

Course on Phase Equilibrium Thermodynamics
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Lecture No 41
Non Ideal solutions(Contd.)

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$$\begin{aligned}
 U^E &= U_{\text{actual}} - U_{\text{ideal}} \\
 &= \sum x_i \bar{U}_i - \sum x_i U_i = \sum x_i (\bar{U}_i - U_i) = \Delta U_M \\
 h^E &= h_{\text{actual}} - h_{\text{ideal}} = \sum x_i (\bar{h}_i - h_i) = \Delta h_M \\
 U^E &= \Delta U_M \\
 g^E &= g_{\text{actual}} - g_{\text{ideal}} = \Delta g_{\text{actual}} - \Delta g_{\text{ideal}} \\
 &\quad \text{at same } T, P, \text{ compn.} = \sum x_i (\bar{g}_i - \bar{g}_i^{\text{ideal}}) \\
 \bar{g}_i^{\text{ideal}} &= RT \sum x_i \ln x_i = \sum x_i (\bar{g}_i^{\text{actual}} - g_i) - \sum x_i RT \ln x_i \\
 &= \sum x_i (\bar{g}_i - g_i) - RT \sum x_i \ln x_i
 \end{aligned}$$

So therefore let us see what are the excess properties that we were dealing with? Just as I have told you, so therefore if we go to the previous slide it will be clear to you that what do we have then in this particular case? We have v excess what is v excess it is v actual minus v ideal. Actual ideal everything refers to solution. What is v actual then? It is $\sum x_i \bar{v}_i$, what is v ideal you know? It is $\sum x_i v_i$, so therefore this should be $\sum x_i \bar{v}_i - \sum x_i v_i$ had the solution been ideal \bar{v}_i would have been equal to v_i and v^E would have been equal to 0.

This case this is not equal to 0, therefore what is this? It is actually the volume change on mixing of the solution. Same way we can write down h^E just the same way we can repeat it h actual minus h ideal, right? Which is nothing but equal to $\sum x_i \bar{h}_i - \sum x_i h_i$ which is nothing but equal to Δh_M for a real solution same thing u^E will be equal to ΔU_M . Let us see what is g^E equals to?

For g^E , what is this? Again in the same way it should be g actual minus g ideal, okay. So therefore what is this remember one thing this is the Gibbs free energy of the solution actual or the real solution, this is the Gibbs free energy of the ideal solution both at same T , P , composition. Now remember one thing as I had already mentioned we cannot define absolute values of any properties we always define the property changes, right?

So therefore this actual Gibbs free energy of the solution is better expressed as the actual change in Gibbs free energy on forming the solution, isn't it? So we had 2 components as we mixed them due to this mixture there was a change in Gibbs free energy, what is this Gibbs free energy change for a real solution? What is this Gibbs free energy change for an ideal solution? The difference between the 2 should be a better measure of the excess property as compared to the Gibbs free energy of actual solution minus the Gibbs free energy of the ideal solution, why?

Because we cannot define absolute value of Gibbs free energy for any particular substance in any particular state we always need a datum as you remember. So therefore this can be expressed as $\Delta g_M^{\text{actual}} - \Delta g_M^{\text{ideal}}$, agreed? Which can also be referred to as $\bar{g}_i - \bar{g}_i^{\text{ideal}}$ this is actual. Now if you recollect what was $\Delta g_M^{\text{ideal}}$? If you recollect, so therefore \bar{g}_i for an ideal solution what was this? Your \bar{g}_i^{ideal} or rather \bar{g}_i^{ideal} . Let us take it; it was $RT \sum x_i \ln x_i$ that we have already derived.

So therefore what should this become? This should become $\bar{g}_i - \sum x_i RT \ln x_i$, so we can we can take this out or else we can define this as $\sum x_i \bar{g}_i - \sum x_i \bar{g}_i^{\text{ideal}}$ minus $RT \sum x_i \ln x_i$. This should have been $\bar{g}_i^{\text{actual}} - \bar{g}_i^{\text{ideal}}$, agreed?

Okay, so therefore what did I do this $\Delta g_M^{\text{actual}}$ that that is actually the $\Delta g_M^{\text{actual}}$ change for the actual solution which is given by this the , what happens during formation of the solution? The molar Gibbs free energy changes to the partial molar Gibbs free energy for each component i . So this is for the actual solution and this is for the real solution, right?

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$$\begin{aligned}
 g^E &= \sum x_i (\bar{g}_i - g_i) - RT \sum x_i \ln x_i \\
 \bar{g}_i - g_i &= RT \ln \frac{\hat{f}_i}{f_i} \quad \left| \hat{f}_i = \gamma_i x_i f_i \right| \\
 &= RT \ln \frac{\gamma_i x_i f_i}{f_i} = RT \ln \gamma_i + RT \sum x_i \ln x_i \\
 g^E &= \sum x_i (\bar{g}_i - g_i) - RT \sum x_i \ln x_i \\
 &= RT \sum x_i \ln \gamma_i + RT \sum x_i \ln x_i - RT \sum x_i \ln x_i \\
 \boxed{\frac{g^E}{RT} = \sum x_i \ln \gamma_i} \quad g^E &= x \bar{g}^E
 \end{aligned}$$

Now tell me one thing, how is this \bar{g}_i minus g_i related? This so I will just repeat it once more, so that it is easier for you to understand g excess this is equal to $\sum x_i \bar{g}_i$ minus g_i minus $RT \sum x_i \ln x_i$, fine. What is this \bar{g}_i minus g_i ? This is why because the pure component i was taken into a solution that is why this particular change occurred. Can we not write it down as $RT \ln \frac{\bar{f}_i}{f_i}$? What does it show?

The fugacity change of pure component i when it is taken into solution. So what is my standard state in this particular case pure component i . So from there and the standard states as same for both the left inside and right-hand side of the equation, so from the pure component i , I am taking it to the solution state as a result of which it's Gibbs free energy is changing to \bar{g}_i and its fugacity is changing to \bar{f}_i , agreed?

So therefore this particular equation this particular exact equation can be written relating the molar Gibbs free energy or the partial molar Gibbs free energy with the fugacity and the partial molar fugacity, agreed? I can do this, so what is this again what is this \bar{f}_i equals to? For a real solution this is equals to $\gamma_i x_i f_i$. So therefore can I not write it down as $RT \gamma_i x_i \ln f_i$ by f_i ? Both the cases remember the f_i are the same it is the pure component fugacity at temperature, pressure of the solution.

This was the fugacity of the pure component and this is also the fugacity of the pure component, can I not write it down in this particular way? So therefore what is my \bar{g}_i minus g_i then in this case this is $RT \ln \gamma_i + RT \sum x_i \ln x_i$. I can write it down in this particular way, fine. And so therefore if I substitute this in this particular

equation, what do I get? Excess Gibbs is nothing but $\sum X_i \bar{g}_i - RT \sum X_i \ln X_i$.

What is, I just substitute \bar{g}_i so what do I get? This is equal to $\sum X_i RT \ln \gamma_i$ can be taken outside $\ln \gamma_i$ plus $RT \sum X_i \ln X_i$ minus $RT \sum X_i \ln X_i$. What do I get as a result of this? I find that the γ_i can be related in a very simple way with this is the relationship of excess Gibbs free energy with γ_i , right? And remember one thing just because the solution is not ideal. So therefore there will be some excess Gibbs free energy and that decides whether the solution forms spontaneously or not and as a result of this non-ideality γ_i has come into picture.

So therefore we find that the γ_i of each and every component can be related to the molar Gibbs free energy change of the solution in this particular summation form. Now what is this g^E tell me? g^E is nothing but equals to your $\sum X_i \bar{g}_i^E$, yes or no? Agreed?

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Handwritten derivation on a blue background:

$$\bar{g}_i^E = \left(\frac{\partial g^E}{\partial N_i} \right)_{T, P, X_j \neq i}$$

$$\bar{g}_i^E = \frac{\partial [(N_1 + N_2) g^E]}{\partial N_i} \Big|_{T, P, N_2}$$

$$= \frac{\partial [(N_1 + N_2) [X_1 \ln \gamma_1 + X_2 \ln \gamma_2]]}{\partial N_i} \Big|_{T, P, N_2}$$

$$\boxed{\bar{g}_i^E = RT \ln \gamma_i}$$

partial molar
(excess Gibbs free energy change of component i)
in solution

So therefore how can I get this \bar{g}_i^E ? This \bar{g}_i^E it is nothing but equal to $\partial g^E / \partial N_i$ at constant $T, P, X_j \neq i$, agreed. Or in other words can I not write it down in this particular way $\partial g^E / \partial N_i$ of? Say suppose it is a your binary mixtures. So therefore $\partial g^E / \partial N_1$ is $\partial g^E / \partial N_1$ at constant T, P, N_2 . And what is this g^E equals to? This is nothing but equal to $\partial g^E / \partial N_1$ at constant T, P, N_2 $X_1 \ln \gamma_1 + X_2 \ln \gamma_2$ constant T, P, N_2 .

Simply differentiate this and what do you get? You just differentiate it you are going to get g by g_i bar E that is the excess, I will write it down excess Gibbs free energy change, excess E excess partial molar, why? The bar is there excess partial molar Gibbs free energy change of component i in solution, what does what is this? This is g_i bar E equals to $RT \ln \gamma_i$. So if you can calculate the excess Gibbs free energy the partial molar excess its free energy of component i then you should be in a position to calculate the activity coefficient of that particular component, agreed?

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Excess Properties (contd.)

$$g^E = g - g^I = \Delta g_m - \Delta g_m^I = \sum_{i=1}^c x_i (\bar{g}_i - g_i) - \sum_{i=1}^c RT x_i \ln x_i$$

$$g^E = RT \sum_{i=1}^c x_i \ln \left(\frac{f_i}{x_i f_i^*} \right)$$

$$\frac{g^E}{RT} = \sum_{i=1}^c x_i \ln \gamma_i \quad \frac{\bar{g}_i^E}{RT} = \left[\frac{\partial (N g^E / RT)}{\partial N_i} \right]_{T, P, N_j} = \ln \gamma_i$$

$$s^E = s - s^I = \Delta s_m - \Delta s_m^I = \Delta s_m + R \sum_{i=1}^c x_i \ln x_i$$

$$h^E = u^E + P v^E$$

$$g^E = h^E - T s^E$$

$$a^E = u^E - T s^E$$

$$\left(\frac{\partial G^E}{\partial T} \right)_{P, N} = -S^E$$

$$\left(\frac{\partial G^E}{\partial P} \right)_{T, N} = V^E$$

$$\left(\frac{\partial (G^E / T)}{\partial T} \right)_{P, N} = -\frac{H^E}{T^2}$$

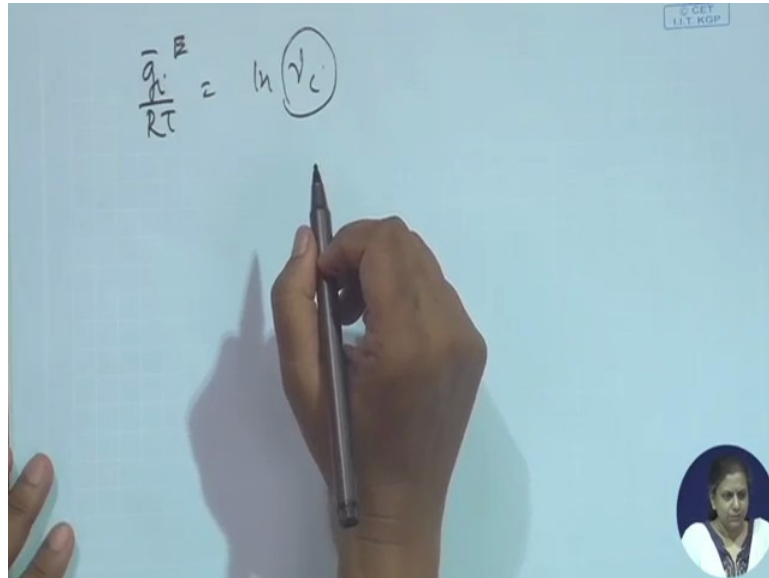
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So therefore we find that we have come across these 2 equations which I have already written down here if you observe. We find the molar Gibbs excess Gibbs free energy of the solution is given in terms of composition or activity coefficient by this equation and the partial molar excess Gibbs free energy change of component i in solution is nothing but equal to \ln of γ_i , right? So therefore this should be one particular way of finding out g^E of finding out γ_i and it's important for you to recollect that just like we had done for ideal solutions we can always write down or rather we can always find out the excess entropy change of the solution.

What it is going to be? This is nothing but equals to h^E minus, if I write it down what is s equals to? Recollect g equals to h minus Ts . So therefore s will be equal to g by T minus h by T , right? And therefore once this equation was written for a for a molar quantity we can always add a superscript s for the in extensive properties and this is the relationship between the excess properties. So therefore we can easily find out Gibbs free energy excess entropy in

terms of excess Gibbs free energy and excess enthalpy and once we do it we find that the excess entropy is given by this particular equation, right?

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So therefore the interesting part which we found out was the first thing which we found out \bar{g}_i^E by RT equals to $\ln \gamma_i$ γ_i should also be related to other excess properties, how would it be related let us see?

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Excess Properties (contd.)

$$g^E = g - g^I = \Delta g_m - \Delta g_m^I = \sum_{i=1}^c x_i (\bar{g}_i - g_i) - \sum_{i=1}^c RT x_i \ln x_i$$

$$g^E = RT \sum_{i=1}^c x_i \ln \left(\frac{f_i}{x_i f_i^*} \right)$$

$$\frac{g^E}{RT} = \sum_{i=1}^c x_i \ln \gamma_i \quad \quad \frac{\bar{g}_i^E}{RT} = \left[\frac{\partial (N g^E / RT)}{\partial N_i} \right]_{T, P, N_j} = \ln \gamma_i$$

$$s^E = s - s^I = \Delta s_m - \Delta s_m^I = \Delta s_m + R \sum_{i=1}^c x_i \ln x_i$$

$$h^E = u^E + P v^E$$

$$g^E = h^E - T s^E$$

$$a^E = u^E - T s^E$$

$$\left(\frac{\partial G^E}{\partial T} \right)_{P, x} = -S^E$$

$$\left(\frac{\partial G^E}{\partial P} \right)_{T, x} = V^E$$

$$\left(\frac{\partial (G^E / T)}{\partial T} \right)_{P, x} = -\frac{H^E}{T^2}$$



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How γ_i varies with temperature pressure and composition etc. Just try to do it yourself and then see what do you get?

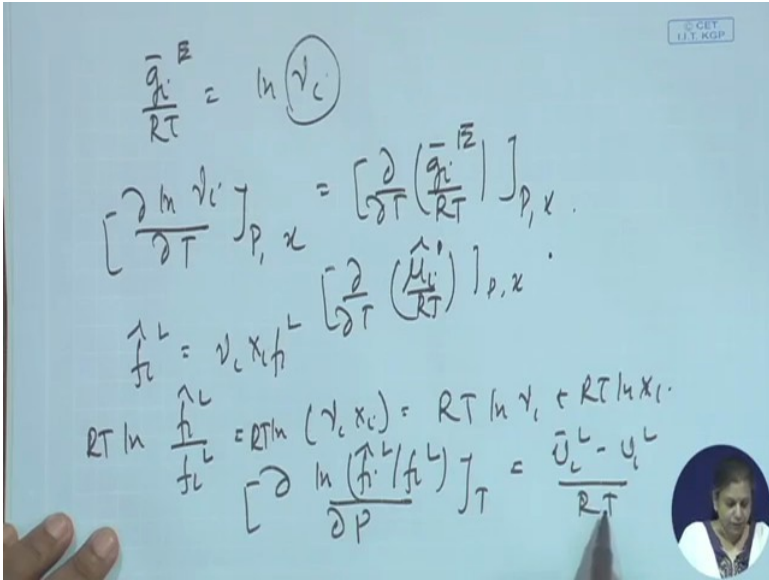
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Gibbs – Duhem Relation for Activity Coefficient	Influence of Temperature & Pressure on Activity coefficient
$\frac{h_i^E}{T} dT - v_i^E dP + RT \sum_{i=1}^c x_i d \ln \gamma_i = 0$	$\left(\frac{\partial \ln \gamma_i}{\partial T} \right)_{P, x_i} = \left[\frac{\partial \left(\frac{g_i^E}{RT} \right)}{\partial T} \right]_{P, x_i} = - \frac{h_i^E}{RT^2}$
$\sum_{i=1}^c x_i d \ln \gamma_i = \frac{v_i^E}{RT} dP \quad (\text{at constant } T)$	$\left(\frac{\partial \ln \gamma_i}{\partial P} \right)_{T, x_i} = \left[\frac{\partial \left(\frac{g_i^E}{RT} \right)}{\partial P} \right]_{T, x_i} = \frac{v_i^E}{RT}$
$\sum_{i=1}^c x_i d \ln \gamma_i = - \frac{h_i^E}{RT^2} dT \quad (\text{at constant } P)$	
$\sum_{i=1}^c x_i d \ln \gamma_i = 0 \quad (\text{at constant } T \text{ and } P)$	$\frac{g^E}{RT} = \sum x_i \frac{g_i^E}{RT} = \sum x_i \ln \gamma_i$

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$$\frac{\bar{g}_i^E}{RT} = \ln \gamma_i$$

$$\left[\frac{\partial \ln \gamma_i}{\partial T} \right]_{P, x} = \left[\frac{\partial \left(\frac{\bar{g}_i^E}{RT} \right)}{\partial T} \right]_{P, x}$$

$$\frac{\bar{g}_i^E}{RT} = \ln \gamma_i$$

$$RT \ln \frac{\bar{f}_i^L}{f_i^L} = RT \ln (\gamma_i x_i) = RT \ln \gamma_i + RT \ln x_i$$

$$\left[\frac{\partial \ln (\bar{f}_i^L / f_i^L)}{\partial P} \right]_T = \frac{\bar{v}_i^L - v_i^L}{RT}$$



Suppose you try to find out $\partial \ln \gamma_i / \partial T$, right? At constant pressure and composition, what is this equals to? You already know what is $\ln \gamma_i$? It is nothing but equals to \bar{g}_i^E / RT , please do not forget there are 3 things which have to be mentioned at constant P and x_i , right? And what is this \bar{g}_i^E this is nothing but equals to $\partial \mu_i / \partial T$ at constant P and x_i , right? We can write it down in this particular way.

So therefore from here what do we get then? From here we find out or in other words this can also be written down as, we can start it in a slightly different way and which will be easier for you to understand. Let us start from the basics then it will be easier for you to understand. This we have already found out, right? So therefore what is $\ln f_i^L / f_i^L$? Pure component

nothing but equal to $\ln \gamma_i X_i$. Now this is equal to RT , so if we have a RT here you have a RT here you have $\ln \gamma_i$ plus $RT \ln X_i$, agreed? So what is $\frac{\partial \ln f_i^L}{\partial P}$?

Say $\frac{\partial P}{\partial P}$ if we take at constant temperature, recollect what is this equal to? This will be equal to \bar{v}_i^L minus \bar{v}_i^L by RT , if you remember dg equals to $-sdT + v dP$. So therefore this is what precisely we have done.

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Handwritten derivation on a blue background:

$$\left[\frac{\partial \ln(A_i X_i)}{\partial P} \right]_T = \frac{\bar{v}_i^L - \bar{v}_i^L}{RT} \quad \text{For an ideal soln}$$

$$= \frac{\bar{v}_i^E}{RT} \quad \bar{v}_{i, \text{ideal}}^L = \bar{v}_i^L$$

\bar{v}_i^E = excess partial molar volume for component i

$$= \frac{\text{actual molar vol of component i in real soln} - \text{molar volume of component i in ideal soln (at same T, P, X)}}{RT}$$

So in the same way we, can you not write it down as $\frac{\partial \ln \gamma_i}{\partial P}$? This should be equal to \bar{v}_i^L minus \bar{v}_i^L by RT . What is \bar{v}_i^L ? It is the partial molar excess volume of component i in the liquid solution. What is this? It is the molar volume of component i in the liquid state for an ideal solution we know that if the for an ideal solution what do we know? For an ideal solution $\bar{v}_{i, \text{ideal}}^L$ is nothing but equal to \bar{v}_i^L .

So therefore what is this then in that case? It is the partial molar volume change for the case of a real solution minus the partial molar volume change for an ideal solution. So therefore what is it then? This is nothing but \bar{v}_i^E by RT , \bar{v}_i^E by RT , agreed? Which is what? This \bar{v}_i^E excess, what is this? Excess partial excess \bar{v}_i^E means partial molar volume, agreed? For component i which is nothing but actual molar volume of component i in solution minus the, in real solution real is within bracket minus molar volume of component i in ideal solution, very important at same T, P, x . This you have to keep on adding because the standards states have to be the same, right?

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Handwritten derivation on a blue background:

$$\left[\frac{\partial \ln(\gamma_i x_i)}{\partial P} \right]_T = \frac{\bar{V}_i^L - V_i^L}{RT}$$

For an ideal soln $\bar{V}_i^L = V_i^L$

$$\left(\frac{\partial \ln \gamma_i}{\partial P} \right)_T + \left(\frac{\partial \ln x_i}{\partial P} \right)_T = \frac{\bar{V}_i^L}{RT}$$

$\bar{V}_i^E =$ excess partial molar volume for component i

$=$ actual molar volume in soln - molar volume in ideal soln at T, P, X

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Gibbs – Duhem Relation for Activity Coefficient	Influence of Temperature & Pressure on Activity coefficient
$\frac{h^E}{T} dT - v^E dP + RT \sum_{i=1}^c x_i d \ln \gamma_i = 0$	$\left(\frac{\partial \ln \gamma_i}{\partial T} \right)_{P, x_i} = \left[\frac{\partial \left(\frac{g_i^E}{RT} \right)}{\partial T} \right]_{P, x_i} = - \frac{h_i^E}{RT^2}$
$\sum_{i=1}^c x_i d \ln \gamma_i = \frac{v^E}{RT} dP \quad (\text{at constant } T)$	$\left(\frac{\partial \ln \gamma_i}{\partial P} \right)_{T, x_i} = \left[\frac{\partial \left(\frac{g_i^E}{RT} \right)}{\partial P} \right]_{T, x_i} = \frac{v_i^E}{RT}$
$\sum_{i=1}^c x_i d \ln \gamma_i = - \frac{h^E}{RT^2} dT \quad (\text{at constant } P)$	$\frac{g^E}{RT} = \sum x_i \frac{g_i^E}{RT} = \sum x_i \ln \gamma_i$
$\sum_{i=1}^c x_i d \ln \gamma_i = 0 \quad (\text{at constant } T \text{ and } P)$	

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And therefore and what is this $\Delta \ln \gamma_i$ by ΔP ? So we can write it down as $\Delta \ln \gamma_i$ ΔP at constant T plus $\Delta \ln x_i$ ΔP at constant T. We know that x_i the mole fraction does not change with pressure. So therefore $\Delta \ln \gamma_i$ ΔP is nothing but it can be related to the excess partial molar volume for component i which I have also written down. Same way suppose we would like to find out the temperature, the dependence of γ_i on temperature. It should again go on in the same way.

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Handwritten equations on a blue background:

$$\left(\frac{\partial \ln f_i}{\partial T}\right)_P = \frac{h_i^0 - h_i}{RT^2}$$

$$\left(\frac{\partial \ln \hat{f}_i}{\partial T}\right)_P = \frac{h_i^0 - \bar{h}_i}{RT^2}$$

$$\left(\frac{\partial \ln \gamma_i}{\partial T}\right)_P = \left(\frac{\partial \ln \hat{f}_i / f_i}{\partial T}\right)_P = \frac{-\bar{h}_i + h_i}{RT^2}$$

$$= \left[\frac{-\bar{h}_i^E}{RT^2} \right]$$

Below the equations, it is noted: $\bar{h}_i^E = \text{Partial molar excess enthalpy of component } i$

On the right side, additional notes are present:

$$\frac{\hat{f}_i}{f_i} = \gamma_i X_i$$

$$\ln \frac{\hat{f}_i}{f_i} = \ln \gamma_i + \ln X_i$$

It should be $\partial \ln f_i / \partial T$ at constant P this is nothing, if you recollect h_i^0 minus h_i by RT^2 square. Same way, can we not write down for the partial molar fugacity h_i^0 minus \bar{h}_i by RT^2 square? So therefore can I not write and what do I know? I know \hat{f}_i by f_i equals to $\gamma_i X_i$, right? So therefore $\ln \hat{f}_i$ by f_i is nothing but equal to $\ln \gamma_i$ plus $\ln X_i$ agreed? So therefore can I not write this down as $\partial \ln \gamma_i$?

Again I know that X_i is not a function of temperature it been composition does not depend on temperature. So can I not write this down as $\partial \ln \hat{f}_i$ by f_i ∂T at constant P? Is this not equal to minus of \bar{h}_i plus h_i by RT^2 square h_i^0 is the same for both the equations. What is this equal to? Isn't it equal to minus \bar{h}_i excess by RT^2 square? What is this? This is nothing but the partial, I will write it down \bar{h}_i^E it is the partial molar enthalpy of component i . For partial there is a bar partial molar excess, See I am also missing a lot of things partial molar excess enthalpy of component i which is nothing but the partial molar enthalpy of i minus the molar enthalpy of component i at the same conditions of temperature and pressure, right?

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Gibbs – Duhem Relation for Activity Coefficient

$$\frac{h^E}{T}dT - v^E dP + RT \sum_{i=1}^c x_i d \ln \gamma_i = 0$$

$$\sum_{i=1}^c x_i d \ln \gamma_i = \frac{v^E}{RT} dP \quad (\text{at constant } T)$$

$$\sum_{i=1}^c x_i d \ln \gamma_i = -\frac{h^E}{RT^2} dT \quad (\text{at constant } P)$$

$$\sum_{i=1}^c x_i d \ln \gamma_i = 0 \quad (\text{at constant } T \text{ and } P)$$

Influence of Temperature & Pressure on Activity coefficient

$$\left(\frac{\partial \ln \gamma_i}{\partial T} \right)_{P, x_i} = \left[\frac{\partial \left(\frac{g_i^E}{RT} \right)}{\partial T} \right]_{P, x_i} = -\frac{\bar{h}_i^E}{RT^2}$$

$$\left(\frac{\partial \ln \gamma_i}{\partial P} \right)_{T, x_i} = \left[\frac{\partial \left(\frac{g_i^E}{RT} \right)}{\partial P} \right]_{T, x_i} = \frac{\bar{v}_i^E}{RT}$$

$$\frac{g^E}{RT} = \sum x_i \frac{g_i^E}{RT} = \sum x_i \ln \gamma_i$$

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So variation with temperature can be related with the partial molar excess enthalpy of the of the solution and the gamma variation with pressure can be related with partial molar excess volume of component i in the solution and we know that the you're the gamma i it is related with the with the excess Gibbs free energy of each and every partial molar Gibbs free energy of each and every component in the mixture by this equals to ln gamma i and the excess molar Gibbs free energy of the mixture by this particular equation.

So therefore we find as we have anticipated that excess properties arising to the real the deviation of the solution from the ideal behaviour and we have used gamma to account for this particular deviation. So therefore gamma can be related with the excess properties and we have shown how it is related to excess molar Gibbs free energy of the solutin excess molar the partial molar enthalpy of each component, partial excess partial molar volume of each particular component.

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Excess Properties (contd.)

$$g^E = g - g^I = \Delta g_m - \Delta g_m^I = \sum_{i=1}^c x_i (\bar{g}_i - g_i) - \sum_{i=1}^c RT x_i \ln x_i$$

$$g^E = RT \sum_{i=1}^c x_i \ln \left(\frac{f_i}{x_i f_i^*} \right)$$

$$\frac{g^E}{RT} = \sum_{i=1}^c x_i \ln \gamma_i \quad \frac{\bar{g}_i^E}{RT} = \left[\frac{\partial (Ng^E/RT)}{\partial N_i} \right]_{T,P,N_j} = \ln \gamma_i$$

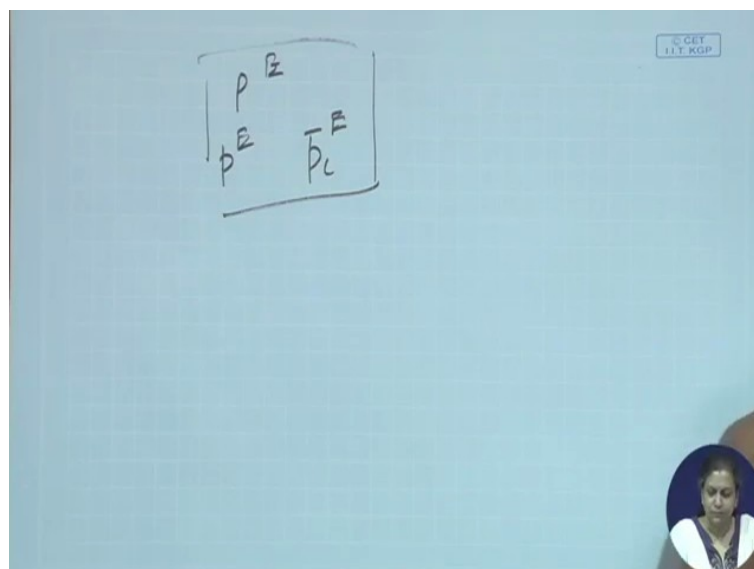
$$s^E = s - s^I = \Delta s_m - \Delta s_m^I = \Delta s_m + R \sum_{i=1}^c x_i \ln x_i$$

$$\begin{aligned} h^E &= u^E + Pv^E \\ g^E &= h^E - Ts^E \\ a^E &= u^E - Ts^E \\ \left(\frac{\partial G^E}{\partial T} \right)_{P,x} &= -S^E \\ - \left(\frac{\partial G^E}{\partial P} \right)_{T,x} &= V^E \\ - \left(\frac{\partial (G^E/T)}{\partial T} \right)_{P,x} &= - \frac{H^E}{T^2} \end{aligned}$$

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Now since we have defined another set of excess properties it is very interesting to find out that these particular excess properties they also obey the same equations as that of the the molar properties as that of the total properties whatever equations we have defined in terms of total properties in terms of molar properties you just add a superscript E and you find that each and every particular relationship is applicable and all these equations you can actually derive and you can find it out that all these equations which you have derived for the your molar and total properties are applicable for total excess properties, for partial molar excess properties for molar excess properties, right?

(Refer Slide Time: 22:03)



Total excess properties given by this, your molar excess property is given by this, partial molar excess property for each component is given by this. So these are the 3 symbols that we will be using we just should be little careful about the symbols since we are dealing with a large number of properties, right?

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Excess Properties (contd.)

$$g^E = g - g^I = \Delta g_m - \Delta g_m^I = \sum_{i=1}^c x_i (\bar{g}_i - g_i) - \sum_{i=1}^c RT x_i \ln x_i$$

$$g_i^E = RT \sum x_j \ln \left(\frac{f_{ij}}{x_i f_i^*} \right)$$

$$\frac{g_i^E}{RT} = \sum x_j \ln \gamma_{ij} \quad \frac{\bar{g}_i^E}{RT} = \left[\frac{\partial (N g^E / RT)}{\partial N_i} \right]_{T,P,N_j} = \ln \gamma_i$$

$$s^E = s - s^I = \Delta s_m - \Delta s_m^I = \Delta s_m + R \sum_{i=1}^c x_i \ln x_i$$

$$h^E = u^E + P v^E$$

$$g^E = h^E - T s^E$$

$$a^E = u^E - T s^E$$

$$\left(\frac{\partial g^E}{\partial T} \right)_{P,x} = -s^E$$

$$\left(\frac{\partial g^E}{\partial P} \right)_{T,x} = v^E$$

$$\left(\frac{\partial (g^E / T)}{\partial T} \right)_{P,x} = -\frac{h^E}{T^2}$$

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There is one more thing which is very interesting we have defined rather we have tried to incorporate the non ideal behaviour by incorporating gamma we have related to the excess properties of the solution. Now whenever we have been dealing with solutions we found out that for mixtures there is a very important relation which tells us that all properties of the mixtures are not ideal, what was that particular equation?

It was the Gibbs Duhem equation; we have derived the Gibbs Duhem equation in terms of chemical potential, right? The same can be derived for in terms of fugacity and we should be also in a position to derive Gibbs Duhem equation for activity coefficient, why do we need to do it? We need to do it because we have seen that if Gibbs Duhem equation gives us one particular clue by which we can find out any property of component a if the same property for component b is known provided it is a binary mixture. If it is a N component mixture if we know the property for N minus 1 components we will be in a position to find the same property for other nth component provided the entire thing is being performed under the conditions of same temperature, pressure and composition.

So therefore since finding out gamma is so very important gamma is so very important as far as vapor liquid equilibrium for nonideal solution are concerned and we come across nonideal

solutions very frequently so therefore it is important to find out gamma or rather to express Gibbs Duhem equation in terms of gamma. So that for a binary solution which we usually come across is we know gamma 1 we will be in a position to find out gamma 2.

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$$\boxed{P^E}$$

$$P^E \quad \bar{P}_i^E$$

G.D $SdT - Vdp + Nd\mu = 0$ (single component)
 $SdT - Vdp + \sum N_i d\mu_i = 0$ Multi component
 $SdT - Vdp + \sum x_i d\mu_i = 0$ (In terms of molar properties)
 $S^E dT - V^E dp + \sum x_i (d\bar{g}_i^E) = 0$
 $\bar{g}_i^E = RT \ln \gamma_i$ (RTH)

Let us start from the beginning and see how we can derive the Gibbs Duhem equation in terms of gamma? Remember the basic equation it was SdT minus Vdp plus $Nd\mu$ equals to 0 this we had found out for single component, agreed? For multi-component what should happen? The same equation but this should be Σ should come up $Nd\mu_i$ equals to 0, this is for multi-component case.

In terms of molar property everything becomes small, plus $\Sigma x_i d\mu_i$ equals to 0 in terms of molar properties, agreed? So therefore in terms of excess molar properties again let us write down, can I not write it down as μ_i is nothing but \bar{g}_i equals to 0, right? And again I know what is this \bar{g}_i . We have derived it it is nothing but $RT \ln \gamma_i$, agreed? So therefore instead of this \bar{g}_i I can just write down $RT \ln \gamma_i$ then what happens to the Gibbs Duhem equation?

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$$s^E dT - v^E dp + \sum_{i=1}^N x_i d(RT \ln \gamma_i) = 0$$

$$s^E dT - v^E dp + \sum_{i=1}^N x_i R \ln \gamma_i dT + \sum_{i=1}^N x_i RT d \ln \gamma_i = 0$$

$$s^E dT - v^E dp + R \sum_{i=1}^N x_i \ln \gamma_i dT + RT \sum_{i=1}^N x_i d \ln \gamma_i = 0$$

$$s^E = \frac{h^E - g^E}{T} \rightarrow \frac{g^E}{RT} = \sum x_i \ln \gamma_i$$

$$s^E dT - \frac{h^E}{T} dT - R \sum_{i=1}^N x_i \ln \gamma_i dT$$

The Gibbs Duhem equation then becomes $s^E dT - v^E dp + \sum_{i=1}^N x_i d(RT \ln \gamma_i) = 0$, agreed? We can write it down in this particular way, so therefore and now if we expand this part what do we get? We get $s^E dT - v^E dp + \sum_{i=1}^N x_i R \ln \gamma_i dT + \sum_{i=1}^N x_i RT d \ln \gamma_i = 0$, agreed? So therefore what do I get finally $s^E dT - v^E dp + R \sum_{i=1}^N x_i \ln \gamma_i dT + RT \sum_{i=1}^N x_i d \ln \gamma_i = 0$, fine.

What is s^E equals to? It is nothing but equals to $h^E - g^E$ by T we have already done it. What is this g^E ? Again I would like to (re) recollect g^E by RT it is equal to $\sum x_i \ln \gamma_i$, right? So therefore this particular term g^E by T , can this not be written down as $R \sum x_i \ln \gamma_i$? Let us substitute it here what do we get? Do we not get $s^E dT - h^E$ by $T dT - R \sum_{i=1}^N x_i \ln \gamma_i dT$, fine. This particular term, this term then can be written down as this term can be written in this particular form, okay. And so therefore on substituting this particular this and this in this equation, what do we get?

(Refer Slide Time: 27:43)

The image shows a whiteboard with handwritten mathematical equations. At the top, the equation is written as:
$$\frac{h^E}{T} dT - R \sum x_i \ln \gamma_i dT - v^E dp + R \sum x_i \ln \gamma_i dT + RT \sum x_i d \ln \gamma_i = 0$$
The first three terms are grouped together in a box, and the last two terms are also boxed. The boxed equation is:
$$\left[\frac{h^E}{T} dT - v^E dp + RT \sum x_i d \ln \gamma_i \right] = 0$$
Below the boxed equation, a note says:
$$\rightarrow \text{G.D. eqn in terms of activity coefficient}$$

We get equation like this $\frac{h^E}{T} dT - R \sum x_i \ln \gamma_i dT - v^E dp + R \sum x_i \ln \gamma_i dT + RT \sum x_i d \ln \gamma_i = 0$. We immediately find that this and this and this they cancel out and when all these cancel out, what is the final equation that we get? Final equation it becomes $\frac{h^E}{T} dT - v^E dp + RT \sum x_i d \ln \gamma_i = 0$. This is the final equation this is the Gibbs Duhem equation in terms of activity coefficient γ , right?

So therefore this is the equation that that we get under this particular condition.

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Gibbs - Duhem Relation for Activity Coefficient

$$\frac{h^E}{T} dT - v^E dP + RT \sum_{i=1}^c x_i d \ln \gamma_i = 0$$

$$\sum_{i=1}^c x_i d \ln \gamma_i = \frac{v^E}{RT} dP \quad (\text{at constant } T)$$

$$\sum_{i=1}^c x_i d \ln \gamma_i = -\frac{h^E}{RT^2} dT \quad (\text{at constant } P)$$

$$\sum_{i=1}^c x_i d \ln \gamma_i = 0 \quad (\text{at constant } T \text{ and } P)$$

Influence of Temperature & Pressure on Activity coefficient

$$\left(\frac{\partial \ln \gamma_i}{\partial T} \right)_{P, x_i} = \left[\frac{\partial \left(\frac{g_i^E}{RT} \right)}{\partial T} \right]_{P, x_i} = -\frac{h_i^E}{RT^2}$$

$$\left(\frac{\partial \ln \gamma_i}{\partial P} \right)_{T, x_i} = \left[\frac{\partial \left(\frac{g_i^E}{RT} \right)}{\partial P} \right]_{T, x_i} = \frac{v_i^E}{RT}$$

$$\frac{g^E}{RT} = \sum x_i \frac{g_i^E}{RT} = \sum x_i \ln \gamma_i$$

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And then remember one thing that when we are dealing with properties this is what I have written down this is the final equation that I have written down so this is the equation that we have obtained, right? Now here I would like to mention one more thing before I go further. Since this is a property therefore we can have this particular derivation in an alternative form as well.

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At const T & P G.D. eqn in terms of μ

$$\sum x_i d\mu_i = 0$$

$$\sum x_i d \ln f_i = 0 \quad f_i = \gamma_i x_i f_i^L$$

$$\sum x_i d \ln (\gamma_i x_i f_i^L) = 0$$

$$\sum x_i d \ln \gamma_i + \sum x_i d \ln x_i + \sum x_i d \ln f_i^L = 0$$

At const T & P $\sum x_i \frac{d x_i}{x_i} = \sum d x_i = 0$

$$\sum x_i d \ln \gamma_i = 0$$

Instead of starting from this particular way we could have also started the Gibbs Duhem equation in terms of μ and we could have proceeded. At constant temperature and pressure Gibbs Duhem equation in terms of μ , in this particular case we have started with g_i^E in

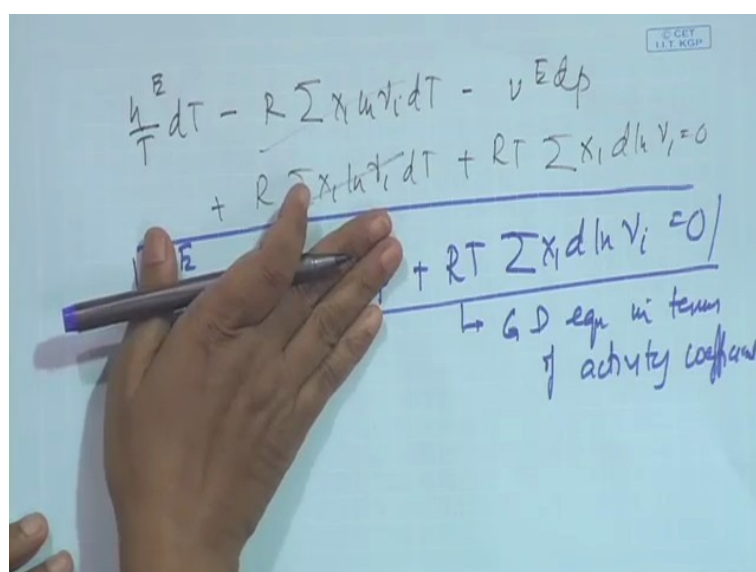
terms of fugacity or in terms of μ , suppose we write we can also start with this particular equation, okay. In terms of fugacity this becomes $\sum_i x_i d \ln f_i^{\text{bar}} = 0$, right?

We know f_i^{bar} is nothing but equal to $\gamma_i x_i f_i^{\text{pure}}$ everything is for is for the liquid phase if you take, so therefore can I not write it down in this particular way $\sum_i x_i d \ln \gamma_i + \sum_i x_i d \ln f_i^{\text{pure}} = 0$, right? So therefore we if you break it down what happen? This is $\sum_i x_i d \ln \gamma_i + \sum_i x_i d \ln f_i^{\text{pure}} = 0$ this is a easier derivation. So that is why I am just doing it for you.

Now try to understand we have started with constant temperature and pressure. At constant temperature and pressure, what is f_i^{pure} equals to? It is a fugacity of the pure component liquid at the same conditions of temperature and pressure and we know that from low to moderate pressure it is a saturated vapor pressure. So when T and P are constant f_i^{pure} automatically becomes constant. So therefore even if it is at low to moderate pressure or at any pressure we know that this component becomes equal to 0.

What about this part? This is nothing but equal to $\sum_i x_i dx_i$ by x_i , isn't it? Or in other words this is $\sum_i dx_i$. What is this? This $\sum_i dx_i$ means the variation of the total number of moles we know the total number of moles of the component is constant. So therefore automatically this becomes equal to 0. So therefore what does it imply? It implies that at constant T and P automatically $\sum_i x_i d \ln \gamma_i = 0$.

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Handwritten derivation on a whiteboard:

$$\frac{h^E}{T} dT - R \sum_i x_i \ln \gamma_i dT - v^E dp + R \sum_i x_i \ln \gamma_i dT + RT \sum_i x_i d \ln \gamma_i = 0$$

$$\frac{h^E}{T} dT - v^E dp + RT \sum_i x_i d \ln \gamma_i = 0$$

↳ G.D. eqn in terms of activity coefficient

Just the same equation which I have derived here but this was the generalized expression at constant T and P this goes out. So therefore this is the equation which I have derived in this particular case as well, right?

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Gibbs – Duhem Relation for Activity Coefficient

$$\frac{h^E}{T} dT - v^E dP + RT \sum_{i=1}^c x_i d \ln \gamma_i = 0$$

$$\sum_{i=1}^c x_i d \ln \gamma_i = \frac{v^E}{RT} dP \quad (\text{at constant } T)$$

$$\sum_{i=1}^c x_i d \ln \gamma_i = \frac{h^E}{RT^2} dT \quad (\text{at constant } P)$$

$$\sum_{i=1}^c x_i d \ln \gamma_i = 0 \quad (\text{at constant } T \text{ and } P)$$

Influence of Temperature & Pressure on Activity coefficient

$$\left(\frac{\partial \ln \gamma_i}{\partial T} \right)_{P, x_i} = \left[\frac{\partial \left(\frac{g_i^E}{RT} \right)}{\partial T} \right]_{P, x_i} = - \frac{\overline{h}_i^E}{RT^2}$$

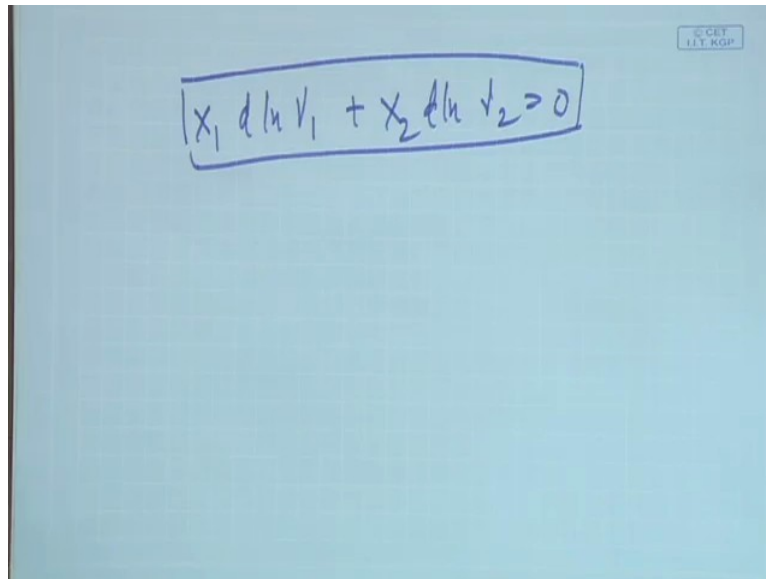
$$\left(\frac{\partial \ln \gamma_i}{\partial P} \right)_{T, x_i} = \left[\frac{\partial \left(\frac{g_i^E}{RT} \right)}{\partial P} \right]_{T, x_i} = \frac{\overline{v}_i^E}{RT}$$

$\frac{g^E}{RT} = \sum x_i \frac{\overline{g}_i^E}{RT} = \sum x_i \ln \gamma_i$

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So therefore this is the generalized equation which we have we find that at constant temperature naturally this term goes off and this is the equation at constant pressure this term goes off and therefore this is the equation at constant temperature and pressure I have derived this equation in two particular ways and we find that this is the equation. Now this equation just like I had told you previously this equation is very important particular importance or can be better appreciated if we can write it down in terms of a binary mixture.

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A handwritten equation is shown on a blue grid background. The equation is enclosed in a hand-drawn rectangular box and reads: $x_1 d \ln v_1 + x_2 d \ln v_2 = 0$. In the top right corner of the grid, there is a small logo that says "© CET" and "I.I.T. KGP".

In terms of a binary mixture what do how can we write down the equation it is $x_1 d \ln \gamma_1 + x_2 d \ln \gamma_2 = 0$, agree? So therefore from this particular equation there are a number of important information that we can get which you are going to discuss in the next class.