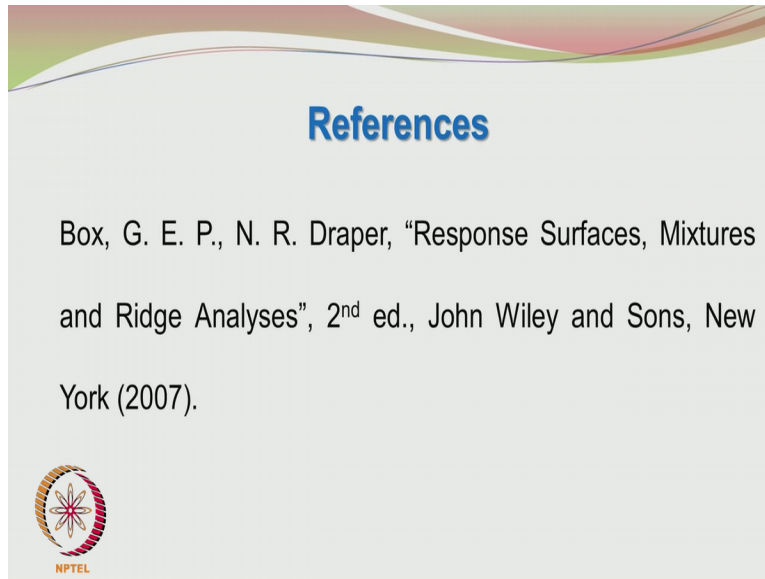


Statistics for Experimentalists
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Lecture - 44
Orthogonal Model Fitting Concepts - Part A

Hello, in this lecture 28, we will be looking at concepts pertaining to orthogonal models.

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The references are given in the current slide and the slide to follow. The first book is by Box and Draper, Responses Surfaces, Mixtures and Ridge Analyses, it is slightly advanced book for people who want to deepen their understanding and knowledge on the subject may refer to this book.

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References for Linear Regression, RSM and CCD

Meyers, R. H., D. C. Montgomery, C. M. Anderson-Cook, “
Response Surface Methodology – Process and Product
Optimization Using Designed Experiments”, 3rd ed., John
Wiley and Sons, New York (2009).



The other book where this slide material is mainly based upon is the one written by Meyers, Montgomery, Anderson-Cook, the title of the book is Response Surface Methodology Process and Product Optimization Using Designed Experiments, 3rd edition, John Wiley and Sons, published in 2009. This is an excellent book, where the concepts are explained in a very clear manner, it is not very mathematically regress, so people with the basic knowledge in linear algebra should be able to follow the material given in this book quite easily.

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References

Montgomery, D. C., “Design and Analysis of Experiments”, 7th
ed., John Wiley and Sons, New York (2010).



And of course the other book is the book written by Montgomery Design and Analysis of Experiments, 7th edition, John Wiley and Sons, New York 2010.

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References

Kutner, M. H., C. J. Nachtsheim, J. Neter "Applied Linear Regression Models", 4th ed., McGraw Hill, Singapore (2004).

Draper, N., H. Smith, "Applied Regression Analysis", 3rd ed., John Wiley and Sons, New York (1998).



Other few references are by Kutner, Nachtsheim and Neter, Applied Linear Regression Models. And Draper and Smith Applied Regression Analysis. So there are quite a few interesting books written on this subject.

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Orthogonal Designs

An orthogonal design involves an X matrix viz. **X**. It comprises of vectors that relate directly to the model factors

i.e.

A, B, ..., AB, ..., A², B², ... OR

1 $x_1, x_2, \dots, x_1 x_2, \dots, x_1^2, x_2^2, \dots$ etc.




Now let us come to orthogonal designs. What is an orthogonal design? An orthogonal design involves a matrix X, and it comprises of vectors that relate directly to the model factors. So if your model is having the contribution from factor A, factor B, interaction AB, A squared, B squared, then the model will look something like this, it will have 1 $x_1, x_2, x_1 x_2, x_1^2, x_2^2, \dots$ etc. these are all column vectors.

So when you enter the model in the matrix form, the first column could be the matrix of 1's, the second column would be the values corresponding to the settings of factor x_1 , similarly, the settings of factor x_2 , and then settings corresponding to $x_1 x_2$, then x_1 squared, x_2 square etc. depending upon the complexity and length of the model.

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Orthogonal Designs

Here **1** refers to the vector of ones, while x_i refers to the single factors, $x_i x_j$ refers to the interaction between factors and x_i^2 refers to higher order quadratic terms that more completely account for curvature.




So here 1 refers to the vectors of 1's, and x_i refers to the single factors, $x_i x_j$ refers to the interaction between factors, and x_i square refers to higher order quadratic terms that more completely account for the curvature.

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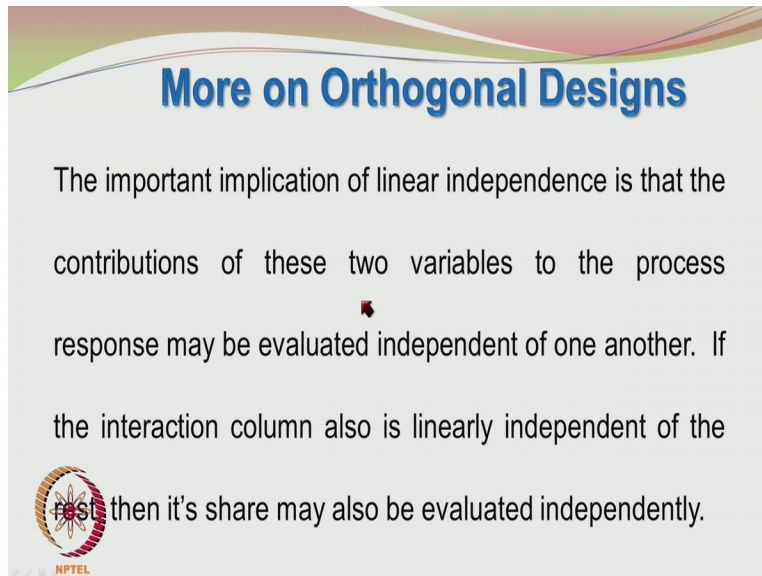
More on Orthogonal Designs

If two columns of the design matrix are orthogonal it implies that the levels of the these two variables are **linearly independent**.




Now if 2 columns of the design matrix are orthogonal, it implies that the levels of these 2 variables are linearly independent.

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More on Orthogonal Designs

The important implication of linear independence is that the contributions of these two variables to the process response may be evaluated independent of one another. If the interaction column also is linearly independent of the rest, then its share may also be evaluated independently.

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The important implication of linear independence is that the contributions of these 2 variables to the process response may be evaluated independent of one another, if the interaction column is also linearly independent of the rest then its share may also be evaluated independently. So this is a very useful concept in regression analysis and design of experiments, in planned design of experiments the way the experimental points are set, it makes the design orthogonal in nature.

So we can say that the factor A contributes to the model independent of how factor B is contributing to the model. Similarly, even if you have interaction AB in an orthogonal design, AB contributes to the model independent of how A and B contribute to the model, because the column vectors in the matrix are linearly independent of one another. So this is a very beautiful concept, what I am trying to say here is suppose you will have a model.

And in the model you say that the \hat{Y} or Y predicted = $\hat{\beta}_0 + \hat{\beta}_1 x_1 + \hat{\beta}_2 x_2$, then you will find the coefficients $\hat{\beta}_1$ and $\hat{\beta}_2$. Suppose you for some reason decide to omit the factor A altogether in the orthogonal design, then your model will be $\hat{\beta}_0 + \hat{\beta}_2 x_2$, the value of $\hat{\beta}_2$ will be same as it was in the previous full model. So let me go to the board and explain what I mean by that.

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$$\hat{Y} = \hat{\beta}_0 + \hat{\beta}_1 X_1 + \hat{\beta}_2 X_2$$
$$\hat{Y}_{\text{new}} = \hat{\beta}_0 + \hat{\beta}_2 X_2$$

Orthogonal Design

Suppose you have an existing model okay, so this is the existing model and you want to try a new model where you put only $\hat{\beta}_0 + \hat{\beta}_2 X_2$, you do not have the contribution from $\hat{\beta}_1 X_1$, then you will find that the parameters $\hat{\beta}_2$ in this old model is = the parameter $\hat{\beta}_2$ in the new model, this is because of the orthogonal design. So the contribution of factor X_1 and the contribution of factor X_2 are evaluated independent of each other.

Their contribution is independent of each other to the observed response, this is only true in the case of orthogonal design, so you can see the advantages of this. We have already seen examples of the orthogonal design in our examples set on regression analysis.

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1	x_1	x_2	$x_1 x_2$	x_1^2	x_2^2
1	-1	-1	1	1	1
1	-1	1	-1	1	1
1	1	-1	-1	1	1
1	1	1	1	1	1

Model **Greedy Model**

$$\hat{Y} = \hat{\beta}_0 + \hat{\beta}_1 x_1 + \hat{\beta}_2 x_2 + \hat{\beta}_{12} x_1 x_2 + \hat{\beta}_{11} x_1^2 + \hat{\beta}_{22} x_2^2$$

So let us look at the X matrix and you can see that this is 2 power 2 design, this is the column vector of 1's, this would be the settings corresponding to factor 1 -1, -1, 1 1. This would be the settings corresponding to factor 2 -1, +1, -1, +1. And you will have $x_1 x_2$ and that would be product of these 2 columns -1*-1 would be +1, -1*1 would be -1, 1*-1 is -1, 1*1 is 1, x_1 squared is obtained by squaring these terms in this column, x_2 squared is obtained by squaring these terms in this column okay.

So we are having essentially 1, 2, 3, 4 columns, and we also have the additional column shown in red x_1 squared and x_2 square. Let us now develop the model $\hat{Y} = \hat{\beta}_0 + \hat{\beta}_1 x_1 + \hat{\beta}_2 x_2 + \hat{\beta}_{12} x_1 x_2$, you can see that the green colored model is having 1, 2, 3, 4 parameters, and that would be the maximum number of parameters which can be estimated from this design, because you are having only 4 independent settings.

And so the maximum number of parameters would be 4, but if you have a greedy model and you also try to evaluate the additional terms like $\hat{\beta}_{11}$ and $\hat{\beta}_{22}$, then can you run into trouble because you do not have 6 independent settings to obtain these 6 parameters.

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$X =$ $\begin{bmatrix} 1 & -1 & -1 & 1 \\ 1 & -1 & 1 & -1 \\ 1 & 1 & -1 & -1 \\ 1 & 1 & 1 & 1 \end{bmatrix}$ Rank of $X = 4$	$X^T X =$ $\begin{bmatrix} 4 & 0 & 0 & 0 \\ 0 & 4 & 0 & 0 \\ 0 & 0 & 4 & 0 \\ 0 & 0 & 0 & 4 \end{bmatrix}$
--	---


Diagonal Matrix:
 Columns of X are
 mutually orthogonal

$X =$ $\begin{bmatrix} 1 & -1 & -1 & 1 & 1 & 1 \\ 1 & -1 & 1 & -1 & 1 & 1 \\ 1 & 1 & -1 & -1 & 1 & 1 \\ 1 & 1 & 1 & 1 & 1 & 1 \end{bmatrix}$  Rank of X is still 4	$X^T X =$ $\begin{bmatrix} 4 & 0 & 0 & 0 & 4 & 4 \\ 0 & 4 & 0 & 0 & 0 & 0 \\ 0 & 0 & 4 & 0 & 0 & 0 \\ 0 & 0 & 0 & 4 & 0 & 0 \\ 4 & 0 & 0 & 0 & 4 & 4 \\ 4 & 0 & 0 & 0 & 4 & 4 \end{bmatrix}$
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Now let us look at the X matrix, this is X matrix again exactly same as the X matrix corresponding to the green colored vectors. So the rank of this X matrix=4, and X prime X would be taking transpose of the X matrix and multiplying the transpose with X matrix again, you will get a diagonal matrix having 4 along the diagonals. And when you look at the matrix which is made up of the entries corresponding to x_1 squared and x_2 squared.

Then you have in addition to the old X matrix also these 2 additional columns of 1's, and of course you can see that this x_1 squared is exactly same as the vectors of 1's, x_2 squared also replica of the vector of 1's. Now when you look at this augmented matrix X , the rank of X is still 4, and when you look at the X prime X you get a matrix as shown here, and the problem is we run into trouble when we take the inverse for this particular matrix.

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$$X^*X = \begin{bmatrix} 4 & 0 & 0 & 0 \\ 0 & 4 & 0 & 0 \\ 0 & 0 & 4 & 0 \\ 0 & 0 & 0 & 4 \end{bmatrix}$$

$$(X^*X)^{-1} = \begin{bmatrix} 0.25 & 0 & 0 & 0 \\ 0 & 0.25 & 0 & 0 \\ 0 & 0 & 0.25 & 0 \\ 0 & 0 & 0 & 0.25 \end{bmatrix}$$

$$X^*X = \begin{bmatrix} 4 & 0 & 0 & 0 & 4 & 4 \\ 0 & 4 & 0 & 0 & 0 & 0 \\ 0 & 0 & 4 & 0 & 0 & 0 \\ 0 & 0 & 0 & 4 & 0 & 0 \\ 0 & 0 & 0 & 0 & 4 & 4 \\ 0 & 0 & 0 & 0 & 4 & 4 \end{bmatrix}$$

Inverse of X^*X is NOT defined

So you have X^*X inverse, for this case has $1/4$, $1/4$, $1/4$, $1/4$ along the diagonals, there is no problem in evaluating this particular matrix. But if you try to take the inverse of this X^*X matrix as given here then you will find that it is not defined, so what I am trying to say here is do not try to expand the scope of your model when the number of independent settings in the model is limited.

In the current case of a 2^2 design, we had only 4 independent settings and so we could estimate only 4 independent parameters, and the moment we try to increase the scope of the model by adding the quadratic terms, then we found that we cannot estimate the parameters because the X^*X inverse matrix was not defined in such a situation.

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In an orthogonal design

$$\mathbf{x}_i' \mathbf{x}_j = 0$$

for any column $i \neq j$

If \mathbf{x}_i' is given by $[1 \ 1 \ 1 \ 1]$ and

\mathbf{x}_j is $\begin{bmatrix} -1 \\ -1 \\ 1 \\ 1 \end{bmatrix}$ it may be easily shown that $\mathbf{x}_i' \mathbf{x}_j = 0$



So what is an orthogonal design if you take the transpose of any vector and then multiply the transpose with the another vector a different one, suppose I am taking the i th column vector take a transpose of i th column vector, then I pre-multiply the transpose of the i th column vector against the column vector \mathbf{x}_j $i \neq j$ I will get 0. So if you take this particular case, if I take the transpose of this it will be a 1 row by 4 column vector a transpose of a vector, and that would be 1, 1, 1, 1 horizontally.

And then I multiply this with the column vector here -1, -1, 1, 1, I will find that it will be a -1, -1, -2, +1, +1, +2, so -2+2 will become 0. The same concept applies for any binary combinations of vectors 1 being a transpose and another being the regular column vector, if I multiply that too, I will get 0. So this is the property of the orthogonal design, the important precautions you should take is that you should not take $i=j$. Then the negative and positive elements would be squared, and all of them would be positive and the sum will $\neq 0$.

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First Order Orthogonal Designs

In first order designs (say 2^k factorial design) keeping the levels at the extremes of ± 1 enables the variance associated with the following predicted model's coefficients a minimum.

$$\hat{\beta}_1 \hat{\beta}_2 \dots \hat{\beta}_k$$



Now let us look at first order orthogonal designs, let us take care 2^k factorial designs where k is the number of factors keeping the levels at the extremes of $+1$ or -1 enables the variance associated with the predicted model's coefficients at a minimum. So this is another advantage of factorial design, we are keeping the design settings at the extremes $-1, +1, -1, -1, +1, -1, +1, +1$. So we are having a design space the experimental settings are kept at the extreme ends, and this helps to minimize the variance of the estimated parameters.

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First Order Orthogonal Designs

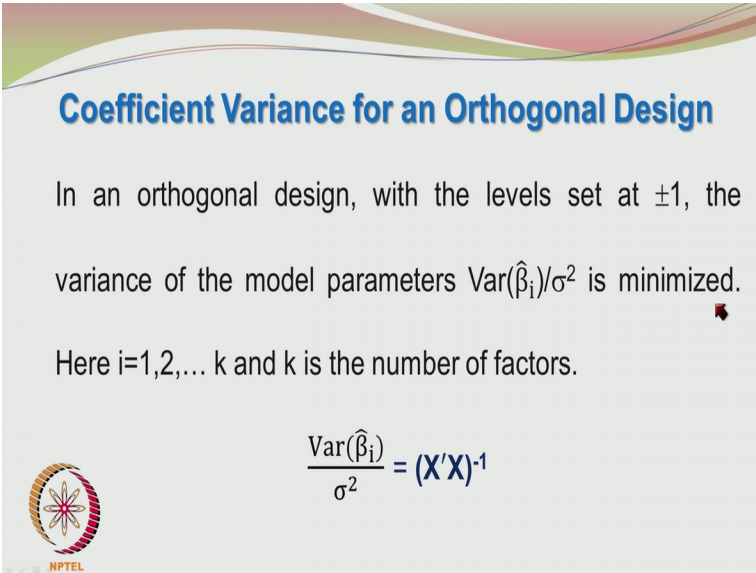
- ❖ The question that arises naturally is how the proposed model coefficients are predicted in a 2^k design.
- ❖ There are two approaches viz. the DOE approach and the regression approach.



So the question that arises naturally is suppose you have an orthogonal design, how do you go about estimating the parameters. Well you can do it in 2 ways, 1 you can use the regular design

of experiments approach, and estimate the effects and then the model positions, or you can use the matrix approach in linear regression.


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Coefficient Variance for an Orthogonal Design

In an orthogonal design, with the levels set at ± 1 , the variance of the model parameters $\text{Var}(\hat{\beta}_i)/\sigma^2$ is minimized.

Here $i=1,2,\dots,k$ and k is the number of factors.

$$\frac{\text{Var}(\hat{\beta}_i)}{\sigma^2} = (\mathbf{X}'\mathbf{X})^{-1}$$


So as I said earlier in an orthogonal design with levels set at + or -1 the variance of the model parameters variance of beta hat i/sigma square is minimized. Here, $i = 1, 2, \dots, k$, and k is the number of factors, here obviously you are not including that intercept beta hat 0, and if you can include that also you will have $k+1$ which =P number of parameters.

The variance of the predicted coefficient is given by the variance of beta hat i and that you scale it by sigma squared you will get the variance covariance matrix $\mathbf{X}'\mathbf{X}$ inverse. So this $\mathbf{X}'\mathbf{X}$ and the $\mathbf{X}'\mathbf{X}$ inverse matrix are very, very important.

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Coefficient Variance for an Orthogonal Design

For an orthogonal design we know that $(X'X)^{-1}$ is a diagonal matrix (an off diagonal elements as zero) and setting the X vectors at the extremes (± 1) minimizes the estimated parameter variance.



And for an orthogonal design, we know that the X prime X inverse is a diagonal matrix with the off diagonal elements are 0, and setting the X vector at the extremes minimize the estimated parameter variance. So we have already seen that for an orthogonal designed such as the one we considered previously, this is an orthogonal design that 2 power 2 design, and you can see that the X prime X matrix is a diagonal matrix.

And the X prime X inverse matrix is also diagonal matrix at $1/4, 1/4, 1/4, 1/4$, so this arrangement minimizes the variance of the estimated regression coefficients.

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Implications of different models

$$X = \begin{matrix} & 1 & x_1 & x_2 & x_3 \\ \begin{matrix} 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \end{matrix} & \begin{bmatrix} 1 & 1 & -1 & -1 \\ 1 & 1 & -1 & -1 \\ 1 & -1 & 1 & -1 \\ 1 & -1 & 1 & -1 \\ 1 & -1 & -1 & 1 \\ 1 & -1 & -1 & 1 \\ 1 & 1 & 1 & 1 \\ 1 & 1 & 1 & 1 \\ 1 & 1 & 1 & 1 \end{bmatrix} \end{matrix}$$



Half fraction i.e. a 2^{3-1}
model with repeats

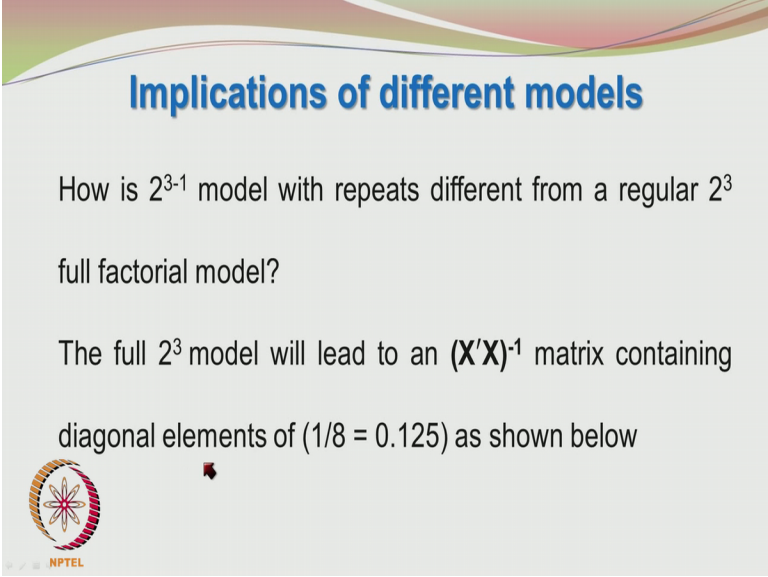
$$X = \begin{matrix} & 1 & x_1 & x_2 & x_3 \\ \begin{matrix} 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \end{matrix} & \begin{bmatrix} -1 & 1 & 1 \\ 1 & -1 & 1 \\ 1 & 1 & -1 \\ 1 & 1 & -1 \\ 1 & -1 & -1 \\ 1 & -1 & -1 \\ 1 & -1 & -1 \\ 1 & 1 & 1 \\ 1 & 1 & 1 \end{bmatrix} \end{matrix}$$

Regular 2^3 full factorial
model

Now let us look at the implications of different models. So the first model we are considering on the left hand side is a half fraction of 2^3 design that means we should be having 4 runs only, but it is clear that we are having 8 runs here, the reason for that is quite simple we are repeating the 4 experiments of a 2^3 design. So you can see that the first 2 rows are identical, the 3rd and 4th rows are identical, the 5th and 6th rows are identical and the 7th and 8th cross are identical.

That means each experimental setting in the 2^3 design is repeated. We also look at the regular 2^3 full factorial model, here you have all the possible settings for a 2^3 factorial design, and the main thing to notice is there are no repeats. On the other hand, for 2^3 design you had repeats, but on the other hand you would not have the full set, you do not have the full set of independent settings possible.


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Implications of different models

How is 2^{3-1} model with repeats different from a regular 2^3 full factorial model?

The full 2^3 model will lead to an $(X'X)^{-1}$ matrix containing diagonal elements of $(1/8 = 0.125)$ as shown below



So when you look at the 2^3 full design it will lead to an $X'X$ inverse matrix containing diagonal elements of $1/8$ which $=0.125$.

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Implications of different models


Full 2^3 factorial

$X =$

1	-1	1	1
1	1	-1	1
1	1	1	-1
1	-1	-1	1
1	1	-1	-1
1	-1	1	-1
1	-1	-1	-1
1	1	1	1

$(X'X)^{-1} =$

0.1250	0	0	0
0	0.1250	0	0
0	0	0.1250	0
0	0	0	0.1250




So you are having an X matrix corresponding to a full 2 power 3 design, if I take X prime X inverse matrix which is the straight forward think to do by now, I will get I think 1/8, 1/8, 1/8, 1/8 along the diagonals, and off diagonal terms would not be present.

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Implications of different models

The 2^{3-1} design strategy involving repeats enables the finding of the error mean square. However, the model cannot detect lack of fit as the only allowed coefficients are those which prefix to x_1, x_2, x_3 and of course the intercept coefficient viz. $\hat{\beta}_0$.

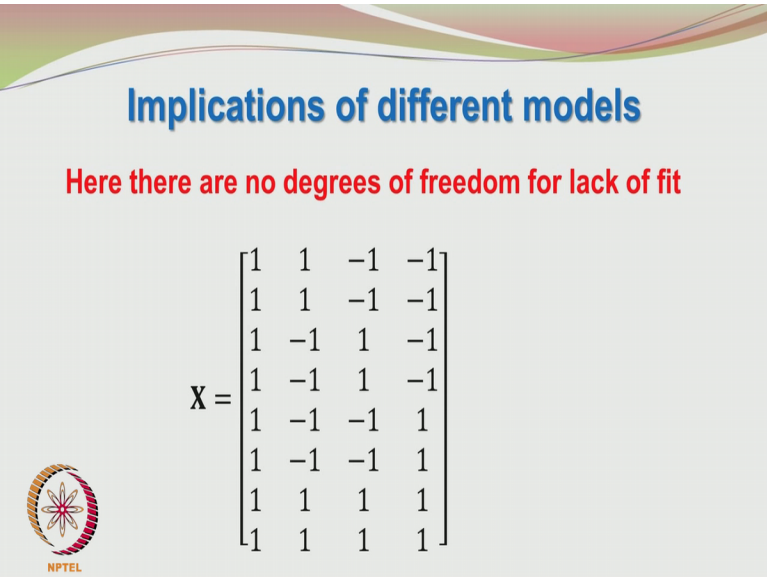


Right, but what is the advantage of here 2 power 3-1 design? Why do we have to go for 2 power 3-1 design? May be performing 2 power 3 full design was expensive, so the experimenter decided to go for 2 power 3-1 design. On the other hand, he still conducted the 8 experiments the same number as a full 2 power 3 design, so the experimenter was more focusing on the estimation of the pure error.

He probably had some insight into the model based on previous experience, and so instead of wasting time and resources and doing the complete set, he probably wanted to get more information on the pure error term. So a 2 power 3-1 design strategy will unfortunately not enable you to find the full set of parameters that are possible from a full 2 power 3 design, a 2 power 3 design has 8 independent settings and so you should be theoretically able to estimate 8 parameters of the model, so you can build your model up to 8 parameters.

However, for 2 power 3-1 design you are having only 4 independent settings, and so you will be able to estimate only 4 parameters. So you are losing the ability to estimate 4 parameters, and so your 2 power 3-1 design strategy will not have any degree of freedom for lack of fit, if you estimate the 4 parameters. But on the other hand, if you look at the 2 power 3 design and you are estimating only 4 or 5 parameters, then you have sufficient degrees of freedom to test your model for lack of fit.


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Implications of different models

Here there are no degrees of freedom for lack of fit

$$X = \begin{bmatrix} 1 & 1 & -1 & -1 \\ 1 & 1 & -1 & -1 \\ 1 & -1 & 1 & -1 \\ 1 & -1 & 1 & -1 \\ 1 & -1 & -1 & 1 \\ 1 & -1 & -1 & 1 \\ 1 & 1 & 1 & 1 \\ 1 & 1 & 1 & 1 \end{bmatrix}$$

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So when you look at the 2 power 3-1 design where each design setting is repeated you do not do the full design you do only half the complete design but you do repeats. So in this if you are estimating 4 parameters since there are only 4 independent settings, you do not have any degrees of freedom for testing the lack of fit.

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Implications of different models

In the full 2^3 design, in addition to the intercept coefficient viz. $\hat{\beta}_0$ seven other coefficients may be detected. These are the coefficients corresponding to

$$\hat{\beta}_1, \hat{\beta}_2, \hat{\beta}_3, \hat{\beta}_{ij(i \neq j)}, \hat{\beta}_{123}$$



So in the full 2^3 design, in addition to the intercept coefficient namely β_0 , 7 other coefficients may be detected these are the coefficients corresponding to the main factors $\beta_1, \beta_2, \beta_3$, and then you can also look at the interactions between the 2 factors $\beta_{ij} \ i \neq j$, and then ternary interaction term $\beta_{1, 2, 3}$. So you can estimate the main effects, and you can estimate the binary interactions and you can also estimate the ternary interaction between the factors. So these are the 8 coefficients including β_0 .

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Implications of different models

Hence, if a model is fitted with only the main factors, then the ANOVA table indicates 4 degrees of freedom for lack of fit. However, this model does not have estimate of mean square error as there are no repeats in the considered



And if you are fitting a model with only the main factors that out means out of the 8 possible parameters you are estimating only 4 β_0 , and then the regression coefficient corresponding to factor A, regression coefficient corresponding to factor B, regression coefficient

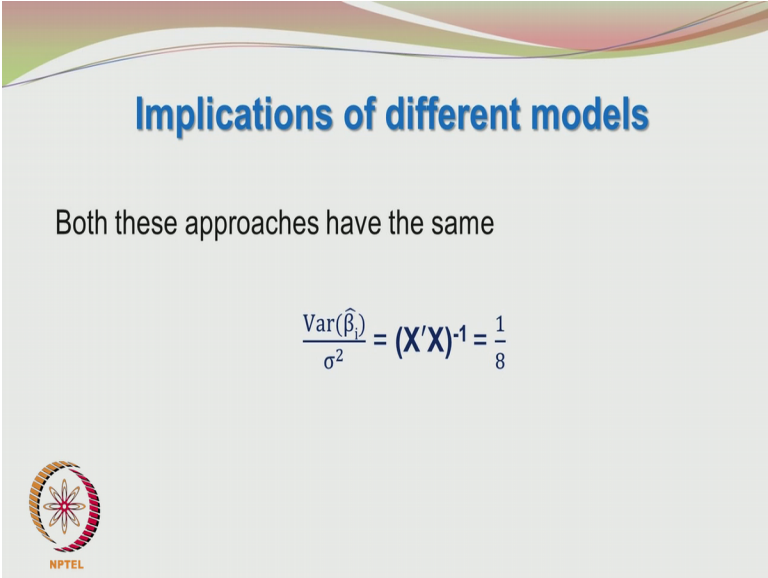
corresponding to factor C that would make it as only 4 parameters. And in such a case that our table indicates 4 degrees of freedom for lack of fit.

So $8-4=4$, 8 parameters are maximum possible but you have estimated only 4, so you have $8-4=4$ degrees of freedom for testing the lack of fit. But what is the drawback in the full 2^3 model you exhausted all the settings all independent settings have been exhausted, and that consumed all the full 8 runs, so you are not in a position to repeat your experimental settings. Suppose your management says that fine you can do a maximum of 8 experiments.

So one group proposes a 2^{3-1} designs with repeats, on the other hand there is another group which goes in for a full 2^3 model, on one hand the group which proposed 2^{3-1} design will have an estimate of the pure error but it not be able to estimate all the interactions including the ternary interaction. Whereas the group which went in for a 2^3 design will not be able to get an idea on the pure error.


And on the other hand, it would be able to estimate as many as 8 parameters. So which model is good that depends upon the process and the prior knowledge on the process you have.

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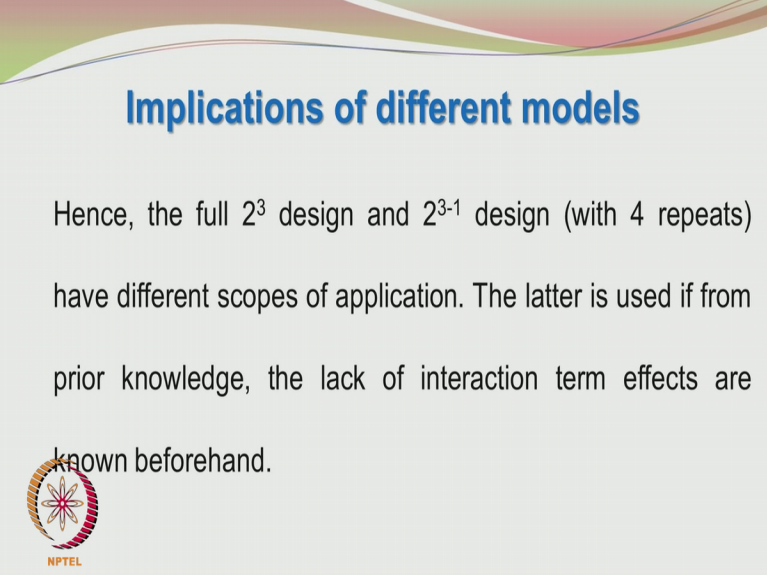
Implications of different models

Both these approaches have the same

$$\frac{\text{Var}(\hat{\beta}_i)}{\sigma^2} = (\mathbf{X}'\mathbf{X})^{-1} = \frac{1}{8}$$



So when you look at the 2 approaches, they have the same variance of $\hat{\beta}_i / \sigma^2$, because the $\mathbf{X}'\mathbf{X}$ inverse matrix is same in both the cases, and that is actually $1/8$.

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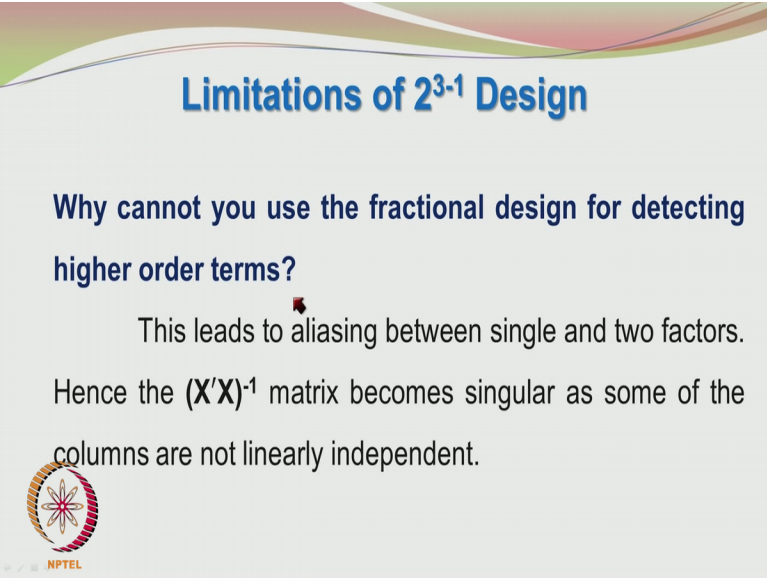
Implications of different models

Hence, the full 2^3 design and 2^{3-1} design (with 4 repeats) have different scopes of application. The latter is used if from prior knowledge, the lack of interaction term effects are known beforehand.



So the 2^3 and 2^{3-1} design with 4 repeats have different scopes of application, the latter is used the 2^{3-1} design is used if you have prior knowledge or experience that the lack of interaction term effects are known beforehand, so you know previously that there is no interaction between the factors of your model, so the interaction terms are neglected. And if the binary interaction terms are neglected, then there is even a very little chance the ternary interactions would kick in.


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Limitations of 2^{3-1} Design

Why cannot you use the fractional design for detecting higher order terms?

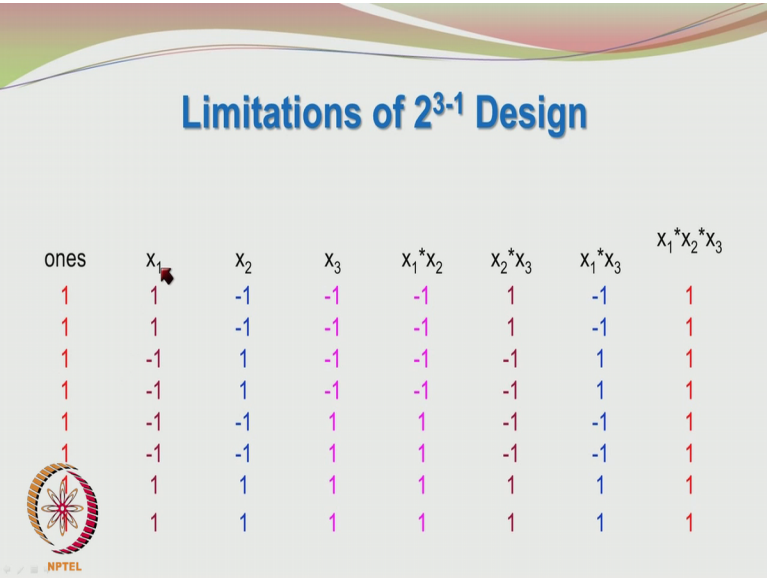
This leads to aliasing between single and two factors. Hence the $(X'X)^{-1}$ matrix becomes singular as some of the columns are not linearly independent.



So let us expand on this topic a bit more the query is, why cannot you use the fractional design for detecting higher order terms? So the main problem is there is aliasing between single and 2

factors, and the X' inverse matrix becomes singular as some of the columns are not linearly independent.

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ones	X_1	X_2	X_3	$X_1 * X_2$	$X_2 * X_3$	$X_1 * X_3$	$X_1 * X_2 * X_3$
1	1	-1	-1	-1	1	-1	1
1	1	-1	-1	-1	1	-1	1
1	-1	1	-1	-1	-1	1	1
1	-1	1	-1	-1	-1	1	1
1	-1	-1	1	1	-1	-1	1
1	-1	-1	1	1	-1	-1	1
1	1	1	1	1	1	1	1
1	1	1	1	1	1	1	1

So let us look at 2^{3-1} design, so you have the 1's, you have the settings corresponding to factor 1, settings corresponding to factor 2 and settings corresponding to factor 3. So obviously the runs are repeated so you are doing 8 runs, but you have only 4 independent settings. Now I can estimate only the intercept β_0 , β_1 , β_2 and β_3 , suppose I am trying to estimate the interaction also.

If I do $X_1 X_2$ to bring in that interaction effect into that model unfortunately, this $X_1 X_2$ column vector will be exactly identical to the X_3 column vector. Similarly, $X_2 X_3$ column vector which is the second binary interaction would be identical with the X_1 column vector, and you can figure out that $X_1 X_3$ column vector would be identical with X_2 column vector, and $X_1 X_2 X_3$ is aliasing with the column vector of 1's.

So this X matrix made up of all these elements is definitely going to have a lower rank, and the inverse of the X' matrix will lead to difficulties, it cannot be estimated, because the columns in the design are not linearly independent of each other.

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Orthogonal Term involving Higher Order Terms

Construct an orthogonal design involving one-half fraction of a 2^5 factorial design. This involves 16 runs.

What are the terms in the model that may be fitted using the given design?



Now let us look at the orthogonal design involving an experimental scheme with as many as 5 factors. So let us construct an orthogonal design involving one-half fraction of 2^5 factorial design, the full factorial design will involve $2^5 = 32$ runs, obviously this is too many, so we want to restrict the number of runs. So we are going for a 2^{5-1} factorial design which is one-half fraction of a full 2^5 design and so we have 16 runs. So what are the terms in the model that may be fitted using the given design?

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Orthogonal Term involving Higher Order Terms

One intercept, 5 first order coefficients, 10 binary interactions, no ternary interaction (among $5C_3 = 10$ ternary interactions), no quaternary interaction coefficients among $5C_4 = 5$ possible ones, no 5-factor coefficient (among one possible).

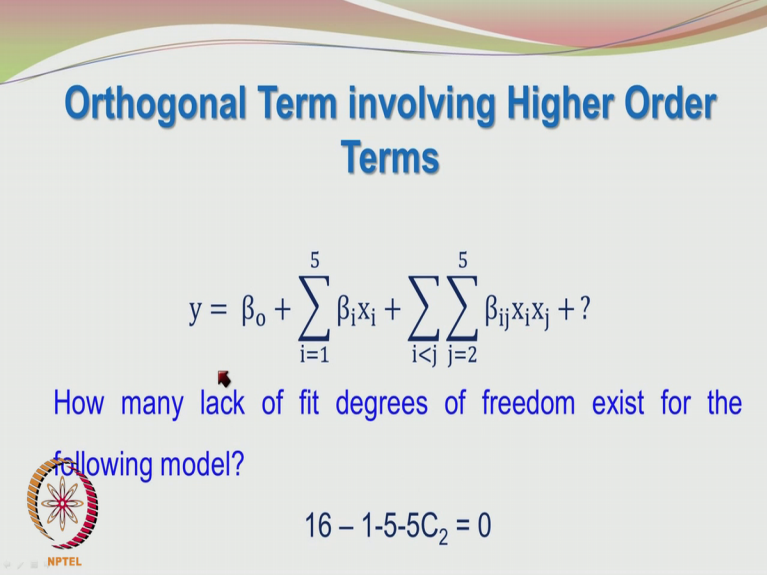


When we consider the 2^5 design we have 1 intercept, 5 first order coefficients, 5 main factors, 10 binary interactions, and then you have again 10 ternary interactions, and 5 quaternary interactions and 1 5 factor interaction. So this is the complete set in a model, where we consider

only the main effects and the interaction between the factors. So that would be a total of $1+5=6$, $6+10=16$, $16+10=26$, $26+5=31+1=32$.

So in a full 2^5 design involving 32 independent settings, you would have been in a position to estimate the constant β_0 , the 5 main factors, 10 binary interactions, 10 ternary interactions, 5 quaternary interactions and one 5 factor interaction. But we are having only 16 independent settings and so. If we are going sequentially in the model development, we have possible the estimation of 1 intercept, 5 first order coefficient that makes it 6, and 10 binary interactions that makes it 16, beyond it we cannot estimate any more parameters.

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Orthogonal Term involving Higher Order Terms

$$y = \beta_0 + \sum_{i=1}^5 \beta_i x_i + \sum_{i < j} \sum_{j=2}^5 \beta_{ij} x_i x_j + ?$$

How many lack of fit degrees of freedom exist for the following model?

$16 - 1 - 5 - 5C_2 = 0$

NPTL

So when you have such a case 2^{5-1} design, and you have estimated the intercept, the main factors and the binary interaction, what would be the lack of fit degrees of freedom? Since you have exhausted all the 16 independent settings to estimate the parameters associated with these terms, the lack of fit degrees of freedom would be 0.

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Orthogonal Term involving Higher Order Terms

Show that the design is indeed orthogonal not only with respect to main factors but also with all the associated interactions.

It may be seen that the conditions of orthogonality do indeed apply. Any inner product of any two column vectors (that are not from identical columns) is indeed zero.



And the next query is quite simple, show that the design is indeed orthogonal not only with respect to main factors but also with the associated interactions. This is a very straightforward thing to do, you can write down the X matrix, you can first write the vector of 1's corresponding to the 16 experiments, and then you can write the half fraction design, so you write the full factorial for a 2 power 4 design.

And then we know from our concepts of fractional factorial design, how to accommodate for 5th factor, let us say the 5th factor is factor E, then to set up the column of factor E, we have to use the design generator $I=ABCDE$ or $E=ABCD$. I request you to refresh these concepts, and you can write down the X matrix corresponding to a 2 power 5-1 fractional factorial design. And once you have written down this matrix.

And you have also included the possible binary interactions in the X matrix, you can see that they are comprising of number of columns, these columns are having a set of -1 and +1 values, except the first column which is the matrix of 1's which will have all elements as 1, the other columns would be having a mixture of +1's and -1's, and if you take any 2 columns you take the transpose of the first column and then you multiply that with the other column vector, you will get it as 0.


So any inner product of any 2 column vector that are not from identical columns is indeed 0 that can be easily shown.

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Orthogonal Term involving Higher Order Terms

Is there any aliasing in this design?

No, all the columns are independent of each other and hence the experimental levels may be varied independent of each other.




And is there any aliasing in this design? No, all the columns are independent of each other and hence the experimental levels may be varied independent of each other, there is no aliasing in this 2 power 5-1 design. As long as you restrict yourself to the constant, the main factors and the binary interactions. The moment you go for ternary interactions or quaternary interactions then there would be aliasing.

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Orthogonal Term involving Higher Order Terms

$$y = \beta_0 + \sum_{i=1}^5 \beta_i x_i + \sum_{i < j} \sum_{j=2}^5 \beta_{ij} x_i x_j + ?$$

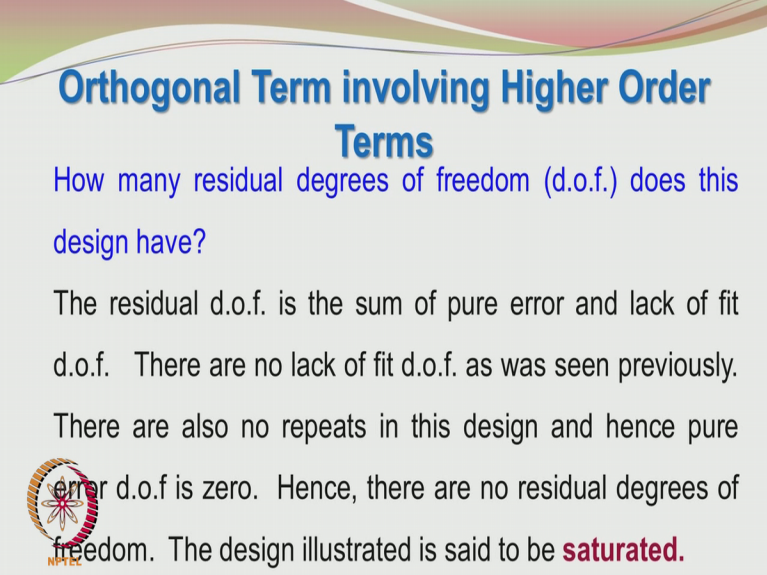
How many lack of fit degrees of freedom exist for the following model?



$$16 - 1 - 5 - 5C_2 = 0$$

So up to this model you are not going to have the dangerous aliasing, because you can estimate the parameters from different experimental settings.

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Orthogonal Term involving Higher Order Terms

How many residual degrees of freedom (d.o.f.) does this design have?

The residual d.o.f. is the sum of pure error and lack of fit d.o.f. There are no lack of fit d.o.f. as was seen previously.

There are also no repeats in this design and hence pure error d.o.f is zero. Hence, there are no residual degrees of freedom. The design illustrated is said to be **saturated**.

And how many residual degrees of freedom does this design have? If you have utilized all the 16 independent settings to find 16 model parameters, the residual degrees of freedom would be 0, the lack of repeats also ensure that the degrees of freedom for pure error is also=0, and you also unable to test for lack of fit, so the lack of fit degrees of freedom is also 0. The residual degrees of freedom is the sum of the pure error and the lack of fit degrees of freedom.

There are no lack of fit degrees of freedom as was seen previously, there are also no repeats in this design and hence pure error degrees of freedom is 0. Hence, there are no residual degrees of freedom, and the design illustrated is said to be saturated.

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Orthogonal Term involving Higher Order Terms

What would be the R^2 for this saturated design?

Percentage $R^2 = 100\%$ as the number of model parameters is equal to number of independent variables. This in general should be avoided and the experimenter should design the experiment in such a way that he is able to estimate pure error and also have some d.o.f. for lack of fit.



What would be the R square for this saturated design? R squared value would be =100%, because you are using all the independent settings to estimate a corresponding number of the model parameters. So we will be able to achieve the perfect fit to your model, and that R square value would be=1 or expressed in percentage would be=100%. Well this is misleading because your model has now got as many as 16 parameters.

These 16 parameters are difficult to work with unwieldy, and when you tried for a different setting there maybe give completely different predictions. So there are a lot of issues with 16 parameters, normally your model even an empirical one or a linear regression model would be having and not more than 4 or 5 parameters at the most. Now let us talk about Center Runs.

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What are Center Runs? Why are they required?

Center runs are either single or multiple repeats of the experiment at the geometric center of the experimental design in the coded format (i.e. at $(0,0,\dots,0)$).



So what are center runs? And why are they required? Center runs are either single or multiple repeats of the experiment at the geometric center of the experimental design in the coded format. Suppose we have an experimental design and it is coded in terms of -1, +1 and so on, we look at the geometric center of such a design and that would be at 0, 0, 0 corresponding to the midpoints of the independent factors.

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What are Center Runs? Why are they required?

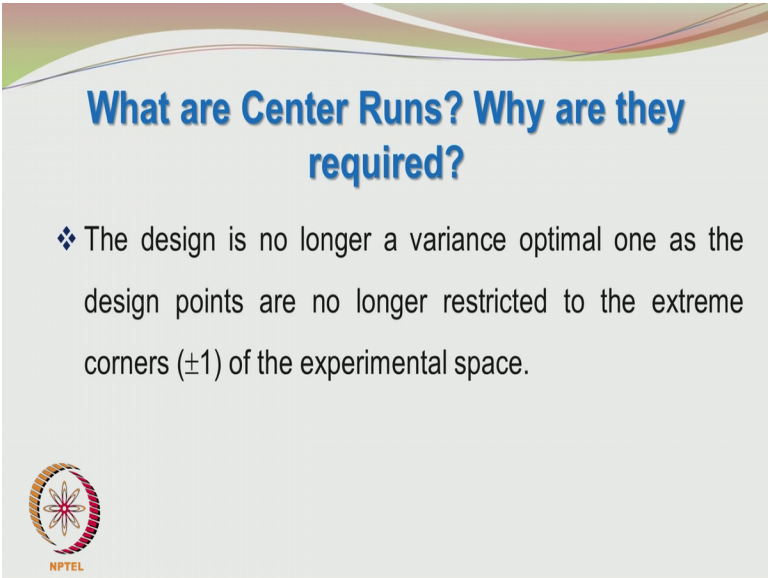
- ❖ Center runs act as important augmentation to the factorial design
- ❖ The addition of center runs to an orthogonal design does not alter the orthogonal property as they simply comprise of zeros in the coded format.



So center runs are very important to experimental design, you have a factorial design and you add center points you are enhancing or augmenting the factorial design. The addition of center runs to an orthogonal design does not alter the orthogonal property as they simply comprised of


0's in the coded format. So if you have an orthogonal design and you add center points to it, it does not disturb the orthogonality.

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What are Center Runs? Why are they required?

- ❖ The design is no longer a variance optimal one as the design points are no longer restricted to the extreme corners (± 1) of the experimental space.



And the design including the center points will unfortunately make the variance of the parameters slightly higher. So it is no longer a variant optimal design, as the design points are no longer restricted to the extreme corners of the experimental space. In the previous factorial designs without center points all the experimental settings were at $+1$, -1 combinations, and since these are located at the very edge of the boundaries, the variance of the estimated parameters was minimum.

And so it was a variance optimal design, but the moment you have center points you are having some design conditions or experimental conditions at the center also, they are no longer at the extreme ends. So this makes the design a non-variance optimal one. So if that is so why do we need center runs? What help or what additional benefit do they bring about?

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What are Center Runs? Why are they required?

- ❖ These do not contribute to the linear effects and the interaction.
- ❖ The center runs are useful for detecting curvature if not explicitly estimating them.



Before we get into that let us understand about the center runs a bit more, the center runs do not contribute to the linear effects and the interaction, they do not contribute to the main effects and the interaction. Suppose you have a factorial design without center runs and you estimate the main effects and the interaction, then you include the center runs in this orthogonal design the main effects and the interactions values and the corresponding coefficients will not be altered. Suppose you have a design with the center runs, you have another design without center runs.

Both of them will predict the same value of the main factor affects and the interaction effects. So it does not really matter whether you have center runs or not, as far as the estimation of these coefficients are concerned. So center runs are repeated runs, so they help you to get an idea about the experimental error which is very important. Only when you know the extent of experimental error would you be able to comment upon the significance and relevance of the factors in the experiment.

And depending upon the significance or relevance of the factors in the experiment that corresponding coefficients will appear in the model developed. And so in addition to the estimation of the pure experimental error, the center runs are also helpful for detecting whether curvature effects are important are not. The center runs cannot explicitly bring in the contribution due to curvature, but it can only indicate whether the curvature effects are important or not important. So we will take a small break here.