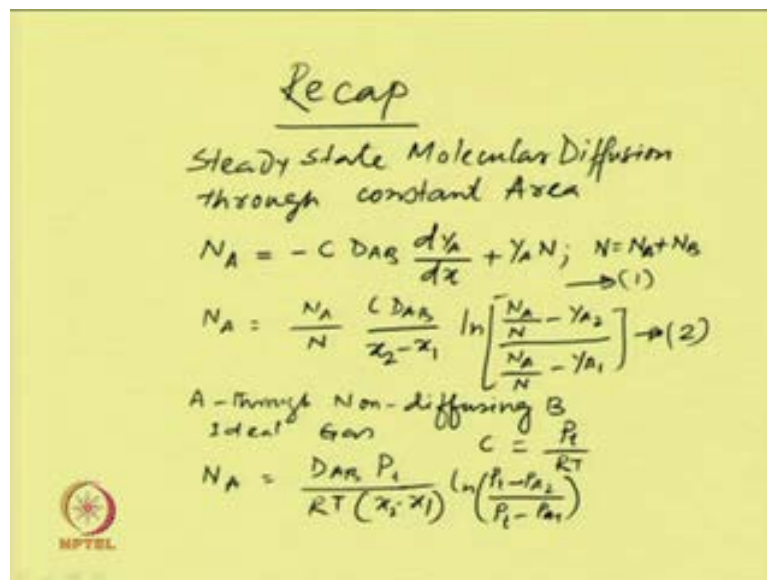


Mass Transfer Operations I
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Module - 1
Diffusion Mass Transfer
Lecture - 5
Steady state molecular diffusion in fluids
Part 2

Welcome to the fifth lecture on diffusion mass transfer, which is module 1. This lecture, we will cover the steady state molecular diffusion through variable area.

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Recap

Steady state Molecular Diffusion
through constant Area

$$N_A = -C D_{AB} \frac{dY_A}{dx} + Y_A N; \quad N = N_A + N_B \quad \rightarrow (1)$$

$$N_A = \frac{N_A}{N} \frac{C D_{AB}}{x_2 - x_1} \ln \left[\frac{\frac{N_A}{N} - Y_{A2}}{\frac{N_A}{N} - Y_{A1}} \right] \quad \rightarrow (2)$$

A - Through Non-diffusing B
Ideal Gas $C = \frac{P_i}{RT}$

$$N_A = \frac{D_{AB} P_i}{RT (x_2 - x_1)} \ln \left(\frac{P_i - P_{A2}}{P_i - P_{A1}} \right)$$

Before going to this lecture, let us have a quick recap on our previous lecture. In the previous lecture, we have considered steady state molecular diffusion through constant area, constant area. Here we have seen from the basic equations of flux of a component A is equal to $C D_{AB} \frac{dY_A}{dx}$ in the x direction plus $Y_A N$, where N is equal to for two component system N_A plus N_B . So this is equation number 1, and then we have seen the flux of A will be equal to N_A by $N C D_{AB}$. Between the two different points x_1 and x_2 will be this distance $\ln \left(\frac{N_A}{N} - Y_{A2} \right) / \left(\frac{N_A}{N} - Y_{A1} \right)$.

So this is equation number 2, and if we consider the case of diffusion of a particular component A through non-diffusing B diffusing B component; that means the B is

stagnant in that case, and also if we consider ideal gas mixture; ideal gas in that case, this C we can write P_t total pressure by RT .

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$$\Rightarrow \frac{D_{AB} P_t}{RT(x_2 - x_1)} (p_{A1} - p_{A2}) \rightarrow (3)$$

$$P_{BLM} = \frac{p_{B2} - p_{B1}}{\ln(p_{B2}/p_{B1})}$$

A & B
steady state Equimolar counter diffusion
For ideal gas

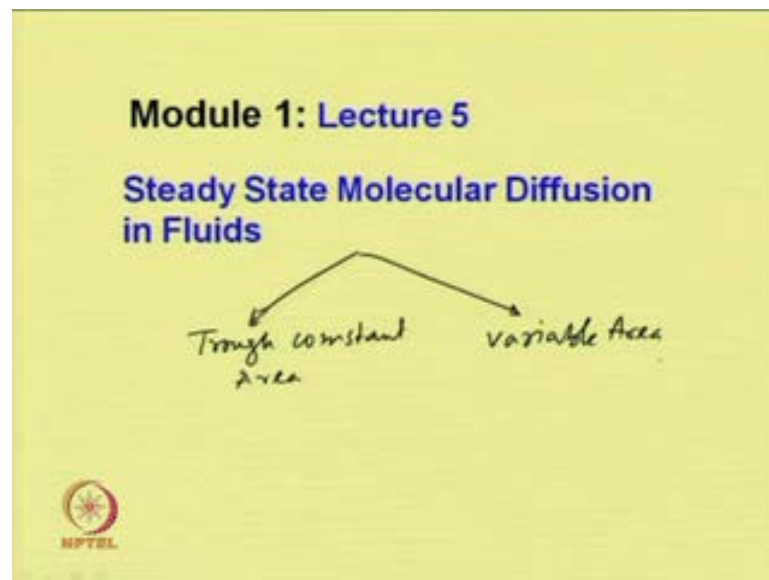
$$N_A = \frac{D_{AB}}{RT(x_2 - x_1)} (p_{A1} - p_{A2}) \rightarrow (4)$$

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So that, we can write the flux equation N_A will be $\frac{D_{AB} P_t}{RT(x_2 - x_1)} \ln \frac{P_t - p_{A2}}{P_t - p_{A1}}$, or which is we can write $\frac{D_{AB} P_t}{RT(x_2 - x_1)}$ into P_{BLM} ($p_{A1} - p_{A2}$), and this P_{BLM} is equal to $\frac{p_{B2} - p_{B1}}{\ln(p_{B2}/p_{B1})}$; this is at the partial pressure difference.

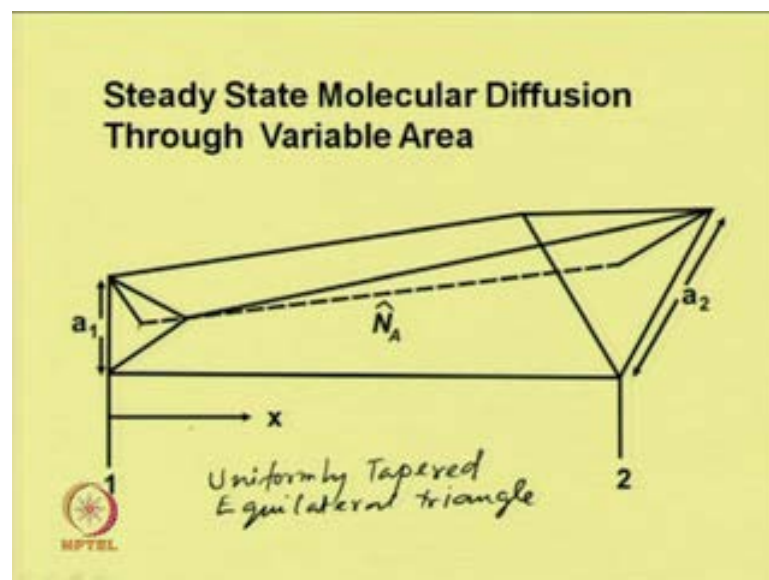
So, this is the flux equations of a component A through non-diffusing B, and also we have seen the steady state equimolar counter diffusion. If between component A and B, the diffusion is steady state equimolar counter diffusion. So in this case for ideal gas, we have seen N_A the flux is equal to $\frac{D_{AB}}{RT(x_2 - x_1)}$ into the partial pressure difference ($p_{A1} - p_{A2}$). So these are the quick review of our previous class, where we have considered the diffusion is occurring through the constant area of the system.

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So today, we will also discuss the steady state molecular diffusion in fluids. As we said these has two separate classifications; one is through constant area and this is through variable area.

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So now, consider steady state molecular diffusion of component A through equilateral triangle, which is uniformly tapered equilateral triangle, where the diffusion this is point one. From this plane it is diffusing to point a 2, where the N_A cap is the diffusion rate of component A, and the cross-sectional area is varying along the

length of the conduit. If we consider this is point 1 and this is point 2, the length of the side of the triangle is a 1 at point 1 and a 2 at point 2. So, the relations between this side of the triangle, which is gradually increasing from the left hand to the right hand we can write.

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**Steady State Molecular Diffusion
Through Variable Area**

$$A = \frac{1}{2} \text{ side} \times \text{altitude}$$

$$= \frac{1}{2} a \times \frac{\sqrt{3}}{2} a = \frac{\sqrt{3}}{4} a^2$$

Diffusion of A through Non Diffusing B

$$N_A \left(1 - \frac{P_A}{P_t}\right) = \frac{-D_{AB}}{RT} \frac{dP_A}{dx} \quad (\text{For ideal gas})$$

$$N_A = \frac{\hat{N}_A}{A} = \frac{1}{\sqrt{3}} \frac{\hat{N}_A}{a^2}$$

$$- \frac{RT}{D_{AB}} \times \frac{1}{\sqrt{3}} \frac{\hat{N}_A}{a^2} dx = P_t \frac{dP_A}{P_t - P_A}$$

$$a = f(x)$$


So, area will be half into side into altitude. So, which is equal to its side is a. It will be a into height will be for equilateral triangle it will be root 3 by 2 a. So, it will be root 3 by 4 a square. Now if we return back to the Fick's law diffusion of A through non-diffusing B. So in this case, the governing equations of the flux N_A into $(1 - \text{partial pressure of A by } P_t) \text{ total pressure}$ is equal to minus D_{AB} by RT d P_A by dx for ideal gas. Now if we consider as N_A is the molar flux.

So, N_A is equal to $\hat{N}_A$ cap by area, which is equal to 4 by if we substitute area over here, 4 by root 3 $\hat{N}_A$ cap by a square, and if we substitute this this one over here N_A . So, it will be minus RT by D_{AB} into 4 $\hat{N}_A$ cap divided by root 3 a square dx , will be equal to P_t total pressure into d P_A partial pressure of a divided by $P_t - P_A$. So before we integrate this equations, we have to impose the limit where a is function of x. Since a is function of (a) x, the size of the triangle will continuously change.

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**Steady State Molecular Diffusion
Through Variable Area**

$$a = a_1 + \frac{a_2 - a_1}{x_2 - x_1} (x - x_1)$$

$$= a_1 + \frac{a_2 - a_1}{x_2 - x_1} x - \frac{a_2 - a_1}{x_2 - x_1} x_1$$

$$\therefore \frac{da}{dx} = 0 + \frac{a_2 - a_1}{x_2 - x_1} \times 1 - \frac{a_2 - a_1}{x_2 - x_1} \times 0$$

$$\frac{da}{dx} = \frac{a_2 - a_1}{x_2 - x_1}$$

$$dx = \frac{x_2 - x_1}{a_2 - a_1} da$$


So, we can have the relation a will be a_1 at x_1 plus $a_2 - a_1$ by $x_2 - x_1$ into $(x - x_1)$. So, this is the relations how a is changing with x for the equilateral triangular shape. So, in this case we can write this will be a_1 plus $a_2 - a_1$ by $x_2 - x_1$ into $x - x_1$.

Now if we differentiate, this will be da by dx . So, since this is constant; so this will be 0 plus $a_2 - a_1$ into by $x_2 - x_1$ into 1 minus $a_2 - a_1$ by $x_2 - x_1$ into 0 . So, this will be $a_2 - a_1$ by $x_2 - x_1$. So, we can write da by dx is this. So, dx we can write $x_2 - x_1$ divided by $a_2 - a_1$ da . So, if we substitute in our previous relation, say this is equation 1.

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Steady State Molecular Diffusion Through Variable Area

$$\begin{aligned}
 & -\frac{RT}{D_{AB}} \bar{N}_A \frac{x_2 - x_1}{a_2 - a_1} \int_{a_1}^{a_2} \frac{4}{\sqrt{3} a^2} da = P_t \int_{P_{A1}}^{P_{A2}} \frac{dP_A}{P_t - P_A} \\
 \Rightarrow & -\frac{RT \bar{N}_A}{D_{AB}} \cdot \frac{x_2 - x_1}{a_2 - a_1} \cdot \frac{4}{\sqrt{3}} \left[-\frac{1}{a} \right]_{a_1}^{a_2} = -P_t \left[\ln(P_t - P_A) \right]_{P_{A1}}^{P_{A2}} \\
 \Rightarrow & \frac{-4 RT \bar{N}_A}{\sqrt{3} D_{AB}} \cdot \frac{x_2 - x_1}{a_2 - a_1} \left(\frac{1}{a_1} - \frac{1}{a_2} \right) = P_t \ln \left(\frac{P_t - P_{A1}}{P_t - P_{A2}} \right) \\
 \Rightarrow & \bar{N}_A = \frac{\sqrt{3} D_{AB} P_t}{4 RT} \times \frac{a_1 a_2}{x_2 - x_1} \ln \left(\frac{P_t - P_{A1}}{P_t - P_{A2}} \right) \quad \text{--- (2)}
 \end{aligned}$$


If we substitute here, the relations between a and x in this limit we can have RT by D_{AB} N_A cap x_2 minus x_1 by a_2 minus a_1 integral a_1 to a_2 4 by $\sqrt{3} a^2$ da , which is equal to P_t integral partial pressure of a at 0.1 partial pressure of a at 0.2 dP_A by P_t minus P_A . Now if we integrate, we can get minus $RT N_A$ cap by D_{AB} into x_2 minus x_1 by a_2 minus a_1 into 4 by $\sqrt{3}$ and this integration of these will be minus 1 by a with the limit a_1 to a_2 will be equal to minus P_t into $\ln(P_t - p_A)$ into and limit is p_{A1} to p_{A2} .

So, if we simplify this one then we will have 4 minus $4 RT N_A$ cap by $\sqrt{3} D_{AB}$ into x_2 minus x_1 by a_2 minus a_1 into $(1$ by a_1 minus 1 by $a_2)$. So, will be equal to $P_t \ln(P_t - p_{A1})$ by $P_t - p_{A2}$; N_A cap is the diffusion rate will be equal to root of $\sqrt{3} D_{AB}$ into P_t by $4 RT$ into, a_2 minus a_1 will cancel out; so it will be $a_1 a_2$ by x_2 minus $x_1 \ln(P_t - p_{A1})$ by $P_t - p_{A2}$. So, this is the molar flow rate equations of component A through the variable area of equilateral triangular cross section.

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Example 1

The CO_2 is diffusing through non-diffusing N_2 at steady state in a conduit of 2m long at 300K and a total pressure of 1 atmosphere. The partial pressure of CO_2 at the left end is 20kPa and 5kPa at the other end. The cross section of the conduit is in the shape of an equilateral triangle being 0.025m at the left end and tapering uniformly to 0.05m at the right end. Calculate the rate of transport of CO_2 . The diffusivity is $D_{AB} = 2 \times 10^{-5} \text{ m}^2/\text{s}$.



If we consider a simple example like we consider before the CO_2 is diffusing through non-diffusing nitrogen at steady state in conduit of 2 meter long and at 300 Kelvin and 1 atmosphere pressure and the partial pressure at the left end is 20 kilo Pascal and at the right end is 5 kilo Pascal. The cross section of the conduit is equilateral triangle of side 0.025 meter at the left end and tapering uniformly to 0.05 meter at the right end. So, we have to calculate the rate of transport of CO_2 , and the diffusivity between A and B; that is CO_2 into through nitrogen is given $2 \times 10^{-5} \text{ m}^2/\text{s}$.

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Example 1: Solution

Given

$$D_{\text{CO}_2-\text{N}_2} = 2 \times 10^{-5} \text{ m}^2/\text{s}$$

$$R = 8314 \frac{\text{N m}^3/\text{Kmol}}{\text{K}}$$

$$T = 300 \text{ K}$$

$$P_t = 1 \text{ atm} = 101.3 \text{ kPa} = 101.3 \times 10^3 \text{ Pa}$$

$$P_{A1} = 5 \text{ kPa} = 5 \times 10^3 \text{ Pa}$$

$$P_{A2} = 20 \text{ kPa} = 20 \times 10^3 \text{ Pa}$$

$$a_1 = 0.025 \text{ m} \quad | \quad x_2 - x_1 = 2 \text{ m}$$

$$a_2 = 0.05 \text{ m}$$



So now, let us consider the values which are given. The diffusion coefficient of CO₂ into nitrogen is given is 2×10^{-5} meter square per second. R is known to us; 8314 meter cube Pascal by Kmol Kelvin. T the temperate of the system is 300 K. Pressure P_t is given is 1 atmosphere, which is equal to 101.3 kilo Pascal is equal 101.3×10^3 Pascal. Partial pressure p_{A1} is given is 5 kilo Pascal, which is 5×10^3 Pascal. p_{A2} is also given 20 kilo Pascal, which is 20×10^3 Pascal, and the a₁ is 0.025 meter; a₂ is 0.05 meter. The side of the triangle and the distance x₂ minus x₁ is given as 2 meter.

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Example 1: Solution

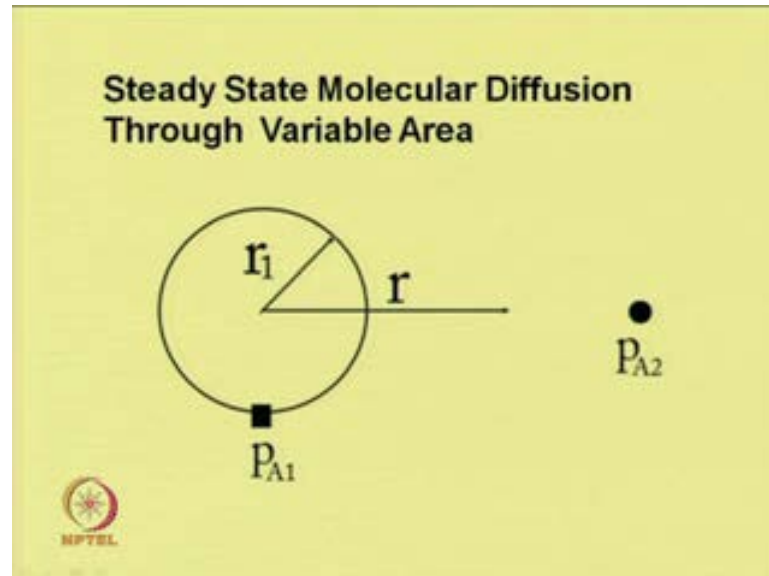
$$\begin{aligned} \dot{N}_A &= \frac{\sqrt{3} D_{AB} P_t}{4 R T} \frac{a_1 a_2}{x_2 - x_1} \ln \left(\frac{P_t - p_{A1}}{P_t - p_{A2}} \right) \\ &= \frac{\sqrt{3} \times 2 \times 10^{-5} \frac{\text{m}^2}{\text{s}} \times 101.3 \times 10^3 \text{ Pa} \times 0.025 \text{ m} \times 0.05 \text{ m}}{4 \times 8314 \frac{\text{m}^3 \text{ Pa}}{\text{Kmol K}} \times 300 \text{ K} \times 2 \text{ m}} \times \ln \left(\frac{101.3 \times 10^3 \text{ Pa} - 5 \times 10^3 \text{ Pa}}{101.3 \times 10^3 \text{ Pa} - 20 \times 10^3 \text{ Pa}} \right) \\ &= 3.75 \times 10^{-11} \frac{\text{Kmol}}{\text{s}} \end{aligned}$$


So, now if we substitute the values which are given N_A cap will be root 3 D_{AB} P_t by four RT a₁ a₂ by x₂ minus x₁ ln (P_t minus p_{A1} by P_t minus p_{A2}). So, if we substitute the values which is root 3 into 2 into 10 to the power minus 5 meter square per second into 101.3 into 10 to the power 3 Pascal total pressure and then into the a₁ a₂ which is 0.025 meter into 0.05 meter; this divided by 4 into 8314 meter cube Pascal divided by Kmol Kelvin temperature 300 Kelvin into 2 meter multiplied by ln (101.3 into 10 to the power 3 Pascal minus 5 into 10 to the power 3 Pascal divided by 101.3 10 to the power 3 Pascal total pressure minus 20 into 10 to the power 3 Pascal).

So, if we solve this is equal to 3.75 into 10 to the power minus 11 Kmol per second. So, if we look into the unit balance, the pressure term will cancelled; this this will cancelled

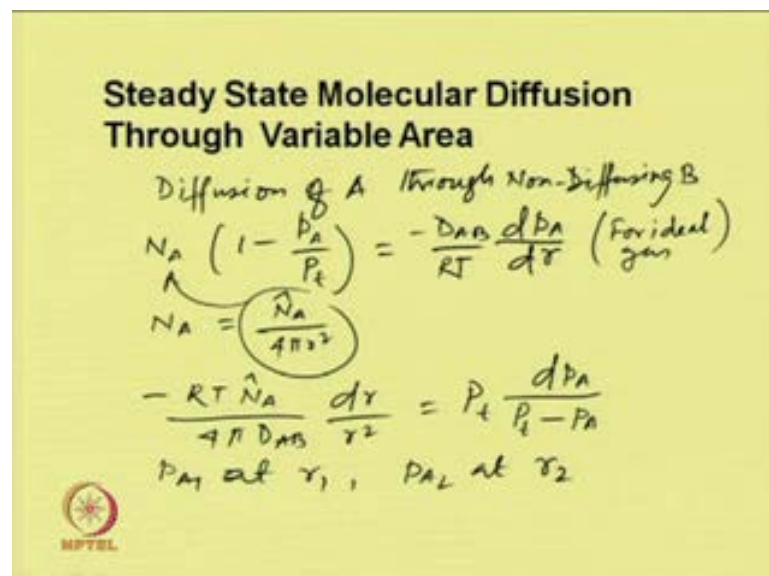
out and Kelvin will cancel. So, you will have Kilo mol per Kilo mol per second. So, this is the molar fluoride or of component A through non-diffusing B.

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Let us consider another example. The evaporation of a drop of liquids occurs and area continuously gets changed; or if we have a naphthalene ball and diameter of the ball is reduced and suddenly the area and its flux gets changed. So we will consider this, where at 0.1 the partial pressure is p_{A1} ; at 0.2 partial pressure of component A is P_2 , and the radius is changing. So the initial radius is r_{A1} ; this is on the surface of the ball.

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So if we apply the Fick's law of diffusion, consider the case diffusion of A through non-diffusing to B. So in this case, we know the flux is related with the partial pressure p_A by P_t the total pressure is equal to minus $D_{AB} RT \frac{d p_A}{d r}$ for ideal gas. ideal gas N_A we can write the flux N_A cap by $4 \pi r^2$, which is the area. So now, we can have the relation between this two we can substitute this N_A over here.

So, we will essentially have minus $RT N_A$ cap by $4 \pi D_{AB} dr$ by $d r^2$ is equal to $P_t d p_A$ by P_t minus p_A . So now, if we include the limit partial pressure of A_1 at (r_1) and partial pressure of P_{A_2} at r_2 .

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Steady State Molecular Diffusion Through Variable Area

Diffusion of A through Non-Diffusing B

$$-\frac{RT \hat{N}_A}{4\pi D_{AB} P_t} \left(\frac{1}{r_1} - \frac{1}{r_2} \right) = \ln \frac{P_t - P_{A2}}{P_t - P_{A1}}$$

$r_1 \ll r_2 \Rightarrow \frac{1}{r_2} \approx 0$

$$\frac{\hat{N}_A}{4\pi r_1^2} = \frac{D_{AB} P_t}{RT P_{BLM} r_1} (P_{A1} - P_{A2}) = N_{A1}$$

$N_{A1} = \text{flux at the surface}$



If we include this limit and integrate the equation this will be minus $RT N_A$ cap by $4 \pi D_{AB}$ into $P_t (1/r_1 - 1/r_2)$ is equal to $\ln P_t - p_{A2}$ by $P_t - p_{A1}$. So, if we consider r_1 is very, very less than r_2 then $1/r_2$ approximately equal to 0. So, if we substitute this then N_A cap is equal to $D_{AB} P_t$ by $RT p_{BLM}$ into $r_1 (p_{A1} - p_{A2})$ is divided by $4 \pi r_1^2$ square. So, this is nothing but N_{A1} ; N_{A1} is the flux at the surface.

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Example 2

A sphere of naphthalene having a radius of 5 mm is suspended in a large volume of still air at 310 K and 1 atm. The partial pressure at the surface of naphthalene at 310K is 50 Pa. Assume dilute gas phase. The D_{AB} of naphthalene in air at 310 K is $6 \times 10^{-6} \text{ m}^2/\text{s}$. Calculate the rate of evaporation of naphthalene from the surface.



Now let us have the example. A sphere of naphthalene ball having a radius of 5 millimeter is suspended in a large volume of still air at 310 Kelvin and 1 atmosphere pressure. The partial pressure at the surface of naphthalene at 300 K is 50 Pascal. Assume dilute gas phase. So, and the D_{AB} of naphthalene in air at 300 Kelvin is given 6 into 10 to the power minus 6 meter square per second. Calculate the rate of evaporation of naphthalene from the surface.

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Example 2: Solution

$$\begin{aligned} D_{AB} &= 6 \times 10^{-6} \text{ m}^2/\text{s} \\ P_{A1} &= 50 \text{ Pa} \\ P_{A2} &\approx 0 \quad (\text{for large volume of air}) \\ r_1 &= 5 \text{ mm} = 5 \times 10^{-3} \text{ m} \\ R &= 8314 \frac{\text{m}^3 \text{ Pa}}{\text{kmol K}} \\ T &= 310 \text{ K} \\ P_{A, \text{LM}} = P_t &= 1 \text{ atm} = 1.013 \times 10^5 \text{ Pa} \end{aligned}$$



Now the data which are given is D_{AB} is 6 into 10 to the power of minus 6 meter square per second. Partial pressure p_{A1} is given is 50 Pascal. p_{A2} we can, since this is large volume of air we can consider approximately equal to 0 (for large volume of air), and r_1 is given is 5 millimeter, which is 5 into 10 to the power minus 3 meter; equal to 5 into this, and R is known to us. R is 8314 meter cube Pascal by Kmol Kelvin. T is given 310 Kelvin, and P_{BLM} since it is very dilute solution we can considered as P_t total pressure, which is equal to 1 atmosphere is equal to 1.013 into 10 to the power 5 Pascal.

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Example 2: Solution

$$\frac{\dot{N}_A}{4\pi r_1^2} = \frac{D_{AB} P_t}{RT P_{BLM} r_1} (p_{A1} - p_{A2})$$

$$= \frac{6 \times 10^{-6} \text{ m}^2/\text{s} \times 1.013 \times 10^5 \text{ Pa} \times (50 \text{ Pa} - 0)}{8314 \times 310 \text{ K} \times 1.013 \times 10^5 \text{ Pa} \times 5 \times 10^{-3} \text{ m}}$$

$$= 0.023 \times 10^{-6} \frac{\text{Kmol}}{\text{m}^2 \text{ s}}$$

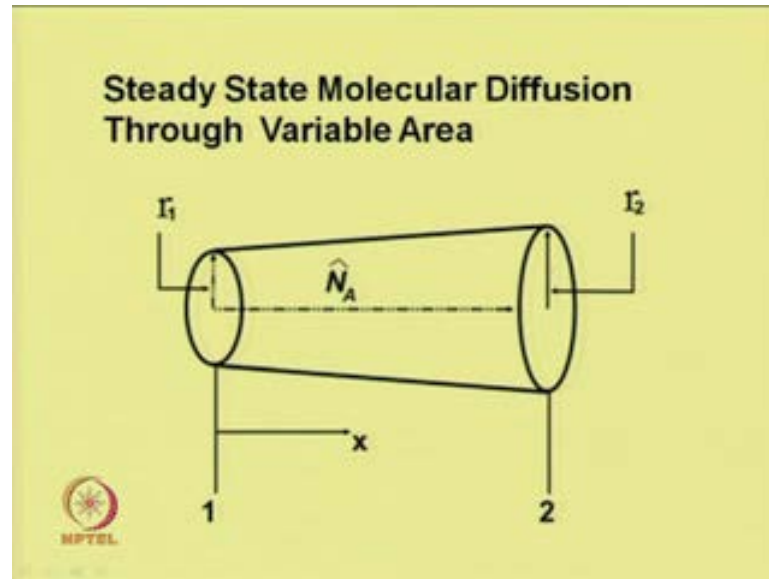
$T = 310 \text{ K}$
 $P_{BLM} = P_t = 1 \text{ atm} = 1.013 \times 10^5 \text{ Pa}$



So now, if we substitute these values in our governing equations flux N_A cap by $4\pi r_1^2$ square will be equal to $D_{AB} P_t$ by $RT P_{BLM}$ into r_1 into the partial pressure difference (p_{A1} minus p_{A2}). So p_{A1} is 50, which is given and p_{A2} is 0 we are assuming for large volume of air.

So, if we substitute that values, which is 6 into 10 to the power minus 6 meter square per second; P_t is 1.013 into 10 to the power 5 Pascal into (50 Pascal minus 0) divided by 8314 into 310 into 1013 1.013 into 10 to the power 5 into 5 into 10 to the power minus 3; this is meter, this is Pascal, and this is Kelvin, and this is meter cube Pascal Kmol Kelvin. So now, after substitution of this we will have this is 2.023 0.023 into 10 to the power minus 6 Kmol per meter square second.

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Now, we will consider steady state molecular diffusion through another geometry which is uniformly tapered, cylindrical in nature, and that point 1 the radius of the cylinder is r_1 and at point 2 the radius is r_2 .

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Steady State Molecular Diffusion Through Variable Area

Steady-State Equimolar Counter Diffusion

$$N_A = -C D_{AB} \frac{dy_A}{dx} + y_A N$$

ideal gas = $-\frac{D_{AB} P_t}{RT} \frac{dy_A}{dx} + y_A N$

$$N_A = -N_B, \quad N = N_A + N_B = 0$$

$$N_A = -\frac{D_{AB}}{RT} \frac{dP_A}{dx}$$

$$N_A = \frac{N_A}{\pi r^2} = -\frac{D_{AB}}{RT} \frac{dP_A}{dx}$$

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In this case, we will consider steady state equimolar counter diffusion. steady state equimolar counter diffusion As we know, the flux is minus $C D_{AB} \frac{dy_A}{dx}$ plus $y_A N$. So for equimolar counter diffusion and if we consider ideal gas, then this will be minus $\frac{D_{AB} P_t}{RT} \frac{dy_A}{dx}$ plus $y_A N$.

Now for two component system and equimolar counter diffusion N_A will be minus N_B and N is N_A plus N_B , and which is equal to 0. So then this term will be 0, and we have the flux N_A will be minus D_{AB} by RT to dP_A/dx ; and also N_A we can write N_A cap by πr^2 , and this is equal to minus D_{AB} by RT dP_A/dx .

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Steady State Molecular Diffusion Through Variable Area

$$r = \frac{x_2 - x_1}{x_2 - x_1} x + r_1$$

$$\frac{N_A}{\pi} \int_{x_1}^{x_2} \frac{dx}{\left[\left(\frac{x_2 - x_1}{x_2 - x_1} \right) x + r_1 \right]^2} = - \frac{D_{AB}}{RT} \int_{P_{A1}}^{P_{A2}} \frac{dP_A}{P_A}$$

At $x = 0$, $P_A = P_{A1}$
 At $x = L$, $P_A = P_{A2}$



If we use the geometry, then we can have a relations between r is equal to r_2 minus r_1 by x_2 minus x_1 x plus r_1 . So, this is the change of radius along the distance; along the length of the cylinder. We can replace this r in these equations and we can then differentiate. So, it will be N_A cap by π integral x_1 to x_2 dx by $(r_2$ minus $r_1)$ by $(x_2$ minus $x_1)$ into x (by) plus r_1 square is equal to minus D_{AB} by RT integral P_{A1} to P_{A2} dP_A/P_A . If we integrate with the limit at x is equal to 0, P_A is P_{A1} at x is equal to L , P_A is P_{A2} .

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Steady State Molecular Diffusion Through Variable Area

$$\dot{N}_A = \frac{D_{AB}}{RT} \times \pi \frac{r_1 r_2}{L} (p_{A1} - p_{A2}) \rightarrow$$


So, if we integrate this with the limits it will be $\dot{N}_A$ will be $\frac{D_{AB}}{RT}$ into $\pi r_1 r_2$ by L into $(p_{A1} - p_{A2})$. Like earlier example for equilateral triangle we can integrate in similar way, and we will have these diffusion rate equations of component A.

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Example 3

The CO_2 is diffusing at steady state through N_2 by equimolar counter diffusion in a conduit 2 m long at 300K and a total pressure of 1 atmosphere. The partial pressure of CO_2 at the left end is 20 kPa and 5 kPa at the other end. The cross section of the conduit is in the shape of cylindrical of radius is 0.025m at the left end and tapering uniformly to a radius of 0.05m at the right end. Calculate the molar flow rate of CO_2 . The diffusivity is $D_{AB} = 2 \times 10^{-5} \text{ m}^2/\text{s}$.



Now let us consider these examples where carbon dioxide is diffusing steady state through nitrogen by equimolar counter diffusion in the similar conduit of 2 meter length at 300 Kelvin and at 1 atmosphere pressure. The partial pressure at the left end is 20 kilo Pascal and 5 kilo Pascal at other end. The cross section of the conduit is in the shape of

cylindrical of radius 0.025 meter and at the other end the radius is 0.05 meter. We have to calculate the molar flow rate of CO₂, and the diffusion coefficient is given.

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Example 3: Solution

$$\begin{aligned}\hat{N}_A &= \frac{D_{AB}}{RT} \pi \frac{(r_1 r_2)}{L} (p_{A2} - p_{A1}) \\ &= \frac{2 \times 10^{-5} \frac{\text{m}^2}{\text{s}} \times 3.14 \times 0.025 \text{ m} \times 0.05 \text{ m}}{8314 \frac{\text{m}^3 \text{ Pa}}{\text{kmol K}} \times 300 \text{ K} \times 2 \text{ m}} \times (20 \times 10^3 \text{ Pa} - 5 \times 10^3 \text{ Pa}) \\ &= 7.87 \times 10^{-10} \frac{\text{kmol}}{\text{s}}\end{aligned}$$


If we substitute in this equations $\hat{N}_A$ cap is D_{AB} by RT pi $(r_1 r_2)$ by L $(p_{A2} - p_{A1})$. So, the value is given 2×10^{-5} meter square per second into 3.14 into 0.025 meter into 0.05 meter divided by 8314 meter cube Pascal by Kmol Kelvin into 300 K into 2 meter multiplied by $(20 \times 10^3 \text{ Pascal} - 5 \times 10^3 \text{ Pascal})$. So, this will be equal to 7.87×10^{-10} Kmol per second .

So, this is end of our lecture 5, and in the next class we will consider the diffusion coefficient measurements. We will first consider the measurement of the diffusion coefficient in the gas phase, and then for the liquid phase, and then diffusion in solid phase.

Thank you.