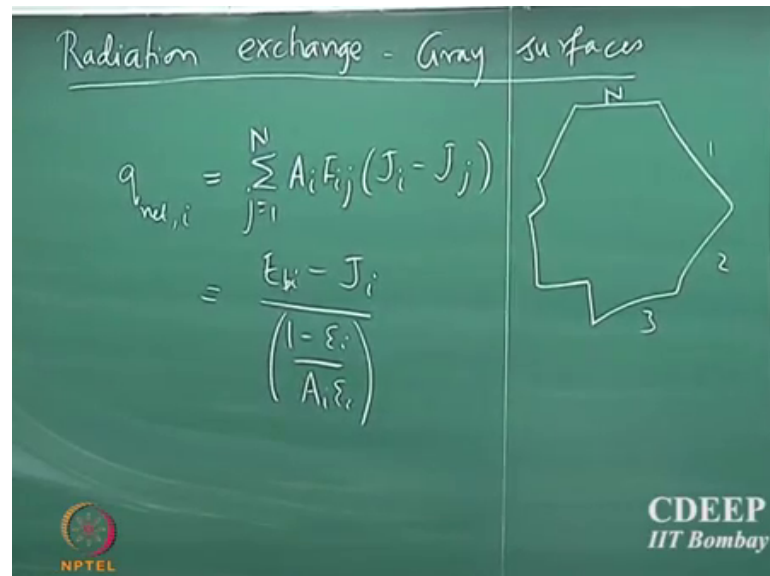


Heat Transfer
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Lecture - 53
Resistances: Oppenheim Matrix Method

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We looked at the energy balance or radiation exchange in gray surfaces. So, we said that the net radiation exchange, if we have an enclosure with N objects with N surfaces and each of them are exchanging radiation with each other. Then we said that the net radiation exchange is given by sum over all $A_i F_{ij}$, j going from 1 to N and that is also equal to $E_{b,i} - J_i$ by $1 - \epsilon_i$ by $A_i \epsilon_i$.

So, we identified that $1 - \epsilon_i$ by $A_i \epsilon_i$ is the resistance offered by the surface because of its surface properties for radiation exchange from that surface ok. So, now, in a similar way we could also identify resistances for radiation exchange between different surfaces ok. So, note that this is the resistance for radiation from the surface i , and we can identify resistances for radiation exchange between surfaces between surfaces ok.

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Resistance for radiation exchange between surface i & j

$$q_{net,ij} = A_i F_{ij} (J_i - J_j)$$
$$= \frac{J_i - J_j}{(1/A_i F_{ij})} = \frac{\text{Driving force}}{\text{Resistance}}$$

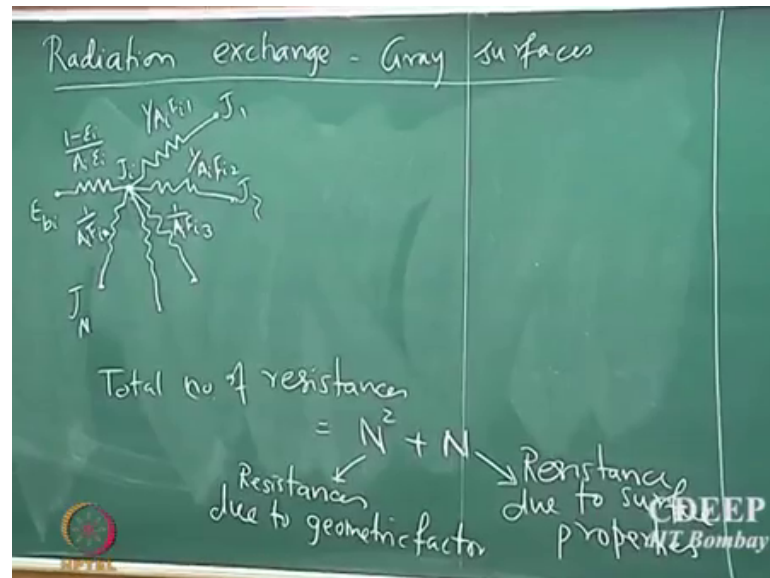
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So, radiation exchange between surface i and surface j is given by is $A_i F_{ij} J_i - A_i F_{ij} J_j$ ok. So, now we can rewrite this as J_i divided by $1/A_i F_{ij}$. So, if the driving force for radiation exchange is the difference between the corresponding total emission from each of these surfaces so that is the driving force, driving force divided by the resistance ok.

So, one could identify that the resistance that is offered for radiation exchange between surface i and j, would be $1/A_i F_{ij}$ ok. So, this resistance is nothing but $1/A_i F_{ij}$. So, note that this resistance is the resistance offered because of orientation this is the geometric resistance that is offered by the system because of the orientation of different surfaces.

So, therefore, one could write a resistance network $1/A_i F_{ij}$ ok. So, that is the resistance which is offered for radiation exchange between surface i and surface j whose total emission are J_i and J_j ok. So, now based on these 2 resistances, we can now construct the resistance network for the whole system ok.

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So, supposing $E_{b,i}$ is the blackbody radiation for surface i and J_i is the corresponding total emission from that surface then the resistance offered is $1 - \epsilon_i$ by $A_i \epsilon_i$. Now this is exchanging radiation with all other surfaces therefore, you have resistance for which are occurring in parallel, because it is simultaneously exchanging radiation with all other surfaces.

Therefore, you have resistances which is appearing parallel, so this is $1/j_1, J_2$, spectra up to J_N . And these resistances are $1/A_i F_{i,1}$ $1/A_i F_{i,2}$ and this will be $1/A_i F_{i,3}$ and this will be $1/A_i F_{i,N}$ ok. So, that is the resistance network for radiation exchange of surface i with all other surfaces in the enclosure ok.

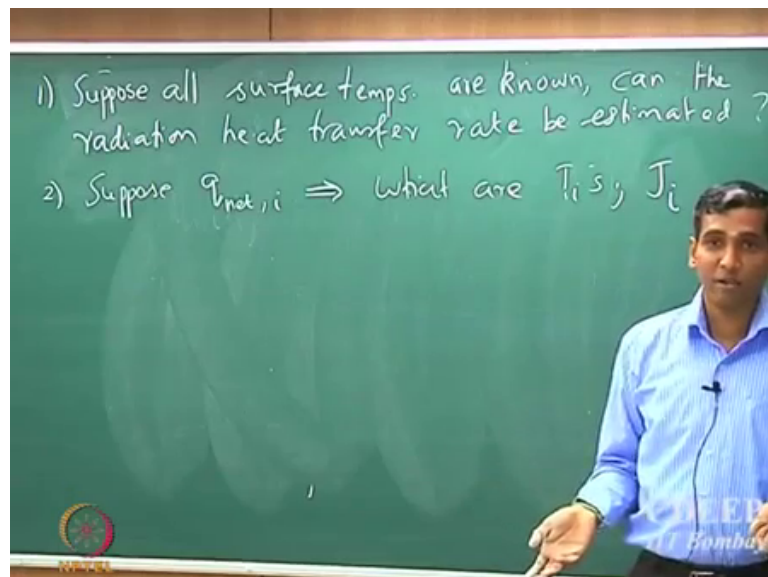
So, one could similarly write the radiation exchange for all the other surfaces right, one could similarly write radiation exchange network for all the other surfaces going from 1 to N . So, in principle from every node you will have N resistances which are actually coming out of every node.

So, how many resistances are there total number of resistances, for this system total number of resistances what is the total number of the resistances. So, every entity you have N of them so that gives you N^2 . But you have the resistance that is offered by the properties of the surface right. So, you have 1 resistance for every surface. So, the total number of resistances is equal to N^2 plus N ok.

So, this N^2 is the resistance offered because of orientation resistances due to geometric positions or geometric factor. So, these N^2 resistances are because of the geometric factors and; obviously, they are symmetrical right. And N resistances are because of the resistances due to surface properties; due to surface property what is the resistance offered by the surface due to its surface properties. So, the total number of resistances are N^2 plus N alright.

So, where do we use all this the question is where do we use all this information. So, there are 2 kinds of questions one who typically ask ok.

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The question one is suppose I know all the temperatures suppose all surface temperatures are known ok. Can I estimate can the radiation so that is the first class of questions you can answer with some of the things that we have derived so far ok.

The second class of questions you can answer is suppose I know the classes suppose I know q_i I know the net radiation exchange from every surface. Now that is possible to measure because if you know how much heat you are supplying or removing in order to maintain an isothermal condition and that is what will give you what unit i , then given that what is the temperature.

You can answer different kinds of questions not just that you can also say what are the individual total emission so that and that question also can be answered ok. So, let us

What else do I know? What does do I know? I know the temperatures what else do I know?.

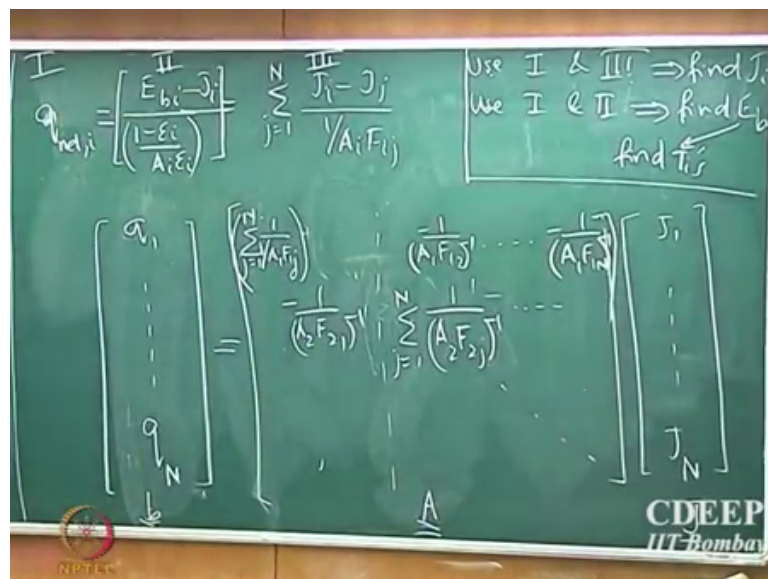
Student: (Refer Time: 12:47).

You know E_{bi} is just the blackbody radiation at that temperature right. So this means E_{bi} equal to σT_i^4 is a known quantity right. So, what do we need to estimate we need to find out all the J_i 's. We need to find out the total emission from every surface given these quantities is it a solvable problem. How many equations are there? How many?

Student: N.

N equations, so you have 1 equation for every value of i right. So, this is so this equation is valid for all i going from 1 to N ok. Is it a linear or a non-linear problem? It is linear; linear in J. So, we should be able to find the solution.

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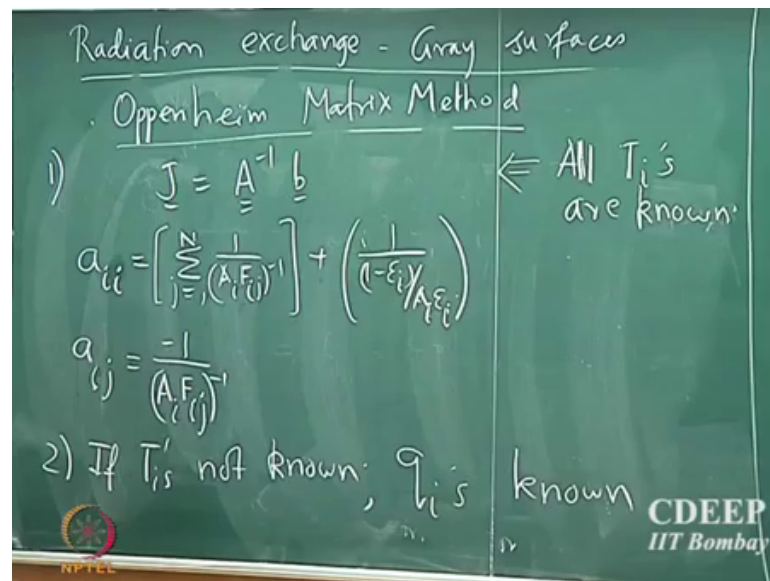
So, the way to represent this is so E_{bi} divided by $1 - \epsilon_i$ by $A_i \epsilon_i$ that is equal to $\sum_{j=1}^N \frac{J_j - J_i}{A_i F_{ij}} + \frac{J_i}{1 - \epsilon_i}$ ok. So, now I can write this in the matrix vector form.

So, note that this is for all i going from 1 to N, now I can write this as a matrix vector problem so that is E_{b1} by $1 - \epsilon_1$ by $A_1 \epsilon_1$ $A_N \epsilon_N$ and that is

equal to we have a matrix multiplied by J 1 all the way up to J N. What is the first element in the matrix that is only for the first term, that is summed over all 1 to N right.

So, similarly you have a summation here j going from 1 to N ok. So, I will open up and write it out write all the terms separately in a minute, but you should understand the structure of this matrix ok. So, let us just quickly so if I call this matrix as A ok, if I call this matrix as A matrix and if I call this a j vector, and if I call this as b vector ok.

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So, the total emission from all the surfaces was just the solution of this matrix problem right. So, J will be A inverse times b ok. So, where if I open up the A matrix a 1 1 the first element in the matrix will be sum over all j 1 by A 1 F 1 j inverse plus 1 by 1 minus epsilon 1 divided by A 1 epsilon 1 so that will be the first term.

So, if I now want to find out what is the general diagonal term. So, a i i this will simply be I replace 1 with i so that is the general diagonal term. And then if I look at the off diagonal terms a 1 2 will be 1 by minus 1 by A 1 F 1 2 inverse right.

So, if I replace if I want to find the general non diagonal term. So, a ij will be A 1 F 1 j ok. And then I replace the first index with I Ai Fi so that is it. So, it is so easy to find out what this matrix is ai i is sum over j equal to 1 to; 1 by Ai Fi i inverse F ij inverse excuse me plus 1 by 1 minus epsilon i divided by Ai epsilon i and the off diagonal terms are Ai j is minus 1 by Ai Fi j inverse.

Student: (Refer Time: 18:03).

Yes it is because of the reciprocity relationship it is symmetric and it has to be symmetric. Because if surface 1 is exchanging with surface 2, surface 2 is in turn exchanging with 1 so it has to be symmetric. So, we can find out the total emission simply by following this matrix problem and so j will be a inverse times b ok. So, this is if all the temperatures are known ok. What if all the fluxes are known or the rate heat transport rate is known. So, this is the first problem.

What about the second one where if temperatures are not known, but we know how to estimate the q_i s how do we solve this problem and we still use the same framework.

Student: (Refer Time: 19:20).

No u_i minus j_i that is right. So, that is the expression.

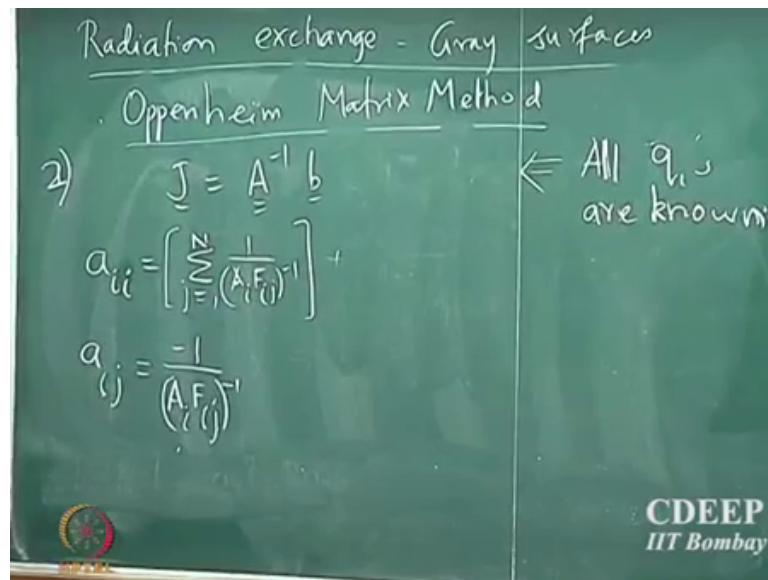
Student: (Refer Time: 19:31).

We do not know so we want to find out j_i you are going to find j_i . So, we know q_{net} you are going to find j_i now if you know j_i you know E_{bi} from this expression. So, there are three terms here there is a first term, there is a second term, and there is a third term right so there are 3 terms here. Now what I can do is I can equate first and the third. So, use the first and third so use 1 and 3 term, 1 and 3 and find j_i . Find j_i they find all the total emissivity, then use 1 and 2 and find E_{bi} so you can find E_{bi} .

So, once you know E_{bi} from here you can find temperature that is it algorithm is very simple it is still the same framework except that these elements inside the matrix is going to be different. So, that is going to be q_1 and q_N and the diagonal elements will not have this summation term this will not have this additional term here. So, that will be so this will be \sum_j equal to $1 \ 2 \ N \ 1$ by $A \ 2 \ F \ 2 \ j$ inverse etcetera and you just complete the matrix ok.

So, this will give you again it is a and this b vector. So, solving this matrix vector problem will actually give you the total emission from all the surfaces if $q_{net \ i}$ is known. And then equating 1 and 2 you will be able to find the E_{bi} for every surface and from that you can find out the temperatures ok. So, if we just so this is for problem 2 where all q_i 's are known.

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The elements will simply be the diagonal elements will be summation of all the view factors and the off diagonals their terms will remain the same ok. So, this is for the second class of problem where you can still use the same Oppenheim matrix method except that you will have to equate different terms in your energy balance.