial u_i}{\partial x_j}) / \delta x_j\}]^n / \delta x_i - \Delta t / \rho (\frac{\partial p}{\partial x_i})^n / \delta x_i$$
- From the computed u_i^n , we wish to evaluate p such that the u_i^{n+1} satisfies the continuity equation. Therefore, set $\frac{\partial (u_i^{n+1})}{\partial x_i} = 0$.
- Also, the velocity field at u_i^n satisfies continuity $\implies \frac{\partial (u_i^n)}{\partial x_i} = 0$
- The resulting equation can now be written as an equation for pressure:

$$1 / \rho \delta \{(\frac{\partial p}{\partial x_i})^n\} / \delta x_i = \delta \{[\delta \{-u_i u_j + \nu (\frac{\partial u_i}{\partial x_j}) / \delta x_j\}]^n\} / \delta x_i$$



If we do that then we get an explicit solution scheme of solution can be written as $u_{i,n+1} - u_{i,n}$ divided by Δt we take the Δt to this side Δt times all the right hand side terms which are evaluated at n th time step. So, this is $u_i u_j$ term $\frac{\partial}{\partial x_j}$ of $u_i u_j$ with a minus n because it is taken to the right hand side and the diffusion term

here. So, this is evaluated as at nth time step, and even the pressure gradient is evaluated at the nth time step.

So, here we are not doing any cheating we are just writing it like this. We are we are putting down a scheme of solution. So, that scheme of solution is saying that forward difference for the time derivative, and explicit differentiation as of now we are not specifying what these difference operative should be we can use for example, the up end differencing and central differencing and this will see.

So, now we take divergence of this equation. So, that is $\frac{d}{dx} u$ because i is index here. So, when we take the divergence we get $\frac{d}{dx} u_{i+1} - \frac{d}{dx} u_i$. So, every term is put as $\frac{d}{dx}$ operator is put here and Δt is a constant, $\frac{d}{dx}$ of this whole thing minus Δt divide by ρ times $\frac{d}{dx}$ of this particular term here. And in this is the modified momentum equation, and here we want to impose the idea that if we get the from the computed u_i^n that is at the previous time step values, we want to evaluate p such that if this p is substituted into the momentum equation which then we get u_{i+1}^{n+1} this u_{i+1}^{n+1} which should satisfy the continuity equation and what is a continuity equation $\frac{d}{dx} u_{i+1}^{n+1}$. So, we want to we want to a velocity field such that it is satisfies continuity equation. So, this term is 0.

We are starting we are we already have the previous times step value, the previous time step value must also satisfy the continuity equation. So, $\frac{d}{dx} u_i^n$ must also be equal to 0. So, when you look at this equation here, if you are imposed the condition that u_{i+1}^{n+1} must satisfy the bound the continuity equation then this is 0 since u_i^n satisfies the continuity equation because, you now moving on to u_{i+1}^{n+1} and by then you have already got u_i^n and for u_i^n to be correct solution it must satisfy the continuity equation. So, $\frac{d}{dx} u_i^n$ is also equal to 0.

So, if you said these things to 0 here; 0 this because this would have satisfy the continuity equation and this to 0 because we want to it satisfy the continuity equation. That gives us a condition for pressure. So, these two are 0 and we can now cancel out Δt here and will get an equation for pressure at nth time step like this.

So, this equation contains on the right hand side, velocity at the nth time step and these are also velocity set nth time steps. So, these are all explicit terms and since we have already got u_i^n and we moving on to u_i^{n+1} you use this 1 to evaluate pressure, and this pressure is at p_i^n so; that means, that $p_i^j k n$. So, we put that into this equation here. If you put that p here and then all this right hand side is known and this is known. So, from this we can get u_i^{n+1} . So, we start with u_i^n and then we get p_i^n and is substitute in this and then we get u_i^{n+1} .

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Pressure Equation Method

- an explicit scheme of solution:

$$u_i^{n+1} - u_i^n = \Delta t [\delta \{-u_i u_i + v(\delta u / \delta x_i) / \delta x_i\}_i^n - \Delta t / \rho (\delta p / \delta x_i)_i^n]$$
- Taking divergence to get

$$\partial(u_i^{n+1}) / \partial x_i - \partial(u_i^n) / \partial x_i = \Delta t \partial \{[\delta \{-u_i u_i + v(\delta u / \delta x_i) / \delta x_i\}_i^n] / \partial x_i - \Delta t / \rho \partial \{(\delta p / \delta x_i)_i^n\} / \partial x_i$$
- The resulting equation can now be written as an equation for pressure:

$$1 / \rho \partial \{(\delta p / \delta x_i)_i^n\} / \partial x_i = \partial \{[\delta \{-u_i u_i + v(\delta u / \delta x_i) / \delta x_i\}_i^n] / \partial x_i$$
- Above equation permits the evaluation of p_i^n from continuity satisfying u_i^n . This pressure field can then be used to evaluate the continuity-satisfying u_i^{n+1} . This can then be used to obtain p_i^{n+1} , and then u_i^{n+2} , p_i^{n+2} , and so on.
- Start with continuity satisfying u_i^0 , get p_i^0 and then u_i^1 and p_i^1 and so on.
- Applicable for 3-d, time-accurate flows



So, that is what is shown here. So, these equations permit evaluation of this equation here permit the evaluation of p_i^n from continuity satisfying u_i^n . So, this pressure field can be used to evaluate continuity satisfying u_i^{n+1} here. So, this can then be used to obtained p_i^{n+1} . So, once you get u_i^{n+1} you can put this on to $n+1$ here, and then get p_i^{n+1} and once you get p_i^{n+1} you can put this on to this you can get u_i^{n+2} and then you come here to get p_i^{n+2} . So, in that way you can use these 2 equations alternately, to get u_i^{n+1} here from u_i^n you first solve this to get p_i^n and then, you put that p_i^n here to get u_i^{n+1} and you put this here back to get p_i^{n+1} and then you move on like this.

So, you are satisfying the momentum equation and pressure equation which is obtained by imposing the condition that the velocity field that we getting here satisfies this. Each of these is explicit method. So, we start with a continuity satisfying u_i^0 get p_i^0 from this and then put this p_i^0 here and all the u_i zeros here and get u_i^1 and then you put u_i^1 here, and then we get p_i^1 and then move on like this. So, this method is applicable for 3-Dimensional flows and also time accurate flows and it is explicit.

So, in this way we are this method is differentiated from the two previous methods by the fact that we are solving an explicit equation for pressure, along with the velocity along with the momentum equations in the stream function vorticity method we completely eliminated pressure and it is not necessary for us to evaluate pressure in order to in order to get $u_n v$.

In fact, we need not evaluate if you are not interested in p , then we need not evaluate u and you need not evaluate p you can get u_i and v_i^{n+1} without having to compute pressure, but here we have to compute pressure, but and we are doing in in a hopscotch manner first you get get this and then you get this from initial condition. Initial condition which is in which the initial condition is such that the velocity filed satisfies the continuity equations.

So, that this is 0 here, if it does not become 0 then the initial condition does not satisfy the continuity equation it is not a true velocity boundary condition. It is not a true initial solution. So, we have we need to adjust that here. So, hopscotch we can construct this.


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Implicit Pressure Equation Method

- Implicit evaluation for pressure:

$$1/\rho^{n+1} (\delta p / \delta x_i)^{n+1} / \delta x_i = \partial / \partial x_i \{ [\delta / \delta t - u_i u_j + v (\delta u_i / \delta x_j)] / \delta x_j \}^{n+1} / \delta x_i$$
- Implicit evaluation of velocity:

$$u_i^{n+1} - u_i^n = \Delta t \{ \delta / \delta t - u_i u_j + v (\delta u_i / \delta x_j) / \delta x_j \}^{n+1} - \Delta t / \rho (\delta p / \delta x_i)^{n+1}$$
- Solve above two equations iteratively at time step (n+1) to get u_i^{n+1} and p_i^{n+1} and then move to time step (n+2)
- Applicable for 3-d, time-accurate flows



We can also construct an implicit pressure equation by the in a very similar concept. We got this equation here for the equation for pressure by writing this in as explicit form here, but we make this implicit. If you make the velocity field implicit here, then this is the equation, and we started by put in this to be equal to we made an explicit scheme like this if you make it implicit then this becomes n plus 1 and this becomes n plus 1.

So, that is what we have here, and we take divergence of that and we have this as n plus 1 this will be still be there, and this whole thing is such that we put n plus 1 here and n plus 1 here. We use a same argument that the velocity if the new velocity of u i n plus 1 must satisfy the continuity equation. So, this equal to 0 the old velocity field anyway satisfies a continuity equation. So, this anyway equal to 0 and then you have an implicit equation for pressure which is given by this thing here. So, now, if you want to evaluate pressure at n plus 1 you need to know the velocity at n plus 1, but you do not know the velocity at n plus 1 you can evaluate it only if pressure is known.

So, you have an implicit evaluation of velocity here which requires p at n plus 1 and all the values u at n plus 1. So, what we do is that we start with some guess velocity field and then we can use this to get pressure field at n plus 1. Then we put this pressure filed

here then we get new velocity field we put this back into this and then we get p^{n+1} you put this back here and then we get u^{n+1} .

So, just to evaluate the velocity and pressure field at $n+1$, we have to solve this and then we have to solve this and then go back and solve this and update, update, update we need to iteratively solve these things together to get u^{n+1} and p^{n+1} which satisfy the discretized momentum equation, the discretized implicit form of the momentum equation and discretized pressure equation derived subject to the condition that the velocity field at $n+1$ satisfies the continuity equation.

So, in this way we can solve implicitly for pressure this implicit method is differentiated from the explicit method that we have here, in which from starting from u^0 we put that here and get p^0 and we evaluate all p^0 over all i, j, k s here and then we immediately go on to this and solve this for all u^1 once u^1 at first time step and then, we come back here and then solve in 1 go the pressure at all i, j, k s and then we come back here. So, we are not solving repeatedly for u^{n+1} and p^{n+1} like that. You get this u^{n+1} immediately go on to get p^{n+1} and then you are not coming back u^{n+1} you are going u^{n+2} in this case.

Where as in the case of implicit pressure equation you are solving this for you are solving this equation here for pressure at p^{n+1} with an assumed velocity field u^{n+1} and once you get this p^{n+1} we substitute here and then we solve this to get u^{n+1} and because, now u^{n+1} exchanged the velocity pressure field also get exchanged.

So, you put this back here and then you do this you solve these iteratively together until convergence, and at that point you have p^{n+1} and u^{n+1} . So, having got in a solution for these 2 equations simultaneously then you go back and then solve for u^{n+2} and p^{n+2} again by solving these 2 iterations, these 2 equations iteratively.

So, at each time step you are moving back and forth between this equation this equation several times, until you get converge solution and then only you move on to $n+2$.

Where as in the explicit method you solve this once and then you come here and then you solve this and then you solve this, and then you solve this, you are not coming back to both the equations in the same time step you solve for 1 time step you solve it once.

So, what is a difference? This is an explicit solution this is an implicit solution. When you are looking at coupled equations and all that implicit solution is better it is more stable. So, in that sense we can have probably much larger delta ts that a possible with this than with this. That is the advantage that we get this method is also applicable for 3-D time accurate flows just as this method is, where as in the explicit method we have forced to choose very small delta ts. So, that we do not get into instability problems in the case of implicit methods we can drive this to steady state and get a steady state solution.

Just as we are if you are not interested in time accurate solution, we can take large time steps and then get to the steady state solution. So, that is 1 advantage of this. So, this pressure equation method is one which is applicable for 3-D time accurate flows. In the next lecture we look at pressure correction approach which is similar to this in some sense, but 1 particular form of the pressure equation method which is known as the semi implicit method as proved to be very robust for range of incompressible flows both external flows and internal flows, and that is a method that we look at in the next lecture for the solution of incompressible flows.

So, that method is a semi implicit method whereas here we have seen an explicit method and an implicit method in both of which we are using a pressure equation, to be solved along with the momentum equation. In the pressure correction method that we are going to look at, we are going to use a semi implicit method which is not fully implicit not fully explicit, it is a semi implicit method again we are solving some modified form of the pressure equation and momentum equations together and that is a method that will discuss in the next lecture.