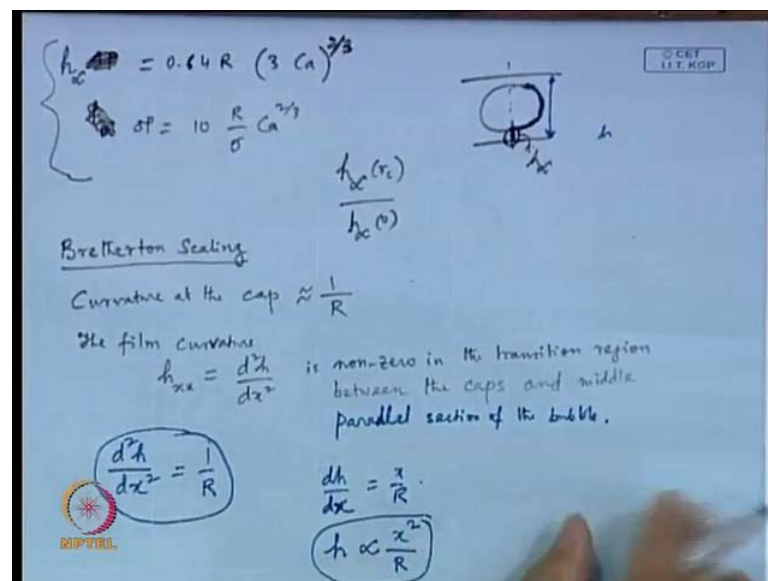


Microscale Transport Processes
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Lecture No.# 33
Immiscible Flow in Microchannel (Contd.)

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Welcome to this lecture of microscale transport process what we have been discussing in the last class is flow of two phases flow of two immiscible phases through a microchannel. That means, flow of droplets or bubbles. And what we talked about is a relationship, which is referred as Bretherton's model or Bretherton's equation to find out, what would be the pressure drop if a series of droplets or bubbles flow through the microchannel.

The results that we got if we try to summarize the results it would be something like this. The pressure drop that we talked about is ΔP is equal to 0.64 into three capillary number to the power two third and we said that there is a theoretical basis to say that this would be the dependence. So, if somebody wants to find out what would be the pressure drop along a microchannel. This would be the pressure drop and the thickness

of the annular liquid layer at the mid plane; that means, if the bubble is one x symmetric bubble placed.

In the microchannel then the thickness at the at mid position of bubble this thickness of liquid annular liquid layer that is referred as h_∞ . I am sorry this is this is not Δp I mean I wanted to say this as h_∞ that thickness. This is the thickness this h_∞ and the Δp is equal to $10 \sigma r_c$ by capillary number to the power two third. This is the relationship that we had talked about in the last class what I have on top of it then we discussed few things for example, we discussed about this $h_\infty r_c$ divided by h_∞ .

Where there is these bubbles are not exactly separated by spherical cap rather it is a very thin lamellar that separates a separates a two droplets or two bubbles. So, the for that this r_c was the contacted radius and we discussed about what would be the functional relationship. And for a noncircular channel how you will address this. So, I talked about this in the last class at a end of the last class on top of this understanding of bretherton's equations or bretherton.

The solution of bretherton's analysis or the analysis we have another point to be noted here before we move to other topics is something called a bretherton scaling. The bretherton scaling is something like this one may not that the curvature at the cap. At the cap is somewhere similar to one by r what is r . r is the radius of the tube radius of that micro capillary. So, it can be this can be approximate this an approximate 1 defiantly. I mean this is not true, but, this is an approximate one on the other hand the film curvature. The film curvature is written as second derivative of h ; that means, $d^2 h / dx^2$.

Now, this is this is nonzero in the transition region. Region between the caps and middle

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Parallel section of the bubble. So, this $h(x)$ now it can be said in a that these two curvatures are they are to be balanced at the transition. So, what was done in bretherton scaling is they have equated this. Basically they said that if somebody wants to know the scaling if somebody wants to know say I have these parameters. That I have this is the dimension of the micro channel this is what I have now can you tell me what would be this value of h_∞ or what would be the value of h .

Can you give me some idea of the average h that is there I mean instead of going through this analysis? I mean whatever we discussed in the last class simply by looking at it as this problem of scaling. If somebody gives me an idea that this is the capillary number, this is the radius of the micro channel and this is what I have flowing through this micro channel can you tell me what would be the average value of h or an approximate scale. For example, let say it is 10 to the power minus 4 or 10 to the power minus 1 or 10 to the power. There can you give me some idea what portion would be occupied by the liquid and what portion would be occupied by the gas.

So, if can somebody give me this idea. That is that is something which if somebody interested in that fact rather than a rigorous solution what the way it has been done here is this has been equated with 1 by r . That means, what they are saying is in some portion it is $d^2 h$ $d x^2$ and at the end this is going to be close to 1 by r . So, if somebody wants to know what is the approximate h ? As far as this bubble annular region is concerned then one should what one should do is he should equate this with this and try to find out how the h depends.

Now, what they have done is they have. So, they equated this, they are trying to find out what would be the scale of h . What would be an approximate order of magnitude as far as this h is concerned. If I talk about h divided by that radius or radius or two r of the micro channel what is that order it is close to 0.5 ? Or is it close to 0.5 in 10 to the power minus 5 . So, that order if somebody wants to know probably this analysis could be useful. So, that is what has been done in Bretherton scaling now this has been probably was integrated with some boundary condition maybe at x equal to 0 x starts from here.

So, at x equal to 0 , $d h$ $d x$ equal to 0 . So, with these uses of these boundary conditions. I mean they ended up with very likely $d h$ $d x$ is equal to x by r and then they further integrated. I mean what they have what the bottom line is that they have said that h scale. h is proportional to x^2 divided by r this relationship they have come up with by integrating it twice. It is not a rigorous analysis once again what they have, what this the objective here is to find out what would be the scaling all right.

So, given these now, if somebody wants to find out what would be the viscous stress and relate that relate viscous stress with pressure drop relate viscous stress with drop. What he will write in that case is $\mu \frac{d u}{d y}$ now I make this $\frac{d u}{d y}$ I write it as u divided by h u

divided by h at y is equal to 0 the velocity is 0 at y is equal to h the velocity is u . So, it is μu by h . So, once you have μu by h . So, that means, it is basically $d u$ $d y$. Now, what you do in this case is when you relate viscous stress with pressure drop. Then what you would be doing is μu divided by h that divided by h is proportional to $d p$ x . That is what you would be writing and you know that this Δp you know this on top of this you know that this Δp is equal to 2σ by r .

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$\sigma P = \frac{2\sigma}{R}$
 $\mu \frac{u}{h} \propto \frac{\sigma}{R x}$
 $\frac{h^2}{R x} \propto \frac{\mu u}{\sigma} \propto Ca No.$
 $\begin{cases} h \propto R Ca^{2/3} \\ x \propto R Ca^{1/3} \end{cases}$

Ca No. $\begin{cases} U \\ R \\ \sigma \end{cases}$

Contact Line resistance has been considered.

Electrokinetic flow with bubbles

In case of electroosmosis

$u = - \frac{\epsilon \zeta(E)}{\mu}$

By simple current-voltage calculation in longitudinal dir.

$E \propto \frac{1}{\{Area of electrolyte\} across capillary}$

Microchannel

So, from this you can conclude that this μu by h divided by h is proportional to σ by r all right. So, on one hand you have this relationship on the other hand you have said that this h is proportional to x square over r or you can say. Here x is proportional to square root of $r h$. So, this is another relationship coming from here x is proportional to square root of $r h$. So, x is proportional to square root of $r h$ this is what you have and otherwise you have this relationship. If you club them together what you get is h square divided by $r x$ is proportional to μu divided by σ , which is basically.

That means, it is proportional to capillary number and on top of that I have this relationship x is proportional to square root of $r h$. Now, if you put this in here what you get is h is proportional to r capillary number to the power two third. All right and also x is proportional to r capillary number to the power one third. So, you have some idea what would be this average h . So, you have some idea that you are introducing multi phases. You are using immiscible phases into the micro channel, but it would be splitted

into there would be an annular portion for the liquid part. And then you will have the other part droplet or the bubble at an axisymmetric location, but what are their dimensions without getting into a rigorous calculation.

You can get some idea of these dimensions simply from scaling of course. This is a scaling analysis I mean what this means is if somebody knows the capillary number then it is easy for an example for a bubble speed of one micrometer of course. It depends on a dimension I mean depending on what is the bubble speed. That means, what is u you can find out depending on what is a value of r what is the value of σ say. If you know these values you can probably find out, what is the capillary number? And from that you can find out, what would be the film thickness what h we are referring to what h we are referring to that can be found out here.

So, whether it is that means, whether this portion this annular portion is one tenth of the actual dimension of the channel or one hundredth or one thousandth that understanding. You can get from this scaling and one thing I must point out before I move to other topics is that nowhere in this analysis the contact line resistance has been considered. But still I am I mean you have a pressure drop because of two immiscible phases present in the channel, but, it is not a contact line the distance.

So, that is needs to be that needs to be understood here. I mean we are we are not talking about the contact angle, we are not talking about the hydrophobicity etcetera. So, we are just talking about we are not talking about these contact line resistance. I mean that is that is one assumption in this entire analysis, but still you have a pressure drop just because you have two immiscible phases flowing. Now, in the last class I just mentioned probably one line that there is some interesting issue here of these flow of two immiscible phases through a micro channel.

If you want to induce the flow through the through say electro kinetic mode. That means if you want to have an electro osmotic flow of these two immiscible phases. If you want to have electro osmotic flow through this micro channel then there are some points that would be. That you need to consider here. So, what I let us write this here what is discussing we are going to discuss is electro kinetic flow with bubbles. That means, you have this microchannel. You have a bubble placed axisymmetrically and then you have

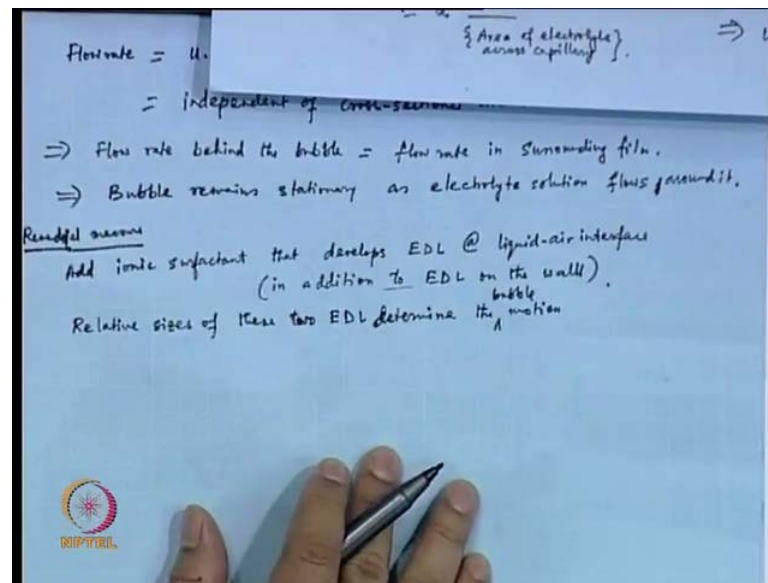
an electrode here and you have an electrode there just the way you have conducted conducted electro osmotic flow or at the electro kinetic.

So, you have this electrodes here and you have you want to induce a flow. Then what happens if you do this the problem here is that in case of electro osmosis velocity u is equal to minus $\epsilon \psi \zeta e$ divided by μ . This is these expression we have already we have this is called electro osmotic velocity. This expression for velocity we have derived sometime back not in last or last to last classes, but some other in the non-linear part of this lectures.

So, lecture series. So, we have this expression there this defines the velocity under electro osmotic flow now if I look at this term e if I look at this term e by simple current voltage calculation in longitudinal direction e is inversely proportional to area of electrolyte across capillary I hope you can you can appreciate the fact that here in this case you are applying voltage, but, voltage means you are basically say for example, I have $n a c l$ here. So, $n a c l$ breaks down into $n a$ plus and $c l$ minus right and these are the ions and they would be responsible for movement. Right now here I am talking about this much of cross section for the liquid and this much of the cross section for the liquid.

So, this case the electric field e that you get and the case where you have the entire channel filled with liquid these two would be different because the it is it is you are applying the same voltage same voltage is applied, but, over a smaller volume of electrolyte this case and the larger volume of electrolyte in the other case. So, when it comes to you are applying the same voltage, but, when it comes to the electric field that you get that would be proportional to the area of electrolyte across capillary. So, what these means is what this implies is if we if this is the velocity if this is the expression for velocity then you can say u is proportional to 1 divided by this area all right. Now, you have on the other hand the flow rate.

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Flow rate is basically u multiplied by area all right. So, what you will have here is then flow rate is equal to since u is inversely proportional to area the. So, the flow rate will be equal to independent of cross sectional area. So, what the implication this would be that the flow rate here where the bubble is not there the flow rate here and flow rate in this surrounding films that would be same. So, what; that means, is that flow rate behind the bubble is equal to the flow rate in surrounding film. So, the what these implies is bubble remains stationary as electrolyte electrolyte solution flows around it.

So, that means, the bubble remain stationary, but the liquid will be flowing around. I mean you increase a voltage you expect there would be more there would be movement, but it would be the liquid that would be flowing through the surrounding film, but the bubble will remain in that same position. So, this is one issue with electro kinetic flow electro kinetic flow with bubbles this is this appears to be very interesting. But and this does not happen in case of a pressure driven flow. So, that that you must you must understand that is there is a difference.

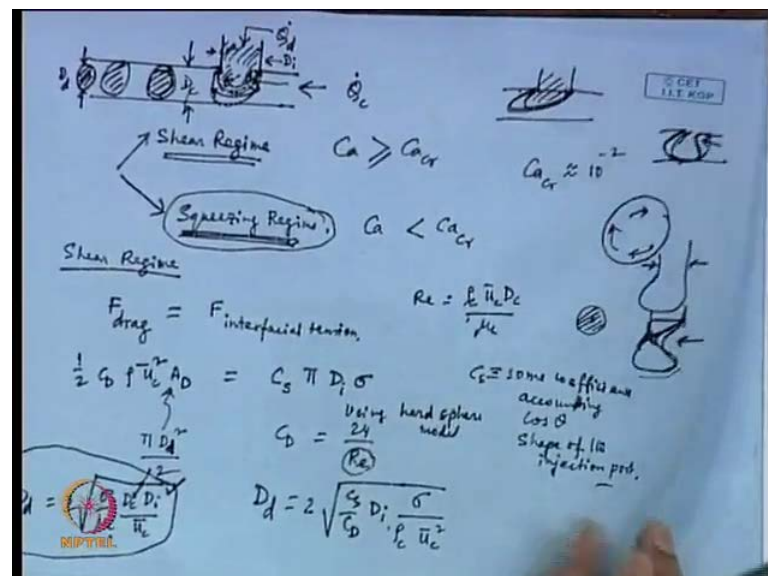
So, the remedial measure that is there I mean remedial measure that has been studied here is add remedy remedial measure. That researchers have thought about is add ionic surfactant that develops electric double layer at liquid air interface. If it is a bubble liquid air interface this is on top of I mean this is in addition to mind it. Because already you

have some electric double layer in addition to e d l on the wall because to implement electroosmotic flow. You have to have an electric double layer at the wall and that is how you are dragging right.

So, here in case of here you have ionic surfactant that is added to develop over and above this electric double layer on the wall, which is responsible for the flow. You have additional electric double layer at liquid air interface now relative size relative sizes of these two e d l that means. So, what is the size of e d l we know as for as size is that is basically d by length. So, the relative size of these two electric double layer one electric double layer is at the wall, which is responsible for electro osmotic flow and the other electric double layer is at the liquid air interface.

Now, the relative size of these two double layers that means, is the Debye lengths of these two double layers. That becomes responsible for that basically determines the determine the motion determine the bubble motion. So, this is one issue, which you need to know. I mean when we are talking about immiscible flow of immiscible phases the pressure driven immiscible flow and the electro kinetic immiscible flow. They have some there is some difference between the two.

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With that being known now, I want to spend some time on the formation of these droplets and bubbles. I mean that is also equally important, how will you form these droplets? how will you form droplet of certain size. Now, when it comes to this I

mean when I go to the literature what I find is that a common way of forming a droplet would be something like this. You have a T-joint where you have one fluid, which is flowing, say, which is flowing. I am calling this carrier fluid, which has a flow rate of q_c and I have a droplet phase, which is flowing at a flow rate of q_d . So, this is the droplet phase now, this droplet is coming out and this is on the other hand you have this carrier flow and what you would be getting is droplets then another droplet.

This is a common way of forming droplets. This is referred to as a T-joint because although I mean I should have drawn it this arm should have been at the bottom side. Then it looks perfectly anyway you can invert this and you can still feel how it is you can still feel here. Now, this one you have here now you have you have the you have the carrier fluid here and the droplet phase here. Coming in now, what you would be interested to know is that I what you would be interested to you know is the what are the forces responsible for generation of this droplet. For that I must point out that there are two regimes possible. When it comes to formation of droplet when it comes to formation of droplet there are there are basically there are basically two regimes

One is one is called shear regime and the other is called squeezing and there is a critical capillary number, which determines you are in which. I mean that formation of droplet in, which regime. If it is if the capillary number of this whole formation process is less than capillary critical then it would be a squeezing regime. On the other hand if it is greater than critical then it would be shear regime. In fact, I should put an equal to sign somewhere because then you are say if $C_s < C_{cr}$.

How will you count that? So, somewhere it has to be put that the critical capillary number it is typically its value is 10 to the power minus 2 what is the difference between this shear regime and squeezing regime. Let us first talk about the shear regime which is easy to understand here the process what is like this you have a flow of carrier fluid this is called carrier and there are other that are I mean there are two phase. So, they are differentiated as c and d carrier and droplet phase. So, you have this flow of carrier fluid. So, this carrier fluid imposes some drag on this on this on this droplet phase now one analysis I mean very common analysis suggests I mean if somebody wants to know if have q_c is this q_d is this and capillary number is this.

What would be the size of the droplet and for doing that for shear regime a simple calculation would be that the drag force by this carrier fluid is equal to the interfacial tension. What this means is this fluid is growing, but, this fluid is held up by the interfacial tension here. So, when this drag force is more than the interfacial tension you can expect that is the threshold point. When this extended plume that has come out of this arm that would detach and then interfacial tension it will continue as a single droplet.

So, if drag is equal to f interval this is a common way somebody can find out the quick way of finding what would be the diameter of the droplet. Now drag is typically given by $\frac{1}{2} C_d \rho u_c^2 A_d$, where the A_d is the projected area. So, A_d would be equal to $\pi d_{\text{droplet}}^2 / 4$. So, that is droplet squared diameter of the droplet square by two π what no if this is this is the area. That means, it would be $\pi d^2 / 4$ square by four I should not be taking it a by two.

Let me point out the dimensions here I have this dimension is given as d_c . That is the diameter of the capillary the diameter of the droplet. I mean this does not necessarily fill the entire part of the channel. I mean. In fact, the drawing is little bit it should portion of the channel occupying and this diameter is d diameter of the droplet. And then maybe this diameter would be d I the injection port this diameter would be d I.

So, I can I mean what you were doing we are going to do here is we would be equating with $C_s \pi d I \sigma$. You understand d I is this basically this is this is the diameter of this is the diameter of the arm and this perimeter is holding by interfacial tension the droplet phase at the time of detachment. So, $\pi d I \sigma$ you can understand and on top of that you have something called a C_s , which is some constant C_s is some coefficient. C_s is some coefficient C_s is some coefficient accounting say $\cos \theta$ then shape of the injection port.

So, there are there are something, which we do not we are not accounting here. So, that is clubbed into this parameter C_s . So, $C_s \pi d I \sigma$ I mean if it comes to this you can take $C_s = 1$. I mean it is like the advection coefficient. You have I mean people who are from fluid mechanics background. So, it is a similar one. So, you can have a C_s that is fine this part I understand and this part is drag. Why it should be $\pi d^2 / 4$ square by two the area. The area would be area would be area would be $\pi d^2 / 4$ square by four actually, but,

that is at the time when droplet has been fully formed and it would be zero when droplet has not formed.

And I do not, but at the time of droplet formation however, the plume this that you have here this may not take the full area. I mean this say for example, if I if I look at this dimension here. It would be something like this it will take a shape like this. In fact, then it would take a shape like this. And then it would break probably we will try to touch upon this point why we should be having this or let me point out let me see what would be the final result in this case.

For a hertz sphere model using hertz sphere model c_d is equal to 24 by Reynolds number using hertz sphere model. So, c_d would be 24 by Re in that case the what would be the droplet diameter? In that case it would be I mean it would be definitely c_s divided by c_d . I see the value σ appearing here then σ is there and if it comes to Re it is based on the based on carrier fluid. So, this Re is nothing, but, $\rho c_u \bar{d}_c$ divided by μ_c .

We can call this $u_c \bar{d}_c$ if we are talking about $u_c \bar{d}_c$ here. So, this is something we have and σ divided by $\rho c_u \bar{d}_c^2$. So, this is something we have and on top of that I have a factor here. All right on top of that I have a factor here that depends on what projected area you take for this for this droplet. I mean if you take this as two then it would be probably 2 into 2 it would be 4 it would be 4 and it goes to that side. So, when you take the square root it will come out as 2 that is the possibility.

Now, if somebody assumes c_s to be equal to 1 and c_d to go there then the droplet diameter would be in that case would be equal to. Then you have square root of σ divided by μc_d . I divided by $u_c \bar{d}_c$ if you bring in this Reynolds number. I think you take c_s as 1 and c_d as 24 by Re this multiplied by 2 . If it is taken as πd^2 by 2 . So, this is basically the equation for droplet diameter, which is equal to the functionality. Here is we have capillary diameter d_c is there. We have d_i is there that is the diameter of the injection port. That is there we have $u_c \bar{d}_c$ the average velocity of the carrier fluid which is nothing, but q_c dot divided by πd_c^2 by four.

So, that $u_c \bar{d}_c$ is there carrier fluid viscosity is there interfacial tension is there. So, that that that gives the diameter of the droplet. So, if somebody wants to produce droplets of certain diameter. He can choose the dimensions, he can choose the velocity of the

carrier fluid and he can come up with the right dimensions that is possible now, this is what you have what I called is shear regime right we have another regime to talk about.

Now, it is one thing I must point out that, when you are working in shear regime then, when you are forming droplet like this. It has been found from imaging studies that there would be some shear going on inside the droplet. I mean after the droplet forms if somebody there is a method called PIV particle image velocimetry, where you put you can see what are the velocity vectors within this droplet. And you will find that this droplet because of the formation process itself the droplet after it formed after you see an isolated droplet. If you study you will see that there is a vortex inside the droplet because you are producing a shear look at it the carrier fluid is shearing it right.

So, within the droplet phase itself there is a shear. So, if this is the droplet phase we are talking about you will find that there is velocity profile like this there is a vortex generating within the droplet itself. In fact, this is why there is a proposition that this droplet can be used as a mixer. That means, you have two streams you mix them you put them together and then you want them to be thoroughly mixed. So, put it in under this regime and you will find because of this small micro vortex inside the droplet you will be carrying out mixing.

So, that this is the one mode of mixing the researchers have suggested also. So, this is this is a possibility now this one second this one second underscore the fact that this process is shear regime; that means, since you have the shear. So, that is why you have caused this type of moment within the droplet. So, the velocity vectors if somebody tries to find out they will find a substantial development of vortex inside the inside this droplet.

On the other hand in case of squeezing regime I do not expect shear to get into this. So, this is this would be in this would be forming this would be again a joint a same thing only thing is the shear would be absent. So, if some if you ask me I mean how do I know a capillary number is greater than a critical. That it is the shear mode that is responsible for the breaking up that already researchers have observed within the droplet that there are remnants of shear already present at the downstream.

So, now I must talk about the squeezing regime in nutshell. What squeezing regime is here? That this thing grows this droplet phase grows and hits the wall it fills this channel completely. Then in that case, where will this  peculiar fluid go the carrier fluid will start eating away or carrier fluid has to push it right. So, you will find that this is this has formed this has filled a channel. Then you will find that this is taking this kind of shape the droplet has advanced a little bit and carrier fluid is pushing it further similarly. So, carrier fluid would be pushing it carrier fluid cannot pass by the side of it. There could be some leakage that is negligible, but predominantly beyond this point the job of the carrier fluid would be to eat away this portion.

So, that means, it was it was originally it was the droplet was forming like this and this is the d I this whole thing is the d i, but at next moment, this is taking, this kind of shape, this is d I and this q_c is q_c is pushing the liquid. It is squeezing that that is why it is the squeezing mode. So, it will continue to squeeze and add some point this thickness would be too small this thickness would be too small and then probably. I mean if you want to consider it you can look at this Rayleigh plateau instability. Or otherwise also you can find out how long it takes for this from the geometric consideration you can find how long it takes to reach the end.

Because moment the end is reached the droplet is released. So, it is completely you can find out the entire analysis would be best on geometry and if you will the Rayleigh plateau instability. I mean if you do not want to give the from geometry. You can say when this thickness gets 0 because this q_c dot that you have that is fixed that is constant. So, it has to eat away and rest of it is geometry now, you can say that it will reach the end when it reaches the end I will consider the droplet to be released.

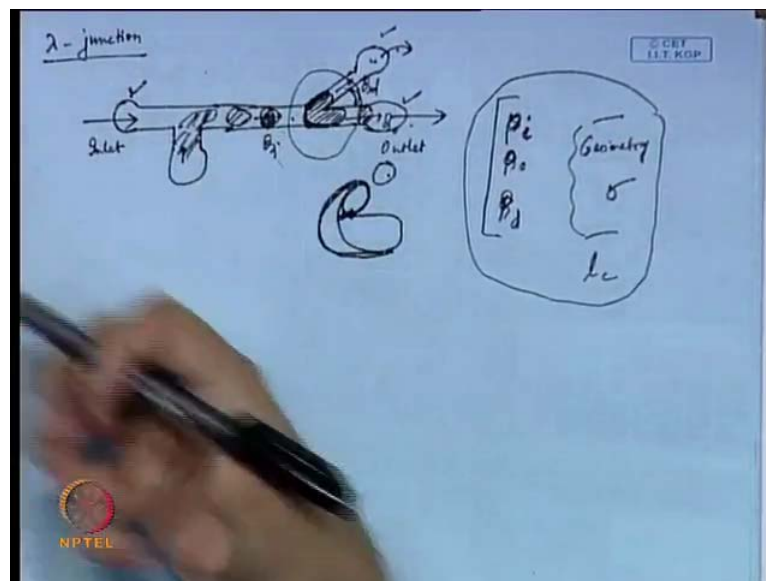
Or you can say that if still there is some δ left and at that point some Rayleigh plateau instability caused. This to rupture because here it is a nick here at this point here. It is a nick. So, at some point there is a rupture. So, but that I knew it that δ would be very small. So, this is coming purely from geometric consideration geometry and you have to satisfy the q_c dot if you assume that there is no leakage around. So, q_c dot cannot pass by.

So, q_c dot will be eating away. So, from geometry where wherever it goes and you it goes that way. So, that defines the diameter of the droplet. So, that is exactly what is

squeezing regime. So, you are not sharing the droplet, but, you are doing it this way. So, this is the difference between the formation of true this is the difference between two droplet regimes. I must say now typically if somebody wants to find out what is what would be the dimension of the droplet. It would be the point of view of geometry that is for certain I mean I can.

I mean if time permits probably I will talk about it further, but how this geometry can be applied to find out what would be the diameter of the droplet. It may not be a simple analytical form like this the way we put it here, but, let us see. I mean for the time being let us just appreciate that there is such possibility, there is such regime and you understand how this regime works? I think that is important and later on we will see can. How we can make use of it further. Now, there is another possibility, which goes by the name lambda junction, which goes by the name lambda junction which is something like this that you have a this a t joint.

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And you have an inlet here you have an outlet here. And you have another outlet here. So, you have that you have the droplet phase coming in and droplet phase is forming. So, you are forming the droplets fine. Now, you are collecting you have a possibility of collecting fluid through this side you have a possibility of collecting fluid from this side as well. So, what will happen is once this droplet comes and reaches here. So, it will tend to take what shape it will go like this do you agree with this.

This is the type of shape it will take. So, this is the type of shape it will take and then you have depending on. What is the pressure here and what is the pressure here. It can one possibility is that it can go in a little bit and later on it negotiates and it just simply comes out. It goes in and then you have interfacial tension, which is pulling the droplet phase together because you have a why is it a sphere because it is there is some reason to be. So, why is it intact why is it a droplet why is it not a completely dispersed one because it has a reason to it I mean it has it has surface tension holding it together.

So, there that you will that will negotiate. I mean on one hand you are trying to push a portion of the droplet out on the other hand you have the surface tension which is trying to pull it together and. So, basically bottom line is that the back side of this droplet if this is the front side and the back side back side of the droplet you are stretching. This side you are stretching all right. So, once you stretch this if you if you if you stretch this too much then you can expect a daughter droplet forming out of it. So, it you will you will see this portion is stretched too much. That means, you have you have a droplet of shape like this and this layer is stretched too much for this.

So, this is layer is gradually it will go like this and then this thickness becomes too they are too close to each other this corner because of this Rayleigh-plateau instability then you see that this is forming a droplet and going in. So, this is referred as daughter droplet. So, this is this is the this is the major you are already in the micro channel that you are in a microscope I mean you are forming small droplet, but if you are interested in forming a smaller one. Then you can negotiate between these two flows and you can literally you can form something called a daughter droplet on the other hand if you are this see you have a pressure here you have a pressure here and you have a pressure here.

So, if the pressure is not if the pressure differential between this point and this point is not sufficient then what will happen is it will go in a little bit, but it is not gone in sufficiently. So, it will refract and again proceed just like a droplet and again this would be forming like a droplet. So, depending on how you play these 3 pressures you can be forming daughter droplet or not I mean that your will. So, and this droplet is expected to be much smaller because it is originally you formed a droplet and then you chopped off a small portion of that and putting it as a daughter droplet. And this because of this shape of this as λ this device is λ there is an angle to it you give this you the name of this is given as λ junction.

Now, there are certain theories already put forward where what you consider in this case because since you are in this squeezing regime this entire formation process is in squeezing regime. So, one thing you must understand that what you are doing here is simply you have the flow rates here. One is say again a carrier or you write it as this q_I q_o and q_d where this is say q_d this is say q_o and this is what is coming in is q_i . So, again you are and depending on the relative values of these q_I q_o q_d and the geometric consideration; that means, what is this thickness.

What is this angle and what is this delta that up to, which it to it can go and beyond which there would be a rupture. So, what is this delta beyond, which is this becomes unstable. So, that. So, the. So, other than this what you need is geometry. That means, the dimension of the channel the angle and that delta etcetera. That governs something called the l_c by up to what extent this what is the length of this back part of the droplet that is been stretched and that governs. So, these factors primarily since you are in squeezing regime.

You do not need to consider shear here this governs what should be the diameter of the droplet and moreover. I mean you do not need to you do not need to write q_I q_o q_d you can write simply p_I p_o p_d the pressures at this point. So, pressures and the geometry that would govern what where the no most importantly, whether you are form a daughter droplet or not it could be that the rate. That p_I p_o p_d that you choose and the geometry that is and geometry and of course, sigma very importantly.

So, that the values that you choose the matrix that you choose is not capable of forming a daughter droplet. Then you see some introduction of droplet phase into this other arm, but then it is again pulled and continued. Where as if you tinker it further you may see at some under some configuration you are forming daughter droplets. So, this is a very interesting point here if I wish I can discuss this squeezing regime more if possible. Let us see anyway that is all I have for today's class and I will meet you again tomorrow thank you.