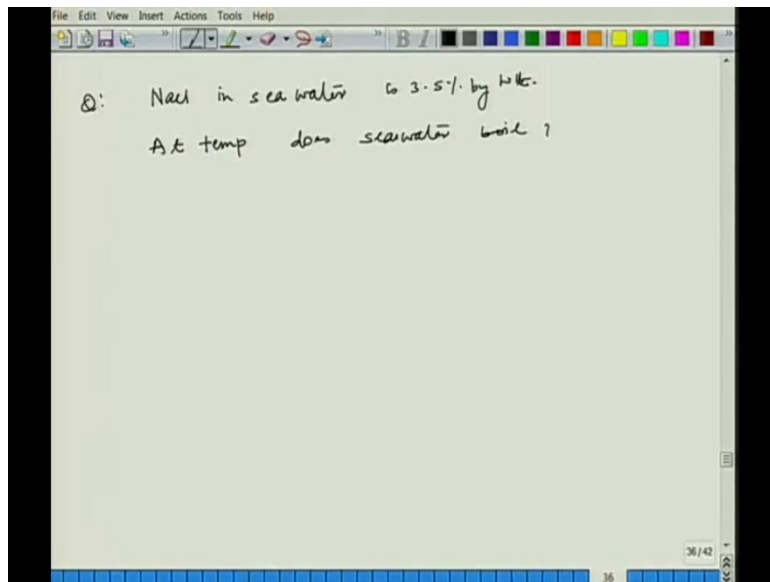


Chemical Engineering Thermodynamics
Professor Jayant K. Singh
Department of Chemical Engineering
Indian Institute of Technology, Kanpur
Lecture 58: Examples of boiling point elevation

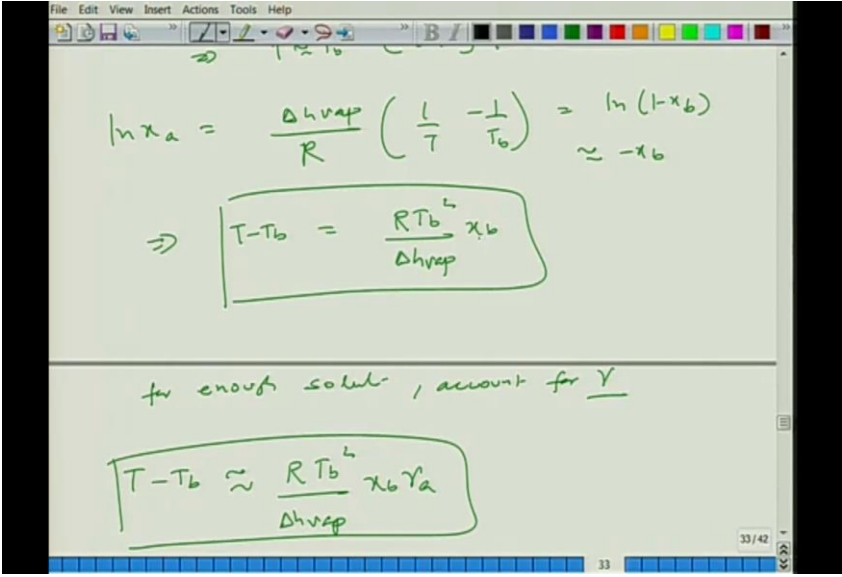
Welcome back! In the last class, lecture was basically on boiling point elevation and freezing point depression that is the effect of a solute on the properties related to the boiling and freezing points. In addition, of course, we are going to talk about other coagulative properties that is osmotic pressure, but currently we looked into two aspect of that. So, we can start with today's lecture with an example illustrating this concept of you know boiling point evolution, particularly let us say for sea or water.

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Okay. So, the simple question could be something like if you consider let us say NaCl in sea water is let us say 3.5 percent by weight, okay. So, at what temperature does sea water boil? So here we have a simple question related to this boiling point elevation.

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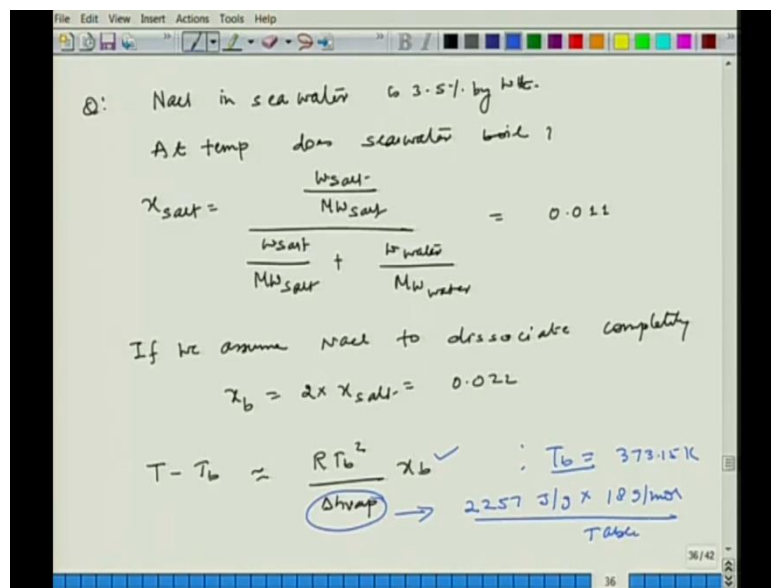


The image shows a handwritten derivation on a digital whiteboard. At the top, the equation $\ln x_a = \frac{\Delta h_{vap}}{R} \left(\frac{1}{T} - \frac{1}{T_b} \right) = \ln(1-x_b) \approx -x_b$ is written. Below this, the equation $T - T_b = \frac{RT_b^2}{\Delta h_{vap}} x_b$ is boxed. A note below the box says "for enough solute, account for γ ". At the bottom, the equation $T - T_b \approx \frac{RT_b^2}{\Delta h_{vap}} x_b \gamma_a$ is boxed. The whiteboard interface includes a menu bar (File, Edit, View, Insert, Actions, Tools, Help) and a toolbar with various drawing tools. A page number '33/42' is visible in the bottom right corner.

$$T - T_b = \frac{RT_b^2}{\Delta h_{vap}} x_b \gamma_a$$

So, if you can see this expression here okay, it talks about a simple like this right like this your expression related to the shift in the boiling point and that depends on your solute concentration. So, let us look at how do we calculate x_b okay and we are also asking we need also this particular expression or value of vaporisation the Δh_{vap} as well as the T_b okay which is the boiling point for the pure substance okay.

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$$x_{\text{salt}} = \frac{\frac{w_{\text{salt}}}{M_{w_{\text{salt}}}}}{\frac{w_{\text{salt}}}{M_{w_{\text{salt}}}} + \frac{w_{\text{water}}}{M_{w_{\text{water}}}}} = 0.011$$

If we assume NaCl to dissociate completely

$$x_b = 2 \times x_{\text{salt}} = 0.022$$

$$T - T_b = \frac{RT_b^2}{\Delta h_{\text{vap}}} x_b = 0.63 \text{ K}$$

So, in this case salt, of course, we are talking about so salt is could be the weight of salt, okay, so what we need is the composition or the mole fraction of it and this would be molecular weight of the salt. And then weight of the salt by M W of the salt plus that of the water divided by M W of water. So, if you do this, of course, this is the 0.35, 0.035 as the weight and then the molecular weight is that of Na and Cl.

So, if you plug in all this information available to you, it is going to be 0.011. Now, the important thing is that the salt here will dissociate in water because of the dielectric constants of the water and considering that you will have Na plus and Cl minus. So, if we assume NaCl to dissociate completely then X of b which is there in expression is two times that of the x of salt okay which is going to be 0.022.

So that will be the effective solute present as the mole fractions are concerned. So now we need to find out the shift or in the boiling point or enhancement in the boiling point. In this case elevation so this we have approximated to T_b square by $\Delta H_{\text{vapour}} \times X_b$. Okay, so now X_b of b is we know, the T_b here original T_b at the atmospheric pressure because it is in sea water.

So, essentially you are talking about just under atmospheric pressure condition that will be your and since we are saying boiling point which is usually refers to that when it comes to normal boiling point. So, T_b at atmospheric pressure would be your 373.15 kelvin. What about Δh_v ? So, Δh_v again at this condition would be 2257 joules per gram multiplied by 18 gram per mole. So, this comes from the table okay this comes from the same table at 373.15 kelvin.

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$$\frac{w_{\text{salt}}}{M_{\text{salt}}} + \frac{w_{\text{water}}}{M_{\text{water}}}$$
 If we assume NaCl to dissociate completely

$$X_b = 2 \times X_{\text{NaCl}} = 0.022$$

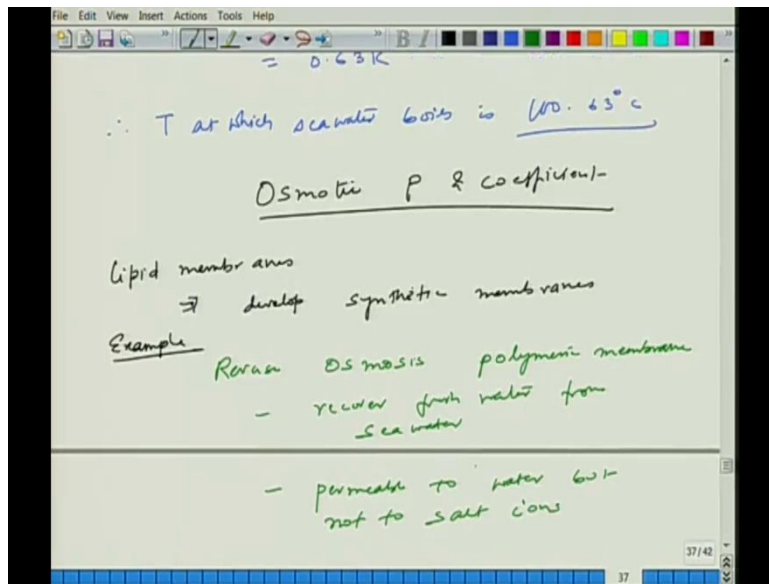
$$T - T_b = \frac{RT_b^2}{\Delta h_{\text{vap}}} X_b \quad ; \quad T_b = 373.15 \text{ K}$$

$$= 0.63 \text{ K}$$

$$\therefore T \text{ at which sea water boils is } \underline{100.63^\circ \text{C}}$$

Okay so given this we can find out the change and that change comes out to be 0.63 kelvin. Thus, the temperature at which sea water boils is 100.63 degree Celsius. So, this is a very simple illustration of how one would be using these expressions which we have evaluated for the case of boiling point elevation or freezing point depression to find out necessary information.

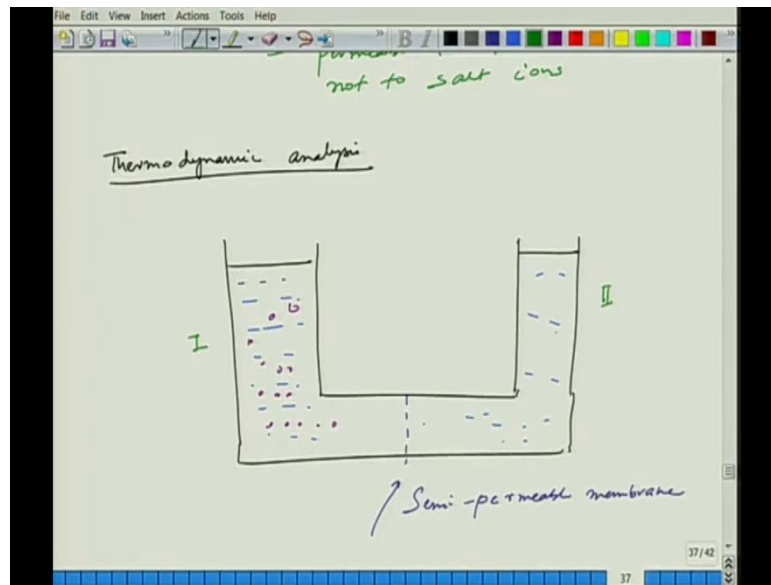
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So, now we can actually move on to the specific case of coagulative property and that is related to the osmotic pressure. So, we move on to the last aspect of this, okay. This is an extremely important aspect because life particularly depends on the lipid membrane which we have in our body and essentially it allows only a certain species to move or transport, you know, and others it rejects. And that is essentially important aspect for our cells, it separates interiors of the cells from the environment and that is some specific kind of a motivation which has led to synthetic membrane.

So, lipid membrane properties have motivated to develop a synthetic membrane which allows only specific species to move. Its example could be, the example could be reverse osmosis polymeric membrane which is often used to recover fresh water from sea water. So, in such a case when its reverse osmosis polymeric membrane it basically is permeable to water but not to salt, salt ions.

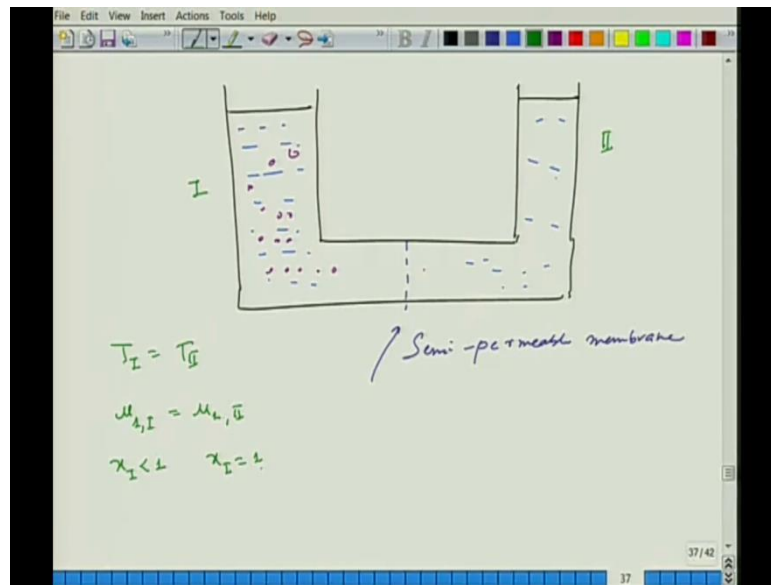
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So, let us look at this concept of this by analysing the thermodynamic basis of such a system. So, let us do a bit of thermodynamic analysis of such membranes which allows only specific components to pass. So, in this case what we are going to do is we will consider two compartments. So, let me just draw that okay, so then let us consider two compartments, so which is maintained at certain pressure and what we have is this semi permeable membrane.

So, essentially you have water, okay, so let me use the same colour water. So, here is also water, but in addition to that you have these salts or solutes which are not permeable to membrane okay. So, I am going to call this compartment as first compartment this another compartment is second compartment. So, we will worry about the pressure acting on this but let us first understand the conditions of the equilibrium which we know that the temperature has to be equal.

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$$T_I = T_{II}$$

$$\mu_{1,I} = \mu_{1,II}$$

$$x_1 < 1 \quad x_1 = 1$$

$$P_I > P_{II}$$

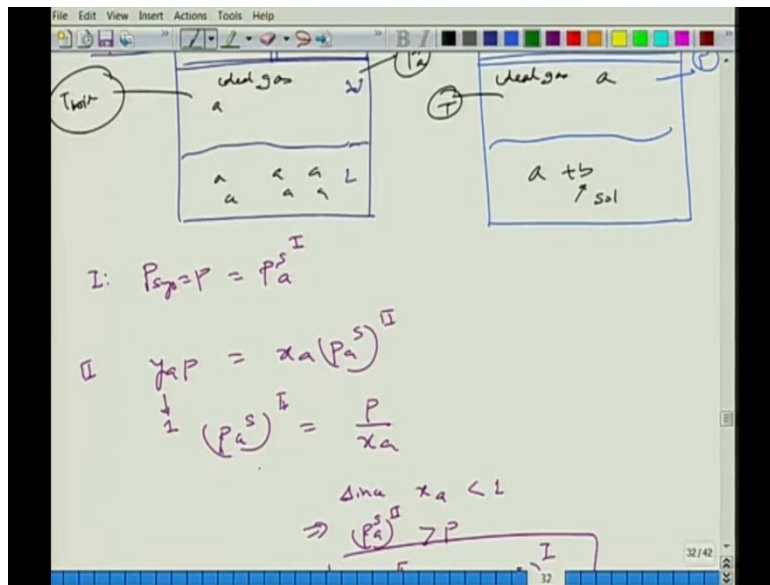
So, the conditions are the temperatures of in the first compartment must be equal to the temperature of the second compartment. And there are two species one is water and the other one is solute so water we can say is one and then we are saying that you know the chemical potential of water in one compartment 1 is should be same as the chemical potential of water in the second compartment.

Or in general the solvent, so one could be solvent and the solute is two. But since there is no solute present in the second compartment there is no condition for mu 2 because species 2 is not allowed to move in. Now, at equilibrium you have this condition but you also note that if I just look at the composition of this the mole fraction of water or solvent then essentially following conditions occur, that x of 1.

If x stands for that of the solvent then this is going to be less than 1 and this in this case this is going to be 1. Now, when you have these two different conditions then how come this is

unequal. So, this must mean that given that the temperature is same the pressure cannot be the same it is clearly the pressure has to be different.

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$$I. P_{sys} = P = P_a^S I$$

$$II. y_a P = x_a (P_a^S) II$$

$$(P_a^S) II = \frac{P}{x_a} \text{ since } x_a < 1 \text{ or, } (P_a^S) II > P$$

Now, this is where we need to go back and see what we used earlier these concepts of change in the composition would lead to the conditions change in the conditions such that the pressure okay in the compartment let us say in this case where we added some solute need to be more than that corresponding to that in the pure case.

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- recover fresh water from sea water

- permeate to water but not to salt ions

Thermodynamic analysis

Diagram showing two compartments, I and II, separated by a semi-permeable membrane. Compartment I has a higher liquid level and is labeled with pressure $P + \pi$. Compartment II has a lower liquid level and is labeled with pressure P .

Diagram showing two compartments, I and II, separated by a semi-permeable membrane. Compartment I has a higher liquid level and is labeled with pressure $P + \pi$. Compartment II has a lower liquid level and is labeled with pressure P .

$T_I = T_{II}$

$\mu_{H_2O, I} = \mu_{H_2O, II}$

$x_I < 1 \quad x_{II} = 1$

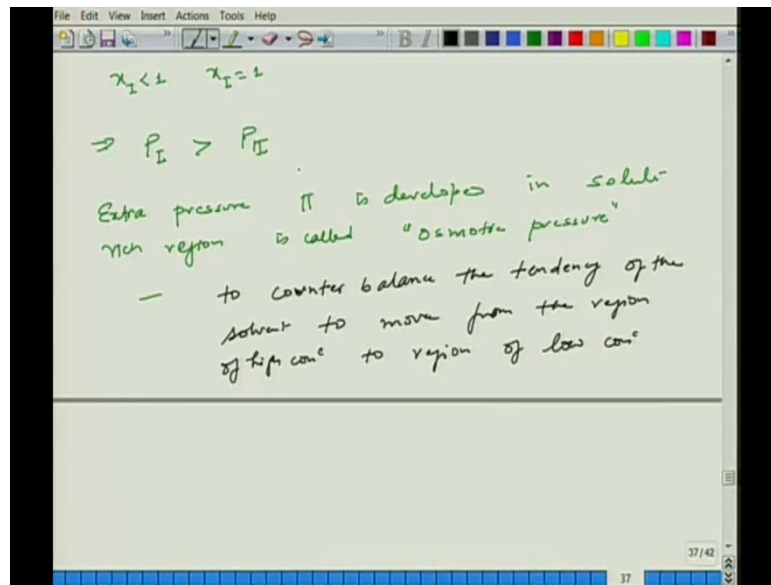
$\Rightarrow P_I > P_{II}$

Semi-permeable membrane

So, if you use that understanding of the past which we have done this exercise. For that case we have used a vapour liquid but the same thing can be used here, that the pressure need to be more in the compartment where you have composition less than 1 and this is necessary for maintaining such an equilibrium okay.

This is also true that your potential would be lower at a lower pressure. So, given this it tells you the pressure in compartment 1 should be greater than pressure in compartment 1. And if that is case then, let us say if the pressure is P here then this pressure should be P plus some additional pressure which I am saying π in order to maintain the equilibrium okay.

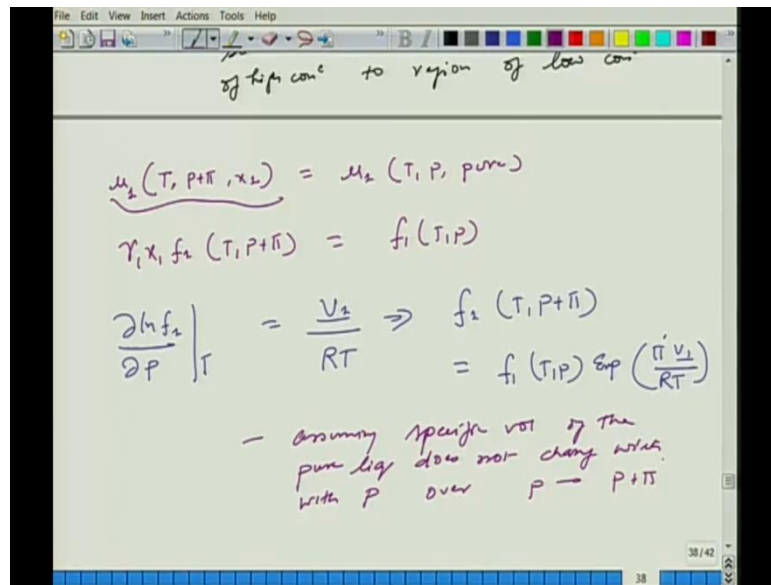
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So, this is extra pressure which π is developed in the solute rich region for such a system is called Osmotic Pressure. So this is necessary in some sense because this will maintain the equilibrium okay. So this π is the required to this extra pressure is required to counter balance the tendency of the solvent which is at a higher concentration in the right compartment transport to the left compartment, tendency of the solvent to move from the region of high concentration to region of low concentration, okay.

So it clearly tells you that since this x is equal to 1 so it will try to move here but then if you want an equilibrium in such a case you need to put extra pressure here in this particular compartment so that you can counter balance the movement of the solvent in the in this direction okay. So, that is how developed this kind of membrane. Now, in such a case you can also apply thermodynamic understanding to come up with a relation of fugacity to compositions of the solute in this case as well as the non-ideality of the mixtures. So, how you are going to go about it?

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$$\mu_1(T, P + \pi, x_1) = \mu_1(T, P, \text{pure})$$

$$\gamma_1 x_1 f_1(T, P + \pi) = f_1(T, P)$$

$$\left. \frac{\partial \ln f_1}{\partial P} \right|_T = \frac{V_1}{RT} \quad \text{or,} \quad f_1(T, P + \pi) = f_1(T, P) \exp(\pi V_1 / RT)$$

$$\frac{\pi V_1}{RT} = -\ln(\gamma_1 x_1)$$

$$\pi = -\frac{RT}{V_1} \ln(\gamma_1 x_1)$$

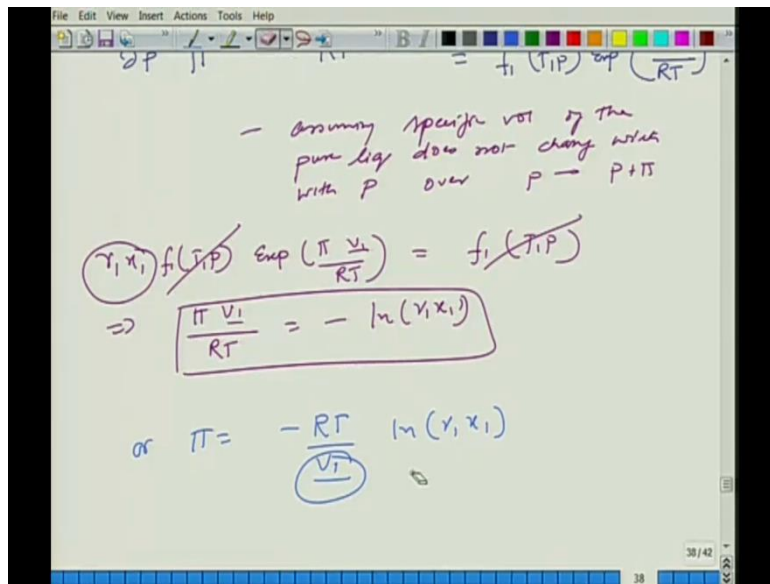
So, we can start with the same concept here because our major condition of equilibrium is related to the chemical potential. So, now, I can write this chemical potential little bit more clearly so I am still talking about the solvent case here okay and here of course is T and the pressure here is different, okay. So this pressure and this composition of that so pressure I am going to expand it, this pressure is nothing but P plus pi this is going to be the same as mu 1 T P and this is pure.

Now, this, I can write this thing as we have done in an earlier case as gamma 1 x 1 f 1 and again this is P plus pi. So, that is the reference case we have particularly the fugacity at that particular condition. So this is the Lewis Randall reference we are considering and this of course I can write this as T P. Alright now if we make use of the relation here of fugacity with

pressure dependency, I can write the earlier expression which we have got. We know this that $\ln f$ with respect to P is nothing but related to molar volume divided by RT .

So this could be written now for the case of water. And if that is the case I can write this as f_1 at T plus P plus π , this would be your f_1 at T of P because we are adding additional pressure and this additional pressure come as a part of π . V_1 bar underscore RT okay. So, this π nothing but ΔP , so this is more like a pointing correction okay. So, now we are assuming here of course we have integrated but we assumed that specific volume of the pure liquid does not change with P over P to P plus π so that is the range we are.

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Now, given this information we can plug in back here, so now I have $\gamma_1 x_1 f_1(T, P)$ and this exponential term π of V_1 bar by RT and this must be equal to $f_1(T, P)$, so this can cancel now and I have π of V_1 bar RT is minus of because I have a log here and if I take log then this will be in the denominator and hence, I am going to get negative log of $\gamma_1 x_1$. So, this is something which I have now I can further simplify to get my relation of π or π is minus RT by V_1 bar $\ln \gamma_1 x_1$ okay. This, I can also write this like this but usually we have this for pure case so we can get rid of this now.

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$\gamma_1 x_1 f(T,P) \exp\left(\frac{\pi v_1}{RT}\right) = f_1(T,P)$
 $\Rightarrow \frac{\pi v_1}{RT} = -\ln(\gamma_1 x_1)$
 or $\pi = \frac{-RT}{v_1} \ln(\gamma_1 x_1)$
 Dilute soln $\gamma_2 \approx 1$
 $\pi = \frac{-RT}{v_1} \ln(1-x_2) \approx \frac{RT x_2}{v_1}$

So, let us consider the case for the dilute solution, so we have this beautiful relation which relates the osmotic pressure with composition and activity coefficient. So, now, I can consider a specific cases of let us say dilute solution which essentially means I can approximate this to 1 and then there is minus $RT V_1$, of course, there is x_1 can be written as log of 1 minus x_2 and now since x_2 is extremely small we can use a Taylor expansion. And this expansion can be written as $RT x_2$ by V_1 bar and this further can be simplified as follows.

Dilute soln. $\gamma_1 \approx 1$

$$\pi = -\frac{RT}{V_1} \ln(1 - x_2) = \frac{RT x_2}{V_1}$$

$$\pi V_1 N = RT N_2$$

$$\pi = \frac{RT N_2}{V} = RTC_2$$

$$MW_2 = \frac{RTC_2}{\pi}$$

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Dilute soln $\gamma_2 \approx 1$

$$\pi = \frac{-RT}{V_1} \ln(1-x_2) \approx \frac{RTx_2}{V_1} \rightarrow \frac{N_2}{N}$$

$$\pi \frac{V_1 \cdot N}{\approx V} = RTN_2$$

$$\pi = RT \frac{N_2}{V} = RT C_2$$

$$\pi = RT \frac{\text{mass}_2}{M_{W_2} V} \quad \text{or} \quad M_{W_2} = \frac{RT C_2 (\text{mass})}{\pi}$$

$\approx V$

$$\pi = RT \frac{N_2}{V} = RT C_2$$

$$\pi = RT \frac{\text{mass}_2}{M_{W_2} V} \quad \text{or} \quad M_{W_2} = \frac{RT C_2 (\text{mass})}{\pi}$$

So, I can write this as N_2 by N , number of moles by N and this N times V_1 can be written as V_1 bar times N . This I can approximate by V because of the dilute part and this RTN_2 it can come okay. And this expression also now can be written as RTN_2 by V this is nothing but RTC_2 concentration. So, this is what we have now so π can be directly related to the concentration of the solute in the case of direct solutions.

I can also write this you know this is a basically, a concentration which essentially means number of moles divided by V . Now you can also rewrite this expression in two if you want to find out let us say molecular weight then I can instead of using N , I can use the mass here and

the mass by molecular weight could be down here. So, this could be something like mass here by V and molecular weight and this is π , so molecular weight of component two okay.

So, this can be written as molecular weight of component two is $R T$ concentration of based on the mass concentration basically mass concentration divided by π . So, if you have a means to find out π you can also find out the molecular weight of the component something which is very useful for obtaining the information of protein molecular weight if we can observe the osmotic pressure and something which we can do in a simple exercise to get the understanding of this okay.

So we will do an example but let me just make a final note here, now, if you very carefully see this equation looks like simply like PB is equal to NRT kind of equation. So this is kind of a similar form of ideal gas equation of state okay.

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$$\pi = RT \frac{\text{mass}}{MW \cdot V}$$

Seawater 3.5% by wt NaCl
 $\rho_{\text{seawater}} = 1030 \text{ kg/m}^3$
 $\pi ?$

$x_{\text{NaCl}} = 0.011$
 $x_{\text{H}_2\text{O}} = 1 - 2 \times 0.011 = 0.978$

$x_{\text{NaCl}} = 0.011$
 $x_{\text{H}_2\text{O}} = 1 - 2 \times 0.011 = 0.978$

$\pi = -RT \ln x_1$

$\frac{1}{1030 \times 10^3 \text{ kg/m}^3}$

$\pi = 3.17 \text{ MPa}$

Minimum P req

So, let us look at an example again, here again this is sea water. And the question is that if you are considering 3.5 percent weight NaCl by weight right and if you are considering the density of the sea water as 1030 kg per meter cube then what is the pi for seawater? What is the necessary pressure in order to have this reverse osmotic membrane working minimum pressure that we can do, but note that seawater does have more than the sodium salt here or NaCl so but we are just considering NaCl to start with.

So whatever extra so basically the first thing of course the first thing we have to do is to get the composition of NaCl okay this we can do that by simply the other way around which we have

done. So based on that if we look at the earlier example it is 0.011 so something which we have done so we simply write this here.

Now, of course, we know that we want to dissociate completely so in that case the x_{H_2O} composition would be $1 - 0.11$ that would be 0.978 right. So π could be written as simply this here so this we can write it $\times 2$, $\times 2$ would be 0.022 right or we can write here if we are considering this γ to be 1 directly $\times 1$.

So, if we are using this developed condition, I can also write this as $\ln x_1$. So x_1 is this temperature we know and molar volume for 1 would be simply $1 \text{ by } 1030$ that we can approximate okay and multiply that by of course 18 and this is something which we will get. And this is your kg per meter cube right so and this molecular weight is 18 gram per mole so we can obtain this by multiplying with 10 to the power 3. So, if we put this information, the amount we got for the π turns out to be 3.17 mega pascal okay.

So this is the minimum pressure required okay usually because of the presence of other component the amount of π which is needed in order to maintain this reverse osmotic condition would be much higher. So, alright you got the idea of at least this aspect of it, so let me also spend bit time on this interesting problem of finding the molecular weight okay. So, if you are able to use some experiment to obtain the pressure. So, this could be something like usual measurement for osmotic pressure for protein solution.

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The slide contains the following handwritten text and diagram:

Minimum π

Example

1.93 g of protein dissolved to make 520 cm³ of aqueous soln at 25°C. The height of the dilute soln visco 0.71 cm above the pure solvent.

Determine π & Mw

ρ_{soln}

$1000 \text{ kg/m}^3 \times 9.8 \text{ m/s}^2 \times 0.0071 \text{ m} = 70 \text{ Pa}$

The diagram shows a U-tube manometer setup. The left side is labeled 'pure solvent' and the right side is 'protein in solvent'. A 'semi permeable' membrane separates the two. The height difference between the two liquid levels is indicated as 0.71 cm. The temperature is given as T = 25°C.

So it is something like this, you have that is the solution okay. This is a pure solvent and if you can have a protein solution in a semi permeable membrane which has got something like this okay. So if you have a membrane then if you this is the protein solution when you put it in this particular pure solvent the solvent the protein solution the protein solvent okay so this may rise to a certain height.

So this is something which is dipped in this pure solvent. Now, being this semi permeable at equilibrium there must be some head we should develop here the let us say that point is 0.71 centimetre okay. So, if this is the case for your system at a temperature of 25 degree Celsius, in such a case one can also find out the molecular weight for protein in this particular solvent.

So this is a an example again where the information is the following that you have been given 1.93 gram of protein dissolved to make 520 centimetre cube of aqueous solution that means this protein dissolves in water at 25 degree Celsius, and of course the height after the dilute solution after the you know putting this particular equipment okay which consists of this semi permeable membrane this particular solution rises by 0.71 centimetre above the pure solvent okay, so the height dilute solution rises 0.71 centimetre above the pure solvent .

So the question is determine π and molecular weight of the protein? So π is very straight forward, π would be simply the ρgh so this is going to be ρgh . ρ is that of the solvent which we are going to consider a 1000, if we consider 1000 kg per metre cube and g as 9.8 metre per second and say h as 0.71 centimetre that will be a 0.0071 metre then this going to be 70 pascal okay. So that will be your π okay.

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dissolved to m.
of aqueous soln at 25°C,
The height of the dilut.
soln rises 0.71 cm above
the pure solvent.

Determine π ρ g h M_w

$\Rightarrow \rho g h$

$1000 \text{ kg/m}^3 \times 9.8 \text{ m/s}^2 \times 0.0071 \text{ m} = 70 \text{ Pa}$

$MW_b = \frac{RT C_b}{\pi} \quad C_b = \frac{m_b}{V}$

$= 13200 \text{ g/mol}$

Now, what about your molecular weight? So that could be your, the other expression which we have got $R T C_b$ that is for the solute. So, if we are using solute here then this will be a π so b is a solute, we can use 2 also. So, π we have calculated what about C_b okay C_b is mass of b which is given to you because it is 1.93 divided by total volume that is the concentration of the solute, π we know T we know R we know so we can find out MW which comes out to be 13200 gram per mole okay.

So, this is how we are going to solve something like this kind of a problem but one of the assumptions I must say that we have taken here we have approximated the density of the solution by the density liquid density of the water at this condition okay. So, that will be the end of this coagulative properties completely and I think we will stop here. We, will take up another problem or another topic in the next lecture. See you in the next lecture.