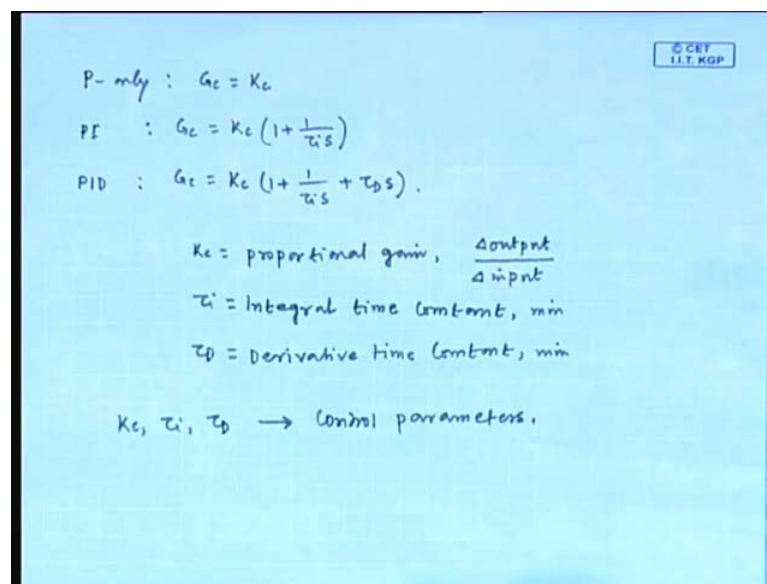


Process Control and Instrumentation
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Lecture - 17
Feedback Control Schemes (Contd.)

In the last class we discussed three different control schemes, proportional controller, proportional integral controller and proportional integral derivative controllers.

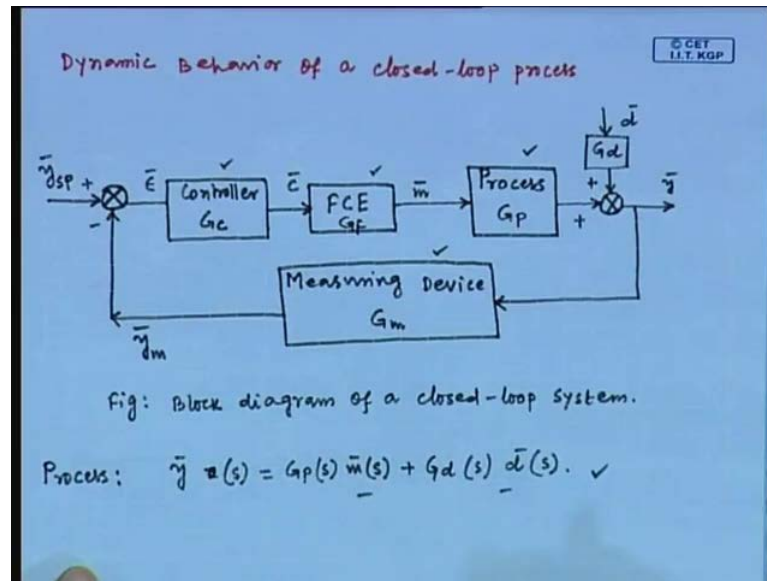
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We discussed P only controller having the transfer function of G_c equals K_c , we discussed P I controller having the transfer function of G_c equals $K_c \left(1 + \frac{1}{\tau_i s}\right)$. We discussed the P I D controller having the transfer function of G_c equals $K_c \left(1 + \frac{1}{\tau_i s} + \tau_d s\right)$. Now, here K_c is basically the proportional gain and this gain equals $\frac{\Delta \text{output}}{\Delta \text{input}}$. I mean change in output per unit change in input, so the unit of proportional gain K_c depends on the unit of output as well as the unit of input.

And τ_i is the integral time constraint, the unit of τ_i is time, I mean it may be minute may be hour, so the unit of integral time constant is say minute. Another term which is involved in derivative term that is τ_d , τ_d is derivative time constant, unit of derivative time constant is minute or it may be hour fine. So, these three parameters are basically the control parameters, K_c , τ_i and τ_d are the control parameters, tuning of these parameters will be discussed later. How you can select the values of these three parameters that will be discussed later fine.

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So, today we will start with the dynamic behavior of closed loop process, first we will discussed in generalized form, then we will considered few specific cases, we will considered few examples. Now, to discuss this we need to develop the block diagram of the close loop process, the block diagram of the close loop process we already discuss in the previous class, so I am just redrawing the block diagram of a typical closed loop process.

So, this block is representing the process having the transfer function of G suffix P , this block is representing the process having the transfer function of G suffix P , in is the input to the process m is the input to the process which is basically the output of final control element. Now, the output of this is added with this output fine, this two outputs are added d is the disturbance and $G d$ is the transfer function of the process with respect to disturbance, output is y bar process output is represented by y , and in Laplace doming that is y bar.

Now, what is run first the process output is measured using tape measuring devise, the process output is measured using a measuring devise, say the measuring devise as the transferring function of $G m$. Now, the measure output, usually defers from the actual output, so we will represent the measured output by $y m$, then this measured output is compared with the step one value of process output. The measured output is compared in the comparator with its step one value, the output of this comparator is ϵ , and this output is supply to the controller, the controller transfer function we are representing by $G c$, controller output is say c .

And this c is implemented through the final control element FCE, and this final control element has the transfer function of suppose G_f . So, this is the block diagram of a closed loop system, now we will discuss different elements of this closed loop transfer function, different elements or process, measuring device, controller final control element. These are the different elements of this closed loop process one is the process, another one is measuring device, then controller and final control element and we will try to represent these elements by mathematical forms.

So, if we considered the process we can write for the process $\bar{y}(s)$ equals $G_p \bar{u}(s)$ multiplied by $\bar{m}(s)$ plus $G_d \bar{d}(s)$, can we write this, the process can be for the process; we can write this equation these two signals are added, this and this signal is added now this equation is representing the process.

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Measuring device: $\bar{y}_m(s) = G_m(s) \cdot \bar{y}(s)$.

Controller: $\bar{e}(s) = \bar{y}_{sp}(s) - \bar{y}_m(s)$ Comparator.
 $\bar{c}(s) = G_c(s) \cdot \bar{e}(s)$ Controller.

FCE: $\bar{m}(s) = G_f \bar{c}(s)$.
 $= G_f \cdot G_c(s) \cdot \bar{e}(s) = G_f G_c \cdot [\bar{y}_{sp} - \bar{y}_m]$
 $\bar{m} = G_f G_c [\bar{y}_{sp} - G_m \bar{y}]$

Next one is the measuring device output is y_m , so in Laplace domain \bar{y}_m is equals $G_m \bar{y}$, for the measuring device we can write this equation output equals transfer function multiplied by input. Next element is the controller, the input signal to the controller \bar{e} equals $\bar{y}_{sp} - \bar{y}_m$, input signal to the controller \bar{e} equals $\bar{y}_{sp} - \bar{y}_m$ this is representing the comparator. Similarly, the controller output is \bar{c} , controller transfer function is G_c and input to the controller is \bar{e} , so \bar{c} equals $G_c \bar{e}$ multiplied by \bar{e} this is representing the control block.

Now, final control element FCE, for final control element the output is m bar transfer function is G_f and input is c bar s , so for final control element we can write output m equals transfer function G_c multiplied by c fine. Now, this m bar is we can write again as G_f multiplied by c s , c s means what c s means G_c s multiplied by ϵ bar s , can we write this, c s equals G_c s multiplied by ϵ bar s .

Now, we will substitute the expression for ϵ bar s now, so $G_f G_c \epsilon$ bar s is y set point bar minus y m bar fine, ϵ bar s is y set point bar s minus y m bar s . In the next step we will substitute the expression of y m, so $G_f G_c y$ set point bar minus y m bar, what is the expression of y m bar G_m s multiplied by y bar s , we are not writing s anymore, so this is the expression of m bar agree.

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$$\begin{aligned} \bar{y} &= G_p \bar{m} + G_d \bar{d} \quad \dots \dots \dots \text{Process.} \\ &= G_p \{ G_f G_c (\bar{y}_{sp} - G_m \bar{y}) \} + G_d \cdot \bar{d} \\ \bar{y} &= \frac{G_p G_f G_c}{1 + G_p G_f G_c G_m} \bar{y}_{sp} + \frac{G_d}{1 + G_p G_f G_c G_m} \bar{d} \end{aligned}$$

Effect of y_{sp} on y d on y .

..... closed-loop Transfer function
CLTF

Now, we have written the expression for the process as y bar equals G_p m bar plus G_d d bar, we are written equation previously for the process fine, now here will substitute the expression of m bar, so G_p multiplied by m bar; that means, $G_f G_c y$ set point minus $G_m y$ bar, this is m bar. Now, the second term is G_d d bar fine, we are just substituted the expression of m bar in the equation of process. Now, if we rearrange this equation we finally, get y bar equals $G_p G_f G_c$ divided by 1 plus $G_p G_f G_c G_m$ y set point bar plus second term is G_d divided by 1 plus $G_p G_f G_c G_m$ d bar, by rearranging we get this equation.

Now, the first right hand term this provides the effect of y set point on y , similarly the second term second right hand term provides the effect of disturbance on y , now this equation is the

closed loop transfer function, this equation is called closed loop transfer function CLTF fine, this is the expression of closed loop transfer function.

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..... closed-loop Transfer function
CLTF

$$G_p G_f G_c = G \quad \checkmark$$

$$\bar{y} = \frac{G}{1 + G G_m} \bar{y}_{sp} + \frac{G_d}{1 + G G_m} \bar{d}$$

$$= G_{sp} \cdot \bar{y}_{sp} + G_{load} \bar{d} \quad \dots \checkmark$$

where, $G_{sp} = \frac{G}{1 + G G_m}$; $G_{load} = \frac{G_d}{1 + G G_m}$.

```

graph LR
    Ysp["y_sp"] --> Gsp["G_sp"]
    d["d-bar"] --> Gload["G_load"]
    Gsp --> Sum((+))
    Gload --> Sum
    Sum --> Ybar["y-bar"]
  
```

Now, if we considered $G_p G_f G_c$ equals G considering $G_p G_f G_c$ equals G , we get the closed loop transfer function \bar{y} equals G divided by $1 + G G_m$ \bar{y}_{sp} plus G_d divided by $1 + G$ multiplied by G_m \bar{d} fine. Considering $G_p G_f G_c$ equals G we get this form of closed loop transfer function, now again will consider this as G set point multiplied by \bar{y}_{sp} plus G load multiplied by \bar{d} .

Here, G set point equals G divided by $1 + G G_m$ and G load equals G_d divided by $1 + G G_m$, considering this two expression for G set point and G load finally, we get this closed loop transfer function. Can we corresponding block diagram what will be the block diagram of this final form of closed loop transfer function? It is very simple we can consider one block for G set point, what is the input? Input is \bar{y}_{sp} , now this output is added, which the output of the this load block I mean this two outputs are added and finally, we get \bar{y} fine.

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$$\bar{y} = \frac{G_c G_p G_f}{1 + G_c G_p G_f G_m} \bar{y}_{sp} + \frac{G_d}{1 + G_c G_p G_f G_m} \bar{d}$$

Servo Test $\bar{d} = 0$ $\bar{y} = \frac{G_c G_p G_f}{1 + G_c G_p G_f G_m} \bar{y}_{sp}$

Regulatory Test $\bar{y}_{sp} = 0$

$$\bar{y} = \frac{G_d}{1 + G_c G_p G_f G_m} \bar{d}$$

This is the block diagram of the final closed loop transfer function, so our original transfer function is $G_c G_p G_f$ divided by $1 + G_c G_p G_f G_m$ plus G_d divided by $1 + G_c G_p G_f G_m$ multiplied by \bar{d} . We will use this transfer function mostly in the analysis of different features. You see here the transfer function of measuring device does not exist in the numerator. And in the denominator in this term particularly all the transfer functions are included, all the individual transfer functions are included in the denominator.

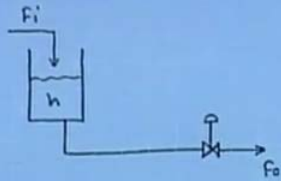
Now, the control performance is usually investigated by performing two tests, one is servo test and another one is regulatory test, so what is servo test, in the case of servo test there is no change introduced in the disturbance, in the servo test there is no change introduced in the disturbance. That means, \bar{d} equals 0 only the set point change is considered, now if \bar{d} becomes 0, what is the closed loop transfer function for the servo problem.

So, close loop transfer function for the servo problem, becomes $G_c G_p G_f$ divided by $1 + G_c G_p G_f G_m$ multiplied by \bar{y}_{sp} , this is the close loop transfer function for the servo problem. Now, introducing step change may be sinusoidal change in y set point and by taking inverse of Laplace transform we can know the transient response $y(t)$ by that wave we can test the controller. This is called servo problem and sometimes another term is used that is set point tracking, so set point tracking performance is absorbed by performing servo test.

Another test is regulatory test, regulatory test is conducting by considering no change in set point; that means, y set point bar equals 0. Regulatory test is conducting by considering no change in set point value accordingly, the closed loop transfer function become y bar equals G_d divided by $1 + G_c G_p G_F G_m d$ bar. So, this is the closed loop transfer function for the case of regulatory problem, another term is again used for this that is disturbance rejection performance, so to absorb the disturbance reaction performance of a controller regulatory test is conducted, set point tracking performance is absorbed by conducting servo test and disturbance rejection performance is absorb by conducting regulatory test.

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Formation of closed-loop Block Diagram:
Liquid Level System.



CV	MV	LV
h	Fo	Fi

Process: $A \frac{dh}{dt} = F_i - F_o$... in terms deviation variables

$AS \bar{h}(s) = \bar{F}_i(s) - \bar{F}_o(s)$... L-transform.

$\bar{h}(s) = \frac{1}{AS} \bar{F}_i(s) - \frac{1}{AS} \bar{F}_o(s)$... Liquid tank.

$\bar{y}(s) = G_p(s) \bar{m}(s) + G_d(s) \bar{d}(s)$... General

So, next we will considered one example, to discuss the formation of closed loop block diagram, so formation of formation of closed loop block diagram, for a liquid level system. So, first we will draw the schismatic of liquid level system, this is the liquid tank, F_i is the inlet floret and out let floret is say F_o naught, height of liquid in the tank is h . Now, the objective is to maintain the liquid height in the tank by manipulating the outlet floret the objective is to maintain the liquid height in the tank at its desired value, accordingly height is the controlled variable.

So, there are two options of manipulated variable I mean we can select either F_i or F_o naught, suppose F_o naught is the manipulated variable, then what will be the load variable F_i . If we considered F_o naught as the manipulated variable then F_i will be the load variable, now we will consider the different elements. So, first we will considered the process I mean, we need to develop the transfer function of the process in terms of G_p and G_d .

So, for developing the transfer function of a process we need the model, so model we can represent by this ordinary differential equation $A \frac{dh}{dt} = F_i - F_o$, this is the modeling equation for the liquid level system. Now, here we are not using the prime to represent the deviation variable, we are not representing the prime superscript to indicate the deviation variable, I mean \bar{h} , \bar{F}_i , \bar{F}_o , these are deviation variables.

So, this equation is written in terms of deviation variable, we are not representing prime superscripts, if we take Laplace transform then we get $A S \bar{h}(s) = \bar{F}_i(s) - \bar{F}_o(s)$. Taking Laplace transform we get this form, now rearranging $\bar{h}(s)$ becomes one by A is multiplied by $\bar{F}_i(s) - \bar{F}_o(s)$, dividing both sides by $A S$ we get this equation.

Now, what is the general form, see general form is $\bar{y}(s) = G_p(s) \bar{m}(s) + G_d(s) \bar{d}(s)$, this is the general form and this is for the liquid tank system. Comparing this last two equation we can easily get the transfer function G_p and G_d , so what is G_p , see all G_p is 1 by s . Yes, G_p is 1 by $A s$, because our disturbance is \bar{F}_i and aim is \bar{F}_o .

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$$\bar{h}(s) = \frac{1}{AS} \bar{F}_i(s) - \frac{1}{AS} \bar{F}_o(s) \dots \text{Liquid tank.}$$

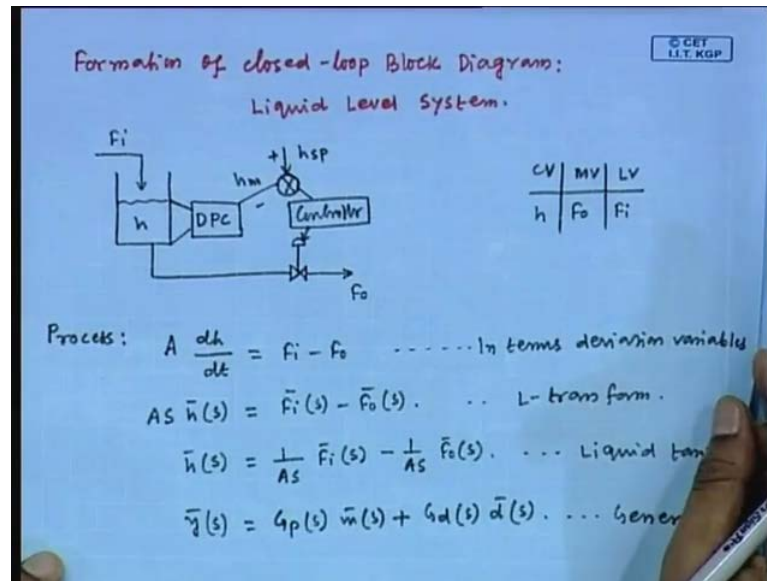
$$\bar{y}(s) = G_p(s) \bar{m}(s) + G_d(s) \bar{d}(s) \dots \text{General form}$$

$$\bar{m} = \bar{F}_o \quad \text{and} \quad \bar{d} = \bar{F}_i$$

$$G_p(s) = -\frac{1}{AS}, \quad G_d(s) = \frac{1}{AS}$$
 Measuring
 Derive :

Here aim is \bar{F}_o and disturbance \bar{d} is \bar{F}_i , so we get the transfer function $G_p(s) = -1/As$ and we get $G_d(s) = 1/As$. So, these two transfer functions we obtain, now what about the next element, I mean what is the next element next element is the measuring device. So, we will consider the measuring device for finding the transfer function.

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I mean in this liquid level system, first we can configure the control scheme, if we configure the control scheme then we need the final control element, sorry first we need the measuring device. So, to measure this liquid height the differential pressure cell is extensively used to measure the liquid height differential pressure cell d p c can be use as a sensor, so what is the output of this differential pressure cell h m, the output of this differential pressure cell is h m.

Original height is h and measured height is h m, this output is compared with the set point value h s p, measured value is compared with set point value. Then this error signal is supplied to the controller and controllers action is implemented through the final control element, this is the control configuration of the example liquid level system. So, here measuring device is the differential pressure cell, we need to find the transfer function of that differential pressure cell.

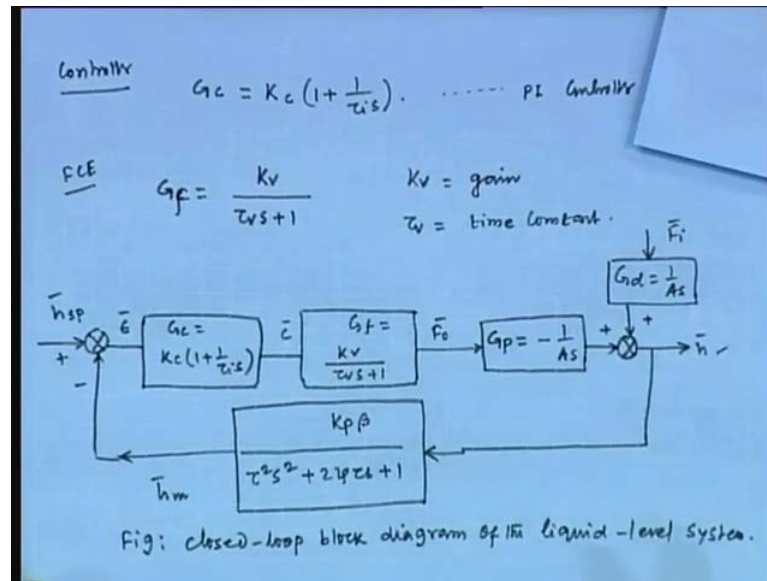
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$\bar{y}(s) = G_p(s)\bar{v}(s) + G_d(s)\bar{d}(s)$
 $\bar{v} = \bar{F}_0 \quad \text{and} \quad \bar{d} = \bar{F}_i$
 $G_p(s) = -\frac{1}{As}, \quad G_d(s) = \frac{1}{As}$
 Measuring Derive:
 $\Delta P \propto h$ \rightarrow **DPC** \rightarrow h_m $\Delta P \propto h$
 $\Delta P \propto h$
 $\Delta P \propto h$
 $\Delta P = \beta h$
 $\tau^2 \frac{d^2 h_m}{dt^2} + 2\tau \zeta \frac{dh_m}{dt} + h_m = K_p \Delta P = K_p \beta h$
 $\Rightarrow G_m(s) = \frac{\bar{h}_m(s)}{\bar{h}(s)} = \frac{K_p \beta}{\tau^2 s^2 + 2\tau \zeta s + 1}$

What is the input to this differential pressure cell, input is the pressure difference Δp and we can consider Δp proportional to liquid height. This Δp proportional to liquid height, what is the output of this differential pressure cell h_m input to this differential pressure cell is differential pressure and output is h_m . Now, considering second order dynamics of this differential pressure cell, we can write the modeling equation as $\tau^2 \frac{d^2 h_m}{dt^2} + 2\tau \zeta \frac{dh_m}{dt} + h_m = K_p \Delta p = K_p \beta h$.

Considering second order dynamics of the differential pressure cell, we can write this equation now the right hand side is $K_p \Delta p$, so we can write again that is equal to $K_p \beta h$, Δp is proportional to height, so $\Delta p = \beta h$. Taking Laplace transform and rearranging we get the transfer function as $G_m(s) = \frac{\bar{h}_m(s)}{\bar{h}(s)}$ which is equal to $K_p \beta$ divided by $\tau^2 s^2 + 2\tau \zeta s + 1$. Taking Laplace transform and rearranging we get finally, this transfer function for the measuring device, next element is the controller, we know the transform function for P PI PID controllers.

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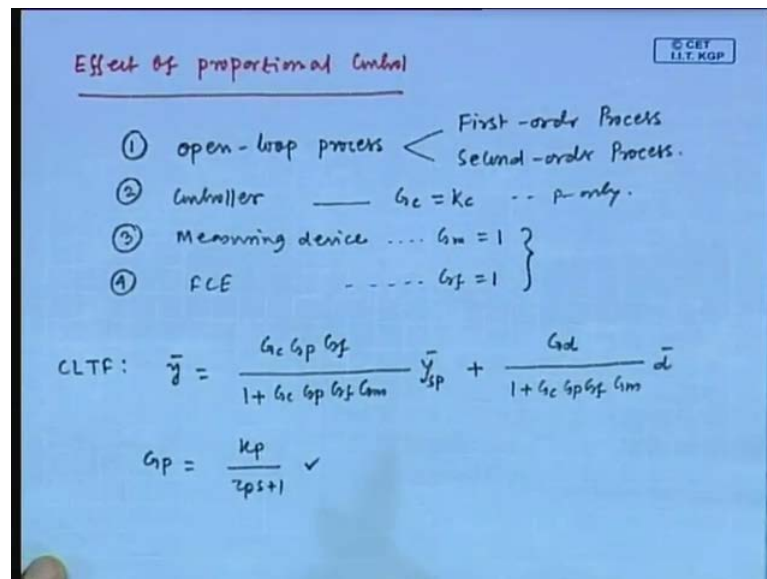
Now, if we consider the PI controller then the transfer function we can write as G_c equals $K_c \left(1 + \frac{1}{\tau_i s}\right)$, if we consider PI controller for the example liquid level system then we can write the transfer function in this form. Another element is the final control element assuming first order dynamics of the control bulb, we can write the transfer function as G_f equals $\frac{K_v}{\tau_v s + 1}$. Assuming first order dynamics of the control bulb we can write the transfer function as G_f this is G_f , so G_f equals $\frac{K_v}{\tau_v s + 1}$, K_v is the gain of the control and τ_v is the time constraint.

Can we make the close loop block diagram, first we need to develop the process having the transfer function of G_p and G_d , how much is G_p . G_p is minus 1 by $A s$, what is G_d is 1 by $A s$ and what is the disturbance, disturbance is F_i what is the output, output is height and what is the input to the process, I mean what is the final control element output that is F_{naught} . So, this is the process, the transfer function of the process with respect to F_{naught} is minus 1 by $A s$, transfer function of the process with respect to F_i is 1 by $A s$ output of that process is h .

For the measuring device we have derived the transfer function that is $K_p \beta$, K_p is the gain of the measuring device, hole divided by tau square s square plus 2 zeta tau s plus 1. So, this is the transfer function of measuring device I mean this is equal to G_m , output is measured height, this is the comparator h set point is compared with measured height. Then the error signal goes through the controller which has the transfer function of $K_c \left(1 + \frac{1}{\tau_i s}\right)$, this is the transfer function of the controller PI controller output is c bar.

The transfer function for the final control element, we have derived that is K_f equals K_v divided by $\tau_v s + 1$, this is the transfer function of the final control element. So, this is the block diagram of the example liquid level system, this is the closed loop block diagram of the liquid level system. In the next we will discuss the effect of proportional action, we have we discussed the three controllers P PI and P I D, basically there are three actions one is proportional action, another one is integral action and derivative action. So, we use to discuss effects of all these actions individually, so first we will discuss the effect of proportional action.

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So, first we will discuss the effect of proportional control we can write proportional action or proportional control, because it only includes the proportional action. For this purpose we will consider one process one open loop process we need to considered. So, first we will considered an open loop process, now to absorb the effect of proportional controller we need to close the loop. So, for closing what do we need one controller, that is p only controller because we are going to discuss the effect of p only controller, then we need one measuring device and also we need one final control element to implement the control action.

So, for absorbing the effect of proportional controller, we need to consider a process that is open loop process, now to close the loop we need to include the controller, we need to include the measuring device and final control element. So, for open loop process we will consider, we will consider two processes one is first order process and second one is second order process and we will discuss one by one.

So, first we will consider first order process in the next we will consider second order process example, next element is the controller. So, here we will include the p only controller, so for p only controller what will be the transfer function for p only controller the transfer function G_c equals K_c . So, for measuring device we will consider G_m equals 1 and for final control element we will consider G_f equals 1. So, for simplicity we are assuming the transfer function of measuring device and final control element both are one fine.

So, we will start from the closed loop transfer function we will start from the closed loop transfer function, the general form of close loop transfer function is \bar{y} equals $G_c G_p G_f$ divided by $1 + G_c G_p G_f G_m$ \bar{y} set point bar plus G_d divided by $1 + G_c G_p G_f G_m$ bar This is the general form of close loop transfer function. Now, in this close loop transfer function we need to substitute the individual transfer functions, like for the process it is mention that first we will consider first order process; that means, G_p equals K_p divided by $\tau_p s + 1$.

For a first order process this is the transfer function, now if we substitute the transfer function G_p G_c equals K_c G_f G_m equal to 1, then what we will get if we substitute all the transfer functions then will get the close loop transfer function for this example system. Now, for the process these is the transfer function with respect to manipulated variable, another transfer function is involved that is G_d with respect to G_d , so what that will be.

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Handwritten mathematical derivation on a blue background:

$$G_p = \frac{K_p}{\tau_p s + 1} \quad \checkmark$$

$$G_d$$

$$\tau_p \cdot \frac{dy}{dt} + y = K_p m + K_d \cdot d$$

$$\left\{ \begin{array}{l} y \rightarrow \text{output} \\ m \rightarrow \text{input} \\ d \rightarrow \text{disturbance} \end{array} \right.$$

$$K_p \rightarrow \text{gain wrt } m$$

$$K_d \rightarrow \text{gain } \dots d.$$

$$\bar{y}(s) = \frac{K_p}{\tau_p s + 1} \bar{m}(s) + \frac{K_d}{\tau_p s + 1} \bar{d}(s) \quad \checkmark$$

$$G_p = \frac{K_p}{\tau_p s + 1} \quad \checkmark$$

$$G_d = \frac{K_d}{\tau_p s + 1} \quad \checkmark$$

So, for that purpose we will first consider the process, we need to derive the modeling equation for the process, the modeling equation for the process we can write as $\tau_p \frac{dy}{dt} + y = K_p m + K_d d$. The first order process we can represent in time domain by this form, where y is the output, m is the input to the process m is basically the output of the final control element and d is the disturbance.

And y , m and d all are in terms of deviation variables, now K_p is the gain of the process with respect to m , another gain is involved in this equation that is K_d , K_d is the gain with respect to disturbance. Now, if we take Laplace transform and if you rearrange then finally, we get $\bar{y} = \frac{K_p}{\tau_p s + 1} \bar{m} + \frac{K_d}{\tau_p s + 1} \bar{d}$, taking Laplace transform and rearranging we get $\bar{y} = \frac{K_p}{\tau_p s + 1} \bar{m} + \frac{K_d}{\tau_p s + 1} \bar{d}$.

So, G_p is equal to $\frac{K_p}{\tau_p s + 1}$ and G_d is equal to $\frac{K_d}{\tau_p s + 1}$, from this equation we can get the transfer function of the process with respect to m that is G_p and the transfer function of the process with respect to disturbance that is G_d . Now, all individual transfer functions are known to us G_p , G_d , G_c , G_F and G_m , so in the next step we need to substitute all these transfer functions in the close loop transfer function, so that we will discuss in the next class.

Thank you.