

Process Control and Instrumentation
Prof. A. K. Jana
Department of Chemical Engineering
Indian Institute of Technology, Kharagpur

Lecture - 25
Feedback Control Schemes (Contd.)

(Refer Slide time: 01:08)

© CET
IIT KGP

Prode plot: first-order system.

$$G(s) = \frac{K}{\tau s + 1} \quad \text{----- TF of a first-order system.}$$

$$AR = \frac{K}{\sqrt{1 + \tau^2 \omega^2}} \quad \phi = \tan^{-1}(-\tau \omega)$$

$$\log \frac{AR}{K} = -\frac{1}{2} \log(1 + \tau^2 \omega^2)$$

Asymptotic considerations.

Amplitude ratio

① $\tau \omega \rightarrow 0$, $\frac{AR}{K} \rightarrow 1$, and $\log(AR/K) \rightarrow \log 1$

MR vs $\tau \omega$: $MR = \frac{AR}{K} = 1$. ✓ low-frequency asymptote.

So, we will continued discussion on the constructions of prode plot in the last class we discuss the construction of prode plot with taking three examples, fine. So, today will discuss the construction of prode plot for a first order system. So, the transfer function of a first order system is return as K divided by tau s plus 1 this is the transfer function of a first order system now we untainted the expirations for amplitude ration and phi in the previous class.

As amplitude ratio equals K divided by root over of 1 plus tau squire omega squire and we obtained the expiration for phase angle as 5 equals ten inverse minus tau omega now we will take the logarithm of this amplitude ratio expiration in both said then we can write as amplitude ratio by K log amplitude ratio by K equals minus half log 1 plus tau squire omega squire fine

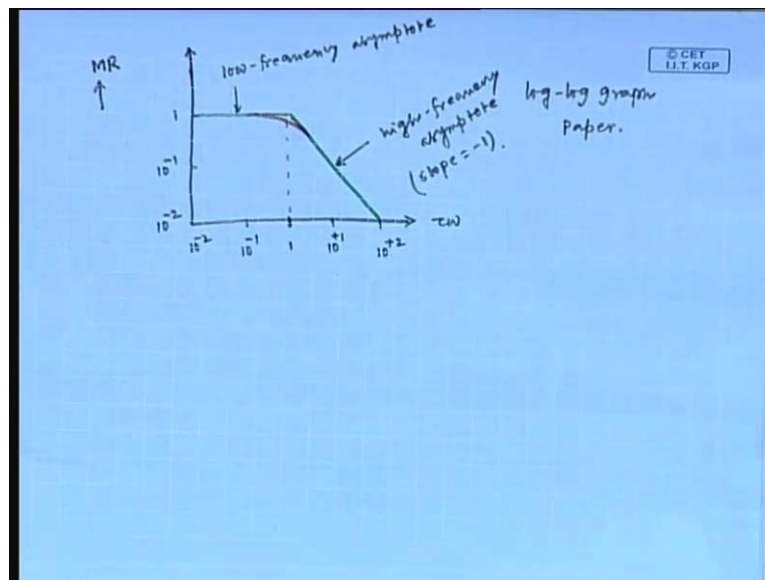
So, this is the magnitude ratio basically next we will considered the asymptotic considerations before making the plot we need to discuss the asymptotic considerations

first we will considered the amplitude ratio first we will discuss the amplitude ratio then we will discuss the phase angle fine now if we considered tau omega tends two 0.

If we considered tau omega tens two 0 then amplitude ratio by K tens to 1 here the amplitude ratio is multiply do it 1 by K that mean this is scaled amplitude ratio and here wear considering scaled omega I mean tau omega we are considering now if we considered tau omega tends to 0 then amplitude ratio by k tends to 1. So, we can write that log amplitude ratio by K tends to log 1 fine. So, at the very low sequence is the log log plot of magnitude ratio verses tau omega tends to the horizontal line.

At very low sequence is the log log plot of magnitude ratio verses tau omega tends to a horizontal line represented by magnitude ratio equals amplitude ratio by K in equals 1 fine since this situations arise is at low frequency is this line is cold low frequency asymptote since this situation arise is act low frequencies this line is cold low frequency asymptote fine now if we if produce the plot considering this equation I mean this line then what we obtained.

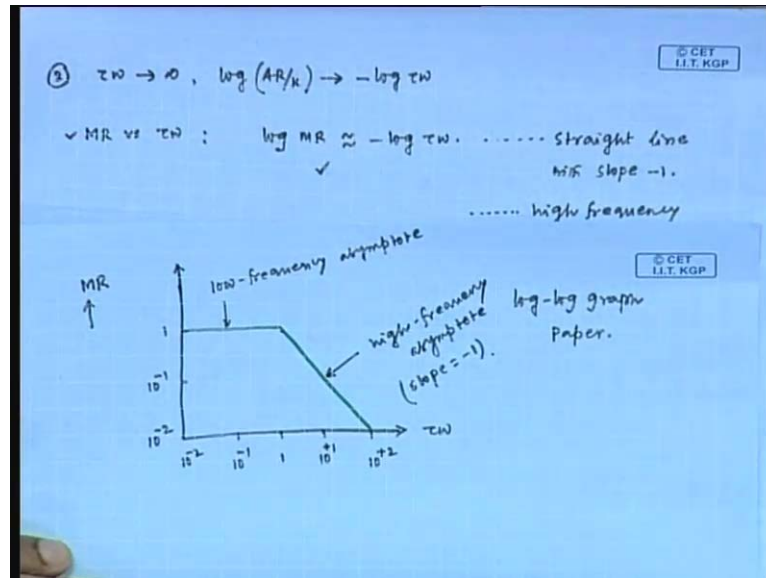
(Refer Slide time: 06:56)



. So, here wear considering tau omega and here magnitude ratio this is a log log plot. So, wear using log log graph paper this is ten to the power minus 2 10 to the power minus 1 1 10 and this is suppose 10 to the power plus 2 and here wear considering 10 to the power minus 2 10 to the power minus 1 than suppose this is 1, fine.

Now, we obtained this form log amplitude ratio by K approximately equal to log 1 when we considered low frequencies; that means, it is clearly a horizontal line fine. So, this is and this is the low frequency asymptote this is low frequency asymptote fine now under asymptotic consideration next we will consider tau omega tends to infinity.

(Refer Slide time: 09:36)

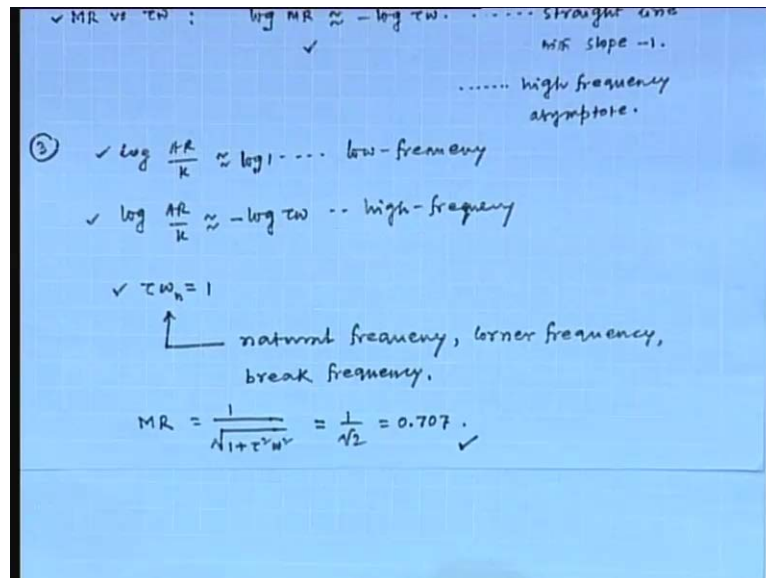


In the next we will considered tau omega tends to infinity as tau omega tends to infinity then we can write log amplitude ratio by K tends to minus log tau omega when tau omega is much much better one we can neglect this one term I mean this is the general form when tau omega tends to infinity we can neglect this one; that means, this right hand said becomes minus log tau omega agree. So, when tau omega tends to infinity we can write log amplitude ratio by K tends to minus log tau omega. So, the log log plot of magnitude ratio verses tau omega tends to the line represented log magnitude ratio approximately equal to minus log tau omega.

in the log log plot of magnitude ratio verses tau omega we obtain we need to considered this equations log magnitude ratio approximately equals to minus log tau omega this is nothing, but a straight line with slope minus one this is a straight line with slope minus one and this situation arise is act high frequencies there for this straight line is cold as high frequency asymptote since this situation arise is act high frequencies this straight line is cold as high frequency asymptote fine. So, using I mean we will next considered this equation in the prode plot. So, it is basically straight line with slope minus 1. So, this

is representing the high frequency asymptote this is representing high frequency asymptote.

(Refer Slide time: 13:45)



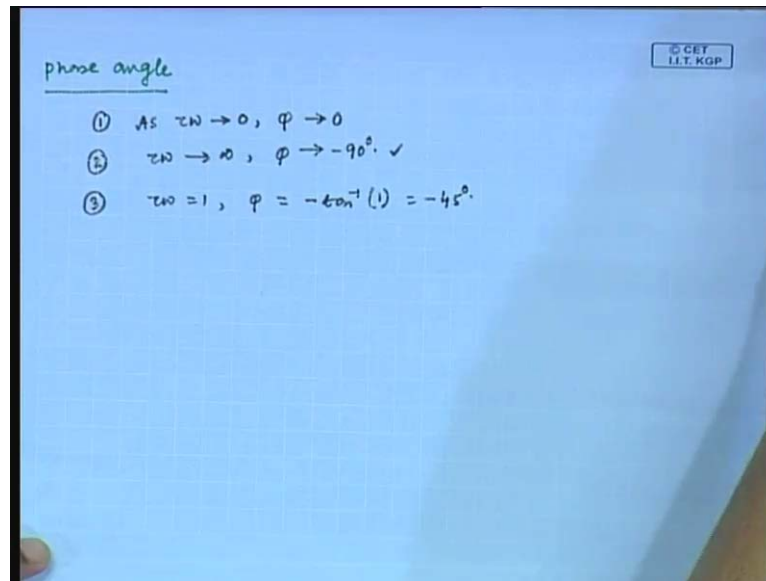
It has slope of minus 1 fine in the next step we need to determined the point of intersection in the third step we need to determined the point at which the two asymptote intersect when we considered tau omega tends to 0, we got log amplitude ratio by K is nearly equal to 1. This we considered low frequency asymptote when we considered tau omega tends to infinity we got now this we got log 1. So, when we considered tau omega tends to infinity we got log amplitude ratio by K which is approximately equal to minus log tau omega fine now if we equate these two equations equating these two equations we obtain.

Tau omega equals one agree equating these two equations this 1 and this 1 we obtain tau omega equals one; that means, they inter set act tau omega equals one, now in this situation we usually use one suffix for this omega that is in act this situations we use the suffix in for omega; that means, we can write tau omega n equals 1 the value of omega act which this two frequency to asymptote inter sets that is cold natural frequency. So, here omega in is the natural frequency.

And most popularly it is cold as corner frequency it is also cold as break frequency fine now can we determined the exact values of the magnitude receive add this corner frequency what is the exact value of magnitude ratio act this corner frequency we have

the expiration of magnitude ratio that is magnitude ratio equals 1 divided by root over of 1 plus tau square omega square fine. So, this is the exact value of magnitude ratio at corner frequency according to we need to construct the Bode diagrams I mean this magnitude ratio versus tau omega plot should look like this like this and the corresponding tau omega is 1 here.

(Refer Slide time: 18:38)



This is the corresponding natural frequency in this first plot. So, this is the asymptotic considerations in terms of amplitude ratio and we obtained this plot similarly we need to consider the asymptote consideration in terms of phase angle. So, next we will consider the phase angle as tau omega tends to 0 phi tends to what zero fine in the second as tau omega tends to infinity how much is phi [vocalized- noise] minus 90; that means, phi tends to minus 90.

So, phi never we lay less than minus 90 fine, it clearly indicates that phi never we less than minus 90 and in the third situation, we will consider the corner frequency at the corner frequency; that means, tau omega equals 1 how much is phi phi is minus 45 minus tan inverse 1.

(Refer Slide time: 20:31)

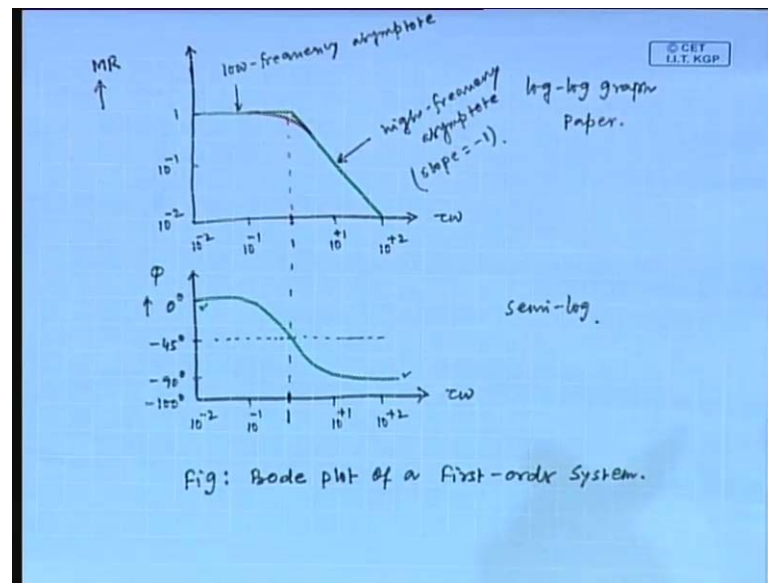


Fig: Bode plot of a first-order system.

So, this is minus forty five. So, these are the asymptote considerations in terms of phase angle now we will draw the plot of ϕ versus $\log \tau \omega$ plot this is the semi log graph paper and this is 1 which corresponds to the corner frequency 10^{-2} to the power minus 1 this is 10^{-1} to the power plus 1 and 10^0 to the power plus 2, this is suppose minus 100 degree minus 90 degree this is a minus 45 degree this is a 0 degree at low frequencies at low frequencies the $\tau \omega$ the five is 0 fine. So, it is somewhat like this at low frequencies ϕ is 0 and when $\tau \omega$ tends to infinity we obtain 5 minus 90.

And when $\tau \omega$ equals 1 we obtained minus 45 degree at low frequencies this ϕ is near to near 0 and as $\tau \omega$ tends to infinity this is minus 90 and at corner frequency this is minus 45. So, this is the Bode plot for a first order system this is the Bode plot of a first order system in the next we will discuss the construction of Bode plot for a second order system.

(Refer Slide time: 23:31)

Bode plot: Second-order System.

$$G(s) = \frac{K}{\tau^2 s^2 + 2\zeta\tau s + 1}$$

$$\frac{AR}{K} = \frac{1}{\sqrt{(1-\tau^2\omega^2)^2 + (2\zeta\tau\omega)^2}}$$

$$\phi = \tan^{-1} \left(\frac{-2\zeta\tau\omega}{1-\tau^2\omega^2} \right)$$

Asymptotic considerations.

Amplitude Ratio

① As $\tau\omega \rightarrow 0$, $\frac{AR}{K} \rightarrow 1$, $\text{mag log } \frac{AR}{K} \rightarrow \log 1$.
horizontal line.

② As $\tau\omega \rightarrow \infty$, $\log \frac{AR}{K} \rightarrow -\frac{1}{2} \log \tau^4 \omega^4 = -2 \log \tau\omega$.

In the next we will discuss the Bode plot of a second order system. So, the transfer function of a second order system we considered earlier taking this form $G(s) = \frac{K}{\tau^2 s^2 + 2\zeta\tau s + 1}$ and in the last class we derived the expressions for amplitude ratio and phase. So, they are amplitude ratio divided by K equals one divided by root over of one minus $\tau^2 \omega^2$ square plus $2\zeta\tau\omega$ square. Similarly the expression of phase is return as \tan^{-1} minus $2\zeta\tau\omega$ divided by $1 - \tau^2 \omega^2$. These two expressions we derived earlier. Now we will discuss the asymptotic considerations in terms of first amplitude ratio and phase angle.

Asymptotic consideration first we will consider amplitude ratio as $\tau\omega$ tends to zero. Amplitude ratio by K tends to one and \log amplitude ratio by K tends to $\log 1$. As $\tau\omega$ tends to 0 we obtained amplitude ratio by K tends to 1 and accordingly \log amplitude ratio by K tends to $\log 1$.

Now, it is clear that the low frequency asymptote is a horizontal line. It clearly says that this is a horizontal line. Next we will consider $\tau\omega$ tends to infinity. So, as $\tau\omega$ tends to infinity \log amplitude ratio by K tends to $-\frac{1}{2} \log \tau^4 \omega^4 = -2 \log \tau\omega$. Here we neglect all lower order terms.

So, this is equal to basically $-2 \log \tau\omega$ as we considered $\tau\omega$ tends to infinity we obtained \log amplitude ratio by K tends to $-\frac{1}{2} \log \tau^4 \omega^4$.

4 omega to the power four here all low order. Terms have been neglected. So, it is than becomes minus two log tau omega. So, this is a straight line with slope minus two. So, this is a straight line with slope minus 2, so the low frequency.

(Refer Slide time: 29:20)

$$\frac{AR}{K} = \frac{1}{\sqrt{(1-\tau^2\omega^2)^2 + (2\tau\omega)^2}} \quad \phi = \tan^{-1} \left(\frac{-2\tau\omega}{1-\tau^2\omega^2} \right)$$

Asymptotic considerations.

Amplitude Ratio

① As $\tau\omega \rightarrow 0$, $\frac{AR}{K} \rightarrow 1$, and $\log \frac{AR}{K} \rightarrow \log 1$.
horizontal line. ✓

② As $\tau\omega \rightarrow \infty$, $\log \frac{AR}{K} \rightarrow -\frac{1}{2} \log \tau^4 \omega^4 = -2 \log \tau\omega$.
... straight line with slope -2. ✓

Asymptote is a horizontal line and the high frequency asymptote is a straight line with slope minus 2 for the first order system we obtained horizontal line as low frequency asymptote, but high frequency asymptote is a straight line with slope minus 1.

(Refer Slide time: 30:18)

③ $\log \frac{AR}{K} \approx \log 1$... low-frequencies.

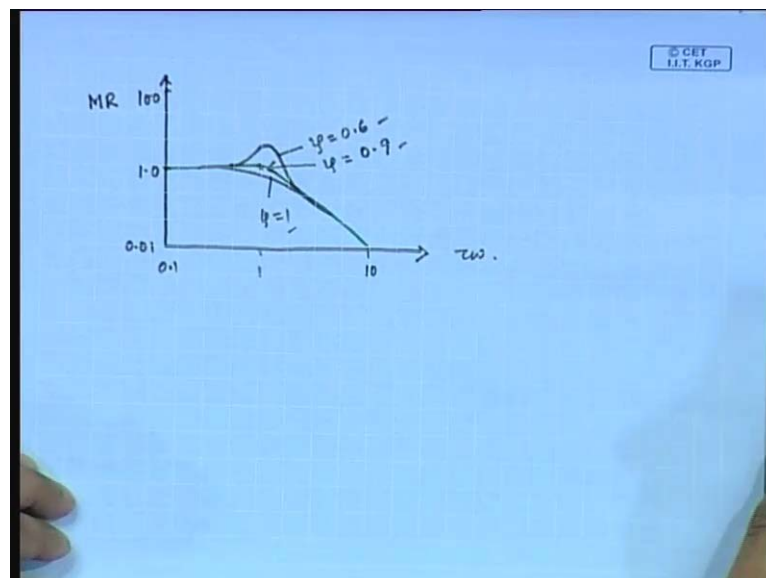
$\log \frac{AR}{K} \approx -2 \log \tau\omega$... high-frequencies.

$\tau\omega = 1$. ✓

MR - 4. ✓

And for second order system the slope is minus two we now we can produce the plot of magnitude ratio verses tau omega before that we need to determined the point of intersection fine. So, this is say third step. So, we got basically log amplitude ratio by K which is approximately equal to log 1 this equation we obtain at low frequencies and for high frequencies. We obtained minus two log tau omega. So, equating these two equations we obtained again tau omega equals one again we obtain tau omega equals one, but here we cannot determine the exact values of magnitude ratio because that is also function of zeta here the exact value at corner frequency we can obtain ally knowing the value of zeta. So, here the magnitude ratio

(Refer Slide time: 32:19)



Can be obtain by knowing the value of zeta and this should be deflected in the prode plot fine next we will construct the prode plot and first we consider magnitude ratio verses tau omega say this is zero point one than one and this is ten zero point zero one the starting value of magnitude ratio next one is one and this is a 100. So, act low frequencies we obtained a horizontal line fine and at high frequencies we obtained a straight line with slope minus two it was mention that the magnitude ratio at the point of intersection depends on the value of zeta. So, accordingly we will considered the three different cases whirring the zeta values.

This type of response we obtained if zeta is say zero point six which is quit lace this one we obtained when zeta is say zero point nine and this plot we obtained zeta is one fine

considering three different values of zeta we obtained three different plots as magnitude ratio verses tau omega.

(Refer Slide time: 35:40)

© CET
I.I.T. KGP

phase angle

① $\tau\omega \rightarrow 0$
 \checkmark \checkmark $\phi \approx \tan^{-1}(-2\zeta\tau\omega)$, $\tau\omega \ll 1$
 $\tau\omega \rightarrow 0, \phi \rightarrow 0$

② $\tau\omega \rightarrow \infty$
 \checkmark $\phi = \tan^{-1}\left(\frac{-2\zeta\tau\omega}{1-\tau^2\omega^2}\right) = \tan^{-1}\left(\frac{-2\zeta}{\frac{1}{\tau\omega} - \tau\omega}\right)$
 $= \tan^{-1}\left(\frac{2\zeta}{\tau\omega}\right)$ $\tau\omega \rightarrow \infty$
 $\phi \rightarrow \tan^{-1}\left(\frac{2\zeta}{\tau\omega}\right) = \tan^{-1}(0) = -90^\circ$

③ $\tau\omega = 1$, $\phi = \tan^{-1}(-1) = -90^\circ$
 \checkmark \checkmark \checkmark \checkmark

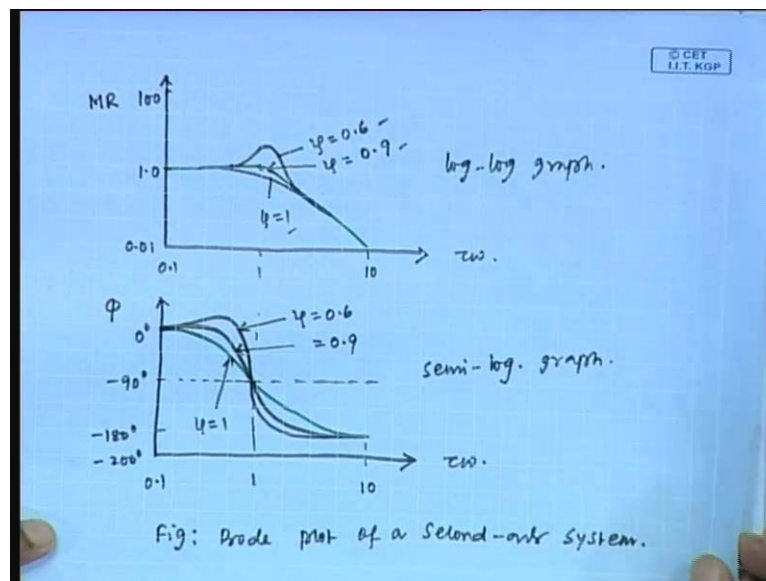
So, these are the three plots this top one corresponds to zeta equals 0.6 next 1 corresponds to zeta equals 0.9 and this bottom was to 1 corresponds to that equals 1 next we will discuss the asymptotic considerations in term of phase angle next we will discuss the asymptotic consideration in term of phase angle when tau omega tends to 0 we can write phi equals tan inverse minus 2 zeta tau omega can we write this.

This we can write when tau omega becomes much less than unity when tau omega much less than unity fine now if we consider tau omega tends to 0 now if we consider tau omega tends to 0 this phi approaches 0 agree if tau omega is much less than 1 we can write the phi expression like this tan inverse minus 2 zeta tau omega now if we consider tau omega tends to 0 the phi approaches 0. Secondly, we consider tau omega tends to infinity. So, in this case we can write the phi expiration as 10 inverse minus 2 zeta tau omega divided by 1 minus tau square omega square this is the original expiration, we can write this as 10 inverse minus 2 zeta divided by 1 by tau omega minus tau omega agree. So, this is equal to tan inverse two zeta by tau omega when we considered tau omega tends to infinity agree. So, this one we can write in this form considering tau omega tends to infinity. So, than phi tends to 10 inverse 2 zeta by tau omega which is equal to

tan inverse 0 agree this expirations we got now we are considering tau omega tends to infinity.

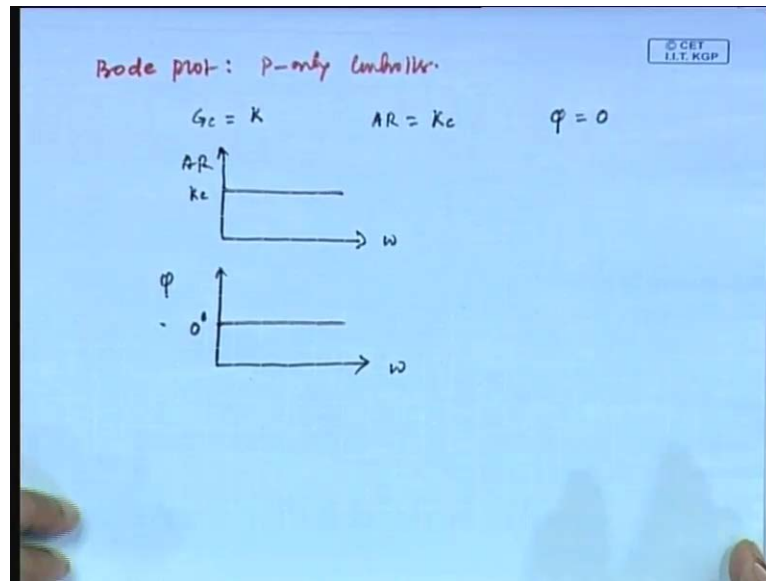
So, we can write tan inverse 0 and this is equal to minus 180 degree this is considered as minus 180 fine in the third case we will considered tau omega equals ,1 I mean the point of intersection tau omega equals 1 now in this case re gall is the value of zeta phi becomes tan inverse minus infinity which is minus 90, which is minus 90 tau omega equals 1 corresponds to the corner frequency and regal less of the value of the zeta we obtain phi equals tan inverse minus infinity; that means, this is minus 90 now you see initially we consider tau omega tense to 0 and this is tau omega equals 1. So, this is the lowest one this is the intermediate 1 and this is the highest 1 fine here the phi value is maximum this is intermediate and this is minimum. So, there is a train in prode plot fine.

(Refer Slide time: 41:10)



Now, we will try to produce the plot between phi verses tau omega and this is phi 0.1 this is indicating one and this is ten and this is suppose minus 200 degree minus 180 degree minus 90 degree 0 degree this plot also considered the different values of zeta This is one plot this is the second plot this is the third plot this top one we obtain for zeta zero point six second one we obtain I mean intermediate 1 we obtain considering zeta 0.9 and this one we obtained considering zeta equals 1 fine. So, this is the prode plot of a second order system the top one is plotted in using log log graph paper and the bottom one is obtain considering semi log graph paper, fine.

(Refer Slide time: 44:29)



In the last example we will consider a feedback control system a feedback controller and we will construct the Bode plot. So, next we want to discuss the construction of Bode plot for a P only controller the transfer function of a P only controller is $G_c = K_c$. So, we can write Amplitude Ratio equals K_c and the phase angle we can write as $\phi = 0$. So, both are independent of ω . So, it is easy to develop the Bode plot this is indicating ω and this is indicating Amplitude Ratio since K_c is independent of ω this should be a straight line across in the top plot. We consider ϕ versus ω and ϕ remains 0 all the time I mean that is also a horizontal line having $\phi = 0^\circ$. So, this is the Bode plot of a P only controller.

(Refer Slide time: 46:25)

Bode plot: PI controller.

$$G_c = K_c \left(1 + \frac{1}{\tau i s} \right)$$

$$G_c(j\omega) = K_c \left(1 + \frac{1}{j\tau\omega} \right) = K_c \left(1 - \frac{j}{\tau\omega} \right)$$

$$\checkmark AR = K_c \sqrt{1 + \frac{1}{\tau^2\omega^2}} \quad \phi = \tan^{-1} \left(-\frac{1}{\tau\omega} \right)$$

$$\log \frac{AR}{K_c} = \frac{1}{2} \log \left[1 + \frac{1}{(\tau\omega)^2} \right]$$

Asymptotic Considerations.

AR: As $\omega \rightarrow 0$, $\frac{1}{(\tau\omega)^2} \gg 1$, $\log \frac{AR}{K_c} \rightarrow \frac{1}{2} \log \frac{1}{\tau^2\omega^2} = -\log \tau\omega$
 ... straight line with slope -1.

Next is the P i controller the P i controller has the transfer function and it can be written as $G_c = K_c \left(1 + \frac{1}{\tau i s} \right)$ replacing a s by $j\omega$ replacing a s by $j\omega$. We can write for the frequency response transfer function as K_c multiplied by one plus one divided by $j\tau i \omega$ we can write this as $K_c \left(1 - \frac{j}{\tau i \omega} \right)$. So, from this cartesian form it is straight forward to determine the expression for amplitude ratio and ϕ . So, amplitude ratio we obtain as $K_c \sqrt{1 + \frac{1}{\tau^2 \omega^2}}$

Similarly, we can write the expression for ϕ $\phi = \tan^{-1} \left(-\frac{1}{\tau i \omega} \right)$ this is the expression for ϕ now we can write this expression of amplitude ratio by taking algorithm as $\log \frac{AR}{K_c} = \frac{1}{2} \log \left[1 + \frac{1}{(\tau\omega)^2} \right]$

If we take the algorithm of this expression we can write $\log \frac{AR}{K_c} = \frac{1}{2} \log \left[1 + \frac{1}{(\tau\omega)^2} \right]$ fine in the next we considered the asymptotic considerations, first we consider the amplitude ratio as ω tends to 0 $\frac{1}{\tau^2 \omega^2} \gg 1$ because much much higher than 1 agree.

So, we can write as $\log \frac{AR}{K_c} \rightarrow \frac{1}{2} \log \frac{1}{\tau^2 \omega^2} = -\log \tau\omega$ which is equal to $-\log \tau\omega$ agree if we considered ω tends to 0 we can say that $\frac{1}{\tau^2 \omega^2}$ is much much higher than one than this expression eldes this. So, the low frequency asymptote is a straight line.

(Refer Slide time: 51:29)

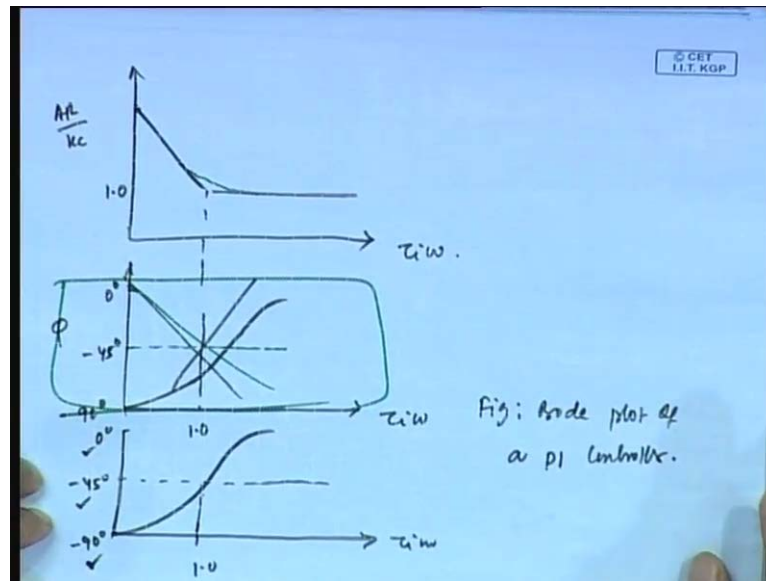
$\phi \rightarrow \tan^{-1}(-\infty) = -90^\circ.$

② $\omega \rightarrow \infty, \frac{1}{\tau^2 \omega^2} \rightarrow 0, \log \frac{A.R}{K_c} \rightarrow \log 1$
... horizontal line.
 $\phi \rightarrow 0^\circ$

③ $\tau_1 \omega_n = 1.0.$ $\phi = -\tan^{-1}(1) = -45^\circ$
 $\frac{A.R}{K_c} = \sqrt{2} = 1.414$

So, this is a straight line with slope minus 1 fine. So, what will be phi than if we consider omega tends to 0 phi becomes tan inverse minus infinity agree which is equal to minus 90 degree it is very straight forward, because we have this expression we are just considering omega tense to 0. In the next step we will consider omega tense to infinity than one by tau i square omega square approach a 0. Accordingly we can write log amplitude ratio by K c tense to log 1. So, at high the frequency into the horizontal line high frequency asymptote is a horizontal line and how much is phi if omega tense to infinity phi becomes 0 degree next one is the determination of corner frequency we obtained the corner frequency, when tau i omega n equals 1.0 fine accordingly phi becomes minus tan inverse 1 which is minus 45 degree and amplitude ratio by K c becomes root 2 which is 1.4 1 4, fine. So, these are the asymptote consideration an next we will make the plot amplitude ratio by K c and next one is phi verses tau i omega.

(Refer Slide time: 54:03)



So, when omega tends to 0 we obtain straight line with minus 1 somewhat like this and this is indicating the corner frequency and when omega tends to infinity this is a straight line like this fine. So, we get this type of Bode plot similarly here, we obtained minus 90 we obtain like this plot for phi versus tau i omega here this this should be like this is 45 I am re join it tau i omega this is suppose 1 this is minus 90 degree

So, this is minus 45 and this is 0 degree. So, it will go like this fine. So, this is indicating the corner frequency at which phi is minus 45 and at low frequency this is minus 90 and at high frequency at high frequency this is 0. So, you just do not consider this 1 fine. So, this is the Bode plot of a P i controller Bode plot of a P i controller thank you any question minus 180. You know in the Bode plot if there is no trained that cannot be used.