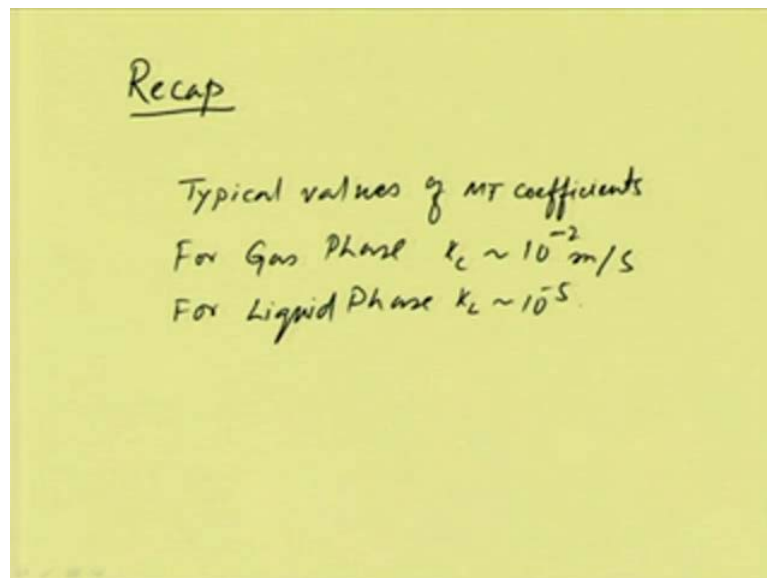


**Mass Transfer Coefficients I**  
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**Module - 2**  
**Mass Transfer Coefficients**  
**Lecture - 2**  
**Dimensionless groups and correlations for**  
**convective mass transfer coefficient**

Welcome to the second lecture of module 2 which is on mass transfer coefficients. So, before going to this lecture, let us have recap on our previous lecture.

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In the previous lecture, we have discussed the concept of mass transfer coefficients, where we have said that, the mass transfer coefficient is important for the convective mass transfer; and these mass transfer coefficients depends on the different systems - whether it is gas phase, or it is liquid phase, or whether the diffusion is occurring through non diffusing b, or the equimolar counter current diffusion. So, for each case, we have discussed the mass transfer coefficient and the relations among them. And finally, we have calculated the mass transfer coefficient for different systems and the typical values; typical values of mass transfer coefficients, coefficients for gas phase is about,  $K_c$  is about  $10$  to the power minus  $2$  meter per second, and in case of liquid phase,  $K_L$  is approximately  $10$  to the power minus  $5$  meter per second.

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## Module 2: Lecture 2

### Dimensionless Groups and Correlations for Convective Mass Transfer Coefficients

$Nu$  = Nusselt Number

$Re$  = Reynolds Number

$Pr$  = Prandtl Number

$$Nu = \phi(Re, Pr)$$

Dittus-Boelter equation

In this lecture, we will consider on two topics; one is dimensionless groups and the correlations for convective mass transfer coefficients. The dimensionless groups is generally important for the simplicity to represent the mass transfer coefficient and other variables, or physiochemical properties of the system. So, like in heat transfer, heat flux can be correlated with the heat transfer coefficient and the temperature gradient. This heat transfer coefficient, which is  $h$ , can be related with the Nusselt number  $Nu$ , which is Nusselt number. The other important dimensionless term in heat transfer is the Reynolds number and Prandtl number. For experimentally obtained data, under post convection in heat transfer, the Nusselt number can be related as a function of Reynolds number and Prandtl number. The very important and useful correlations in case of heat transfer like this, is known as Dittus-Boelter equation.

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**Dimensionless Groups**

$Sh = \text{Sherwood Number}$   
 $Sc = \text{Schmidt Number}$

$$Nu = \frac{\text{convective heat flux}}{\text{heat flux for conduction through a stagnant medium of thickness } l \text{ for same } \Delta T}$$

$$= \frac{h \Delta T}{(k/l) \Delta T} = \frac{hl}{k}; \quad k = \text{thermal conductivity}$$

$$Sh = \frac{\text{convective mass (molar) flux}}{\text{mass (molar) flux for molecular diffusion through a stagnant medium of thickness } l \text{ under same driving force}}$$

Diffusion of a gas phase species A through non-diff. B:  
 $\text{Convective flux} = K_g \Delta P_A$

Similarly, like heat transfer, two important dimensionless groups in case of mass transfer, is the Sherwood number, Sherwood number, and the other one is Schmidt number. So, like in heat transfer, in case of Nusselt number, we define convective heat flux divided by heat flux for conduction through a stagnant medium of thickness  $l$  for same  $\Delta T$ , which is equal to  $h \Delta T$  divided by  $K$  by  $l$  into  $\Delta T$ , which is equal to  $h$  by  $K$ ;  $K$  is the thermal conductivity. Similarly, for mass transfer, the Sherwood number can be defined as convective mass, or molar flux, divided by mass, or molar flux for molecular diffusion through a stagnant medium, medium of thickness  $l$ , under same driving force. So, in case of diffusion of, diffusion of a gas phase species through non diffusing B, convective flux, we can write  $K_g \Delta P_A$ ;  $P_A$  is the partial pressure difference.

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**Dimensionless Groups**

Mass Flux due to molecular diffusion =  $\frac{D_{AB} P_t}{RT L P_{B,M}} \Delta P_A$

$$Sh = \frac{k_f \Delta P_A}{\frac{D_{AB} P_t}{RT L P_{B,M}} \Delta P_A} = \frac{k_f P_{B,M} RT L}{D_{AB} P_t} = \frac{k_f L P_{B,M}}{D_{AB} P_t}$$

For Liquid phase at low conc.  $x_{B,M} \approx 1$

Convective mass flux =  $k_f \Delta C_A$ ; Diffusive flux =  $\frac{D_{AB}}{L} \Delta C_A$

$$Sh = \frac{k_f \Delta C_A}{\left(\frac{D_{AB}}{L}\right) \Delta C_A} = \frac{k_f L}{D_{AB}}$$

$L$  = Characteristic Length ; For sphere -  $d$ , diameter  
 For cylinder -  $d$ , dia  
 For flat plate - distance from the leading edge,  $z$

Now, the mass flux due to molecular diffusion, is equal to, we have learned in the last class,  $D_{AB} P_t$  divided by  $R T L P_{B, M} \Delta P_A$ . So, if we substitute in the Sherwood number definition, we will get, this  $K_f$  into  $\Delta P_A$ , which is convective flux, divided by  $D_{AB} P_t$  by  $R T L P_{B, M}$  into  $\Delta P_A$ , is equal to  $K_f P_{B, M} R T L$  divided by  $D_{AB} P_t$ . It is the total pressure. We can write  $K_f L P_{B, M}$  divided by  $D_{AB} P_t$ . If we consider, the transport occurs through a liquid phase, and at low concentration, for liquid phase, at low concentration,  $x_{B, M}$  approximately equal to 1 and convective mass flux will be  $K_f L$ , concentration gradient, and the diffusive flux is equal to  $D_{AB}$  by  $l$   $\Delta C_A$ . So, the Sherwood number, in this case, is equal to  $K_f L \Delta C_A$  divided by  $D_{AB}$  by  $l$  into  $\Delta C_A$ , which is equal to  $K_f L$ , small  $l$  divided by  $D_{AB}$ . The  $l$  is the characteristic length; for sphere, this  $d$  is the diameter, is the characteristic length; for cylinder,  $d$  dia is the characteristic length; for flat plate, distance from the leading edge, say  $z$ , is the characteristic length.

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**Dimensionless Groups**

$$Pr = \frac{\text{momentum diffusivity}}{\text{thermal diffusivity}} = \frac{\mu/\rho}{\kappa/\rho c_p} = \frac{\mu c_p}{\kappa}$$
$$Sc = \frac{\text{momentum diffusivity}}{\text{molecular diffusivity}} = \frac{\mu/\rho}{D_{AB}} = \frac{\mu}{\rho D_{AB}}$$
$$= \frac{\nu}{D_{AB}}$$

Let us consider another important dimensionless group in case of mass transfer, which is Schmidt number. We know the dimensionless group in heat transfer is Prandtl number  $Pr$ , which is defined as the momentum diffusivity, momentum diffusivity divided by thermal diffusivity, which we can write,  $\mu$  by  $\rho$  divided by  $K$ , thermal conductivity by  $\rho C P$ , which is  $\mu C P$  by  $K$ . The analogous number in case of mass transfer is Schmidt number, which is equal to the momentum diffusivity divided by the molecular diffusivity; so, which is equal to  $\mu$  by  $\rho$  by  $D_{AB}$ , which is equal to  $\mu$  by  $\rho D_{AB}$ , which we can write,  $\nu$  by  $D_{AB}$ . So, this dimensionless number, Sherwood number and Schmidt number, how the magnitude of these two dimensionless numbers varies for different systems?

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**Dimensionless Groups**

Sphere of 2 cm dia, partial pr. of the solute is low i.e.,  $P_{BLM}/P_t \approx 1$

$$Sh = \frac{k_c d P_{BLM}}{D_{AB} P_t} = \frac{10^{-2} \text{ m/s} \times 2 \times 10^{-2} \text{ m}}{10^{-5} \text{ m}^2/\text{s}} \Rightarrow Sh \sim 20$$

$$Sc = \frac{\nu}{D_{AB}} = \frac{10^{-5} \text{ m}^2/\text{s}}{10^{-5} \text{ m}^2/\text{s}} \Rightarrow Sc \sim 1$$

For common gases  $Pr \approx Sc \approx 1.0$

For Liquid Phase  $Sh = \frac{k_c d}{D_{AB}} = \frac{10^{-2} \times 2 \times 10^{-2}}{10^{-9} \text{ m}^2/\text{s}} \Rightarrow Sh \sim 200$

For common liquids except liquid metals  $Sc = \frac{\nu}{D_{AB}} = \frac{10^{-6} \text{ m}^2/\text{s}}{10^{-9} \text{ m}^2/\text{s}} \Rightarrow Sc \sim 1000$

$10 < Pr < 10^2$   
 $1000 < Sc < 10^4$

Let us consider a sphere of 2 centimeter dia, where the gas phase mass transfer is occurring, which is flowing first through this sphere; and the partial pressure of the solute is low; that is,  $P_{BLM}$ , log means special gradient, by total pressure, will be approximately 1. The Sherwood number in this case, will be equal to  $K_C d P_{BLM}$  by  $D_{AB} P_t$ . As we know, the mass transfer coefficient is in the order of  $10$  to the power of minus 2 meter per second and the diameter is given 2 centimeter, which is 2 into  $10$  to the power minus 2 meter, and the typical values for the diffusivity is  $10$  to the power minus 5 meter square per second in case of gas, so, from which we can get the typical Sherwood number is approximately 20.

But Schmidt number, for this case, is equal to  $\nu$  by  $D_{AB}$  and  $\nu$ , which is  $\mu$  by  $\rho$  will be in the order of  $10$  to the power minus 5 meter square per second and this value the diffusivity  $10$  to the power minus 5 meter square per second. From this we can obtain Schmidt number is approximately equal to 1. For common gases, gases, these values, the Prandtl number is equal to Schmidt number and this is equal to 1.0. For the liquid phase, and for similar geometry, Sherwood number is equal to  $K_L d$  by  $D_{AB}$ , which is equal to  $10$  to the power minus 2, into 2 into  $10$  to the power minus 2 divided by  $10$  to the power minus 9 meter square per second, which is the diffusion coefficient in case of the liquid phase. So, from here, the Sherwood number is approximately 200. And Schmidt number, in this case, is  $\nu$  by  $D_{AB}$ , and in this case, the  $\nu$  is to  $10$  to the power minus 6 meter square per second, divided by the diffusivity value is  $10$  to the power minus 9

meter square per second, which leads to Schmidt number is approximately equal to 1000. So, for common liquids, except liquid metals, the Prandtl number is in the range of greater than 10, and less than 100. For the same case, the Schmidt number is greater than 400 and less than 10 to the power 4.

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**Dimensionless Groups**

$St = \text{Stanton number}$

$$St_h = \frac{\text{Convective heat flux}}{\text{heat flux due to bulk flow}} = \frac{h \Delta T}{C_p \rho v \Delta T}$$

$$= \frac{hL/k}{(vL\rho/\mu)(C_p\mu/k)} = \frac{Nu}{Re Pr}$$

$$St_m = \frac{\text{Convective mass flux}}{\text{flux due to bulk flow of the medium}} = \frac{K_L \Delta C}{v \Delta C}$$

$$= \frac{(K_L L/D_{AB})}{(vL\rho/\mu)(\mu/D_{AB})} = \frac{Sh}{Re Sc}$$

Now, let us consider another dimensionless number, which is important in case of mass transfer. A similar number in heat transfer is also exists. For heat transfer, the Stanton number  $St$ , Stanton number. The Stanton number for heat transfer, we define the convective heat flux divided by heat flux due to bulk flow, which is equal to  $h \Delta T$  divided by  $C_p \rho v \Delta T$ ; which we can write,  $hL/k$  divided by  $vL\rho/\mu$  into  $C_p\mu/k$ , which is equal to Nusselt number divided by Reynolds into Prandtl. The analogous number for mass transfer is Stanton number for mass transfer, we can define the convective mass transfer, mass flux, divided by flux due to bulk flow of the material; so, which we can write  $K_L \Delta C$  divided by  $v \Delta C$ , which we can write  $K_L L/D_{AB}$  divided by  $vL\rho/\mu$  into  $\mu/D_{AB}$ ; which is, we can write in terms of Sherwood number divided by Reynolds into Schmidt.

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**Dimensionless Groups**

$Pe = \text{Peclet number}$

$Pe_H = \frac{\text{heat flux due to bulk flow}}{\text{flux due to conduction across a thickness } l}$

$$Pe_H = \frac{C_p \rho v \Delta T}{(k/l) \Delta T} = \left( \frac{v l \rho}{\mu} \right) \times \frac{C_p \mu}{k} = Re Pr$$

$Pe_m = \frac{\text{flux due to bulk flow of the medium}}{\text{diffusive flux across a thickness } l}$

$$Pe_m = \frac{v \Delta C}{(D_{AB}/l) \Delta C} = \left( \frac{v l \rho}{\mu} \right) \left( \frac{\mu}{\rho D_{AB}} \right)$$

$$= Re Sc$$

The another important dimensionless group in mass transfer, similar to heat transfer, is the Peclet number. This Peclet number, in case of heat transfer, we can define, is the heat flux due to bulk flow divided by flux due to conduction, due to conduction across the thickness, thickness  $l$ ; so, which is  $C_p \rho v \Delta T$  divided by  $k$  by  $l$  into  $\Delta T$ , which we can divide into two groups, two dimensionless group,  $v l \rho$  by  $\mu$  into  $C_p \mu$  by  $k$ , which is Reynolds number into Prandtl number. The analogous number for mass transfer is Peclet number, is flux due to bulk flow of the medium divided by diffusive flux across the thickness, thickness  $l$ , which we can write velocity into  $\Delta C$  divided by  $D_{AB}$  by  $l$  into  $\Delta C$ ; which we can write also in two different dimensionless term,  $v l \rho$  by  $\mu$  into  $\mu$  by  $\rho D_{AB}$ , which is equal to the Reynolds number into Schmidt number. So, these are the 4 important dimensionless number, or important, in case of mass transfer, there are two more dimensionless terms are available in case of mass transfer.



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## Correlations for Convective Mass Transfer Coefficient

### Objectives

- Concept and Importance of dimensional analysis
- Buckingham Method to determine dimensionless groups

Now, the correlations for convective mass transfer coefficients; so, what are the objectives for this? It is to explain the concept and the importance of dimensional analysis for the experimental data and to obtain a useful correlation. And, how to use the Buckingham method to determine dimensionless groups involved for a particular systems. Correlations are required for the mass transfer in turbulent flow, where the mass transfer coefficient calculations is not easy from the theoretical considerations.

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## The Buckingham Method

### Steps

- Identify variables significant to a problem
- Determine number of dimensionless groups
  - May be obtained by Buckingham pi theorem

$i_d$  = number of dimensionless groups

$n$  = number of variables

$r$  = rank of dimensional matrix ✓

$$\underline{i_d = n - r}$$

So, we will discuss the Buckingham method to obtain the correlations. So, in this method, first, we have to consider the certain fundamental dimensions. What are those? Length, which we represent by  $l$ . Length, is one fundamental dimensions and which is symbolized as  $l$ ; and like area, we can write  $l$  square; volume, we can write  $l$  cube. Another dimension is time. It is symbolized as  $t$  and velocity, we can represent as  $l$  length per time, and acceleration, we can write, length per time square.

Another fundamental dimensions is mass, which is symbolized as  $m$ . Like density, if we consider density, then, it is mass per volume; this is  $m$  by  $l$  cube. So, we have to have these fundamental dimensions initially, and then, in the Buckingham method we have to identify the variables significant to a particular problem. And then, we have to determine the number of dimensionless groups. And this number of dimensionless groups may be obtained by Buckingham pi theorem. What is that? If  $i$  is the number of dimensionless group for a particular system and there are  $n$  number of variables for that particular problem, and  $r$  is the rank of dimensional matrix, then we can write,  $i$  is equal to  $n$  minus  $r$ , the number of dimensionless groups is equal to number of variables minus rank of the dimensional matrix. So, now, we will talk about what is dimensional matrix and how to determine the number of dimensionless groups.

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**The Buckingham Method**

**Example: Convective Mass Transfer into a dilute stream in a circular tube**

**Step 1**

Variables	Symbols	Units	Dimensions
✓ Tube diameter ✓	$d$	$m$	$L$
✓ Fluid density ✓	$\rho$	$kg\ m^{-3}$	$M\ L^{-3}$
✓ Fluid viscosity ✓	$\mu$	$kg\ m^{-1}\ s^{-1}$	$M\ L^{-1}\ t^{-1}$
✓ Fluid velocity ✓	$v$	$m\ s^{-1}$	$L\ t^{-1}$
✓ Mass diffusivity ✓	$D_{AB}$	$m^2\ s^{-1}$	$L^2\ t^{-1}$
✓ Mass-transfer coefficient ✓	$k_c$	$m\ s^{-1}$	$L\ t^{-1}$

So, let us consider a simple example for convective mass transfer into a dilute stream, in a circular tube. So, the first step is to identify the variables pertaining to that particular

problem. For this problem, these are the variables - tube diameter, which is symbolized as  $d$  and the unit is m and dimension is L; similarly, fluid density, fluid viscosity, fluid velocity, mass diffusivity, mass transfer coefficients. So, these are the variables which incorporate the system geometry, which is diameter. And then, fluid properties – density, viscosity and (( )) properties and the other primary quantities, that is, mass transfer coefficients.

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### The Buckingham Method

Variables	Symbols	Units	Dimensions
Tube diameter	$d$	m	L
Fluid density	$\rho$	$\text{kg m}^{-3}$	$\text{M L}^{-3}$
Fluid viscosity	$\mu$	$\text{kg m}^{-1} \text{s}^{-1}$	$\text{M L}^{-1} \text{t}^{-1}$
Fluid velocity	$v$	$\text{m s}^{-1}$	$\text{L t}^{-1}$
Mass diffusivity	$D_{AB}$	$\text{m}^2 \text{s}^{-1}$	$\text{L}^2 \text{t}^{-1}$
Mass-transfer coefficient	$k_c$	$\text{m s}^{-1}$	$\text{L t}^{-1}$

Step 2

Fundamental dimensions	$k_c$	$v$	$\rho$	$\mu$	$D_{AB}$	$d$
M	0	0	1	1	0	0
L	1	1	-3	-1	2	1
t	-1	-1	0	-1	-1	0

$$A = \begin{pmatrix} 0 & 0 & 1 & 1 & 0 & 0 \\ 1 & 1 & -3 & -1 & 2 & 1 \\ -1 & -1 & 0 & -1 & -1 & 0 \end{pmatrix}$$

✓

Now, if we take the fundamental dimensions M, L and t, and make another table, where the M will represent for all the exponent of the fundamental dimensions, which is in case of  $k_c$ , we have l and t, l 1 and t minus 1. So, l is 1 and t is minus 1 and M is 0, in case of  $k_c$ . Similarly, we will obtain this table for velocity, density, viscosity, diffusivity and diameter. So, M, we can represent all these variables in terms of fundamental dimensions. Then, the exponent of these dimensions will form a matrix which is known as the dimensional matrix. So, this is our dimensional matrix and we have to find the rank of this matrix. The rank of this matrix, we can find out using Matlab or some other program; for this case, the r is equal to rank of A, which is 3.

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### The Buckingham Method

**Step 3**

$$A = \begin{pmatrix} 0 & 0 & 1 & 1 & 0 & 0 \\ 1 & 1 & -3 & -1 & 2 & 1 \\ -1 & -1 & 0 & -1 & -1 & 0 \end{pmatrix}$$
$$r = \text{rank}(A) = 3, \quad n = 6$$
$$i_d = n - r = 6 - 3 = 3$$

So, we can obtain  $i_d$ , the number of dimensionless group for a particular system will be, the number of variables  $n$  is, here is, if we can go back, we can see, there are 6 number of variables, we have considered for a particular system. So,  $n$  is 6 and rank of the matrix  $r$  is 3. So,  $i_d$  is  $n$  minus  $r$ . So, it will be 6 minus 3, is equal to 3. So, there are 3 dimensional groups for this particular system.

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### The Buckingham Method

**Step 4**

- Three dimensionless groups:  $\pi_1, \pi_2, \pi_3$
- Choose a core group of  $r$  variables in each  $\pi$  groups
  - How to choose?
    - Exclude the variables whose effect one wishes to isolate, say in this problem  $k_c$
    - Let arbitrarily also excludes  $v$  and  $\mu$
- Core groups now consists of  $D_{AB}, d$  and  $\rho$

Let us symbolize this dimensionless group as  $\pi_1, \pi_2$  and  $\pi_3$ . So, step four, the three dimensionless group we represent  $\pi_1, \pi_2$  and  $\pi_3$ . Now, from the system, we have to

choose a core group of  $r$  variables in each  $\pi$  groups. So, how to choose these core groups? The one way to choose these core groups, is to exclude the effect of a particular variables which we want to isolate. Say, in this problem, we want to isolate the mass transfer coefficient  $k_c$ . And also, let us arbitrarily exclude other variables velocity and  $\mu$  for the particular system; velocity and viscosity of the fluid, we can exclude, as the variables which will not be included in the core group. So, the core group now consists of diffusivity, diameter and the density of the fluid.

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**The Buckingham Method**

$$\pi_1 = D_{AB}^a \rho^b d^c k_c$$

$$\pi_2 = D_{AB}^d \rho^e d^f v$$

$$\pi_3 = D_{AB}^g \rho^h d^i \mu$$

$$\pi_1 \Rightarrow M^0 L^0 t^0 = 1 = (L^2 t^{-1})^a (M L^{-3})^b (L)^c (L t^{-1})$$

$$\begin{array}{lcl} L: & 0 & = 2a - 3b + c + 1 \\ t: & 0 & = -a - 1 \\ M: & 0 & = b \end{array} \quad \left. \vphantom{\begin{array}{lcl} L: & 0 & = 2a - 3b + c + 1 \\ t: & 0 & = -a - 1 \\ M: & 0 & = b \end{array}} \right\} a = -1, b = 0, c = 1$$

$$\pi_1 = \frac{k_c d}{D_{AB}} = Sh$$

Now, we can write  $\pi_1$  is equal to  $D A B$  to the power  $a$ ,  $\rho$  to the power  $b$  and  $d$  to the power  $c$ , that is core group and we will include the other excluded variables, that is,  $K_c$ ; and,  $\pi_2$  is equal to  $D A B$  to the power  $d$ ,  $\rho$  to the power  $e$  and  $d$  to the power  $f$  and  $v$ ; and,  $\pi_3$  is  $D A B$  to the power  $g$ ,  $\rho$  to the power  $h$  and  $d$  to the power  $i$  and  $\mu$ . These are the 3 groups we have identified. Now, from the dimensional form, we can write,  $M^0 L^0 t^0$  is equal to 1, is equal to  $L^2 t^{-1}$ ; for  $\pi_1$ , we can write  $L^2 t^{-1}$  to the power  $a$ ,  $M L^{-3}$  to the power  $b$  and  $L$  to the power  $c$   $L t^{-1}$ . So, from this, if we solve these equations, we will have for  $L$ , we will have  $0$  is equal to twice  $a$  minus  $3b$  plus  $c$  plus  $1$ ; and  $0$  for  $t$ ,  $0$  is equal to minus  $a$  minus  $1$  and for  $M$   $0$  is equal to  $b$ . So, if we solve these three, we will have  $a$  is equal to minus  $1$ ;  $b$  is equal to  $0$ , and  $c$  is equal to  $1$ . So, with this, we can write,  $\pi_1$ , if we have obtained power of these variables, and if we put this,  $\pi_1$  will be  $K_c d$  divided by  $D A B$ , and which is known as

Sherwood number; and it is analogous to heat transfer of the dimensionless group which is Nusselt number.

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**The Buckingham Method**

$$\pi_2 = \frac{vd}{D_{AB}} = Pe_M ; \quad \pi_3 = \frac{\mu}{\rho D_{AB}} = Sc$$

$$\frac{\pi_2}{\pi_3} = \frac{vd}{D_{AB}} \times \frac{\rho D_{AB}}{\mu} = \frac{\rho vd}{\mu} = Re$$

$$\pi_1 = f(\pi_2, \pi_3)$$

$$Sh = f(Re, Sc) = \phi Re^\alpha Sc^\beta$$

$\phi, \alpha, \beta = \text{dimensionless constants}$

$$Nu = f(Re, Pr)$$

For  $\pi_2$ , we will do the similar analysis, and we will obtain  $\pi_2$  is  $vd$  divided by  $D_{AB}$ , which is equal to Peclet number for mass transfer we have discussed earlier. And, for  $\pi_3$  also, similar analysis will give you,  $\mu$  by  $\rho D_{AB}$ , so, which is Schmidt number. Now, if we divide  $\pi_2$  by  $\pi_3$ , so, it will give you,  $vd$  by  $D_{AB}$  into  $\rho D_{AB}$  by  $\mu$ , so, which is  $\rho vd$  by  $\mu$ , so, which is known as Reynolds number. So, the dimensional analysis will give us  $\pi_1$  is a function of  $\pi_2$  and  $\pi_3$ ; that means, Sherwood number, we can write as function of Reynolds and Schmidt number, which is in the form of  $\phi$  function of, is  $\phi$  into  $Re$  to the power  $\alpha$ , and Schmidt number to the power  $\beta$ ;  $\phi, \alpha, \beta$  are the dimensionless constants. So, this is analogous equations in heat transfer; Nusselt number is equal to function of Reynolds number and Prandtl number.

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Typical Correlations		
System	Range	Correlation
Laminar Flow Through a circular Tube	$Re \leq 2100$	$Sh = 1.62 \left( Re Sc \frac{\mu}{\mu_s} \right)^{1/3}$
Turbulent flow Through a tube	$4000 \leq Re \leq 60,000$ $0.6 \leq Sc \leq 3,000$	$Sh = 0.023 Re^{0.83} Sc^{0.33}$
Liquid Flow Through packed bed	$3 \leq Re \leq 10,000$	$Sh = 2 + 1.1 Re^{0.6} Sc^{0.33}$

Similar correlations, we can get for different systems. Let us consider few examples of correlations like this system, Range and correlation. Laminar flow through a circular tube - if Reynolds number less than 2100, then, Sherwood number is 1.62; Reynolds Schmidt d by 1 to the power 1 by three. Turbulent flow through a tube, turbulent flow through a tube - if Reynolds number greater than equal to 4000 and less than equal to 60000, and Schmidt number greater than 0.6 and less than 3000. So, we have Sherwood number is equal to 0.023; Reynolds number to the power 0.83 and Schmidt number to the power 0.33; similarly, liquid flow through a, liquid flow through packed bed. So, here, Reynolds greater than equal to 3 and less than 10000; the Sherwood number is equal to 2 plus 1.1, Reynolds to the power 0.6 and Schmidt to the power 0.33.



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### Example

Consider a sphere of naphthalene of diameter 20mm is suspended in a flowing air at 45°C. The velocity of air is 1 m/s. The diffusivity of naphthalene in air at 45°C is  $6.9 \times 10^{-6} \text{ m}^2/\text{s}$ . Given that at 45°C  $\rho_{\text{air}} = 1.2 \text{ kg/m}^3$  and  $\mu_{\text{air}} = 1.9 \times 10^{-5} \text{ kg/m s}$ , and sublimation pressure of naphthalene is 1 kPa. Use the following correlation for Sherwood number:

$$Sh = 2 + 0.55(Re)^{0.52} (Sc)^{0.33}$$

Calculate the Mass transfer coefficients and flux for mass transfer

Now, let us consider one example. A sphere of naphthalene of diameter 20 millimeter is suspended in a flowing air at 45 degree Centigrade. The velocity of air is 1 meter per second. The diffusivity of naphthalene in air at 45 degree Centigrade is given. Given that the density and viscosity of the air and sublimation pressure of naphthalene as 1 kilopascal and using this correlation, calculate the mass transfer coefficient and flux of mass transfer.

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### Example : Solution

Diffusion of A through non-diffusing B

$$Sh = \frac{k_g p_{\text{atm}} R T d}{D_{AB} P_t}$$

$$P_t / p_{\text{atm}} \approx 1, \quad R = 8.314 \frac{\text{J}}{\text{mol K}}, \quad T = 318 \text{ K}$$

$$33.7 = k_g \times \frac{8.314 \times 318}{6.9 \times 10^{-6}}$$

$$\Rightarrow k_g = 8.855 \times 10^{-8} \text{ kmol/m}^2 \text{ s}$$



So, given the data, we can calculate, Reynolds number will be  $d v \rho$  by  $\mu$ , which is equal to  $0.02 \text{ into } 1 \text{ into } 1.2$ , divided by  $1.9 \text{ into } 10 \text{ to the power minus } 5$ , which is  $1260$ . And, Schmidt number also we can calculate,  $\mu$  by  $\rho D_{AB}$ , which is equal to  $1.9 \text{ into } 10 \text{ to the power minus } 5$ , divided by  $1.2 \text{ into } 6.9 \text{ into } 10 \text{ to the power minus } 6$ ; so, it will be  $2.29$ . And, Sherwood number, as the equations given, we can calculate  $2 \text{ plus } 0.55$ , Reynolds to the power  $0.53$  and Schmidt to the power  $0.33$ . Substituting the data, it will be  $33.9$ . Now, we can write the diffusion, diffusion of A through non diffusing B. So, we can calculate Sherwood number is equal to  $K_G P_B L M R T$  divided by  $D_{AB} P_t$  and at  $45 \text{ degree Centigrade}$ , the vapour pressure is small. So,  $P_t$  by  $P_B L M$  is approximately  $1$ ;  $R$  is equal to  $8.3066 \text{ meter cube kilopascal per K mol Kelvin}$  and  $t$  is  $318 \text{ Kelvin}$ . So, we can write, Sherwood number is given,  $33.9$  is equal to  $K_G$  into  $8.3066 \text{ into } 318$  divided by  $6.9 \text{ into } 10 \text{ to the power minus } 6$ . So, from this we can calculate  $K_G$ , which is  $8.855 \text{ into } 10 \text{ to the power minus } 8 \text{ K mol per meter square second kilopascal}$ .

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**Example : Solution**

$$\begin{aligned}
 N_A &= K_g (p_{A1} - p_{A2}) \\
 &= 8.855 \times 10^{-8} (1 - 0) \quad \begin{matrix} p_{A1} = 1 \text{ kPa} \\ p_{A2} \approx 0 \end{matrix} \\
 &= 8.855 \times 10^{-8} \text{ kmol}
 \end{aligned}$$

Flux, we can calculate,  $N_A$  is equal to  $K_G P_{A1} \text{ minus } P_{A2}$ . So,  $P_{A1}$  is given; is  $1 \text{ kilopascal}$  and  $P_{A2}$  can be considered approximately equal to  $0$ . So, it will be  $8.855 \text{ into } 10 \text{ to the power minus } 8$ ,  $1 \text{ minus } 0$ . So, it will be  $8.855 \text{ into } 10 \text{ to the power minus } 8 \text{ K mol per meter square second}$ . So, this is end of this lecture.